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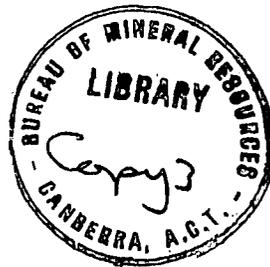
BUREAU OF MINERAL RESOURCES, GEOLOGY AND GEOPHYSICS

RECORD No. 1963/99



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HERBERT RIVER SEISMIC
REFRACTION SURVEYS,
QUEENSLAND 1961



by

M. KIRTON and W.A. WIEBENGA

The information contained in this report has been obtained by the Department of National Development, as part of the policy of the Commonwealth Government, to assist in the exploration and development of mineral resources. It may not be published in any form or used in a company prospectus or statement without the permission in writing of the Director, Bureau of Mineral Resources, Geology and Geophysics.

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SUMMARY

This Record describes a seismic refraction survey of the proposed dam sites, tunnel lines, and penstock lines on the Herbert River hydro-electric investigation, northern Queensland. The survey was requested by the Co-ordinator General's Department of Queensland. Depths to the weathered layers and to bedrock, and longitudinal seismic velocities in the rocks were measured on each site. The mean values of Poisson's ratio and Young's modulus of the bedrock were determined on the three main dam sites.

The results indicate that the bedrock on each of the dam sites is satisfactory for foundation purposes. On the geophysical evidence, the proposal to divert the water from the Kooragwin dam to the Upper Cameron Creek and then by a tunnel to the Upper Blencoe Creek dam is the most satisfactory. The Tanner penstock ridge is more suitable than the Blencoe penstock ridge.

1. INTRODUCTION

The Co-ordinator General's Department of Queensland proposes to use the waters of the Herbert River system to generate hydro-electric power in the area of the Herbert River and Blencoe Creek. The confluence of these streams is about 40 miles west of Cardwell, northern Queensland (Plate 1), at co-ordinates 472095 on the Kirrama one-mile sheet. The scheme will utilize the difference in elevation of about 1200 ft between the top of the Herbert River Falls and the confluence of Blencoe Creek and Herbert River. It has been estimated that the scheme should be able to supply 100MW of electric power at 50 percent load factor to the Cairns-Townsville area.

The Department requested that the Bureau of Mineral Resources, Geology and Geophysics, assist with the investigation by determining the depth to bedrock and the nature of the bedrock and overburden in areas where dam sites, flumes, and tunnel lines were proposed. Accordingly a seismic refraction survey was made between 4th October and 6th December 1961, by a geophysical party consisting of M. Kirton (party leader), and C.J. Braybrook and J.P. Pigott (geophysical assistants). The Department provided the topographical survey and field assistants as required. The Geological Survey of Queensland provided geological information (Wolff, 1960; 1961).

At the time of the survey, the Department's design for the Herbert River scheme was as follows (see Plate 1). The Herbert River would be dammed at the Kooragwin dam site (co-ordinates 216301 on the Cashmere one-mile sheet), and Blencoe Creek would be dammed at either the Upper Blencoe Creek dam site (co-ordinates 477156 on the Kirrama one-mile sheet) or at the Blencoe Creek dam site No. 5 (co-ordinates 459145 on the Kirrama one-mile sheet). The power station would be at the bottom of the gorge near either the confluence of the Herbert River and Blencoe Creek (co-ordinates 470096) or the confluence of the Herbert River and Tanner Creek (co-ordinates 496089, both referred to the Kirrama one-mile sheet).

To convey the water from the dams to the power stations, three possibilities were considered :

- (a) a tunnel would be driven from the Kooragwin dam to the dam on whichever site on Blencoe Creek was found more suitable. From here, the combined waters of the Herbert River and the Blencoe Creek would go in a penstock down the side of the gorge to the power station. This penstock would either be on the Blencoe penstock ridge or the Tanner penstock ridge, depending on the location of the power station,
- (b) a holding weir (locality referred to as 'weir site') would be built just upstream from the Herbert River Falls at map location 205092 on the Cashmere one-mile sheet. The Herbert River water would be conveyed in a flume along the 1750-ft contour level on the north side of the gorge to join the Blencoe Creek water in the Blencoe penstock,
- (c) the water in the Kooragwin reservoir would be diverted into the dammed-off Cameron Creek and taken from there by a tunnel to the Blencoe dam. From here the combined water would run along one or other of the penstocks to the power station.

As time did not allow a complete survey of all the tunnel lines, flumes, and penstocks, certain representative areas were selected and surveyed. The information obtained in these places indicated the most favourable tunnelling depth and the amount of construction work that would be needed, and hence more reliable estimates of the costs of the three schemes could be made.

The line of the tunnel needed in Scheme (a) was investigated by seismic work at the following places:

| | <u>Co-ordinates</u> | <u>Sheet</u> |
|------------------|---------------------|--------------|
| Offside Creek | 290252 | Cashmere |
| Ring-barked area | 377197 | " |
| Middle Creek | 410174 | " |
| Showerbath Creek | 428165 | Kirrama |
| Blencoe Flats | 443159 | " |

The traverses on the Blencoe and Tanner penstock ridges (co-ordinates 466096 and 492105 respectively on the Kirrama one-mile sheet) were located on the descent into the gorge, where the information gained was of greatest value.

To investigate Scheme (b), the weir site was surveyed and some seismic work was done at location 454128 on the Kirrama sheet. This is the area in which the flume would join the Blencoe penstock.

The proposed tunnel portal on the Cameron Creek (co-ordinates 396265 on the Cashmere sheet) and the proposed Herbert River-Cameron Creek diversion line (co-ordinates 225313 on the Cashmere sheet) were surveyed as they were the areas of greatest interest in Scheme (c).

The lengths of the seismic traverses surveyed were:

| | |
|---|--------------|
| | (ft) |
| Kooragwin dam site | 13000 |
| Upper Blencoe dam site | 7000 |
| Blencoe dam site No. 5 | 6000 |
| Weir site | 10000 |
| Blencoe penstock ridge | 2000 |
| Tanner penstock ridge | 4000 |
| Herbert River-Blencoe Creek tunnel line | 6000 |
| Flume line | 2500 |
| Cameron tunnel portal | 1000 |
| Herbert River-Cameron Creek diversion line | 2000 |
| Total | <u>53600</u> |

The seismic refraction technique applied is known as the 'Method of Differences' (Polak and Mann, 1959a; 1959b). The instrument used was a SLE 12-channel refraction seismograph with TIC geophones of natural frequency 20 c/s. The geophone spacings were 25ft and 50ft for normal spreads, and 10ft for weathering spreads.

Two Hall-Sears three-component geophones with a natural frequency of 15 c/s were used to measure transverse wave velocities for experimental purposes.

2. GEOLOGY

The geology and geological history of the project area were described by Wolff (1960) and by White (1961). On certain traverses, the detailed geology was investigated by I.L. Skellet, engineer-in-charge of the project area, and by M. Kirton.

The project area (Plate 1) lies on the Herbert River Batholith, which is of Permian age, although it may include some Carboniferous or Lower Triassic granites. The western edge of the batholith coincides with the Burdekin River Fault Zone (White, 1961, Plate 1) which is possibly responsible for the location of the Herbert River between the Kooragwin dam site and the weir site. The granite has intruded Siluro-Devonian sediments of the Mount Garnet Formation (Wolff, 1960, p.3) in the area of the Kooragwin dam site and north of this.

The batholith was later intruded in places by Elizabeth Creek Granite and certain parts were covered by Cainozoic basalt flows.

A major fault or shear zone with an easterly strike was responsible for the formation of the Herbert River Gorge (White, 1961, Plate 1).

Geological notes referring specifically to the seismic traverses are included separately for each site.

3. KOORAGWIN DAM SITE

Geology

The area was mapped by Wolff (1960). Summarising his findings, the geology along the geophysical traverses can be described as follows (see Plate 2):

- (a) from Stations WK 1 to WK 17 the surface layer is Cameron Creek Formation of unconsolidated sand, mudstone, and sandstone. It is considered to be in general, less than 20 ft thick, of Cainozoic age, and overlies Tertiary basalt,

- (b) between Stations WK 17 and 26, WK 84 and 102, WK 130 and 150, and along the cross traverses WK 341-52, WK 353-64 and WK 365-76, there is Herbert River Granite. This is probably Carboniferous and has intruded the older Mount Garnet Formation and Hall's Reward Metamorphics at depth and on the surface. It was later lateritised and covered with Tertiary basalt flows, most of which have now been eroded away leaving surface outcrops of granite and granite sand. In the river bed the granite is partly covered by a thin layer of alluvial unconsolidated sand. Herbert River Granite is medium to coarse grained and jointing is well developed along three major directions, north-north-east, north-north-west and east-north-east, with nearly vertical dips. Weathering along the joint planes is moderate but tends to be more marked along those roughly parallel to the stream course,
- (c) between Stations WK 36 and 84, 116 and 132, and 324 and 340 on the left bank, and Stations WK 150 and 160, 104 and 115, and 167 and 307 on the right bank, the rocks are of the Mount Garnet Formation. These rocks are of Siluro-Devonian age and consist mainly of quartzite, greywacke, hornfels, limestone, conglomerate, siltstone, slate, and shale.

The sediments are faulted against the older metamorphics to the west. They are intruded by Herbert River Granite in, and close to, the river bed, and the sediments have been metamorphosed in varying degrees to hornfels and quartzite. On the right bank the sediments are covered by unconsolidated sand and silty sand with occasional outcrops of sandstone and greywacke. On the left bank there are outcrops of quartzite, hornfels, hornfels conglomerate, and rubble derived from these rocks.

The sediments trend regionally north-north-east and are steeply tilted with dips ranging from 70 degrees to vertical. Jointing of the sediments occurs mainly in the quartzites, where the predominant directions are north-north-east to north-east, with mainly vertical dips.

Results

Plates 3 to 7 show the seismic cross-sections and the measured longitudinal velocities along the traverses. Table 1 gives the probable interpretation of the seismic velocities in terms of rock type.

TABLE 1

Seismic velocities in terms of rock types

| <u>Longitudinal seismic velocity (ft/sec)</u> | <u>Rock type</u> |
|---|--|
| 1000 - 2000 | Soil and scree |
| 2000 - 3000 | Unconsolidated, unsaturated alluvial material; unconsolidated Cameron Creek sediments; rubble and decomposed rock; laterite |
| 3000 - 5000 | Very weathered and decomposed rock; very jointed rock with open joints; compacted clays and sands |
| 4500 | Unconsolidated Cameron Creek sediments |
| 6000 - 8000 | Very weathered to moderately weathered rock; fractured and weathered rock in a shear zone; or jointed rocks with joints partly closed and cemented |
| 8000 - 10000 | Fractured bedrock in a shear zone; slightly to moderately weathered granite and metamorphics; vesicular and slightly weathered basalt |
| 10000 - 13000 | Unweathered basalt or slightly weathered and jointed granite |
| 14000 - 15000 | Bedrock of Mount Garnet sediments |
| 16000 and over | Slightly weathered to unweathered granite; quartzite, hornfels, or quartz porphyry |

With the help of Table 1 and the available geological information, the seismic velocities shown on the cross-sections can be interpreted in geological terms. In the following discussion, bedrock is defined as the deepest seismic refractor shown on the seismic cross-sections. Generally the recorded seismic velocity in the deepest refractor exceeds 10,000 ft/sec, except in shear or contact zones. Further, only points which may lead to ambiguous interpretation will be discussed.

Between WK 5 and WK 8 (Plate 3), the 4500-ft/sec layer may be interpreted as Cameron Creek sediments overlying vesicular basalt in which the velocity is 10,000 ft/sec. West of WK 8, between WK 8 and WK 24, the 18,000 to 19,000-ft/sec velocity probably represents granite (based on geological evidence). The 8000-ft/sec velocity may indicate weathered granite.

Between WK 24 and WK 39, the bedrock is relatively deep and the average seismic velocity in it is about 14,000 ft/sec. Referring to Plate 2 this zone coincides with the contact zone between granite and the Mount Garnet Formation.

The 8000-ft/sec layer could either be a weathered granite or a weathered metamorphic rock. Depending on the type of dam to be constructed, an 8000-ft/sec layer could have the required properties to serve as a foundation rock. This should be checked by drilling.

From WK 38 to WK 81, the bedrock velocities, generally greater than 17,000 ft/sec, indicate the presence of granite or metamorphic rock. A narrow zone between WK 52 and WK 55 of lower velocities (14,000 to 15,000 ft/sec) may suggest the presence of a shear zone. The 8000-ft/sec layer continues in a westerly direction but seems to change or disappear between WK 74 and WK 79 (Plate 4). Near WK 80 the 6500-ft/sec layer represents a highly weathered rock (see Drill hole HR 3, Table 2).

In the river bed a relatively thin low-velocity layer (about 2000 ft/sec), representing unsaturated alluvial material, overlies a high-velocity bedrock (more than 16,000 ft/sec), representing unweathered granite or metamorphic rock. At certain places there may be an intermediate layer of moderately weathered rock (characterized by a velocity of 6000 to 8000 ft/sec) that is too thin to be detected.

West of the river bed, between WK 150 and WK 160, and between WK 103 and WK 112, a 7000 to 8000-ft/sec layer is present between the surface layers and the high-velocity granite or metamorphic bedrock. This layer probably represents moderately weathered granite or metamorphic rock, and again may be suitable for a foundation rock.

Between WK 171 and WK 220 (Plate 5), the normal sequence of layers for this area is present including an 8000-ft/sec layer between the surface layers and bedrock. Near WK 201, the top of the 8000-ft/sec layer is about 106 ft below the surface, *i.e.* at about the same elevation or level as the top of the unweathered bedrock in the river bed.

From WK 240 to WK 244 (Plate 6), the low bedrock velocity (about 9000 ft/sec) suggests the presence of a shear zone. The depth to the top of the 7000-ft/sec layer probably exceeds 90 ft.

South-west from WK 287, the bedrock dips relatively steeply towards the south-west, and the depths to the top of the 7000 to 8500-ft/sec layer range between about 76 and 95 ft.

As an experiment the transverse wave velocity was measured between WK 132 and WK 138 with three-component geophones, the measured velocity being 10,000 ft/sec. With a measured longitudinal velocity of 18,000 ft/sec (Plate 4), and an assumed rock density of 2.7 g/cm^3 , the computed value of Poisson's ratio is 0.27, and Young's modulus (dynamic determination) is $6.5 \times 10^{11} \text{ dyn/cm}^2$ or $9.4 \times 10^6 \text{ lb/in.}^2$. This method of determining Young's modulus usually gives values that are 10 to 20 percent higher than the corresponding static determinations.

Comparison with drilling information

After the cross-sections had been computed and plotted, they were compared with the logs of the diamond-drill holes on this site (Table 2). Where the drill holes are inclined, the depths given have been corrected for dip.

TABLE 2

Comparison of drilling and seismic results
Kooragwin dam site

| <u>Drill hole No.</u> <u>and position</u> | <u>Drill logs</u> | | <u>Seismic results</u> | |
|--|-------------------|---|------------------------|---|
| | <u>Depth (ft)</u> | <u>Geological formation</u> | <u>Depth (ft)</u> | <u>Velocity (ft/sec)</u> |
| HR 1, 50 ft south of WK 85, dip 45 degrees | 0 - 15 | Talus material | | |
| | 15 - 23 | Moderately weathered pyroxene hornfels | 0 - 20 | 2000 (including a possible 6000- ft/sec layer) |
| | 23 - 42 | Slightly weathered pyroxene hornfels | 20 + | 16,500 |
| | 42 + | Fresh hornfels and granite | | |
| HR 2, 50 ft south of WK 83.5, vertical | 0 - 4 | Overburden | 0 - 12 | 2000 |
| | 4 - 23 | Moderately weathered hornfels conglomerate | 12 - 30 | 6000 |
| | 23 - 52 | Slightly weathered quartzite hornfels | 30 + | 16,500 |
| HR 3, 70 ft south of WK 81, vertical | 0 - 7 | Overburden | 0 - 35 | 2000 (including a possible 6000- ft/sec layer) |
| | 7 - 16 | Moderately weathered hornfels conglomerate | | |
| | 16 - 23 | Highly weathered granite | 35 + | 16,500 |
| | 23 - 69 | Slightly weathered conglomerate | | |
| | 69 + | Fresh conglomerate | | |
| HR 4, 70 ft south of WK 98.5, vertical | 0 - 14 | Decomposed granite | 0 - 24 | 2000 |
| | 14 - 17 | Highly weathered granite | 24 + | 18,500 |
| | 17 + | Fresh granite | | |
| HR 5, 50 ft south of WK 95, dip 35 degrees | 0 - 6 | Highly weathered granite | 0 - 4 | 2000 |
| | 6 + | Slightly weathered granite | 4 + | 18,000 |

| <u>Drill hole No. and position</u> | <u>Drill logs</u> | | <u>Seismic results</u> | |
|--|-------------------|--|------------------------|---|
| | <u>Depth (ft)</u> | <u>Geological formation</u> | <u>Depth (ft)</u> | <u>Velocity (ft/sec)</u> |
| HR 6, at WK 73.3, vertical | 0 - 8 | Soil | 0 - 4 | 1000 |
| | 8 - 24 | Highly weathered hornfels | 4 - 15 | 2700 |
| | | | 15 - 47 | 5000 |
| | 24 - 64 | Moderately weathered hornfels | 47 - 102 | 8000 |
| | 64 - 96 | Slightly weathered hornfels | 102 + | 19,000 |
| | 96 + | Unweathered hornfels | | |
| HR 7, at WK 142, dip 35 degrees | 0 - 50 | Slightly weathered granite | 0 - 14 | 2000 |
| | 50 + | Unweathered granite | 14 + | 19,000 |
| HR 8a, 50 ft south of WK 88, dip 35 degrees | 0 - 18 | Moderately weathered granite | 0 - 15 | 2000 |
| | | | 15 + | 16,500 |
| | 18 + | Slightly weathered granite | | |
| HR 9, 50 ft south of WK 90, dip 30 degrees | 0 - 2 | Alluvium | 0 - 20 | 2000 |
| | 2 - 4 | Moderately weathered granite | 20 + | 16,500 |
| | 4 - 9 | Slightly weathered granite | | |
| | 9 - 10 | Unweathered granite | | |
| | 10 - 14 | Slightly weathered granite | | |
| | 14 - 18 | Unweathered granite | | |
| HR 10, at WK 127.5 dip 35 degrees | 0 - 13 | Decomposed hornfels | 0 - 25 | 2000 (and possibly a 6000-ft/sec layer) |
| | 13 - 15 | Highly weathered hornfels | | |
| | 15 - 24 | Moderately weathered hornfels | 25 + | 18,000 |
| | 24 + | Slightly weathered hornfels conglomerate | | |

| <u>Drill hole No. and position</u> | <u>Drill logs</u> | | <u>Seismic results</u> | |
|--|-------------------|--|------------------------|--------------------------|
| | <u>Depth (ft)</u> | <u>Geological formation</u> | <u>Depth (ft)</u> | <u>Velocity (ft/sec)</u> |
| HR 11, near WK 138, dip 30 degrees | 0 - 3 | Decomposed granite | 0 - 15 | 2000 |
| | 3 - 18 | Slightly weathered granite | 15 + | 18,000 |
| | 18 + | Unweathered granite | | |
| HR 12a, at WK 135, dip 30 degrees | 0 - 6 | Highly weathered granite | 0 - 12 | 2000 |
| | 6 - 14 | Slightly weathered granite and hornfels | 12 + | 18,000 |
| | 14 + | Unweathered hornfels | | |

Conclusions

In the river valley, the shallow depth to bedrock and the seismic velocity in it of greater than 15,000 ft/sec suggest that this site would be suitable for any type of dam. However, depending on the extent of the side walls, the 7000 to 8000-ft/sec layer should be further tested. Such a layer would be a suitable foundation for a gravity dam, providing it is sufficiently impermeable. Suggested drilling sites are WK 201, WK 264, and WK 296. In addition, the postulated shear zones near WK 25, WK 54, and WK 240 should be investigated.

4. BLENCOE CREEK DAM SITE NO. 5

Geology

This site is situated in an area that was mapped by Wolff (1960) as Elizabeth Creek Granite. This granite generally crops out as large tors and rubble surrounded by decomposed granite. The granite on the hillsides is moderately weathered; in the creek the exposures are harder and less weathered. The major joints strike north to north-west, with nearly vertical dips.

Results

Plate 8 shows the layout of the traverses and Plate 9 shows the seismic cross-section and the measured longitudinal velocities. These velocities can be interpreted in geological terms by referring to Table 1. Over the whole area, the velocities in the deepest refractors recorded exceeded 15,000 ft/sec. These refractors are classified as bedrock.

From Stations WL 116 to WL 125, WL 9 to WL 33, WL 136 to WL 145, WL 159 to WL 168, and WL 30 to about WL 55 a thin layer in which the velocity is about 2000 ft/sec covers slightly weathered or slightly jointed to unweathered, unjointed granite bedrock. This 2000-ft/sec velocity is an average value along all these traverses and represents patches of soil, rubble, and unconsolidated unsaturated alluvial sand.

From Stations WL 58 to WL 68, WL 178 to WL 187, and WL 76 to WL 106, the depth of weathering increases to give, in descending order, a layer of soil and rubble, layers of decomposed and weathered rock, and granite bedrock.

The velocity of the transverse wave was measured between Stations WL 136 and WL 145 by three-component geophones, and was found to be 9000 ft/sec. The longitudinal velocity along this traverse is 17,000 ft/sec. Using these values and assuming a value of 2.7 g/cm^3 for the density of unweathered granite, the value of Poisson's ratio is 0.31. The value of Young's modulus for the bedrock is then $5.4 \times 10^{11} \text{ dyn/cm}^2$, or $7.8 \times 10^6 \text{ lb/in.}^2$.

Comparison with drilling information

*

Table 3 gives a comparison of the drilling information on this site with the geophysical results. For inclined drill holes, the depths have been corrected for dip.

Conclusions

In the bed of the river and on the banks, the shallow depth to bedrock and the seismic velocity in it exceeding 15,500 ft/sec suggest that this site would be suitable for any type of dam structure. However the 6500 to 7000-ft/sec layer between Stations WL 58 and WL 106 should be further investigated by drilling and water-pressure testing if the dam extends this far.

5. UPPER BLENCOE CREEK DAM SITE

Geology

The geology of this area was described by Wolff (1960) as Elizabeth Creek Granite, the characteristics of which are given in the notes on the survey of Blencoe Creek dam site No. 5. Quartz-feldspar porphyry dykes up to 40 ft wide intrude the granite. Such dykes can be observed in the river bed.

Results

Plate 10 shows the traverse layout and Plates 11 and 12 show the seismic results obtained on this site. The velocities can be interpreted by referring to Table 1.

Between Stations WU 57 and 80, WU 24 and 40, WU 88 and 117, WU 137 and 155, and WU 160 and 179 a thin layer of soil and rubble in which the seismic velocity is about 1500 ft/sec covers slightly weathered to unweathered bedrock, in which the seismic velocity is 15,500 ft/sec or greater.

* Table 3 is on Page 11.

TABLE 3

Comparison of drilling and seismic results
Blencoe Creek dam site No. 5

| <u>Drill hole No.</u> <u>and position</u> | <u>Drill logs</u> | | <u>Seismic results</u> | |
|--|-------------------|---|------------------------|--------------------------|
| | <u>Depth (ft)</u> | <u>Geological formation</u> | <u>Depth (ft)</u> | <u>Velocity (ft/sec)</u> |
| 5/B1 at WL 18, dip 30 degrees | 0 - 8 | Moderately weathered microgranite | 0 - 11 | 1800 |
| | 8 - 12 | Slightly weathered microgranite | 11 + | 16,000 |
| | 12 - 80 | Bands of moderately and slightly weathered and fresh microgranite | | |
| 5/B2 20 ft east of WL 23.5 dip 35 degrees | 0 - 5 | Moderately weathered microgranite | 0 - 7 | 1800 |
| | 5 - 9 | Slightly weathered microgranite | 7 + | 17,000 |
| | 9 - 90 | Bands of moderately and slightly weathered and fresh microgranite | | |
| 5/B3 at WL 26, dip 30 degrees | 0 - 8 | Slightly weathered microgranite | 0 - 7 | 1800 |
| | 8 - 14 | Moderately weathered microgranite | 7 + | 17,000 |
| | 14 - 29 | Slightly weathered microgranite | | |
| | 29 - 44 | Fresh microgranite | | |
| 5/B4 30 ft south of WL 183, vertical | 0 - 16 | Overburden | 0 - 4 | 1000 |
| | 16 - 21 | Highly weathered microgranite | 4 - 18 | 2200 |
| | 21 - 50 | Moderately weathered microgranite | 18 - 52 52 + | 7000 16,500 |
| 5/B5 at WL 96, vertical | 0 - 135 | Decomposed and highly weathered granite | 0 - 6 6 - 57 | 1000 4500 |
| | 51 | Standing water level for dry weather | 57 - 120 | 7000 |
| | 135 - 146 | Moderately weathered granite | 120 + | 15,200 |
| | 146 - 149 | Slightly weathered granite | | |
| | 149 + | Fresh granite | | |

Between Stations WU 57 and WU 52, WU 189 and WU 199, WU 5 and WU 23, and WU 40 and WU 45 the depth to unweathered rock increases and intermediate layers of heavily and moderately weathered rock are recorded.

Between Stations WU 72 and WU 73 the transverse wave velocity was found to be 6500 ft/sec. This value, together with the longitudinal velocity of 16,000 ft/sec, gives a value of 0.40 for Poisson's ratio. Assuming the density of slightly weathered granite to 2.6 g/cm^3 , Young's modulus is $2.9 \times 10^{11} \text{ dyn/cm}^2$, or $4.2 \times 10^6 \text{ lb/in.}^2$.

Comparison with drilling information

*
Table 4 gives a comparison of the drilling information on this site with the geophysical results. For inclined drill holes, the depths have been corrected for dip. The agreement between seismic results and drilling results is fairly good except at drill holes 2/B1 and 1/B1, where the distances from the nearest seismic stations are 50 ft or more.

Conclusions

The survey shows that on the slopes, and close to (and probably also in) the river bed, the depth to unweathered bedrock is generally less than 15 ft, and the velocity in the bedrock exceeds 15,000 ft/sec.

On the relatively flat hill tops, weathering has progressed to a much deeper level; this is indicated by the occurrence of intermediate layers in which the seismic velocity is 10,000 to 12,000 ft/sec. The maximum depths recorded to unweathered rock are 94 ft near WU 14, and 87 ft near WU 52. A rock in which the seismic velocity is 11,000 to 12,000 ft/sec is usually strong and impermeable enough to be used for foundation purposes.

6. WEIR SITE

Geology

The geology of the area was described by Wolff (1960). From the river, near Station WW 38, to about Station WW 80 there is Herbert River Granite. This is intruded in the river bed and on the bank up to Station WW 25 by a quartz porphyry dyke.

In the neighbourhood of Station WW 92 a basalt ridge commences and extends north-easterly. Between Stations WW 83 and WW 96 the seismic traverse crosses this ridge and from Station WW 103 onwards the traverse continues along the crest of the ridge. Between Stations WW 171 and WW 196 the basalt has been eroded away to form a saddle. There are thin laterite remnants over Herbert River Granite along the floor of the saddle.

The part of Traverse WB surveyed was over Herbert River Granite. On the surface this had decomposed to sandy soil.

*

Table 4 is on Page 13.

TABLE 4

Comparison of drilling and seismic results

Upper Blencoe Creek dam site

| <u>Drill hole No. and Position</u> | <u>Drill logs</u> | | <u>Seismic results</u> | |
|--|-------------------|--|------------------------|----------------------------------|
| | <u>Depth (ft)</u> | <u>Geological formation</u> | <u>Depth (ft)</u> | <u>Velocity (ft/sec)</u> |
| 2/B1 50 ft west of WU 39, vertical | 0 - 44 | Moderately weathered feldspar porphyry | 0 - 4 | 1600 |
| | 44 - 61 | Slightly weathered feldspar porphyry | 4 + | 15,500 |
| 2/B2, 50 ft west of WU 35.5, dip 40 degrees | 0 - 6 | Moderately weathered porphyry | 0 - 4 | 1600 |
| | 6 - 22 | Slightly weathered porphyry | 4 + | 15,500 |
| 2/B3, 50 ft west of WU 32.5, dip 25 degrees | 0 - 10 | Moderately weathered granite | 0 - 6 | 1600 |
| | 10 + | Slightly weathered granite | 6 + | 16,000 |
| 2/B4 at WU 20, vertical | 0 - 27 | Decomposed and highly weathered granite | 0 - 34 | Intermediate layers not known |
| | 27 - 33 | Moderately weathered granite | 34 + | About 20,000 |
| | 33 - 36 | Highly weathered granite | | |
| | 36 + | Slightly weathered granite | | |
| 2/B5 at WU 14.5, vertical | 0 - 53 | Decomposed granite | 0 - 2 | 1200 |
| | 53 - 79 | Moderately weathered granite and porphyry | 2 - 12 | 3000 |
| | | | 12 - 52 | 6000 |
| | 79 - 86 | Slightly weathered porphyry | 52 - 80 | 8000 |
| | | 80 + | 15,500 | |
| 1/B1 100 ft north-west of WU 174, vertical | 0 - 5 | Decomposed granite | 0 - 2 | 1000 |
| | 5 - 55 | Moderately weathered granite | 2 - 28 | 12,000 |
| | 55 - 68 | Moderately and slightly weathered granite | 28 + | 15,500 |
| 1/B2 at WU 191, vertical | 0 - 5 | Decomposed granite | 0 - 7 | 1500 |
| | 5 - 10 | Highly weathered granite | 7 - 20 | 10,000 - 12,000 |
| | 10 - 33 | Moderately weathered granite | 20 + | 17,500 |
| 1/B3 at WU 197 vertical | 0 - 3 | Decomposed granite | 0 - 7 | 1500 |
| | 3 - 7 | Highly weathered granite | 7 - 60 | 10,000 to 12,000 |
| | 7 - 24 | Moderately weathered granite | 60 + | 17,500 |

Results

Plates 13, 14, and 15 show the seismic cross-sections and the measured longitudinal seismic velocities on this site. Using Table 1 these velocities can be translated into geological terms.

From Station WW 67 to WW 96 (Plate 13) there is an increase in depth to the unweathered granite bedrock, suggestive of an old river valley filled with basalt. The 11,000-ft/sec layer probably represents slightly weathered basalt, over which are layers of decomposed and weathered basalt.

From Station WW 91 to WW 126 (Plate 14) along the crest of the ridge the depth is shown to an 11,000-ft/sec layer which is interpreted as slightly weathered basalt. There are indications that a higher-velocity layer exists beneath this, presumably unweathered granite.

At Station WW 166 the seismic cross-section is interpreted as layers of very weathered basaltic material over a layer of slightly weathered vesicular basalt at a depth of about 18 ft. Between Stations WW 176 and WW 196 a 13,000-ft/sec refractor is the deepest one recorded; this could represent slightly to moderately weathered granite or slightly weathered basalt. There were again indications of a high-velocity layer underneath this.

The velocity distribution along Traverse WB (Plate 15) can be interpreted as successive layers of soil and heavily, moderately, and slightly weathered granite over unweathered unjointed granite bedrock.

Conclusions

From WW 20 to WW 67 the 7000 to 8000-ft/sec layer should form a suitable foundation for a low weir. The permeability of this layer should be checked by drilling.

In the area east and north-east of WW 70, the geophysical results suggest the presence of an old river valley filled with basalt. Past experience indicates that with this type of structure, depth determinations are not better than ± 20 percent accurate. To check this area, drilling is recommended at Stations WW 81, WW 86, WW 91, and WW 121. These drill holes should also give information about the permeability of the 5000 to 6000-ft/sec layer.

A drill hole is recommended near Station WW 181 to prove the structure in the saddle area.

7. BLENCOE PENSTOCK RIDGE

Geology

The general geology of the area was described by Wolff (1960). The penstock ridge consists of granite covered by a mantle of weathered to highly weathered and decomposed granite, with scree material on the surface.

The ridge goes down to the Herbert River Gorge, which was formed on a major fault or shear zone (White, 1961, Fig. 8 and Plate 1). At the top of the ridge, near WP 3, the granite is covered by basalt. Basalt scree material is also found along the slope, down to about WP 15.

Results

The results are shown on the seismic cross-section in Plate 16. Overburden is defined as rock in which the seismic velocity is less than 7000 ft/sec. Such rock is not strong enough to support engineering structures such as penstock lines. The overburden consists of scree material, soil, and highly weathered granite, in which the seismic velocities range from 1000 to 5000 ft/sec, and weathered granite in which the velocity is about 6700 ft/sec.

In this locality, bedrock is defined as rock in which the measured seismic velocity is greater than 9000 ft/sec. At WP 4 a 12,000-ft/sec layer probably represents a basalt overlying the granite. The lateral extent of the basalt is not known.

Between WP 7 and WP 15 the calculated depth to bedrock (16,000-ft/sec velocity, probably unweathered granite) ranges from 55 to 99 ft.

Between WP 25 and WP 45 the bedrock is relatively deep; the calculated distance between the surface and the bedrock ranges from 108 to 200 ft. The seismic velocities within the bedrock range between about 13,000 ft/sec near WP 27 and 9500 ft/sec near WP 42. The 13,000-ft/sec layer probably represents slightly weathered and fractured granite. The 9500-ft/sec layer may represent moderately weathered, fractured, or sheared granite possibly belonging to the Herbert River Gorge fault zone.

Conclusions

The depth to bedrock is relatively large. Apart from the relatively high costs connected with deep foundations, the sloping ground surface and bedrock profile may cause future land slips. Hence, this locality is not recommended as a site for penstock lines.

8. TANNER PENSTOCK RIDGE

Geology

The area was mapped by Wolff (1960) as Herbert River Granite with a patch of olivine basalt covering the approximate centre of the traverse. Personal observations along the traverse defined the geology more precisely, as given below.

From Stations WT 187 to WT 195 (Plate 17) the surface cover is rubble derived from decomposed granite. Between Stations WT 195 and WT 208 and Stations WT 217 and WT 254 the granite is capped with very weathered vesicular basalt. Elsewhere the surface cover is sandy loam derived from decomposed granite.

Results

Between Stations WT 187 and WT 195 the 1000-ft/sec layer corresponds to soil, the 4000-ft/sec layer to very weathered and decomposed granite, the 9600-ft/sec layer to moderately weathered granite, and the 13,000-ft/sec layer to slightly weathered or slightly jointed granite. This layer was the deepest refractor recorded. It is possible that unweathered granite exists at a greater depth than the technique used would attain, i.e. more than 200 ft.

In the vicinity of Station P 11 the 1000-ft/sec layer corresponds to soil, the 4000-ft/sec layer to very weathered basalt, the 7700-ft/sec layer to slightly to moderately weathered vesicular basalt, and the 16,000 to 17,000-ft/sec layer to unweathered granite bedrock.

At Station WT 214, the 1000-ft/sec layer corresponds to soil, the 4700-ft/sec layer to very weathered granite, the 7000-ft/sec layer to moderately weathered granite, and the 16,000 to 18,000-ft/sec layer to unweathered granite bedrock.

Between Stations WT 214 and WT 218 the structure is complex and it is difficult to give a reliable interpretation. It is possible that there is a shear zone in the granite bedrock, in which case the inferred 18,500-ft/sec velocity would not be correct over this part of the cross-section. It is recommended that this region be investigated further before any construction work is commenced.

From Stations WT 220 to WT 234 there is a thin cover of highly weathered basalt, in which the velocity is 3000 ft/sec, over unweathered granite bedrock.

From Stations WT 234 to WT 254 there is a thin cover of highly weathered basalt over a solid unweathered basalt bedrock or a slightly weathered or jointed granite bedrock.

Between Stations WT 254 and WT 274, the 1000-ft/sec layer corresponds to soil, the 2000-ft/sec layer to soil and rubble, the 3000-ft/sec layer to very weathered decomposed granite, the 5000 to 6000-ft/sec layer to very weathered granite, and the 16,000 to 18,000-ft/sec layer to unweathered granite bedrock.

Conclusions

Although this is not an ideal site for a penstock line, it is very much better geologically than the Blencoe penstock ridge. The topography suggests that there would be little chance of an earth slip, and so layers in which the seismic velocity is 6000 ft/sec or greater would be suitable foundation rocks. However, the structure between WT 214 and WT 222 is complex and requires further investigation.

9. FLUME LINE

Geology

The area covered by the traverse was mapped by Wolff (1960) as laterite or lateritic soil overlying Tertiary basalt. The basalt in turn overlies Palaeozoic Herbert River Granite. The basalt is vesicular and porous, and closely jointed. In many places it has been eroded away, leaving granite on the surface.

Results

The seismic cross-section and measured longitudinal velocities are shown on Plate 18. Referring to Table 1, these may be interpreted as follows.

Between WF 5 and WF 25, the 5000-ft/sec layer probably represents weathered granite, but could also be weathered basalt or semi-consolidated sediments. The 3000-ft/sec layer could be laterite.

Near WF 25 the bedrock boundary shows a large step which may be a fault. The depths to bedrock shown between WF 25 and WF 35 could be as much as 40 ft too large as insufficient data were available to make accurate calculations.

From WF 25 to WF 55, the 1000-ft/sec layer corresponds to soil, the 3000 to 5000-ft/sec layer to very weathered and decomposed rock or laterite, and the 9000 to 10,000-ft/sec layer to moderately weathered granite or slightly weathered basalt.

The bedrock velocities above 15,000 ft/sec indicate a virtually unweathered, unjointed granite. Between WF 35 and WF 38, the 9000-ft/sec velocity in bedrock suggests a shear zone.

Conclusions

The 9000 to 10,000-ft/sec layer would be strong enough for the foundations of a flume line. However, the seismic cross-section should be checked by drill holes at WF 26 and WF 37.

10. TUNNEL LINE

Offside Creek area

According to Wolff (1960), the geology of this area is lateritic soil over Herbert River Granite.

The seismic cross-section and measured longitudinal velocities are shown in Plate 19. The velocities may be interpreted in terms of weathered granite with the help of Table 1. Owing to the great depth of weathering along the whole spread, it was not possible to obtain depths to bedrock except at the two ends. However, the time/distance curves plotted from the seismic records were sufficiently symmetrical to suggest that the interpolation of the layers between the ends of the spread is correct to within ± 15 percent.

Ring-barked area

Wolff (1960) describes this area as laterite and lateritic soil over basalt.

The seismic cross-section and measured longitudinal velocities are shown on Plate 20. Using Table 1, the velocities can be interpreted as follows:

| <u>Velocity (ft/sec)</u> | <u>Geological formation</u> |
|--------------------------|---|
| 900 | Soil |
| 3000 | Laterite |
| 4100 - 5700 | Weathered basalt |
| 8000 | Slightly weathered basalt or moderately weathered granite |
| 17,000 | Unweathered granite bedrock |

The bedrock profile suggests that in the vicinity of WT 34 there is an old valley which has been filled with a basalt flow. This could be checked by drill holes near Stations WT 34 and WT 24.

Middle Creek area

Wolff (1960) mapped this area as Herbert River Granite. In addition, some laterite was observed on the left bank of the creek, between Stations WT 59 and WT 68.

Plate 21 shows the seismic cross-section and the measured longitudinal velocities. Using Table 1, these velocities may be interpreted as follows:

| <u>Velocity (ft/sec)</u> | <u>Geological formation</u> |
|--------------------------|---|
| 1000 | Soil |
| 7700 - 8000 | Moderately weathered granite |
| 14,000 | Slightly weathered and slightly jointed granite bedrock |
| 16,000 - 17,000 | Unweathered granite bedrock |

The 5200-ft/sec layer could be either dense laterite, or compacted alluvial sediments. This second possibility is suggested by the topography, which has the form of a river terrace. If the tunnel is planned to pass through the 8000-ft/sec layer near Station WT 63, a drill hole is recommended to clarify this point.

Showerbath Creek area

Wolff (1960) records the geology of this area as Herbert River Granite. Personal observations also revealed laterite conglomerate on the creek banks and laterite soil extending to Station WT 112.

Plate 22 shows the seismic cross-section and the measured longitudinal velocities along this traverse. These velocities may be interpreted with the aid of Table 1.

At Station WT 82, the 8500-ft/sec layer is moderately weathered granite. Elsewhere along this cross-section, the 5000-ft/sec layer could be either dense laterite or very weathered granite.

The 14,000-ft/sec velocity in bedrock indicates slightly weathered or slightly jointed granites; the 17,000-ft/sec velocity in bedrock indicates unweathered, unjointed granite.

Blencoe Flats area

This area was mapped by Wolff (1960) as laterite and weathered granite, over granite bedrock.

Plate 23 shows the seismic cross-sections and the measured longitudinal velocities. These velocities may be interpreted as follows:

| <u>Velocity (ft/sec)</u> | <u>Geological formation</u> |
|--------------------------|--------------------------------|
| 1200 | Soil |
| 3000 - 5000 | Decomposed granite or laterite |
| 6500 | Very weathered granite |
| 8000 - 9000 | Moderately weathered granite |
| 17,000 - 20,000 | Unweathered granite bedrock |

It was not possible to obtain depths to bedrock between Stations WT 150 and WT 159, and between Stations WT 121 and WT 131, owing to deep weathering. However, the time/distance curve of the spread WT 150 to WT 159 was sufficiently symmetrical to permit the interpolation of the depths between the ends of the spread to a reasonable degree of certainty.

The structure between WT 121 and WT 131 was inferred from the shape of the time/distance curve. It is only approximate and should be confirmed by a drill hole.

Conclusions

In general, a slightly weathered granite or a slightly weathered to unweathered vesicular basalt in which the seismic velocity is 10,000 to 12,000 ft/sec is suitable for tunnels.

Tunnelling in rocks in which seismic velocities are less than 8000 ft/sec may be relatively expensive because of extra supports needed to keep the tunnel open.

11. CAMERON CREEK TUNNEL PORTAL

Geology

Wolff (1960) does not cover this area, but personal observation showed the rocks to be Herbert River Granite, with the remains of an old basalt flow crossing the seismic traverse between Stations WC 13 and WC 17. The surface basalt has been decomposed to small angular boulders and dark soil. Elsewhere the surface cover was the light sandy loam typical of decomposed Herbert River Granite, with occasional granite boulders.

Results

These are shown on Plate 24. At Stations WC 3 and WC 23, the velocities may be interpreted as :

| <u>Velocity (ft/sec)</u> | <u>Geological formation</u> |
|--------------------------|---------------------------------|
| 1000 | Soil |
| 3000 | Very weathered granite |
| 6500 | Weathered granite |
| 15,000 - 20,000 | Unweathered, unjointed granite. |

In the vicinity of Station WC 13, the 6500-ft/sec layer could be moderately weathered basalt. The 9500 and 12,000-ft/sec bedrock velocities are either due to basalt or to fractured and sheared granite.

Conclusions

This site is not very satisfactory for a tunnel portal because of the considerable thickness of 3000-ft/sec and 6500-ft/sec material.

12. CAMERON CREEK DIVERSION

Geology

The geological information was obtained from Wolff (1960), supplemented by data from drill hole HR 15 situated near Station WD 23. The oldest rock consists of Palaeozoic Herbert River Granite. In a later stage, the eroded granite surface was covered by Tertiary basalt flows. The granite shows well-developed jointing, and in places is deeply dissected and weathered along the joints. The basalt is vesicular, porous, and closely jointed. In many places it has been removed by erosion. In this locality, the basalt and granite are covered by Cameron Creek sediments of unconsolidated sand, sandstone, and mudstone, generally less than 20 ft thick.

Results

Plate 25 shows the seismic cross-section and velocities; the latter may be interpreted as follows :

| <u>Velocity (ft/sec)</u> | <u>Geological formation</u> |
|--------------------------|---|
| 1000 - 2000 | Soil, unconsolidated sand and clay |
| 3000 - 4000 | Water-saturated clay and sand, very weathered and decomposed granite and basalt |
| 8000 - 9000 | Moderately weathered granite, or moderately weathered vesicular basalt |
| 14,000 - 15,000 | Unweathered granite, possibly slightly jointed. |

Between Stations WD 9 and WD 23 the deepest refractor recorded was a 9000-ft/sec layer, which is interpreted as basalt. The seismic data suggest the presence of a subsurface valley in the granite, some 250 ft deep and filled with basalt.

Conclusions

A drill hole between Stations WD 15 and WD 18 is recommended to confirm the structure in the suggested basalt-filled valley. However, the 8000 to 9000-ft/sec layer of slightly weathered basalt or granite should be suitable to carry a diversion channel or tunnel.

13. RECOMMENDATIONS

Of the three proposed schemes mentioned on Page 1, the geophysical results suggest that the third is the most satisfactory. Although no seismic work was done along the line of the tunnel from Upper Cameron Creek to the Upper Blencoe Creek dam, the geology of the area suggests that tunnelling conditions would be similar to those found along the Kooragwin to Blencoe Creek tunnel line. However, a more suitable site for a tunnel portal should be found on Cameron Creek.

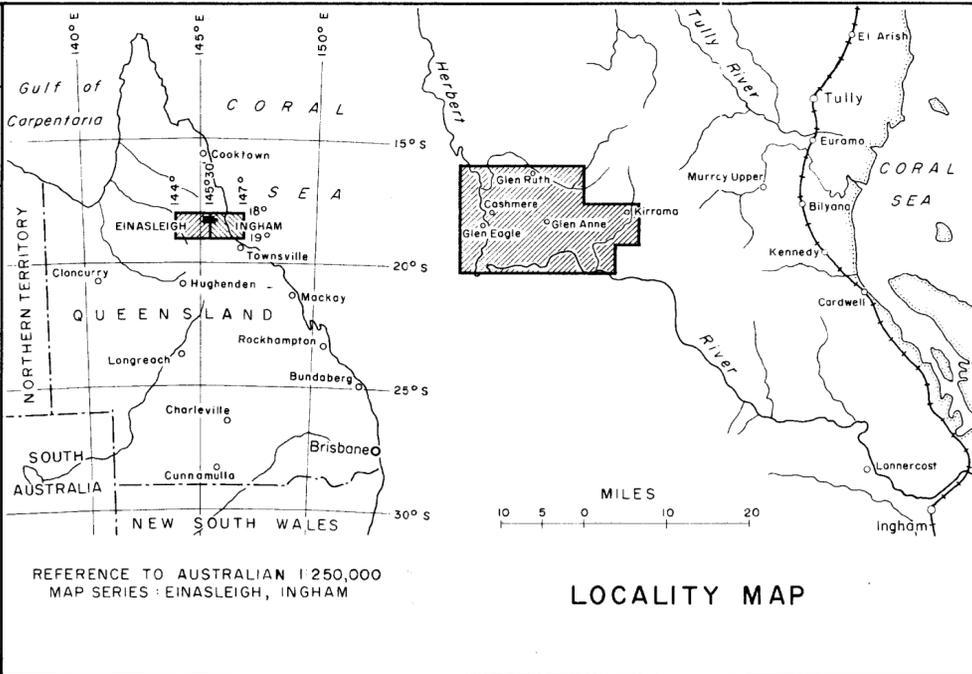
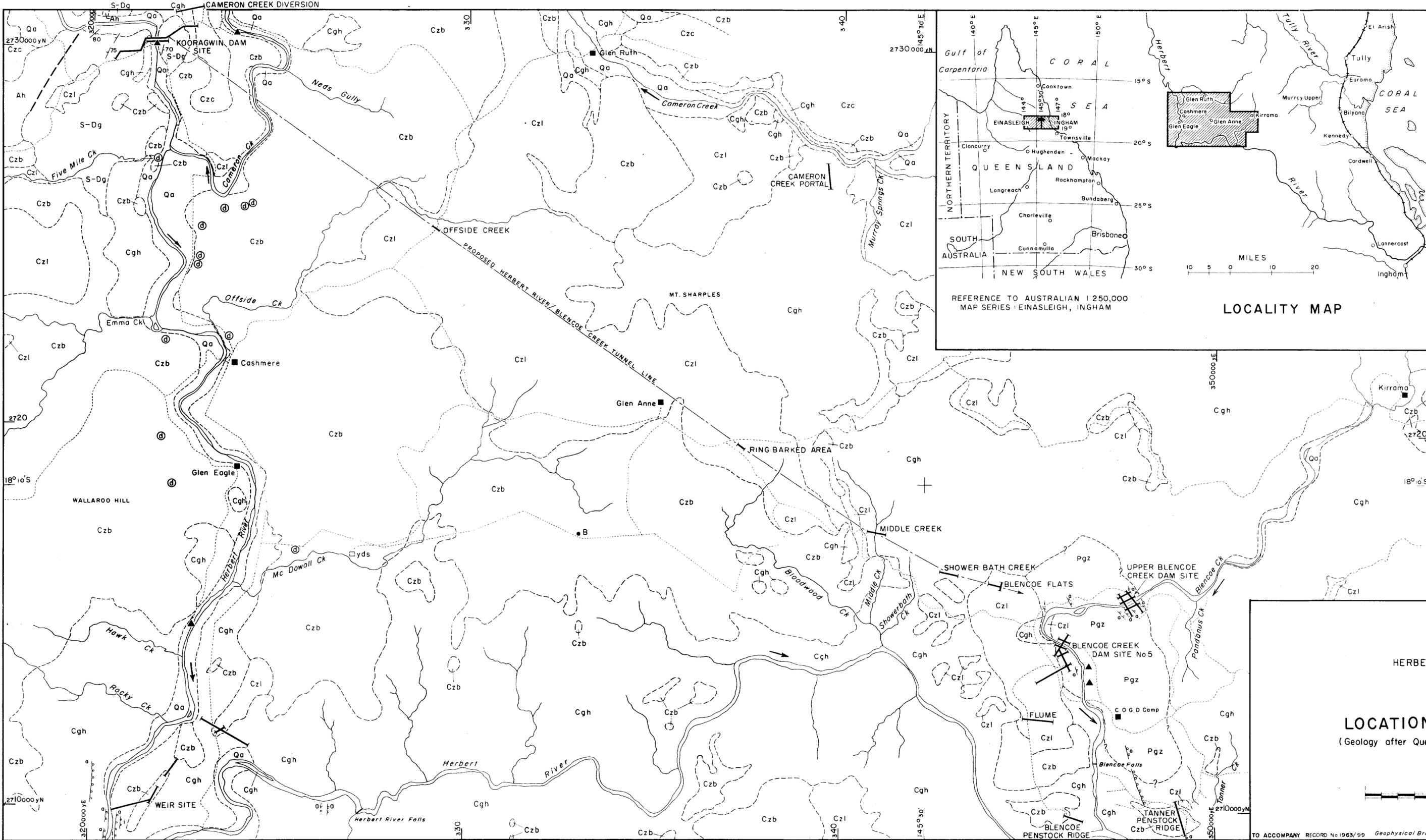
Foundations for both dam sites on Blencoe Creek appear to be satisfactory. However, as the Tanner penstock ridge is much more suitable than the Blencoe penstock ridge, a penstock from Upper Blencoe Creek dam to a power station at the confluence of Tanner Creek and Herbert River is recommended.

As areas of deep weathering and occasional shear zones have been found throughout the investigation area, it is recommended that the total length of the tunnel line and penstock line be surveyed by geophysical methods before any construction work is commenced.

14. REFERENCES

- | | | |
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- | | | |
|-------------|------|---|
| WOLFF, K.W. | 1960 | Herbert River hydro-electric investigation, geological reconnaissance of project area. <u>geol. Surv. Qld. Rep.</u> (unpubl.) |
| WOLFF, K.W. | 1961 | <u>geol. Surv. Qld.</u> , Drawing E14-R-4. |



LEGEND

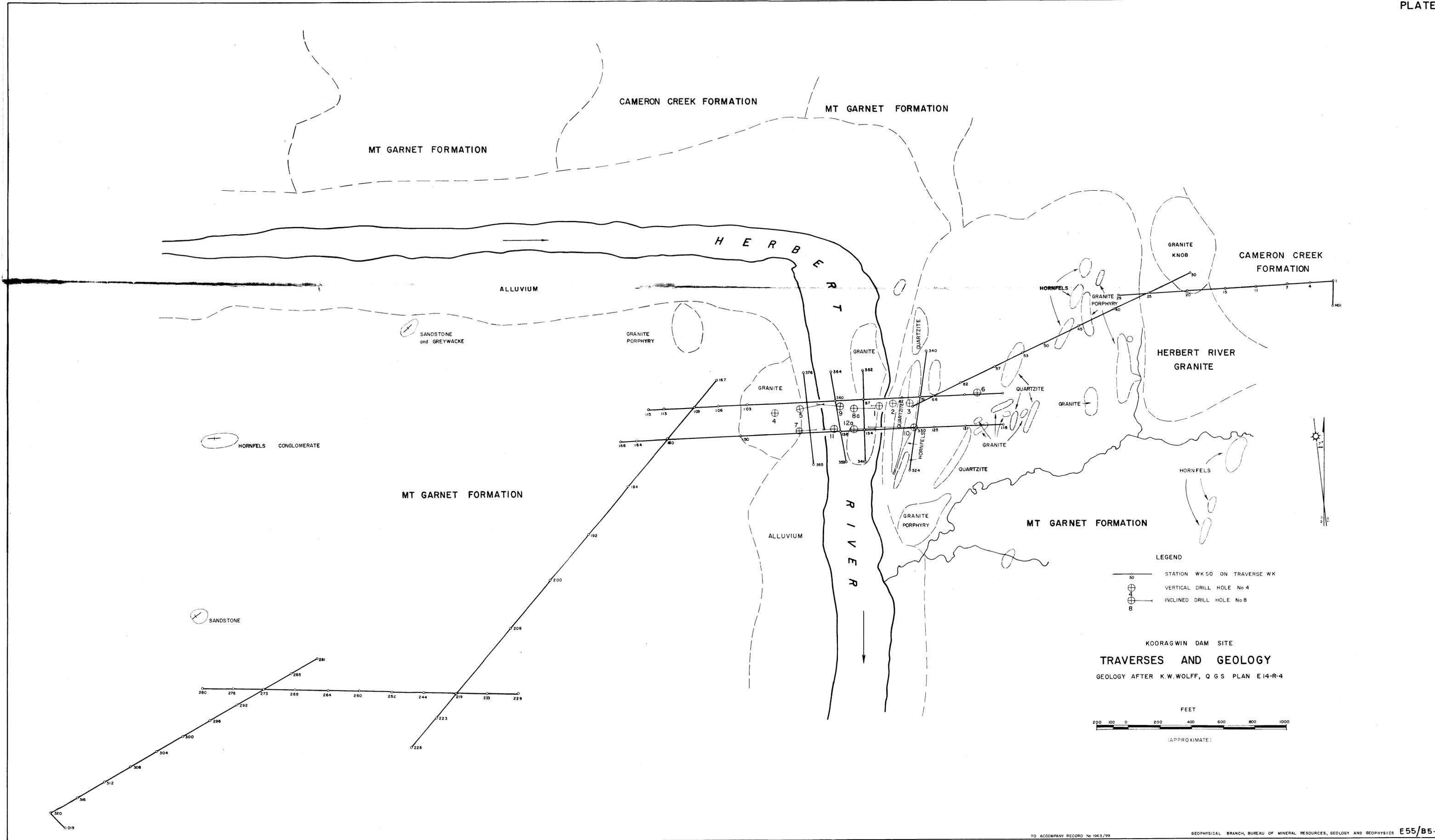
| | | |
|------|----------------------------|-----------------|
| Qa | QUATERNARY | |
| Czc | Cameron Creek Formation | CAINOZOIC |
| Czl | Laterite and Laterite soil | |
| Czb | Olivine basalt | TERTIARY |
| Pgz | Elizabeth Creek Granite | ? PERMIAN |
| Pgt | Tiger Hill Microgranite | |
| Cgh | Herbert River Granite | ? CARBONIFEROUS |
| S-Dg | Mt. Garnet Formation | SILURO-DEVONIAN |
| Ah | Halls Reward Metamorphics | ARCHÆAN |
| | | PRECAMBRIAN |

| | |
|--|-----------------------------------|
| | Geological boundary |
| | Strike and dip of strata |
| | Fault |
| | Diatomite deposit |
| | Dyke a - acid i - intermediate |
| | Vehicle track |
| | Homestead |
| | Bore |
| | Gauging station |
| | Geophysical traverse |

HERBERT RIVER HYDRO-ELECTRIC INVESTIGATION,
QUEENSLAND 1961.

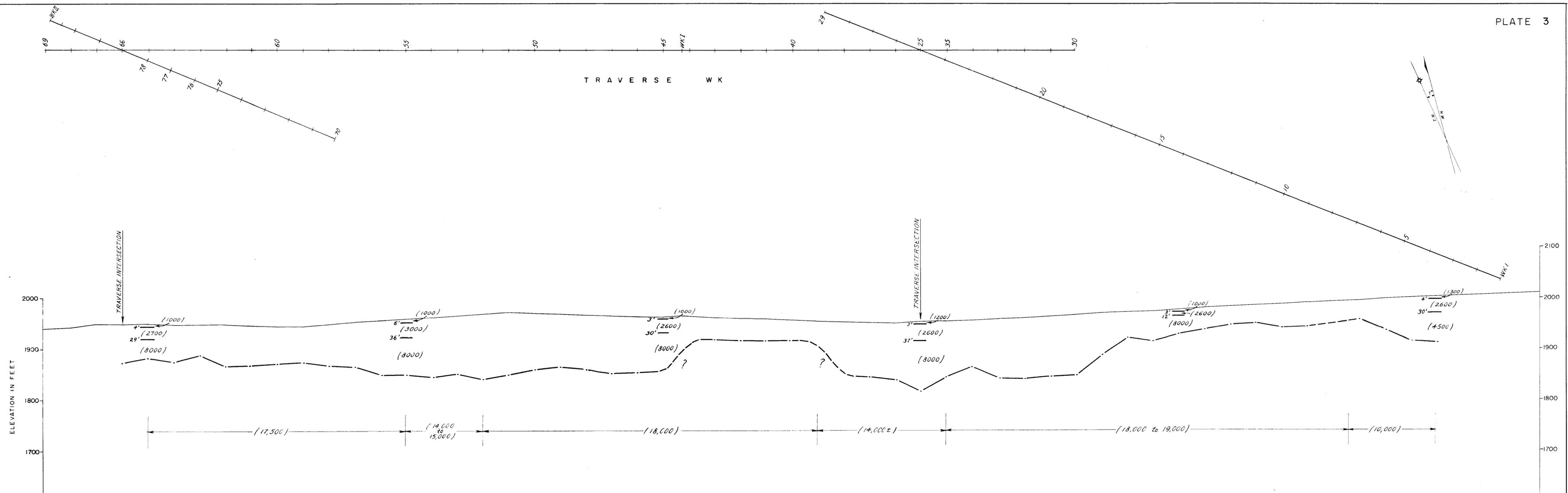
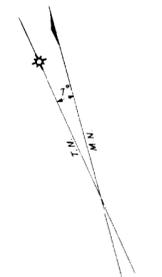
**GEOLOGY AND
LOCATION OF GEOPHYSICAL TRAVERSES**
(Geology after Queensland Department of Development and Mines, plan E14-A-5)





HERBERT RIVER QLD 1962

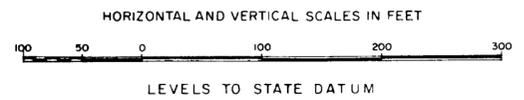
TRAVERSE WK



| STATION NUMBER | STATION ELEVATION | DEPTH TO BEDROCK |
|----------------|-------------------|------------------|
| 1943 WK1 | | |
| 68 | 1945 | |
| 67 | 1950 | |
| 66 | 1950 | (15) |
| 65 | 1950 | 66 |
| 64 | 1950 | 72 |
| 63 | 1949 | 58 |
| 62 | 1950 | 82 |
| 61 | 1947 | 78 |
| 60 | 1947 | 73 |
| 59 | 1944 | 69 |
| 58 | 1949 | 80 |
| 57 | 1955 | 36 |
| 56 | 1958 | 106 |
| 55 | 1961 | 108 |
| 54 | 1963 | 117 |
| 53 | 1966 | 113 |
| 52 | 1969 | 127 |
| 51 | 1973 | 122 |
| 50 | 1974 | 110 |
| 49 | 1972 | 103 |
| 48 | 1970 | 105 |
| 47 | 1968 | 112 |
| 46 | 1967 | 108 |
| 45 | 1966 | 109 |
| WK1 | 1968 | 145 |
| 44 | 1963 | 41 |
| 42 | 1962 | 42 |
| 41 | 1962 | 42 |
| 40 | 1958 | 39 |
| 39 | 1957 | 39 |
| 38 | 1955 | 105 |
| 37 | 1954 | 105 |
| 36 | 1953 | 112 |
| 25 | 1956 | 135 |
| 24 | 1958 | 108 |
| 23 | 1959 | 89 |
| 22 | 1962 | 115 |
| 21 | 1964 | 118 |
| 20 | 1966 | 115 |
| 19 | 1970 | 115 |
| 18 | 1973 | 79 |
| 17 | 1976 | 48 |
| 16 | 1977 | 57 |
| 15 | 1980 | 46 |
| 14 | 1983 | 42 |
| 13 | 1986 | 35 |
| 12 | 1988 | 35 |
| 11 | 1990 | 44 |
| 10 | 1992 | 46 |
| 9 | 1995 | |
| 8 | 1997 | 37 |
| 7 | 1999 | 59 |
| 6 | 2002 | 85 |
| 5 | 2003 | 90 |
| 4 | 2005 | |
| 3 | 2006 | |
| 2 | 2010 | |
| WK1 | 2011 | |

LEGEND

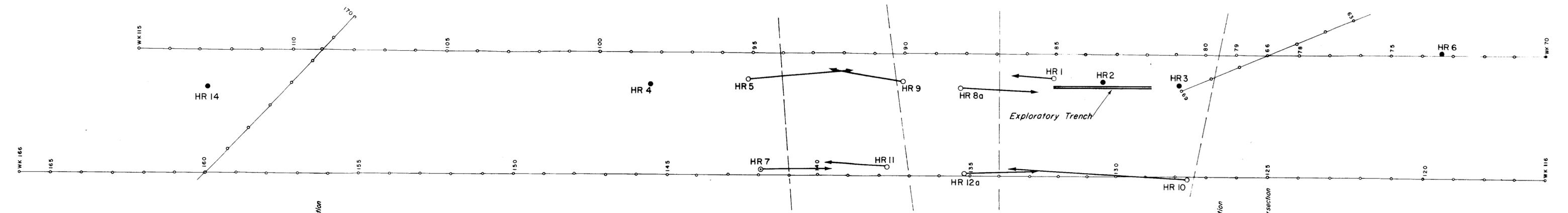
- Geophysical traverse with station number
- Formation with seismic velocity of 2000 ft/sec
- Depth to formation with different seismic velocity
- Bedrock boundary



KOORAGWIN DAM SITE
LAYOUT OF TRAVERSES AND SEISMIC CROSS-SECTION
BETWEEN STATIONS WK 1 & WK 69

NOTE: Topography from Coordinator General's Department Plans H1093 and H1094

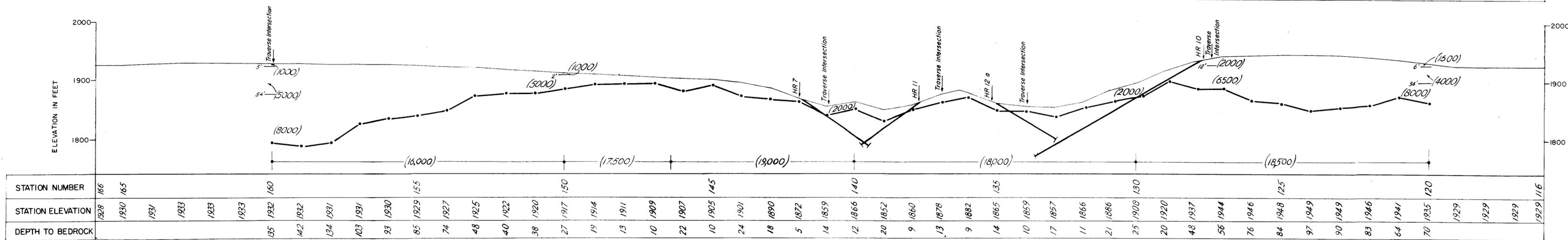
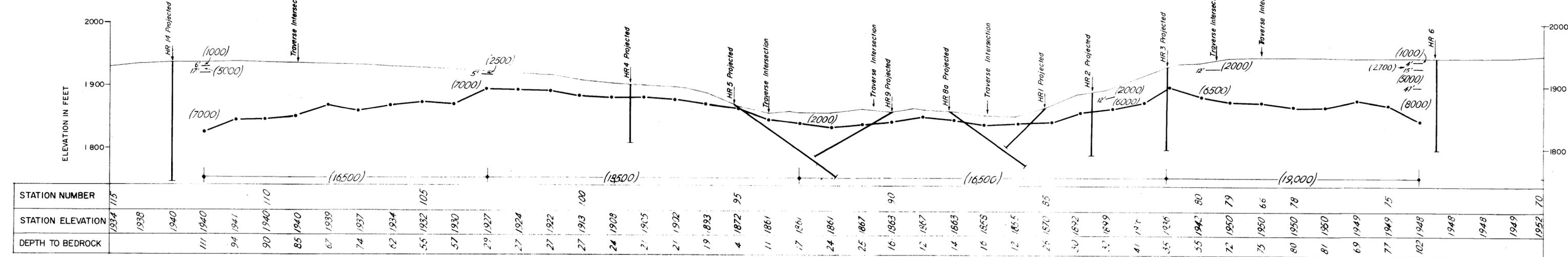
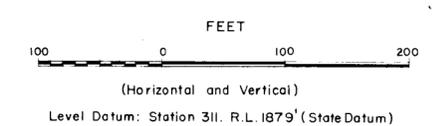
HERBERT RIVER, 1961 Q.L.D.



LEGEND

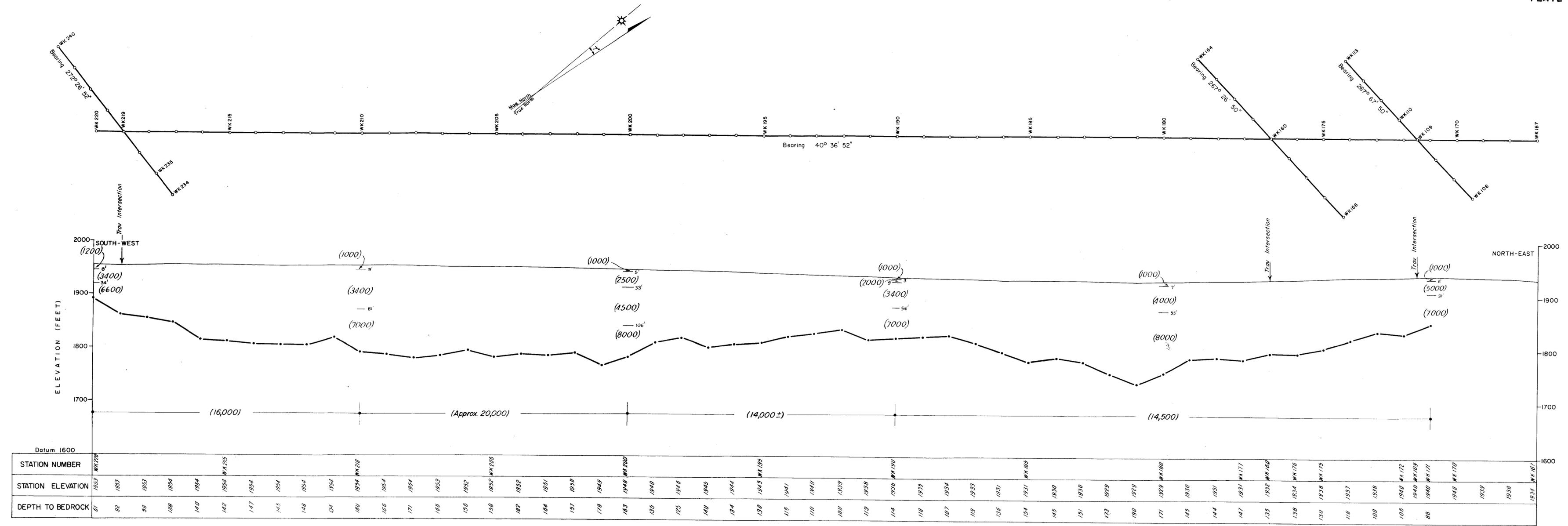
- Geophysical traverse with station number
- (2000) Formation with seismic velocity of 2000 ft/sec
- 15' Depth to formation with different seismic velocity
- Bedrock boundary
- Diamond drill hole (vertical)
- " " " (depressed)

Based on COG Drawing H1095, H1096, H1097

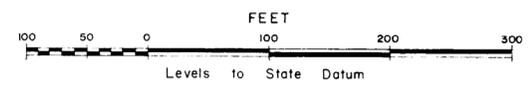


**KOORAGWIN DAM SITE
 LAYOUT OF TRAVERSES AND
 SEISMIC CROSS-SECTIONS
 BETWEEN STATIONS WK 70 AND WK 166**

HERBERT RIVER DAM SITES QUEENSLAND 1962



KOORAGWIN DAM SITE
LAYOUT OF TRAVERSES AND SEISMIC CROSS-SECTION
BETWEEN STATIONS WK 167 & WK 220



Geophysical traverse with station number
 Formation with seismic velocity of 2000 ft/sec
 31' — Depth to formation with different seismic velocity
 — — — — — Bedrock boundary
 Based on C O G Drawing H 1098

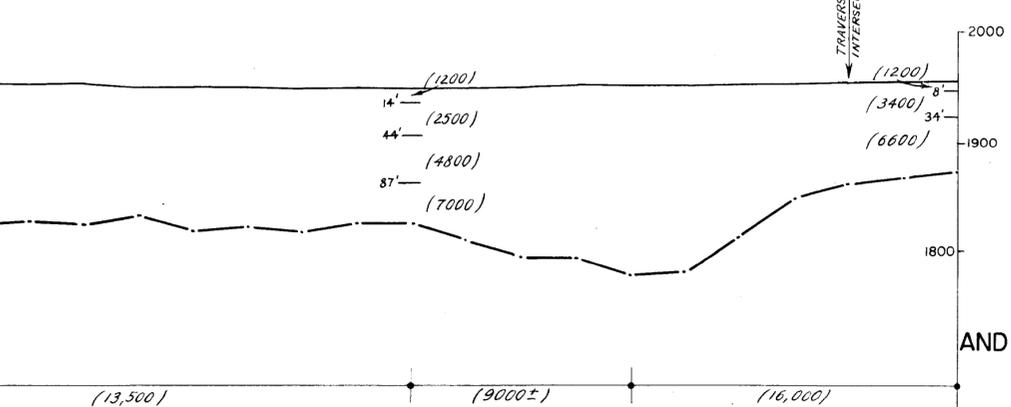
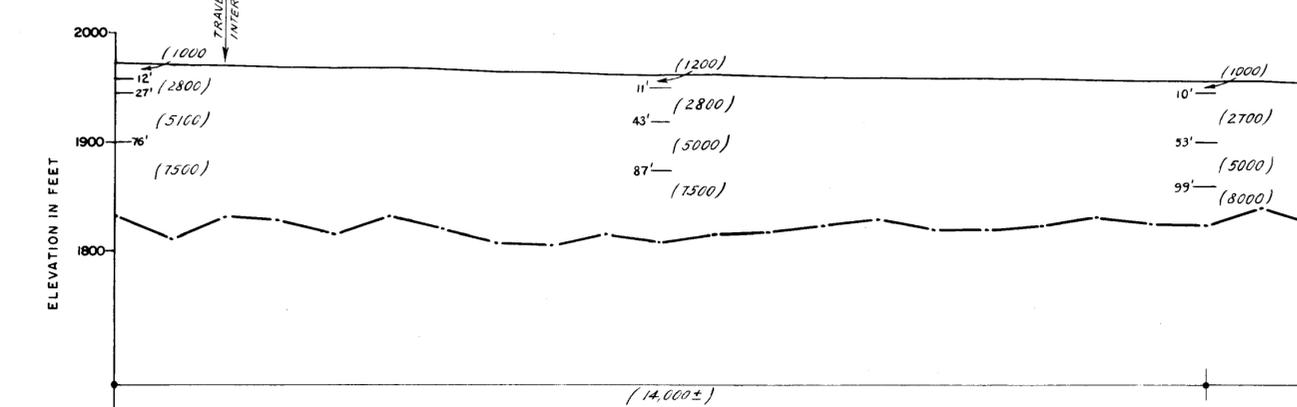
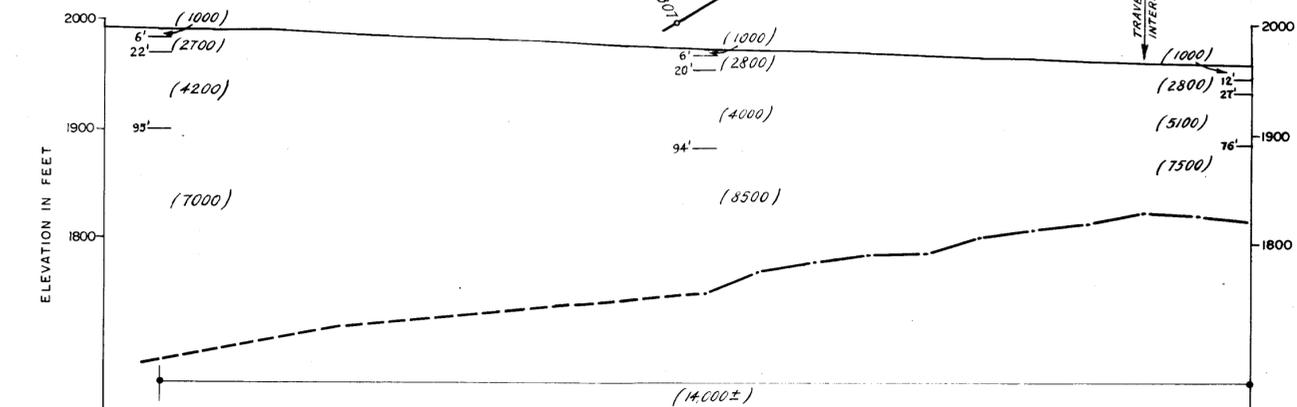
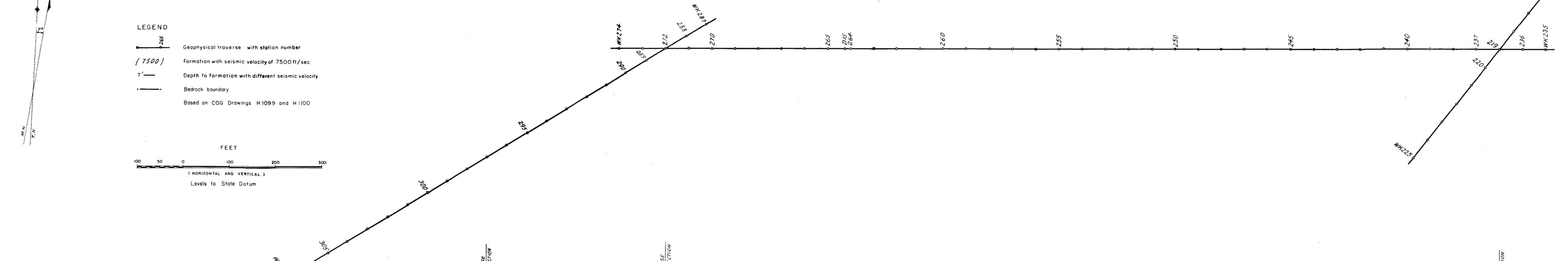
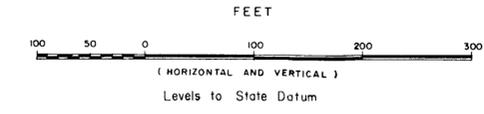
HERBERT RIVER, Q.L.D. 1962



LEGEND

- Geophysical traverse with station number
- (7500) Formation with seismic velocity of 7500 ft/sec
- 7' — Depth to formation with different seismic velocity
- Bedrock boundary

Based on COG Drawings H 1099 and H 1100



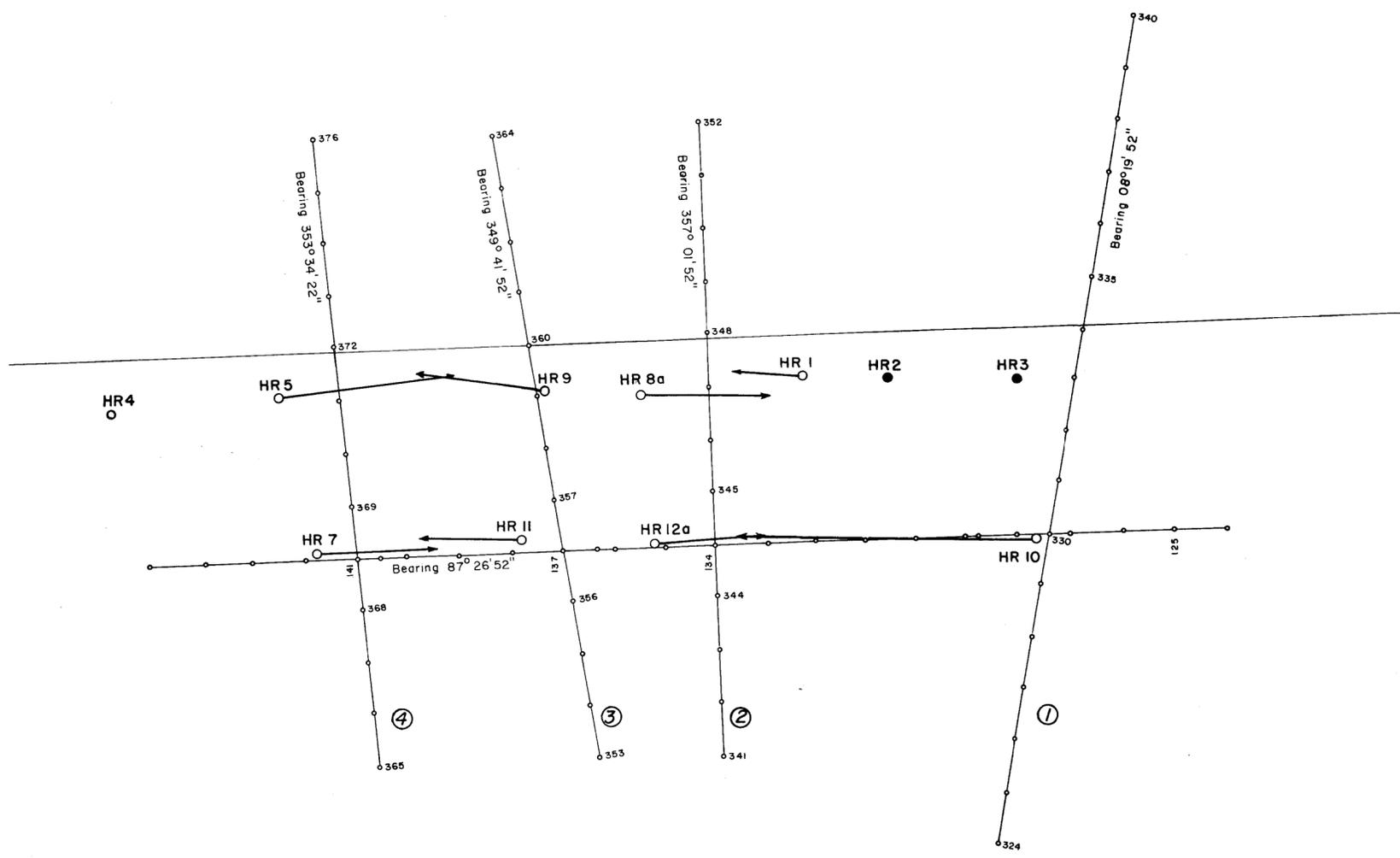
| | | | | | | | | | | | | | | | | | | | | | |
|-------------------|------------|----------|------|------|------|------|----------|------|------|------|------|----------|------|------|------|----------|----------|------------|----------|------------|--|
| STATION NUMBER | 1956 WK307 | 1954 305 | 1953 | 1951 | 1950 | 1948 | 1946 300 | 1946 | 1943 | 1942 | 1941 | 1939 295 | 1937 | 1936 | 1933 | 1932 290 | 1931 289 | 1930 WK272 | 1928 288 | 1927 WK272 | |
| STATION ELEVATION | 1900 | 1995 | | | | | | | | | | | | | | | | | | | |
| DEPTH TO BEDROCK | 180 | | | | | | | | | | | | | | | | | | | | |

| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|-------------------|------------|------|----------|------|------|------|------|------|------|------|----------|-----------|----------|------|------|------|----------|------|------|------|------|----------|------|------|------|----------|------|------|------|------|----------|------|------|------|------|----------|------|------|----------|------------|----------|------------|
| STATION NUMBER | 1917 WK274 | 1917 | 1910 272 | 1909 | 1908 | 1907 | 1906 | 1905 | 1904 | 1903 | 1902 265 | 1901 D.15 | 1901 264 | 1901 | 1900 | 1959 | 1958 260 | 1957 | 1957 | 1957 | 1956 | 1955 255 | 1955 | 1954 | 1953 | 1953 250 | 1952 | 1952 | 1951 | 1950 | 1950 245 | 1949 | 1949 | 1950 | 1951 | 1951 240 | 1952 | 1952 | 1952 237 | 1953 WK219 | 1953 236 | 1954 WK235 |
| STATION ELEVATION | 138 | 156 | 135 | 140 | 150 | 143 | 145 | 153 | 156 | 145 | 150 | 144 | 140 | 135 | 127 | 135 | 135 | 130 | 121 | 128 | 128 | 114 | 128 | 124 | 129 | 117 | 131 | 128 | 131 | 124 | 122 | 139 | 156 | 158 | 174 | 170 | 136 | 101 | 93 | 86 | 81 | |
| DEPTH TO BEDROCK | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

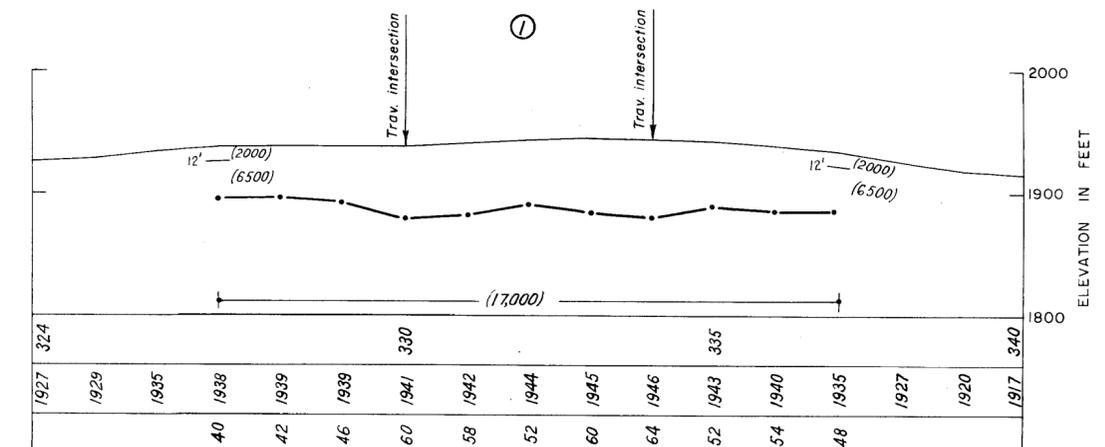
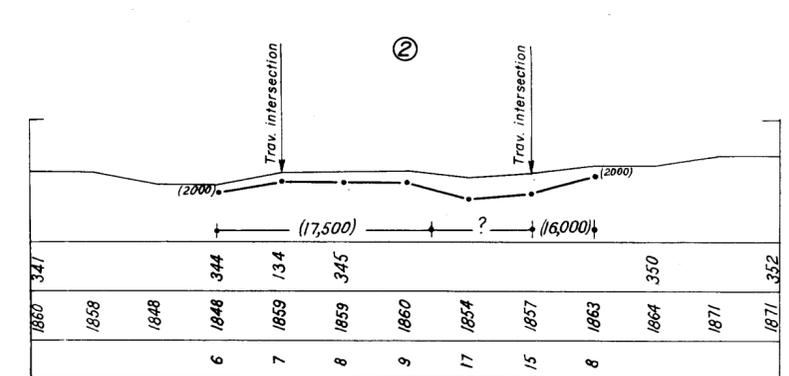
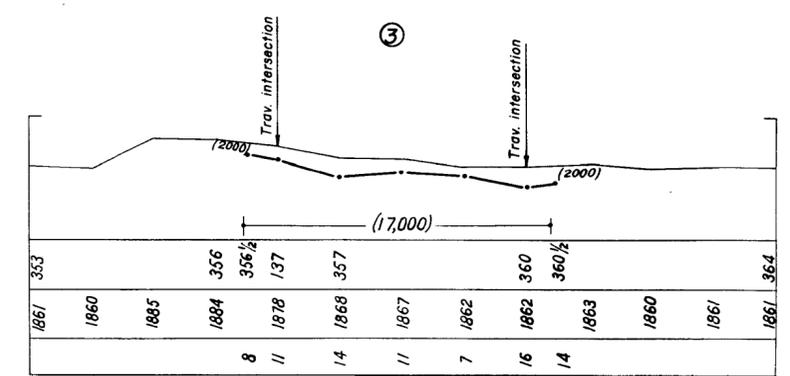
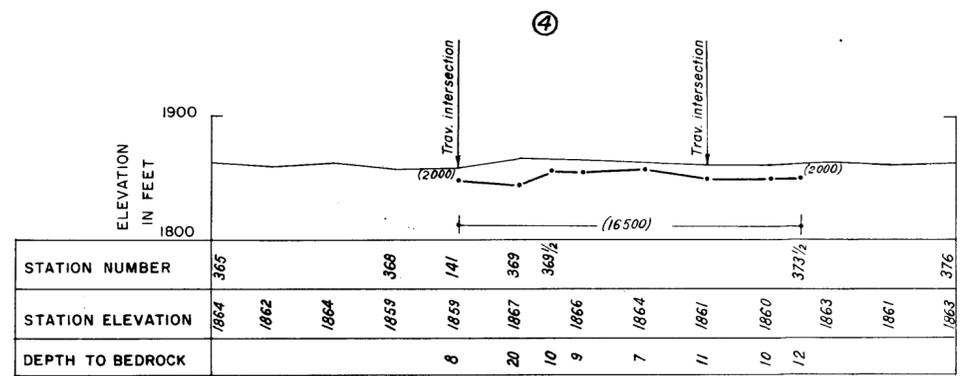
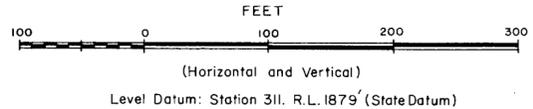
KOORAGWIN DAM SITE
LAYOUT OF TRAVERSES
AND SEISMIC CROSS-SECTIONS
BETWEEN STATIONS
W K 235 AND W K 307

KOORAGWIN DAM SITE, QLD 1961

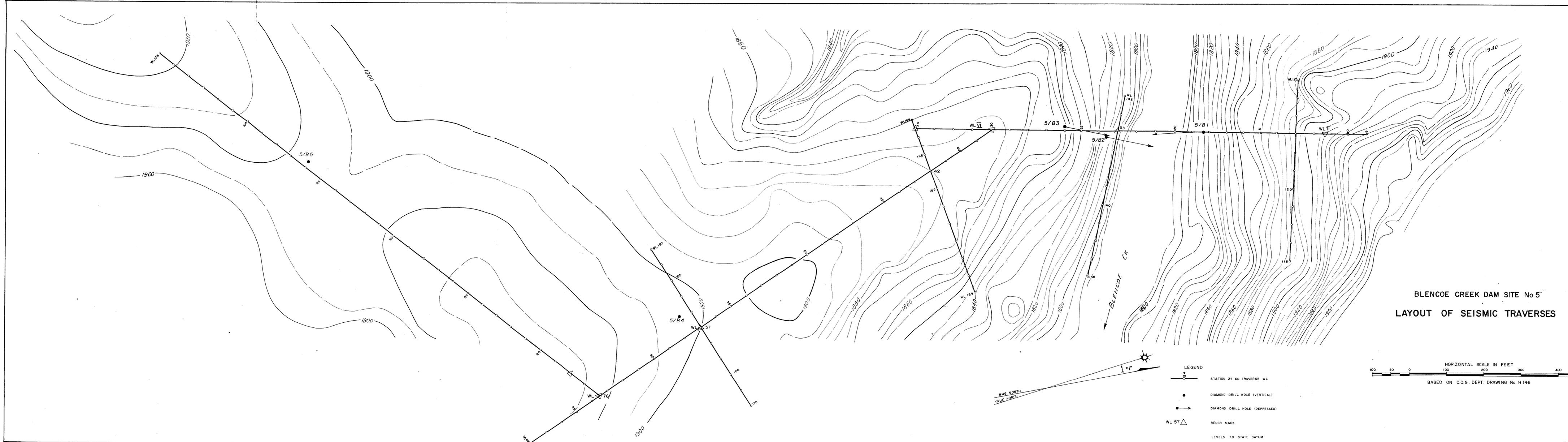
KOORAGWIN DAM SITE
 LAYOUT OF TRAVERSES AND
 SEISMIC CROSS-SECTIONS BETWEEN
 STATIONS WK 324 AND WK 376



LEGEND
 ○ 125 Geophysical traverse with station number
 (2000) Formation with seismic velocity of 2000 ft/sec
 12' Depth to formation with different seismic velocity
 — Bedrock boundary
 ● Diamond drill hole (vertical)
 ○ " " " (depressed)
 Based on COG Drawing H1097



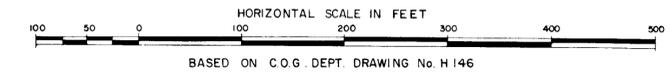
HERBERT RIVER, Kooragwin, Gld., 1961



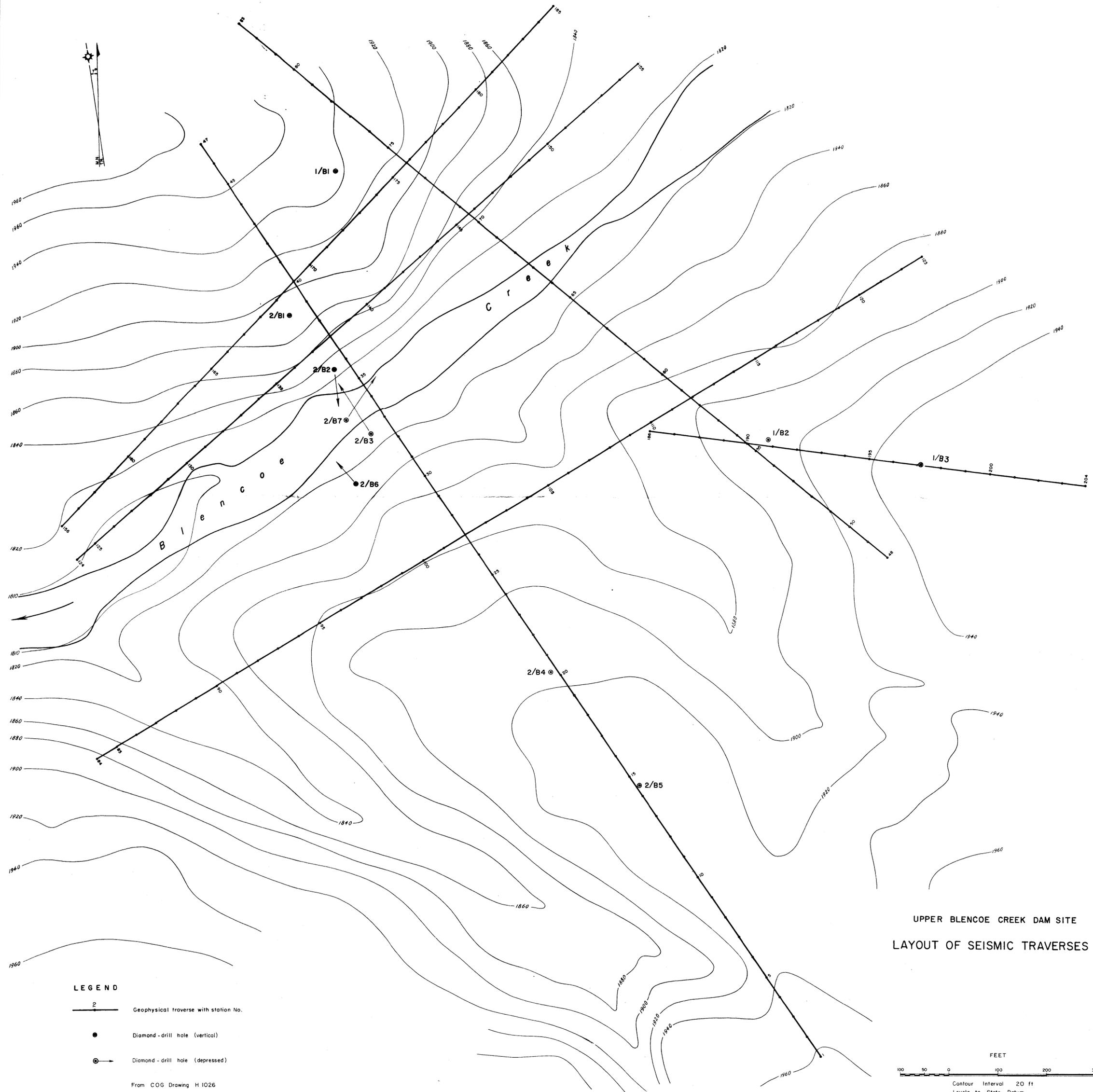
BLENCOE CREEK DAM SITE No 5
 LAYOUT OF SEISMIC TRAVERSES

LEGEND

- STATION 24 ON TRAVERSE WL
- DIAMOND DRILL HOLE (VERTICAL)
- ◐ DIAMOND DRILL HOLE (DEPRESSED)
- △ WL 57
- △ BENCH MARK
- LEVELS TO STATE DATUM



BLENCOE DAM SITE No 5 QLD 1962

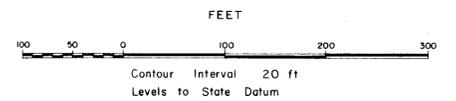


LEGEND

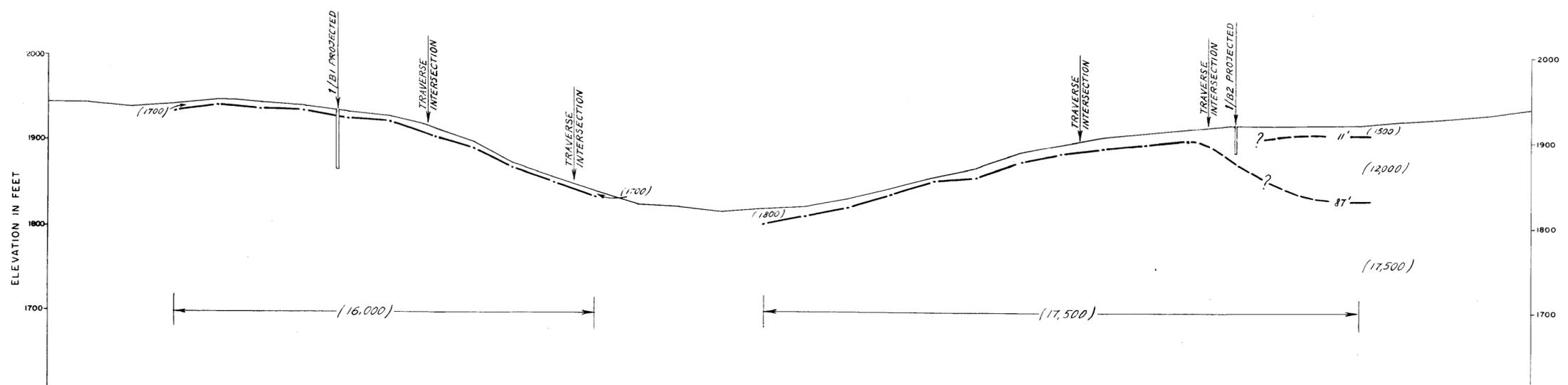
-  Geophysical traverse with station No.
-  Diamond-drill hole (vertical)
-  Diamond-drill hole (depressed)

From COG Drawing H 1026

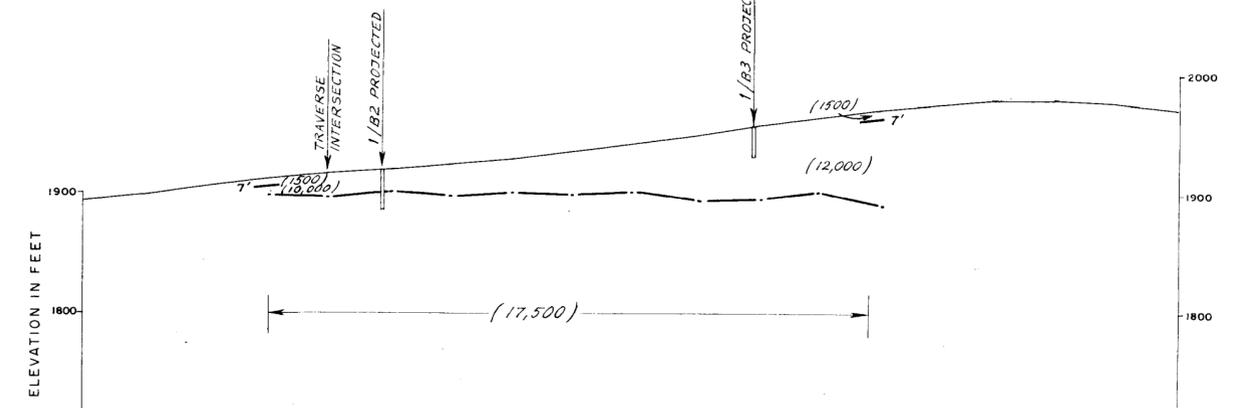
UPPER BLENCOE CREEK DAM SITE
LAYOUT OF SEISMIC TRAVERSES



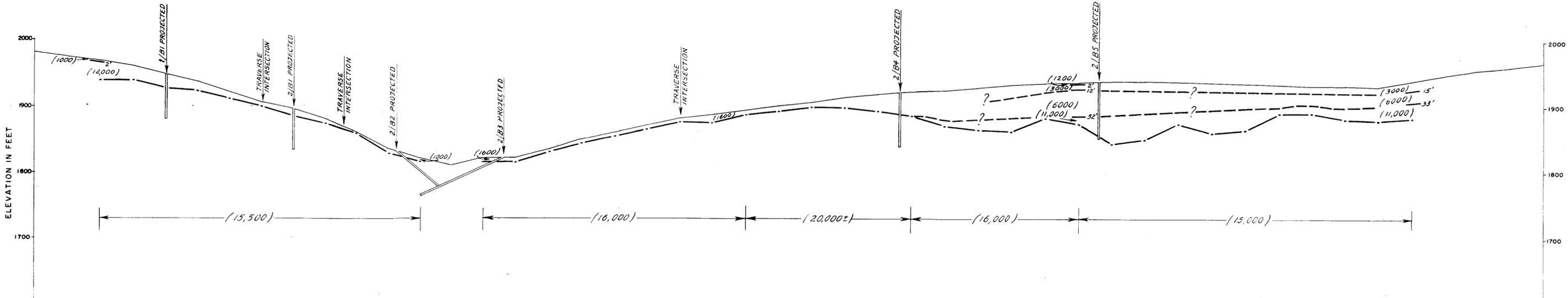
Harbert River Qld. 1961



| STATION NUMBER | STATION ELEVATION | DEPTH TO BEDROCK |
|----------------|-------------------|------------------|
| 1944 WU83 | | |
| 1944 82 | | |
| 1938 81 | | |
| 1943 80 | | 7 |
| 1948 79 | | 6 |
| 1945 78 | | 7 |
| 1940 77 | | 5 |
| 1933 76 | | 7 |
| 1928 75 | | 5 |
| 1915 74 | | 10 |
| 1899 73 | | 5 |
| 1875 72 | | 4 |
| 1858 71 | | 4 |
| 1842 70 | | 5 |
| 1827 69 | | |
| 1823 68 | | |
| 1819 67 | | |
| 1822 66 | | 17 |
| 1824 65 | | 9 |
| 1834 64 | | 8 |
| 1846 63 | | 7 |
| 1860 62 | | 4 |
| 1869 61 | | 10 |
| 1886 60 | | 9 |
| 1897 59 | | 11 |
| 1905 58 | | 12 |
| 1910 57 | | 14 |
| 1915 56 | | 13 |
| 1919 55 | | |
| 1919 54 | | |
| 1919 53 | | |
| 1919 52 | | 87 |
| 1924 51 | | |
| 1928 50 | | |
| 1932 49 | | |
| 1938 WU49 | | |



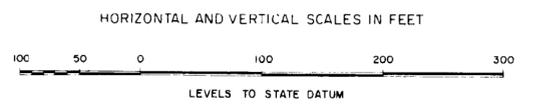
| STATION NUMBER | STATION ELEVATION | DEPTH TO BEDROCK |
|----------------|-------------------|------------------|
| 1893 WU186 | | |
| 1900 187 | | |
| 1907 188 | | |
| 1913 189 | | 14 |
| 1918 190 | | 20 |
| 1921 191 | | 18 |
| 1926 192 | | 26 |
| 1931 193 | | 28 |
| 1936 194 | | 35 |
| 1944 195 | | 40 |
| 1951 196 | | 54 |
| 1959 197 | | 60 |
| 1966 198 | | 61 |
| 1972 199 | | 79 |
| 1977 200 | | |
| 1981 201 | | |
| 1981 202 | | |
| 1979 203 | | |
| 1974 WU204 | | |



| STATION NUMBER | STATION ELEVATION | DEPTH TO BEDROCK |
|----------------|-------------------|------------------|
| 1980 WU47 | | |
| 1974 46 | | |
| 1968 45 | | 28 |
| 1959 44 | | 21 |
| 1948 43 | | 21 |
| 1937 42 | | 12 |
| 1921 41 | | 8 |
| 1905 40 | | 3 |
| 1895 39 | | 8 |
| 1880 38 | | 4 |
| 1861 37 | | 1 |
| 1835 36 | | 5 |
| 1821 35 | | 4 |
| 1811 34 | | |
| 1823 33 | | 6 |
| 1823 32 | | 6 |
| 1837 31 | | 4 |
| 1852 30 | | 6 |
| 1861 29 | | 6 |
| 1872 28 | | 6 |
| 1884 27 | | 7 |
| 1890 26 | | 13 |
| 1899 25 | | 8 |
| 1904 24 | | 8 |
| 1909 23 | | 7 |
| 1917 22 | | 17 |
| 1921 21 | | 27 |
| 1925 20 | | 37 |
| 1928 19 | | 54 |
| 1932 18 | | 66 |
| 1935 17 | | 72 |
| 1938 16 | | 53 |
| 1939 15 | | 65 |
| 1940 14 | | 94 |
| 1940 13 | | 88 |
| 1940 12 | | 63 |
| 1938 11 | | 76 |
| 1936 10 | | 70 |
| 1935 9 | | 45 |
| 1933 8 | | 44 |
| 1933 7 | | 52 |
| 1931 6 | | 53 |
| 1940 5 | | 57 |
| 1950 4 | | |
| 1956 3 | | |
| 1961 2 | | |
| 1967 WU1 | | |

LEGEND
 (1000) Formation with seismic velocity of 1000 ft/sec
 15' Depth to formation with different seismic velocity
 — Bedrock boundary
 T Projection of diamond-drill hole

**UPPER BLENCOE CREEK DAM SITE
 SEISMIC CROSS-SECTIONS
 BETWEEN STATIONS WU 1 & WU 83, & STATIONS WU185 & WU 204**

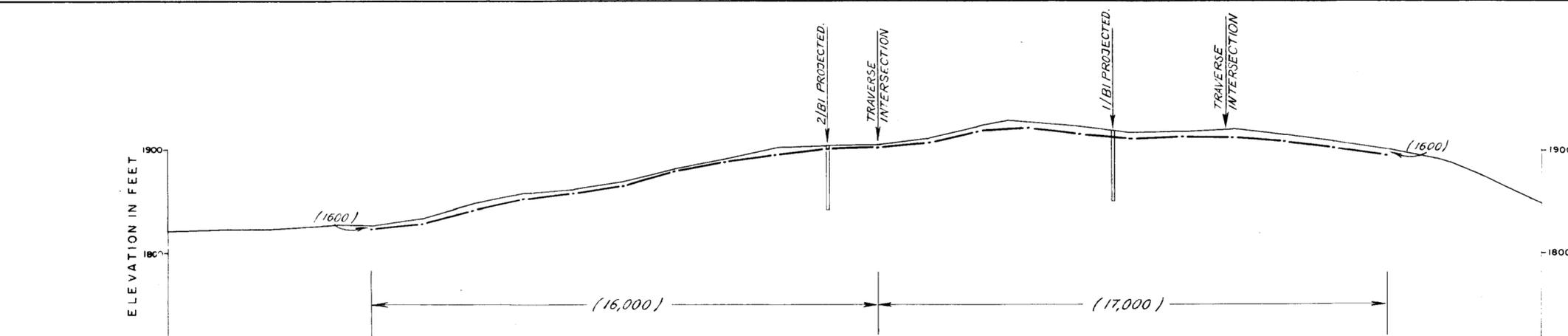


From COG Drawings H1106, H1107, and H1122

TO ACCOMPANY RECORD No. 1963/99

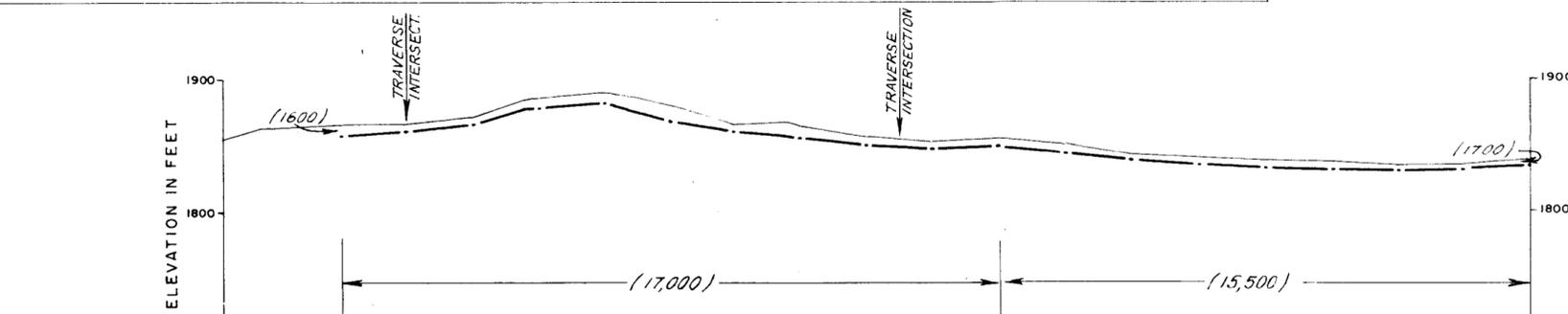
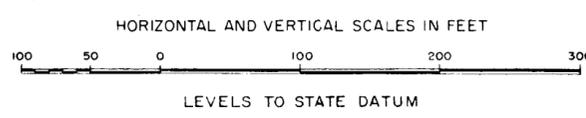
UPPER BLENCOE, 1961 QLD

UPPER BLENCOE CREEK DAM SITE
SEISMIC CROSS-SECTIONS
BETWEEN STATIONS WU 84 & WU185

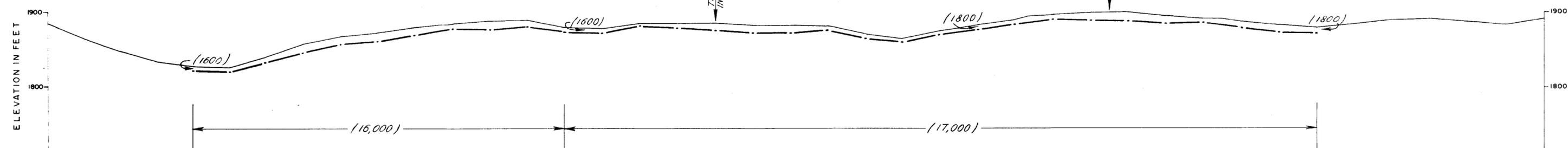


| STATION NUMBER | 1820 WU186 | 1822 157 | 1822 158 | 1826 159 | 1826 160 | 1833 161 | 1847 162 | 1853 163 | 1861 164 | 1869 165 | 1882 166 | 1892 167 | 1901 168 | 1904 169 | 1905 WU140 | 1911 170 | 1923 171 | 1928 172 | 1922 173 | 1918 174 | 1918 175 | 1921 176 | 1915 177 | 1908 178 | 1901 179 | 1892 180 | 1877 181 | 1853 182 |
|-------------------|------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
| STATION ELEVATION | 1820 | 1822 | 1822 | 1826 | 1826 | 1833 | 1847 | 1853 | 1861 | 1869 | 1882 | 1892 | 1901 | 1904 | 1905 | 1911 | 1923 | 1928 | 1922 | 1918 | 1918 | 1921 | 1915 | 1908 | 1901 | 1892 | 1877 | 1853 |
| DEPTH TO BEDROCK | | | | | 2 | 3 | 5 | 5 | 2 | 2 | 1 | 2 | 6 | 2 | 2 | 3 | 4 | 6 | 6 | 5 | 3 | 7 | 6 | 7 | 6 | | | |

LEGEND
 (16,000) Formation with seismic velocity of 16,000 ft/sec
 - - - - - Bedrock boundary

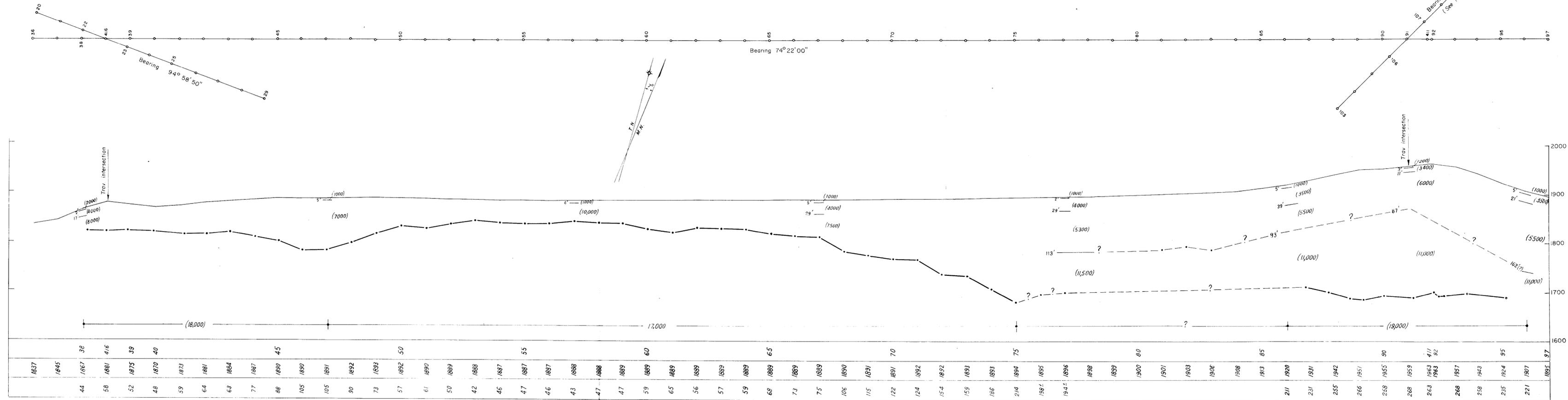
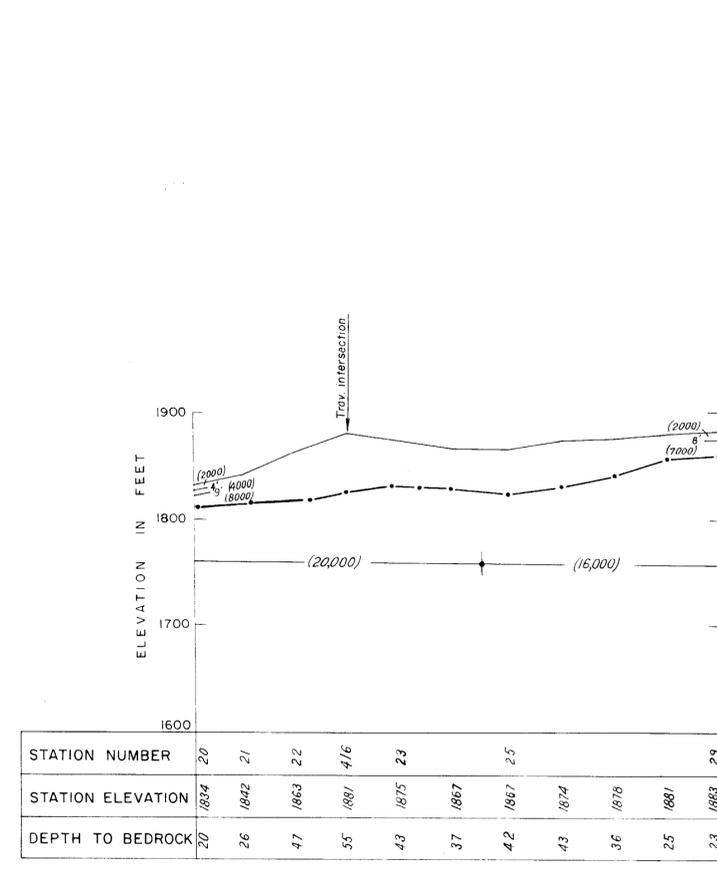


| STATION NUMBER | 1862 WU136 | 1862 WU136 | 1865 137 | 1864 138 | 1870 139 | 1883 140 | 1888 141 | 1878 142 | 1865 143 | 1862 144 | 1854 145 | 1850 146 | 1833 147 | 1849 148 | 1841 149 | 1839 150 | 1837 151 | 1836 152 | 1833 153 | 1834 154 | 1838 155 |
|-------------------|------------|------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
| STATION ELEVATION | 1862 | 1862 | 1865 | 1864 | 1870 | 1883 | 1888 | 1878 | 1865 | 1862 | 1854 | 1850 | 1833 | 1849 | 1841 | 1839 | 1837 | 1836 | 1833 | 1834 | 1838 |
| DEPTH TO BEDROCK | | | 8 | 6 | 5 | 8 | 7 | 10 | 5 | 6 | 5 | 4 | 5 | 6 | 3 | 4 | 5 | 6 | 5 | 3 | 7 |



| STATION NUMBER | 1883 WU123 | 1866 85 | 1849 86 | 1837 87 | 1831 88 | 1823 89 | 1841 90 | 1859 91 | 1869 92 | 1874 93 | 1881 94 | 1886 95 | 1890 96 | 1891 97 | 1881 98 | 1878 99 | 1886 100 | 1884 101 | 1884 WU127 | 1881 102 | 1883 103 | 1881 104 | 1870 105 | 1864 106 | 1875 107 | 1882 108 | 1890 109 | 1895 110 | 1899 111 | 1900 112 | 1894 113 | 1890 114 | 1886 115 | 1883 116 | 1878 117 | 1882 118 | 1888 119 | 1890 120 | 1885 121 | 1881 122 | 1889 123 | |
|-------------------|------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|----------|----------|------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|--|
| STATION ELEVATION | 1883 | 1866 | 1849 | 1837 | 1831 | 1823 | 1841 | 1859 | 1869 | 1874 | 1881 | 1886 | 1890 | 1891 | 1881 | 1878 | 1886 | 1884 | 1884 | 1881 | 1883 | 1881 | 1870 | 1864 | 1875 | 1882 | 1890 | 1895 | 1899 | 1900 | 1894 | 1890 | 1886 | 1883 | 1878 | 1882 | 1888 | 1890 | 1885 | 1881 | 1889 | |
| DEPTH TO BEDROCK | | | | | 6 | 6 | 7 | 10 | 9 | 10 | 10 | 7 | 10 | 8 | 7 | 4 | 2 | 4 | 8 | 9 | 8 | 5 | 5 | 3 | 4 | 7 | 6 | 6 | 9 | 10 | 11 | 5 | 7 | 9 | 6 | | | | | | | |

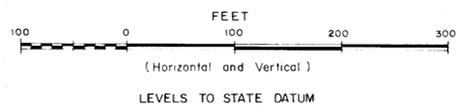
UPPER BLENCOE, 1981, 9LD



LEGEND

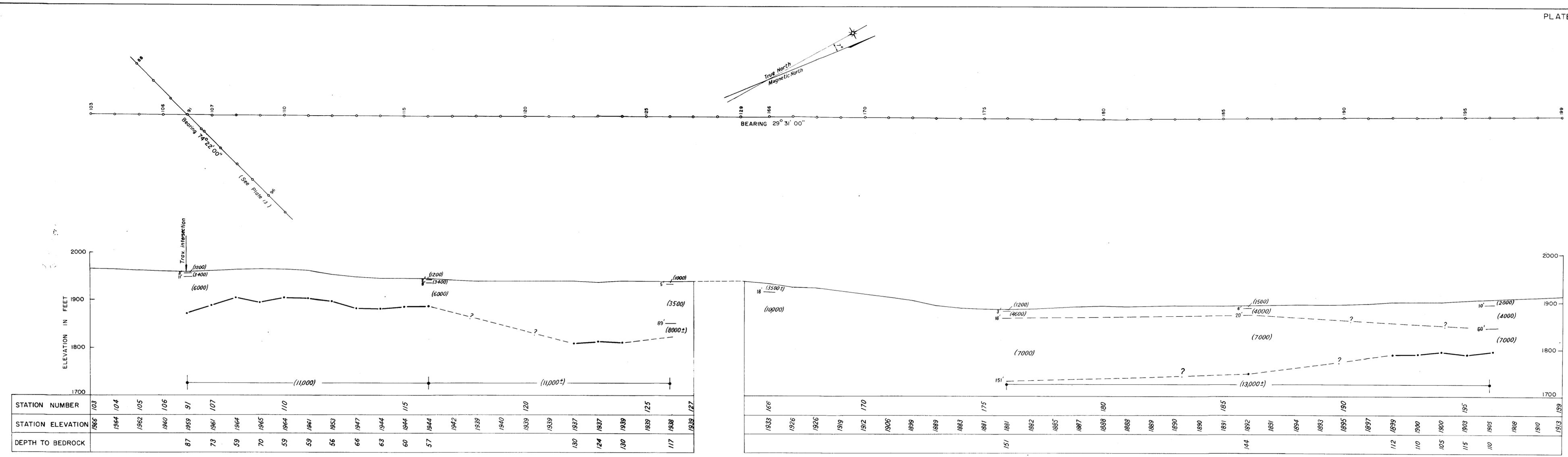
- 45 Geophysical traverse with station number
- (7000) Formation with seismic velocity of 7000 ft/sec
- 8' Depth to formation with different seismic velocity
- Bedrock boundary

Based on COG Drawings H 1127 and H 1128



WEIR SITE
 LAYOUT OF TRAVERSES AND SEISMIC CROSS-SECTIONS
 BETWEEN STATIONS W W 20 & W W 29, AND STATIONS WW 36 & WW 97

HEBERT CIVIL, QLD, 1967, WEIR



| | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|-------------------|------|------|------|------|------|------|------|------|------|------|------|----|----|----|----|------|------|------|------|------|------|-----|------|------|------|-----|------|-----|
| STATION NUMBER | 103 | 104 | 105 | 106 | 91 | 107 | 110 | 115 | 120 | 125 | 127 | | | | | | | | | | | | | | | | | |
| STATION ELEVATION | 1966 | 1964 | 1962 | 1960 | 1959 | 1961 | 1964 | 1944 | 1939 | 1939 | 1939 | | | | | | | | | | | | | | | | | |
| DEPTH TO BEDROCK | | | | | 87 | 73 | 59 | 70 | 59 | 59 | 56 | 66 | 63 | 60 | 57 | 1942 | 1939 | 1940 | 1939 | 1939 | 1937 | 124 | 1937 | 1939 | 1939 | 125 | 1939 | 127 |

| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|-------------------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| STATION NUMBER | 166 | 170 | 175 | 180 | 185 | 190 | 195 | 199 | | | | | | | | | | | | | | | | | | | | | | | | | | |
| STATION ELEVATION | 1933 | 1926 | 1926 | 1919 | 1912 | 1906 | 1899 | 1889 | 1883 | 1881 | 1881 | 1882 | 1885 | 1887 | 1888 | 1888 | 1889 | 1890 | 1890 | 1891 | 1892 | 1891 | 1894 | 1893 | 1895 | 1897 | 1899 | 1900 | 1900 | 1903 | 1905 | 1908 | 1910 | 1913 |
| DEPTH TO BEDROCK | | | | | | | | | | 151 | | | | | | | | | | | 144 | | | | | | 112 | 110 | 105 | 115 | 110 | | | |

LEGEND

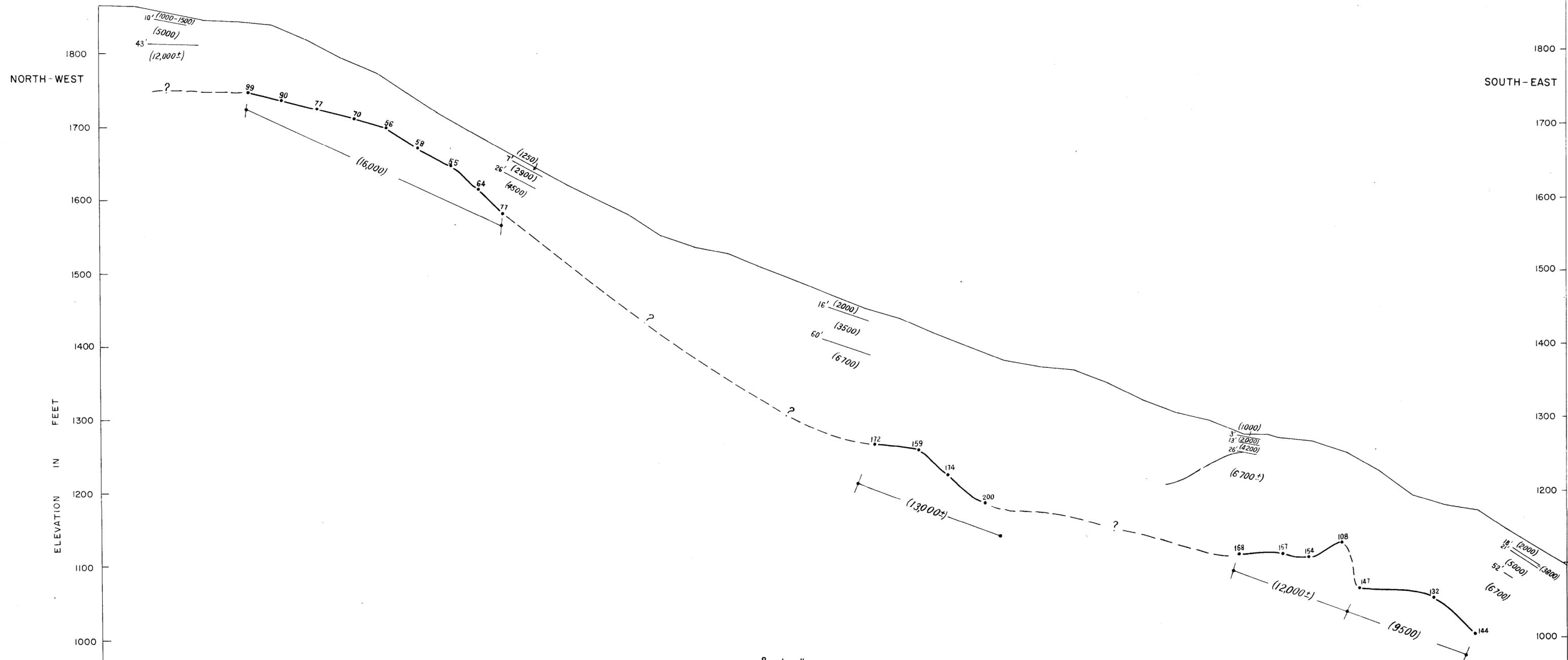
- 110 Geophysical traverse with station number
- (7000) Formation with seismic velocity of 7000 ft/sec
- 8' Depth to formation with different seismic velocity
- Bedrock boundary

Based on COG Drawings H1140 and H1141

100 0 100 200 300
 FEET
 (Horizontal and Vertical)
 Level Datum: Station 311, R.L. 1079' (State Datum)

WEIR SITE
LAYOUT OF TRAVERSES AND SEISMIC CROSS-SECTIONS
BETWEEN STATIONS W W 103 & W W 127, & STATIONS W W 166 & W W 199

HERBERT RIVER, Q.L.D. 1961

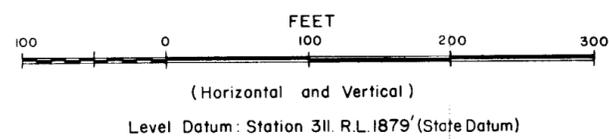


| STATION NUMBER | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 |
|-------------------|------|--------------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| STATION ELEVATION | 1866 | 1865 1864 | 1856 | 1846 | 1843 | 1839 | 1819 | 1795 | 1773 | 1747 | 1720 | 1693 | 1669 | 1644 | 1620 | 1599 | 1578 | 1550 | 1533 | 1523 | 1506 | 1486 | 1467 | 1448 | 1434 | 1415 | 1397 | 1377 | 1368 | 1364 | 1345 | 1322 | 1305 | 1294 | 1275 | 1271 | 1264 | 1248 | 1223 | 1191 | 1176 | 1169 | 1144 | 1119 | 1095 |

LEGEND

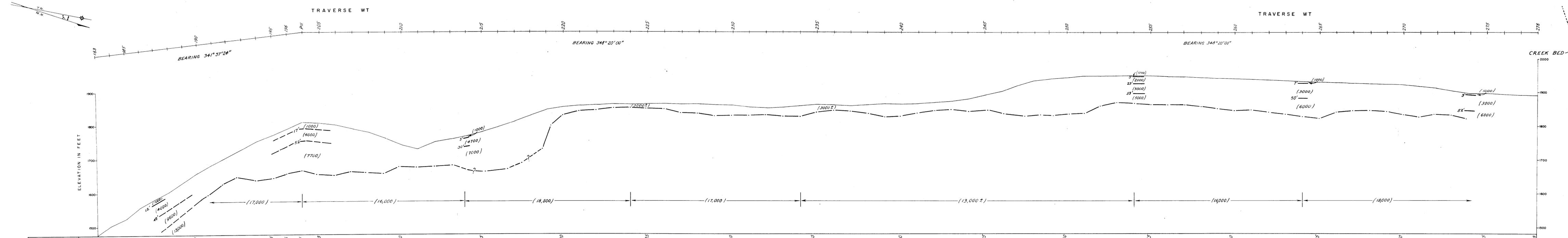
(6700) Formation with seismic velocity of 6700 ft/sec
 3' Depth to formation with different seismic velocity
 56 Bedrock boundary, with depths in feet

Based on COG Drawing H 1111



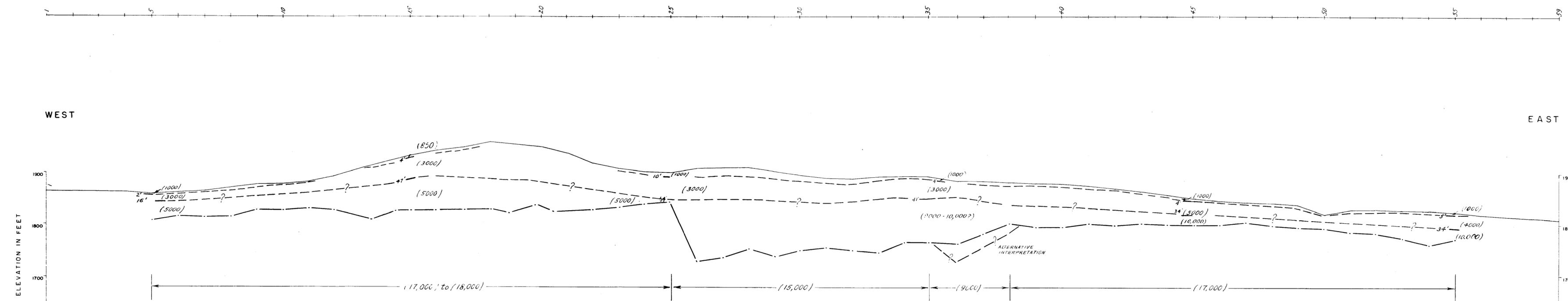
BLENCOE PENSTOCK RIDGE
SEISMIC CROSS-SECTION
BETWEEN STATIONS WP 3 & WP 46

HERBERT RIVER, Q.L.D. 1961, PENSTOCK BLENCOE



| STATION NUMBER | STATION ELEVATION | DEPTH TO BEDROCK |
|----------------|-------------------|------------------|
| 183 | 1473 | |
| 185 | 1502 | |
| 185 | 1529 | |
| 185 | 1554 | |
| 185 | 1577 | 86 |
| 186 | 1600 | 78 |
| 186 | 1626 | 74 |
| 187 | 1653 | 72 |
| 188 | 1680 | 64 |
| 188 | 1700 | 64 |
| 189 | 1721 | 67 |
| 189 | 1745 | 119 |
| 189 | 1764 | 119 |
| 189 | 1783 | 130 |
| 190 | 1802 | 144 |
| 190 | 1820 | 154 |
| 190 | 1839 | 150 |
| 190 | 1858 | 130 |
| 190 | 1879 | 125 |
| 190 | 1898 | 108 |
| 190 | 1918 | 67 |
| 190 | 1937 | 59 |
| 190 | 1956 | 77 |
| 190 | 1975 | 78 |
| 190 | 1994 | 74 |
| 190 | 2013 | 122 |
| 190 | 2032 | 128 |
| 190 | 2051 | 97 |
| 190 | 2070 | 102 |
| 190 | 2089 | 48 |
| 190 | 2108 | 27 |
| 190 | 2127 | 16 |
| 190 | 2146 | 18 |
| 190 | 2165 | 12 |
| 190 | 2184 | 14 |
| 190 | 2203 | 15 |
| 190 | 2222 | 18 |
| 190 | 2241 | 23 |
| 190 | 2260 | 29 |
| 190 | 2279 | 33 |
| 190 | 2298 | 32 |
| 190 | 2317 | 26 |
| 190 | 2336 | 21 |
| 190 | 2355 | 28 |
| 190 | 2374 | 32 |
| 190 | 2393 | 24 |
| 190 | 2412 | 18 |
| 190 | 2431 | 18 |
| 190 | 2450 | 26 |
| 190 | 2469 | 38 |
| 190 | 2488 | 33 |
| 190 | 2507 | 26 |
| 190 | 2526 | 23 |
| 190 | 2545 | 24 |
| 190 | 2564 | 33 |
| 190 | 2583 | 45 |
| 190 | 2602 | 65 |
| 190 | 2621 | 92 |
| 190 | 2640 | 102 |
| 190 | 2659 | 107 |
| 190 | 2678 | 105 |
| 190 | 2697 | 107 |
| 190 | 2716 | 88 |
| 190 | 2735 | 79 |
| 190 | 2754 | 81 |
| 190 | 2773 | 66 |
| 190 | 2792 | 84 |
| 190 | 2811 | 82 |
| 190 | 2830 | 87 |
| 190 | 2849 | 90 |
| 190 | 2868 | 94 |
| 190 | 2887 | 90 |
| 190 | 2906 | 97 |
| 190 | 2925 | 99 |
| 190 | 2944 | 104 |
| 190 | 2963 | 108 |
| 190 | 2982 | 88 |
| 190 | 3001 | 83 |
| 190 | 3020 | 79 |
| 190 | 3039 | 81 |
| 190 | 3058 | 89 |
| 190 | 3077 | 92 |
| 190 | 3096 | 80 |
| 190 | 3115 | 72 |
| 190 | 3134 | 75 |
| 190 | 3153 | 1896 |
| 190 | 3172 | 1893 |
| 190 | 3191 | 1891 |
| 190 | 3210 | 1889 |
| 190 | 3229 | 1887 |
| 190 | 3248 | 1885 |
| 190 | 3267 | 1883 |
| 190 | 3286 | 1881 |
| 190 | 3305 | 1879 |
| 190 | 3324 | 1877 |
| 190 | 3343 | 1875 |
| 190 | 3362 | 1873 |
| 190 | 3381 | 1871 |
| 190 | 3400 | 1869 |
| 190 | 3419 | 1867 |
| 190 | 3438 | 1865 |
| 190 | 3457 | 1863 |
| 190 | 3476 | 1861 |
| 190 | 3495 | 1859 |
| 190 | 3514 | 1857 |
| 190 | 3533 | 1855 |
| 190 | 3552 | 1853 |
| 190 | 3571 | 1851 |
| 190 | 3590 | 1849 |
| 190 | 3609 | 1847 |
| 190 | 3628 | 1845 |
| 190 | 3647 | 1843 |
| 190 | 3666 | 1841 |
| 190 | 3685 | 1839 |
| 190 | 3704 | 1837 |
| 190 | 3723 | 1835 |
| 190 | 3742 | 1833 |
| 190 | 3761 | 1831 |
| 190 | 3780 | 1829 |
| 190 | 3799 | 1827 |
| 190 | 3818 | 1825 |
| 190 | 3837 | 1823 |
| 190 | 3856 | 1821 |
| 190 | 3875 | 1819 |
| 190 | 3894 | 1817 |
| 190 | 3913 | 1815 |
| 190 | 3932 | 1813 |
| 190 | 3951 | 1811 |
| 190 | 3970 | 1809 |
| 190 | 3989 | 1807 |
| 190 | 4008 | 1805 |
| 190 | 4027 | 1803 |
| 190 | 4046 | 1801 |
| 190 | 4065 | 1799 |
| 190 | 4084 | 1797 |
| 190 | 4103 | 1795 |
| 190 | 4122 | 1793 |
| 190 | 4141 | 1791 |
| 190 | 4160 | 1789 |
| 190 | 4179 | 1787 |
| 190 | 4198 | 1785 |
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| 190 | 4255 | 1779 |
| 190 | 4274 | 1777 |
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| 190 | 4331 | 1771 |
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| 190 | 4369 | 1767 |
| 190 | 4388 | 1765 |
| 190 | 4407 | 1763 |
| 190 | 4426 | 1761 |
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| 190 | 4464 | 1757 |
| 190 | 4483 | 1755 |
| 190 | 4502 | 1753 |
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| 190 | 4559 | 1747 |
| 190 | 4578 | 1745 |
| 190 | 4597 | 1743 |
| 190 | 4616 | 1741 |
| 190 | 4635 | 1739 |
| 190 | 4654 | 1737 |
| 190 | 4673 | 1735 |
| 190 | 4692 | 1733 |
| 190 | 4711 | 1731 |
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| 190 | 4787 | 1723 |
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| 190 | 4825 | 1719 |
| 190 | 4844 | 1717 |
| 190 | 4863 | 1715 |
| 190 | 4882 | 1713 |
| 190 | 4901 | 1711 |
| 190 | 4920 | 1709 |
| 190 | 4939 | 1707 |
| 190 | 4958 | 1705 |
| 190 | 4977 | 1703 |
| 190 | 4996 | 1701 |
| 190 | 5015 | 1699 |
| 190 | 5034 | 1697 |
| 190 | 5053 | 1695 |
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| 190 | 5091 | 1691 |
| 190 | 5110 | 1689 |
| 190 | 5129 | 1687 |
| 190 | 5148 | 1685 |
| 190 | 5167 | 1683 |
| 190 | 5186 | 1681 |
| 190 | 5205 | 1679 |
| 190 | 5224 | 1677 |
| 190 | 5243 | 1675 |
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| 190 | 5281 | 1671 |
| 190 | 5300 | 1669 |
| 190 | 5319 | 1667 |
| 190 | 5338 | 1665 |
| 190 | 5357 | 1663 |
| 190 | 5376 | 1661 |
| 190 | 5395 | 1659 |
| 190 | 5414 | 1657 |
| 190 | 5433 | 1655 |
| 190 | 5452 | 1653 |
| 190 | 5471 | 1651 |
| 190 | 5490 | 1649 |
| 190 | 5509 | 1647 |
| 190 | 5528 | 1645 |
| 190 | 5547 | 1643 |
| 190 | 5566 | 1641 |
| 190 | 5585 | 1639 |
| 190 | 5604 | 1637 |
| 190 | 5623 | 1635 |
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| 190 | 5737 | 1623 |
| 190 | 5756 | 1621 |
| 190 | 5775 | 1619 |
| 190 | 5794 | 1617 |
| 190 | 5813 | 1615 |
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| 190 | 5851 | 1611 |
| 190 | 5870 | 1609 |
| 190 | 5889 | 1607 |
| 190 | 5908 | 1605 |
| 190 | 5927 | 1603 |
| 190 | 5946 | 1601 |
| 190 | 5965 | 1599 |
| 190 | 5984 | 1597 |
| 190 | 6003 | 1595 |
| 190 | 6022 | 1593 |
| 190 | 6041 | 1591 |
| 190 | 6060 | 1589 |
| 190 | 6079 | 1587 |
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| 190 | 6117 | 1583 |
| 190 | 6136 | 1581 |
| 190 | 6155 | 1579 |
| 190 | 6174 | 1577 |
| 190 | 6193 | 1575 |
| 190 | 6212 | 1573 |
| 190 | 6231 | 1571 |
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| 190 | 6326 | 1561 |
| 190 | 6345 | 1559 |
| 190 | 6364 | 1557 |
| 190 | 6383 | 1555 |
| 190 | 6402 | 1553 |
| 190 | 6421 | 1551 |
| 190 | 6440 | 1549 |
| 190 | 6459 | 1547 |
| 190 | 6478 | 1545 |
| 190 | 6497 | 1543 |
| 190 | 6516 | 1541 |
| 190 | 6535 | 1539 |
| 190 | 6554 | 1537 |
| 190 | 6573 | 1535 |
| 190 | 6592 | 1533 |
| 190 | 6611 | 1531 |
| 190 | 6630 | 1529 |
| 190 | 6649 | 1527 |
| 190 | 6668 | 1525 |
| 190 | 6687 | 1523 |
| 190 | 6706 | 1521 |
| 190 | 6725 | 1519 |
| 190 | 6744 | 1517 |
| 190 | 6763 | 1515 |
| 190 | 6782 | 1513 |
| 190 | 6801 | 1511 |
| 190 | 6820 | 1509 |
| 190 | 6839 | 1507 |
| 190 | 6858 | 1505 |
| 190 | 6877 | 1503 |
| 190 | 6896 | 1501 |
| 190 | 6915 | 1499 |
| 190 | 6934 | 1497 |
| 190 | 6953 | 1495 |
| 190 | 6972 | 1493 |
| 190 | 6991 | 1491 |
| 190 | 7010 | 1489 |
| 190 | 7029 | 1487 |
| 190 | 7048 | 1485 |
| 190 | 7067 | 1483 |
| 190 | 7086 | 1481 |
| 190 | 7105 | 1479 |
| 190 | 7124 | 1477 |
| 190 | 7143 | 1475 |
| 190 | 7162 | 1473 |
| 190 | 7181 | 1471 |
| 190 | 7200 | 1469 |
| 190 | 7219 | 1467 |
| 190 | 7238 | 1465 |
| 190 | 7257 | 1463 |
| 190 | 7276 | 1461 |
| 190 | 7295 | 1459 |
| 190 | 7314 | 1457 |
| 190 | 7333 | 1455 |
| 190 | 7352 | 1453 |
| 190 | 7371 | 1451 |
| 190 | 7390 | 1449 |
| 190 | 7409 | 1447 |
| 190 | 7428 | 1445 |
| 190 | 7447 | 1443 |
| 190 | 7466 | 1441 |
| 190 | 7485 | 1439 |
| 190 | 7504 | 1437 |
| 190 | 7523 | 1435 |
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| 190 | 7561 | 1431 |
| 190 | 7580 | 1429 |
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| 190 | 7675 | 1419 |
| 190 | 7694 | 1417 |
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| 190 | 7751 | 1411 |
| 190 | 7770 | 1409 |
| 190 | 7789 | 1407 |
| 190 | 7808 | 1405 |
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| 190 | 7865 | 1399 |
| 190 | 7884 | 1397 |
| 190 | 7903 | 1395 |
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| 190 | 7941 | 1391 |
| 190 | 7960 | 1389 |
| 190 | 7979 | 1387 |
| 190 | 7998 | 1385 |
| 190 | 8017 | 1383 |
| 190 | 8036 | 1381 |
| 190 | 8055 | 1379 |
| 190 | 8074 | 1377 |
| 190 | 8093 | 1375 |
| 190 | 8112 | 1373 |
| 190 | 8131 | 1371 |
| 190 | 8150 | 1369 |
| 190 | 8169 | 1367 |
| 190 | 8188 | 1365 |
| 190 | 8207 | 1363 |
| 190 | 8226 | 1361 |
| 190 | 8245 | 1359 |
| 190 | 8264 | 1357 |
| 190 | 8283 | 1355 |
| 190 | 8302 | 1353 |
| 190 | 8321 | 1351 |
| 190 | 8340 | 1349 |
| 190 | 8359 | 1347 |
| 190 | 8378 | 1345 |
| 190 | 8397 | 1343 |
| 190 | 8416 | 1341 |
| 190 | 8435 | 1339 |
| 190 | 8454 | 1337 |
| 190 | 8473 | 1335 |
| 190 | 8492 | 1333 |
| 190 | 8511 | 1331 |
| 190 | 8530 | 1329 |
| 190 | 8549 | 1327 |
| 190 | 8568 | 1325 |
| 190 | 8587 | 1323 |
| 190 | 8606 | 1321 |
| 190 | 8625 | 1319 |
| 190 | 8644 | 1317 |
| 190 | 8663 | 1315 |
| 190 | 8682 | 1313 |
| 190 | 8701 | 1311 |
| 190 | 8720 | 1309 |
| 190 | 8739 | 1307 |
| 190 | 8758 | 1305 |
| 190 | 8777 | 1303 |
| 190 | 8796 | 1301 |
| 190 | 8815 | 1299 |
| 190 | 8834 | 1297 |
| 190 | 8853 | 1295 |
| 190 | 8872 | 1293 |
| 190 | 8891 | 1291 |
| 190 | 8910 | 1289 |
| 190 | 8929 | 1287 |
| 190 | 8948 | 1285 |
| 190 | 8967 | 1283 |
| 190 | 8986 | 1281 |
| 190 | 9005 | 1279 |
| 190 | 9024 | 1277 |
| 190 | 9043 | 1275 |
| 190 | 9062 | 1273 |
| 190 | 9081 | 1271 |
| | | |

TRAVERSE WF

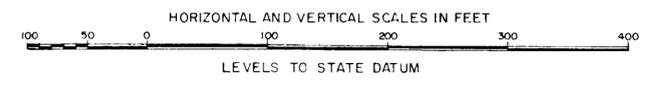


| STATION NUMBER | 1 | 5 | 10 | 15 | 20 | 25 | 30 | 35 | 40 | 45 | 50 | 55 | 59 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|-------------------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|----|----|
| STATION ELEVATION | 1864 | 1862 | 1859 | 1861 | 1866 | 1873 | 1880 | 1885 | 1896 | 1912 | 1925 | 1928 | 1946 | 1953 | 1963 | 1959 | 1952 | 1942 | 1923 | 1912 | 1905 | 1904 | 1912 | 1913 | 1914 | 1905 | 1900 | 1892 | 1892 | 1899 | 1897 | 1888 | 1885 | 1882 | 1882 | 1879 | 1873 | 1865 | 1859 | 1852 | 1845 | 1846 | 1843 | 1839 | 1821 | 1829 | 1832 | 1823 | 1827 | 1819 | 1810 | | |
| DEPTH TO BEDROCK | | 51 | 45 | 51 | 58 | 50 | 51 | 57 | 66 | 90 | 96 | 107 | 115 | 120 | 129 | 130 | 110 | 113 | 92 | 75 | 61 | 56 | 180 | 172 | 198 | 161 | 144 | 132 | 137 | 146 | 127 | 125 | 118 | 99 | 79 | 83 | 83 | 71 | 71 | 60 | 58 | 51 | 44 | 41 | 44 | 44 | 28 | 44 | 46 | 55 | 64 | 53 | 19 |

LEGEND

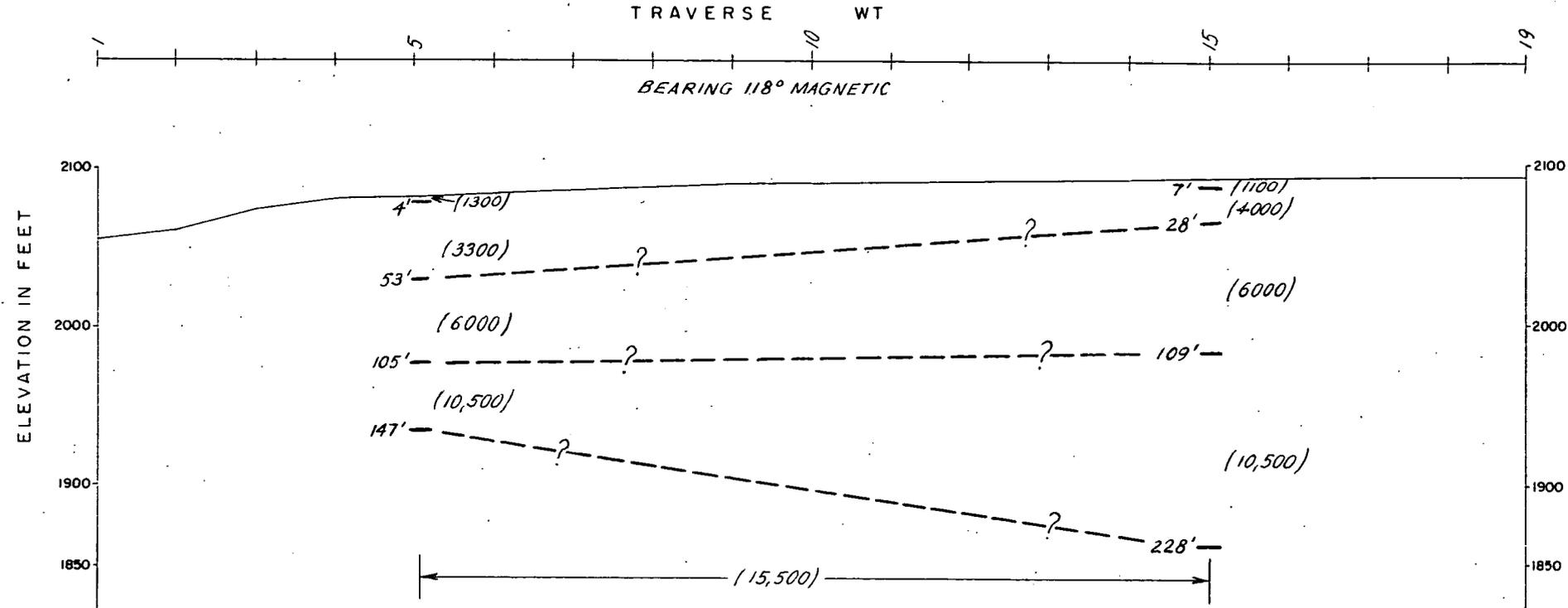
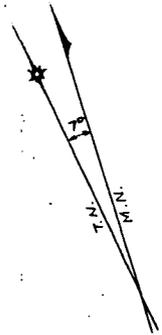
- 15 Geophysical traverse with station number
- (1000) Formation with seismic velocity of 1000 ft/sec
- 4' Depth to formation with different seismic velocity
- Bedrock boundary

BLENCOE FLUME LINE
LAYOUT OF TRAVERSE AND SEISMIC CROSS-SECTION
BETWEEN STATIONS WF 5 & WF 55



From COG drawing H1153-4

HERBERT RIVER, 1961 QLD

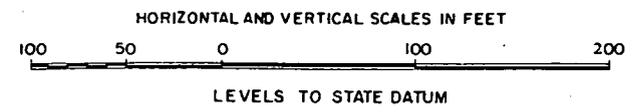


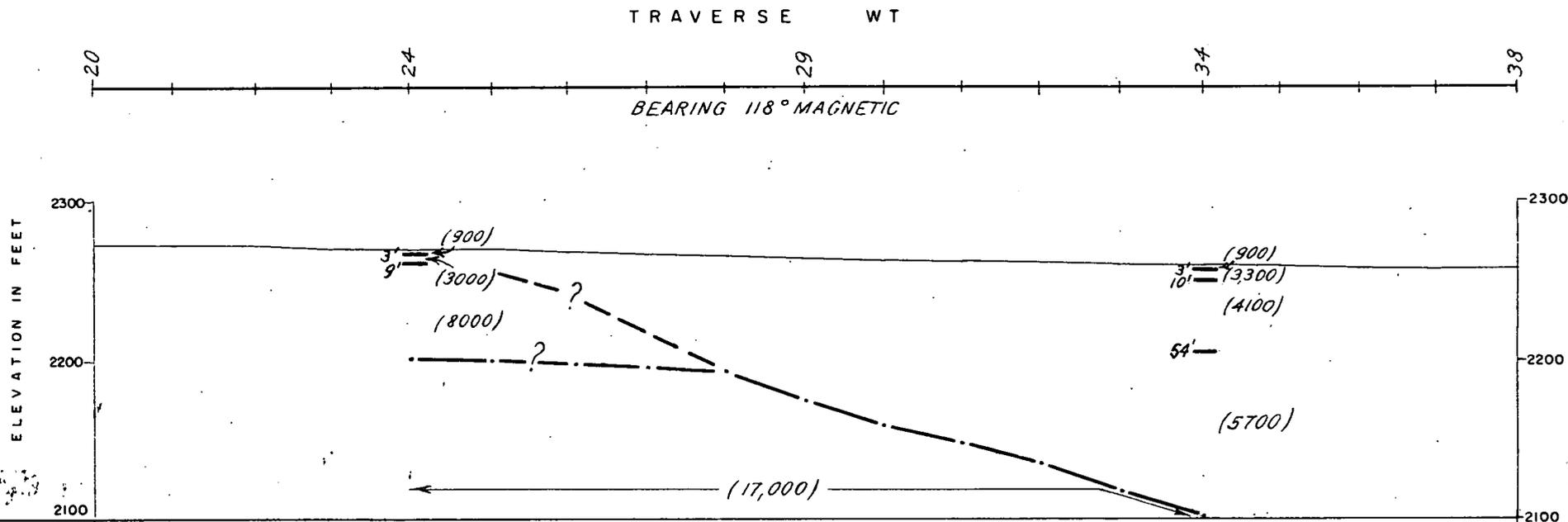
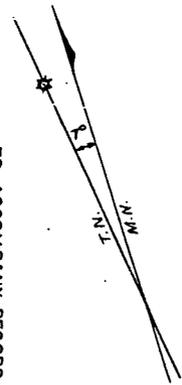
| | | | | | | | | | | | | | | | | | | | |
|-------------------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|----|----|----|------|
| STATION NUMBER | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 |
| STATION ELEVATION | 2054 | 2060 | 2073 | 2079 | 2081 | 2084 | 2086 | 2089 | 2090 | 2090 | 2091 | 2091 | 2092 | 2092 | 2093 | | | | 2095 |
| DEPTH TO BEDROCK | | | | | 147' | | | | | | | | | | 228' | | | | |

LEGEND

- Geophysical traverse with station number
- Formation with seismic velocity of 6000 ft/sec
- Depth to formation with different seismic velocity

TUNNEL LINE-OFFSIDE CREEK AREA
 LAYOUT OF TRAVERSE AND SEISMIC CROSS-SECTION
 BETWEEN STATIONS WT 52 WT 15



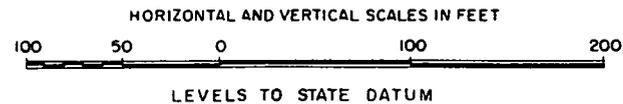


| | | | | | | | | | | | | | |
|-------------------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| STATION NUMBER | 20 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 |
| STATION ELEVATION | 2271 | 2269 | 2268 | 2267 | 2266 | 2264 | 2263 | 2262 | 2261 | 2260 | 2260 | 2259 | 2258 |
| DEPTH TO BEDROCK | | 67 | 68 | 70 | 71 | 73 | 87 | 102 | 112 | 125 | 140 | 157 | |

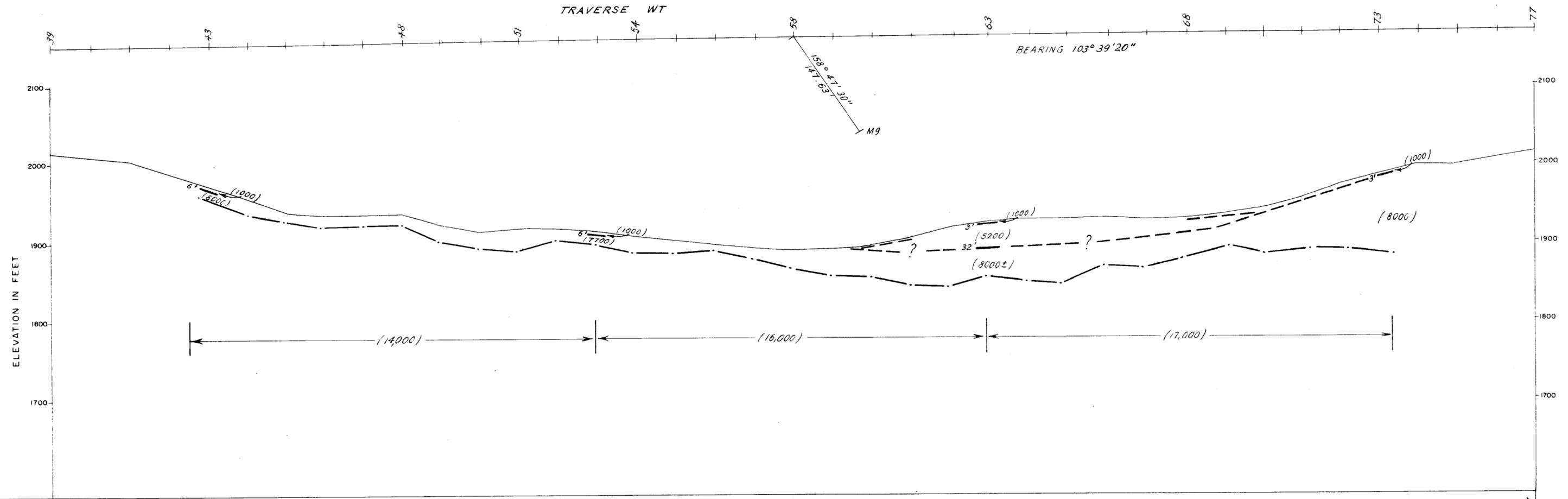
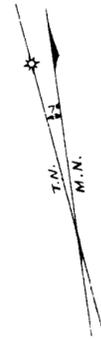
LEGEND

- +—+— Geophysical traverse with station number
- (3000) Formation with seismic velocity of 3000 ft/sec
- 3' Depth to formation with different seismic velocity
- · — · — Bedrock boundary

TUNNEL LINE RING-BARK AREA
LAYOUT OF TRAVERSE AND SEISMIC
CROSS-SECTION BETWEEN STATIONS
WT 24 AND WT 34



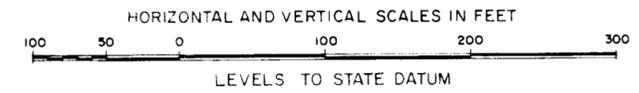
FROM C.O.G. PLAN H1135



| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|-------------------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| STATION NUMBER | 39 | 43 | 48 | 51 | 54 | 58 | 63 | 68 | 73 | 77 | | | | | | | | | | | | | | | | | | | | | | | | |
| STATION ELEVATION | 2014 | 1974 | 1956 | 1938 | 1935 | 1937 | 1931 | 1924 | 1914 | 1918 | 1917 | 1913 | 1908 | 1902 | 1895 | 1890 | 1887 | 1881 | 1883 | 1904 | 1916 | 1923 | 1926 | 1926 | 1927 | 1925 | 1927 | 1930 | 1938 | 1948 | 1966 | 1979 | 1989 | 1991 |
| DEPTH TO BEDROCK | | 18 | 20 | 12 | 16 | 16 | 17 | 24 | 24 | 31 | 18 | 20 | 23 | 18 | 10 | 15 | 24 | 34 | 39 | 57 | 75 | 69 | 78 | 83 | 61 | 62 | 50 | 38 | 57 | 63 | 81 | 102 | | |

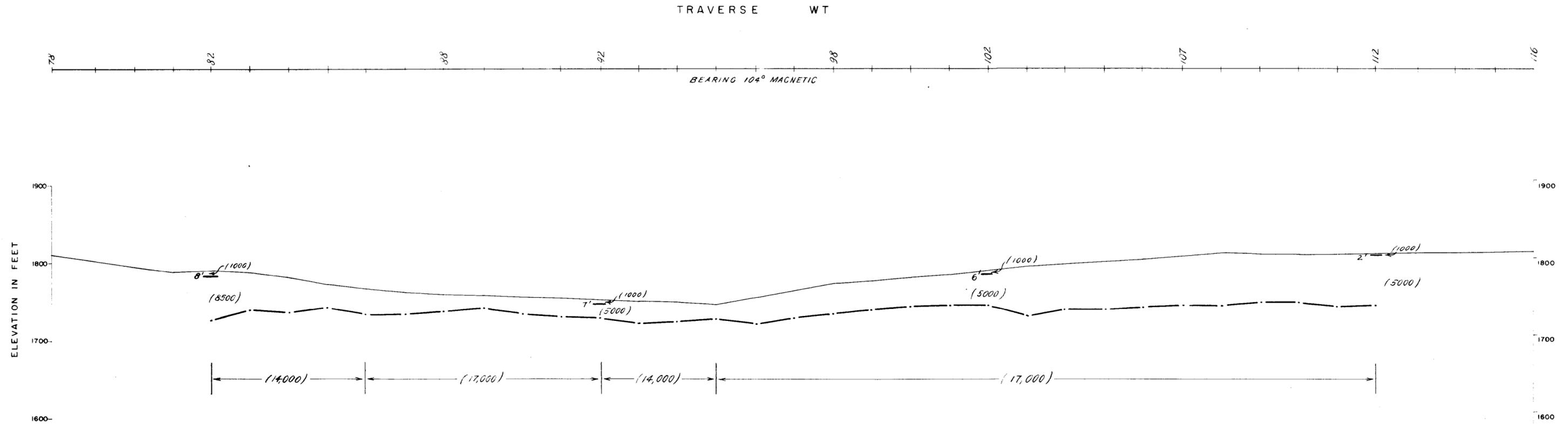
- LEGEND
- Geophysical traverse with station number
 - Formation with seismic velocity of 2000 ft/sec
 - Depth to formation with different seismic velocity
 - Bedrock boundary

TUNNEL LINE - MIDDLE CREEK AREA
 LAYOUT OF TRAVERSE AND SEISMIC CROSS-SECTION
 BETWEEN STATIONS WT 43 & WT 73



From C. O. G. Plan H 1135

HERBERT RIVER, 1961 G.L.D.

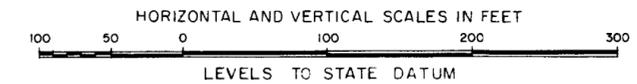


| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|-------------------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|----|----|
| STATION NUMBER | 78 | 82 | | 88 | 92 | 98 | 102 | 107 | 112 | 116 | | | | | | | | | | | | | | | | | | | | | | |
| STATION ELEVATION | 1809 | 1790 | 1787 | 1781 | 1771 | 1765 | 1762 | 1758 | 1758 | 1758 | 1749 | 1745 | 1755 | 1765 | 1771 | 1775 | 1779 | 1782 | 1787 | 1791 | 1796 | 1794 | 1803 | 1807 | 1807 | 1808 | 1808 | 1808 | 1809 | 1808 | | |
| DEPTH TO BEDROCK | | 65 | 50 | 47 | 31 | 34 | 30 | 22 | 17 | 22 | 25 | 26 | 30 | 27 | 18 | 34 | 36 | 39 | 37 | 39 | 40 | 46 | 63 | 58 | 61 | 63 | 65 | 68 | 64 | 65 | 70 | 69 |

LEGEND

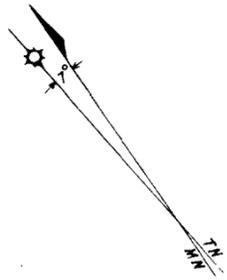
- Geophysical traverse with station numbers
- Formation with seismic velocity of 1000 ft/sec
- Depth to formation with different seismic velocity
- Bedrock boundary

TUNNEL LINE - SHOWERBATH CREEK AREA
SEISMIC CROSS - SECTION
BETWEEN STATIONS WT82 & WT112

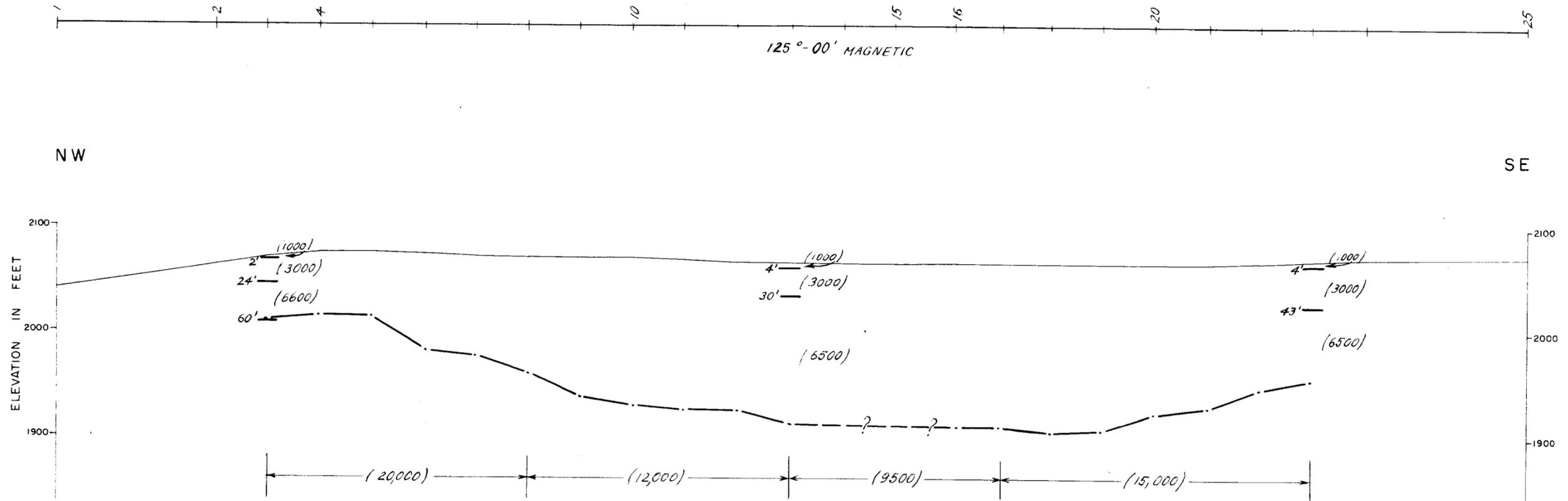


NOTE: From C O G Plan H-1136

HERBERT RIVER, 1961 QLD



TRAVERSE WC



| | | | | | | | | | | | | | | | | | | | | | | | | | |
|-------------------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| STATION NUMBER | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 |
| STATION ELEVATION | 2043 | 2066 | 2074 | 2078 | 2079 | 2077 | 2075 | 2074 | 2073 | 2073 | 2072 | 2070 | 2071 | 2070 | 2070 | 2070 | 2070 | 2070 | 2070 | 2070 | 2070 | 2072 | 2073 | 2074 | 2077 |
| DEPTH TO BEDROCK | | | 60 | 60 | 60 | 91 | 94 | 108 | 128 | 138 | 141 | 141 | 153 | 2070 | 2070 | 156 | 156 | 163 | 162 | 144 | 139 | 120 | 110 | 2074 | |

CAMERON CREEK TUNNEL PORTAL

LAYOUT OF TRAVERSE AND SEISMIC CROSS-SECTION

BETWEEN STATIONS WC3 & WC23

- LEGEND
- + Geophysical traverse with station number
 - (1000) Formation with seismic velocity of 1000 ft/sec
 - 24' Depth to formation with different seismic velocity
 - Bedrock boundary

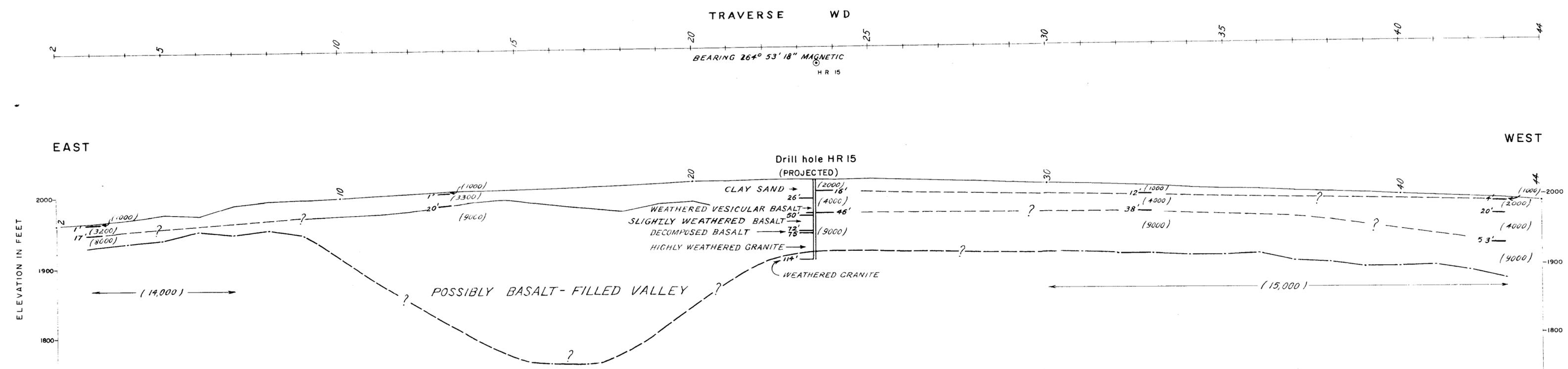
From C O G Plan H 1178



TO ACCOMPANY RECORD No 1963/99

Geophysical Branch, Bureau of Mineral Resources, Geology and Geophysics E55/B5-34

HERBERT RIVER, 1961 QLD



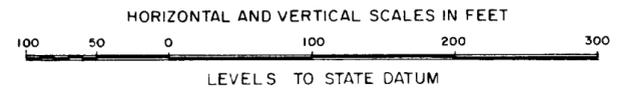
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|-------------------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|-----|-----|------|
| STATION NUMBER | 2 | 5 | 10 | 15 | 20 | 25 | 30 | 35 | 40 | 44 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| STATION ELEVATION | 1964 | 1969 | 1974 | 1989 | 1995 | 1997 | 1999 | 2002 | 2004 | 2006 | 2008 | 2011 | 2013 | 2016 | 2018 | 2020 | 2021 | 2022 | 2022 | 2021 | 2020 | 2019 | 2018 | 2016 | 2015 | 2014 | 2012 | 2011 | 2009 | 2008 | 2006 | 2004 | 2003 | 2001 | 1999 | 1997 | 1995 | 1991 | 1988 | | | |
| DEPTH TO BEDROCK | 33 | 35 | 37 | 23 | 41 | 41 | 24 | 27 | 28 | 26 | 20 | 14 | 14 | 21 | 31 | 39 | 29 | 30 | 40 | 40 | 98 | 94 | 92 | 102 | 98 | 84 | 94 | 102 | 96 | 96 | 96 | 98 | 96 | 92 | 100 | 100 | 106 | 102 | 100 | 106 | 114 | 1988 |

← DEPTH TO (9000) LAYER → ← DEPTH ESTIMATED →

- LEGEND**
- +— Geophysical traverse with station number
 - (2000) Formation with seismic velocity of 2000 ft/sec
 - 15' Depth to formation with different seismic velocity
 - Bedrock boundary



**CAMERON CREEK DIVERSION
SEISMIC CROSS-SECTION
BETWEEN STATIONS WD2 & WD44**



From Co-ordinator General's Dept. Plan No. H 1155