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INVESTIGATION OF SOIL THICKNESS ALONG ROUTE OF WODEN-STROMLO WATER MAIN, A.C.T. 1966.

Compiled by

D.E. Gardner & P.A. Lang

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Compiled by D.E. Gardner and P.A. Lang from results of field work by D. Tarlinton, P.A. Lang and J.P. Staunton

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(Plans and sections).

Scale: Horizontal : 1 inch : 200 feet.

Vertical : 1 inch : 20 feet.

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SUMMARY

Geological and seismic traverses were conducted, and augering was done, along the route of the Woden-Stromlo Water Main, with the purpose of estimating the thickness of soil and weathered bedrock - collectively termed soil - that is soft enough to be excavated by trenching equipment. Experience in similar work has shown that this thickness is indicated approximately by the depth to which the power auger used in the investigation is capable of drilling.

The seismic velocities of the soil and underlying material can be related, empirically, to their amenability to mechanical excavation. Material with a seismic velocity greater than 5000 feet per second is generally too hard to excavate without some blasting.

The geological estimate, made during a brief reconnaissance along the route of the water main, is based on the commonly observed depths of weathering of the bedrock.

The estimates of soil thickness obtained by the three methods are generally in reasonable agreement. Locally, the auger stopped at shallow depths, presumably where it encountered hard rock fragments or boulders in the soil. At some localities the seismic results were indefinite, and the final estimate of soil thickness was based on results of augering.

INTRODUCTION

In response to a request by the Department of Works, geological and seismic investigations were carried out along the route of the Stromlo-Woden Water Main, with the purpose of estimating the thickness of soil and weathered bedrock that could be excavated without blasting (hereafter, in this report, termed excavatable soil).

Power augering along the route was arranged by the Department of Works; the holes were sunk mostly at 50-foot intervals. Auger holes were bored to 6-feet or to point of refusal, whichever was the shallower. Some holes were sunk to greater depths to provide more information about the underlying material.

A locality map showing the route of the water main is given in Plate 1; positions of seismic traverses and auger holes are shown in Plates 2 to 9.

GENERAL RECONNAISSANCE

In a reconnaissance traverse along the route, rough estimates were made of the thickness of soil and weathered rock that would be soft enough to be excavated with earth moving equipment (trenching machinery). The estimates are based on observations of depth of weathering in the same types of rock elsewhere in the Australian Capital Territory. They are probably very approximate but provide a means for interpreting results of seismic surveys and augering.

Along nearly all the route, the bedrock consists of dacitic tuff. This rock weathers deeply but irregularly, locally leaving small to large blocks of fresh, hard rock, surrounded by weathered rock.

The results of the reconnaissance are plotted on Plates 2 to 9.

SEISMIC TRAVERSES

Selected 100-foot sections of the pipeline were tested for thickness of excavatable soil by seismic methods. The equipment used was a Dyna Metric, model 117, seismic timer, which measures in milliseconds the time interval between the hammer impact, and the arrival of the seismic wave at the geophone.

Table 1 shows typical seismic velocities of soil and bedrock and gives estimates of velocities of material that can be excavated by various types of equipment, including a Caterpillar D8 with attached hydraulic ripper. The table is based on experience in the Canberra area, and is not necessarily applicable to other types of rock or other conditions of weathering.

TABLE 1
Seismic Velocities and Excavating Properties

| Velocities (ft./sec.) | Excavating Properties | | | |
|-----------------------|---|--|--|--|
| 800 - 2000 | Soil and sub-soil; readily excavatable | | | |
| 2000- 3500 | Fairly soft; can be excavated with blade and shovel type equipment | | | |
| Up to 4500 or 5000 | Can be ripped | | | |
| 5000 - 6000 | Usually requires some blasting before ripping | | | |
| More than 6000 | Hard to very hard; requires an increasing amount of blasting with increasing seismic velocities | | | |
| 10,000 - 20,000 | Velocity range of the strongest rocks | | | |

Method

Traverses were 100 feet long. A geophone was placed at one end of the traverse and hammer stations were located 2.5, 5, 7.5, 10, 15, 20, 30, 40, 60, 80, 100 feet from the geophone. Five to seven time intervals were recorded at each station. When the traverse was completed from one end, the geophone was positioned at the other end of the traverse and hammer stations sited at 2.5, 5 feet, etc., from the geophone at that end.

Time-distance curves were plotted; seismic velocities were determined, and depth to refractors calculated by the methods outlined in the manual provided with the seismic timer.

The results of the traverses are plotted on Plates 2 to 9.

EVALUATION OF RESULTS

In general the results from the different methods are in fair agreement.

It is assumed that an auger hole will give the thickness of excavatable soil, except where it encounters a hard rock fragment within the soil. At some localities the seismic results indicate depths of excavatable soil greater than the auger penetrated. In these places the seismic results have been taken as the more reliable: it is assumed that local residuals of unweathered rock set in soft material, have stopped the auger. This interpretation is supported by the fact that adjacent holes penetrated to the 6-foot depth.

Along two traverses the auger holes penetrated to greater depths than would have been expected from the seismic results. However at these localities the results of the seismic work are not amenable to a unique interpretation. An alternative interpretation to the one that was adopted, is in agreement with the augering results. In these cases the auger holes are considered to give the better indication of excavatable depth.

Table 2 below, tabulates the estimated excavatable soil thickness at the localities where the auger and seismic results are not in agreement.

TABLE 2
Estimated Depths. Where Auger and Seismic Results Differ

| Locality (Chainage) | Preliminary Estimate of Thickness of Excavatable Soil | | | | Final Estimate | Remarks |
|---------------------|--|--------------------------------|----------------|------------------------|--|---|
| (Plates 2-9) | Augering | | | | Based on seismic | |
| | Depth (feet) | Seismic velocity at this depth | Seismic (feet) | Geological Estimate | results except where otherwise indicated | |
| Sheet 2 ch. 1M 4400 | 213"* | 1500 | 7'0" | 5-7 | 7'0" | Beyond this section in both directions along the route on the main, auger holes went down generally to depths of six feet. Probably shallow holes in the section bottomed on hard residuals |
| Sheet 2 ch. 1M 4300 | 216"* | 1800 | 25'6" | 5-7 | 2516" | |
| Sheet 2 ch. 1M 4100 | 216"* | 1600 | 2116" | 5-7 | 21'6" | |
| Sheet 2 ch. 1M 4000 | 312"* | 2300 | 1616" | 5-7 | 16'6" | |
| | | | | | - | |
| Sheet 2 ch. 1M 2500 | 31.011* | 2500 | 6'6" | 3-5 | 6'6" | Auger probably stopped by hard residuals. Adjacent auger holes penetrated deeper. |
| Sheet 2 ch. 1M 2400 | 31211* | 3000 | 12 t 0" | 3–5 | 12'0" | |
| Sheet 3 ch. 1M 900 | 3'4"* | 3000 | 11 °0" | 3-7 | 11'0" | |
| Sheet 3 ch. 4850 | 316"* | 2500 | 616" | 3 – 5 | 616" | |
| Sheet 4 ch. 2800 | 6'0" and 8'0" | 5000 | 7'0" | 57 | 8'0"(A) | Seismic results not |
| Sheet 4 ch. 2700 | 6'0" and 9'0" | 5000 | 5'0" | 5-7 | 9'0"(A) | definite. They can be re-interpreted to agree with auger results |
| Sheet 4 ch. 850 | 216"* | 2600 | 20'0" | 5–7+ | 20'0" | Auger probably stopped |
| , | | | | | | by hard residual. Adjacent auger holes penetrated deeper. |

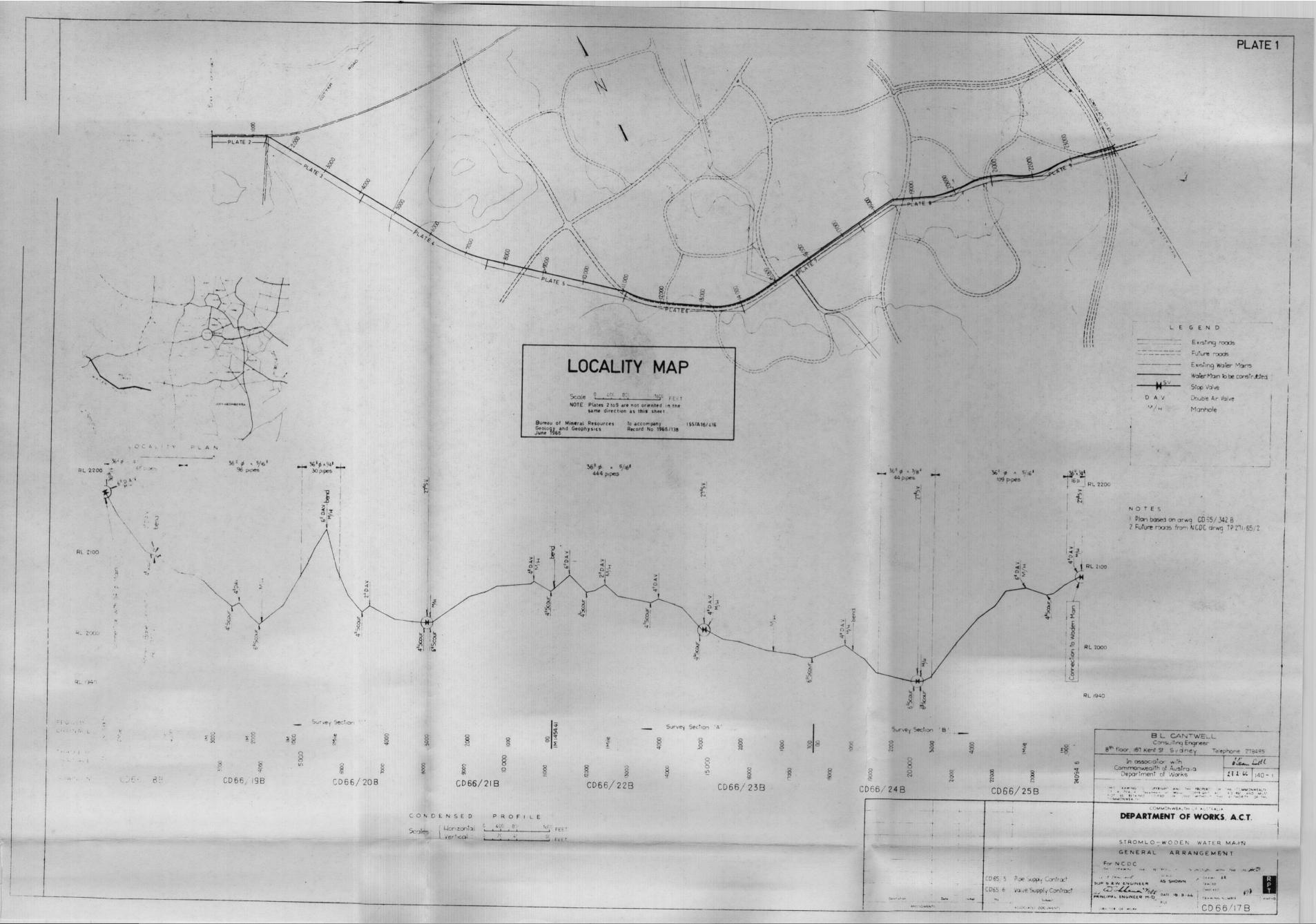
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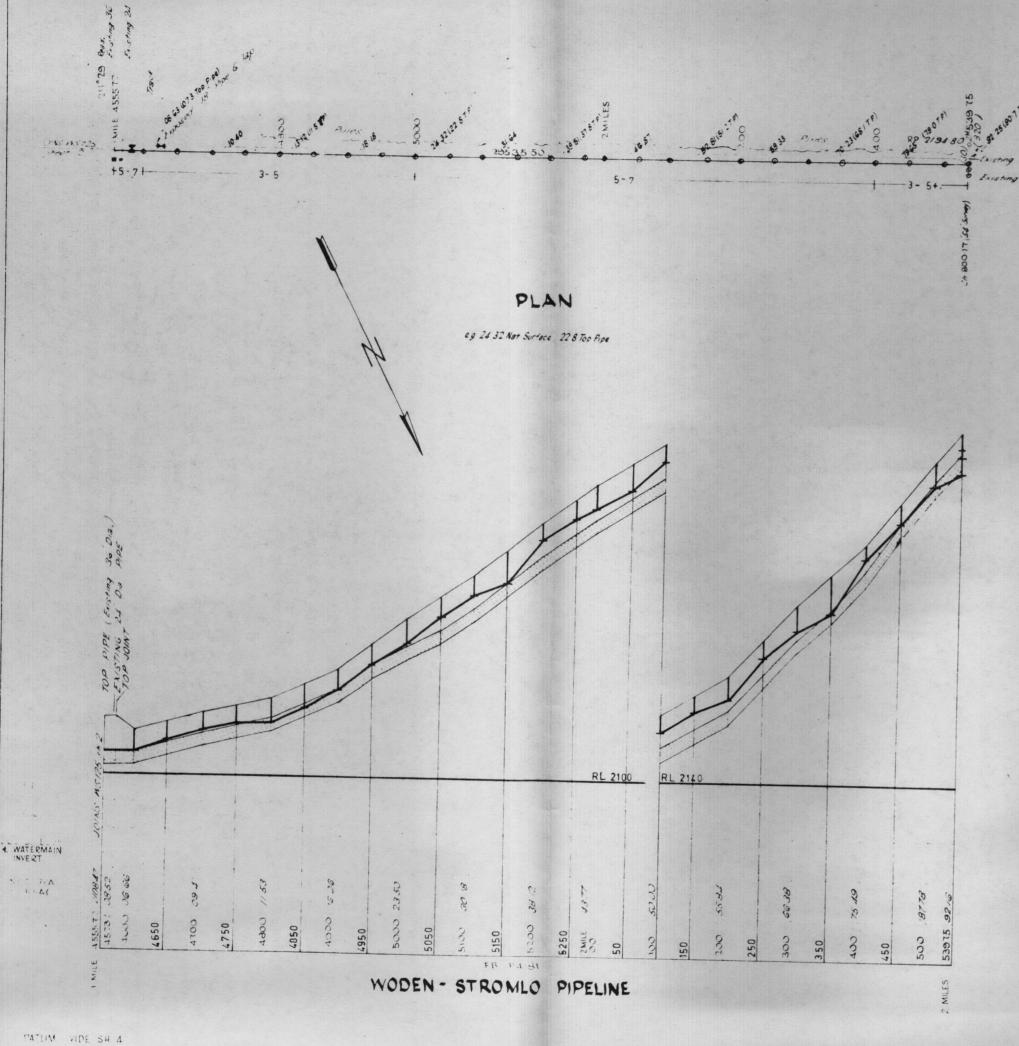
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| | | | | TABLE 2 (c | cont'd) | | |
|------------------|------|---------------|------|------------|---------|------------------|---|
| Sheet 5 ch. 4250 | 4250 | 9!0" 5000 | | | | 9 '0"(A) | Seismic results not definite. |
| Sheet 5 ch. | 4150 | 6'0" and 7'0" | 4500 | 216" | 5-7 | 7'0"(A) | They can be re-interpreted to agree with auger results. |
| Sheet 6 ch. | 2200 | 3'6"* | 2400 | 5'6" | 0-5 | 5'6" | Auger probably stopped by hard residuals. |
| Sheet 6 ch. | 2100 | 3 t 0 "* | 3200 | 81011 | 3-7+ | 810" | |
| Sheet 7 ch. | 600 | 218"* | 1100 | 1616" | 57+ | 1616 " | Adjacent auger holes penetrated deeper. |
| Sheet 7 ch. | 700 | 21811* | 1100 | 17'0" | 5-7+ | 1710" | |
| Sheet 7 ch. | 1000 | 21611* | 1450 | 10°0" | 5-7 | 1010" | |
| Sheet 8 ch. | 4750 | 219"* | 2500 | 11'6" | 5⊸7 | 1116" | |
| Sheet 8 ch. | 4850 | 419"* | 2400 | 19¹6" - | 5-7 | 19'6" | |

^{*} Indicates auger refusal

⁽A) Estimate based on augering





SOIL THICKNESS SURVEY SCALE HORIZONTAL VERTICAL REFERENCE PLAN **├**─3 - 5 + ─ ◀ Estimated range in feet of soil thickness based on geological observation and inference Seismic traverse. SECTION Estimated range in depth of bottom of soil based on geological observations and inference Destred life indicates soil thickness is probably greater. 1500 Seismic velocity in feet per second. Auger hole Final estimate of soil thickness. Broken line indicates probable minimum thickness. Soil and weathered bedrock that can be Note: excavated without blasting . Seismic profile by Engineering Geology group, Geological Branch Bureau of Mineral Resources, Geology and Geophysics June 1966 To accompany Record No 1966

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ASSOCIATED DOCUMENTS

DEPARTMENT OF WORKS

WODEN-STROMLO PIPELINE

SECTION "C"

CANBERRA BRANCH

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