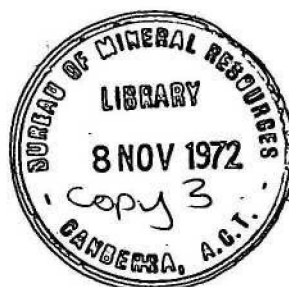


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COMMONWEALTH OF AUSTRALIA

DEPARTMENT OF
NATIONAL DEVELOPMENT
BUREAU OF MINERAL
RESOURCES, GEOLOGY
AND GEOPHYSICS



Record 1972/106

THREE COMPUTER PROGRAMS
FOR CALCULATION OF PETROLOGICAL AND
GEOCHEMICAL PARAMETERS FROM SILICATE ANALYSES

by

S. Henley

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SUMMARY

Three programs are described. The first, CIPWNORM, computes the CIPW norm and a number of petrochemical indices, and also computes and plots values for a number of triangular and tetrahedral diagrams of petrological importance. The second program, NIGGBART, computes Niggli values, the Niggli 'basis' (an intermediate step in the calculation of any of the Niggli-Barth norms), and the Barth 'standard cell' (useful in studies of metasomatism). The third program, ZAVSKY, computes parameters devised by Zavaritsky, and plots their values on the orthotetrahedral projection which has now become standard in Russian petrological literature.

DATA PREPARATION

The format of silicate analysis data on 80-column punched cards is identical for all three programs. An eleven-column identification field is followed by 14 four-column fields containing analysed values for the major oxides usually determined, and a five-column field optionally containing the total. The last eight columns on the card are free, and may be used for any comments or identification for sorting purposes.

(a) Identification field. The first 8 columns are occupied by the standard BMR registered number (of the format yy pp ssss, where yy are the last two digits of the year of sample submission, pp is a unique project code within that year, and ssss is a serial number assigned by the geologist). If the analysis is extracted from the literature, or any other source outside the BMR system, any alphanumeric label may be inserted in this space. The 9th column is reserved for a fraction letter (if any) indicating that separate portions of an original sample have been analysed independently. Columns 10 and 11 are filled in only if the analysis is to be included in the BMR geochemical data storage system, in which case the number 20 is inserted.

(b) Analysis fields. Chemical data are inserted in the format bbaa or Obaa where b represents a digit before the decimal point, and a represents a digit after the decimal point. The numbers inserted are weight percent of the oxide in every case. Data are inserted in the fixed order SiO₂, TiO₂, Al₂O₃, Fe₂O₃, FeO, MnO, MgO, CaO, Na₂O, K₂O, P₂O₅, H₂O(+), H₂O(²), CO₂. If data for any oxides are missing, blanks may be left in the appropriate columns. If data for total H₂O are quoted, the value may be coded in the H₂O+ columns; problems arise, however, if iron is quoted simply as 'total iron as Fe₂O₃' or 'total iron as FeO', since the oxidation ratio of iron significantly affects the CIPW norm and many of the other parameters. If this problem is encountered in an analysis of a volcanic rock, it may be useful to apply the transformation suggested by Irvine and Baragar (1971); Fe₂O₃ = TiO₂ + 1.5, and correct the FeO value accordingly.

(c) Total. This field is optional, but if the total is not filled in, columns 68-72 must be left blank. The format is bbbbaa, the decimal point being assumed after the third digit.

CIPWNORM

(a) Purpose

CIPWNORM is a FORTRAN program for the CSIRO CDC 3600 computer, to calculate CIPW norms from chemical analyses of igneous rocks; it also computes the Solidification Index (Kuno et al., 1957), the Differentiation Index (Thornton & Tuttle, 1960), the Peralkalinity or Alkaline Index, the potash/soda ration, total iron as weight percent Fe₂O₃, calculated density (based on mineral densities quoted by Berry & Mason, 1959), and data on various three-component systems (quartz-albite-orthoclase, quartz-plagioclase-orthoclase, orthoclase-albite-anorthite, K₂O-Na₂O-CaO, wollastonite-ferrosilite-enstatite, iron-magnesium-alkali, and quartz-nepheline-olivine).

Optionally, plots of these various triangles may be obtained on the line-printer for each batch of analyses processed, and graph-plotter routines optionally give accurate plots of orthoclase-albite-anorthite triangles and either iron-magnesium-alkali or quartz-albite-orthoclase triangles, plus orthoclase-albite-anorthite-femica tetrahedra and either iron-magnesium-alkali-quartz or quartz-albite-orthoclase-corundum tetrahedra. All triangular and tetrahedral data are computed in terms of weight proportions.

(b) Program Operation

The program reads a chemical analysis, optionally including trace element data, and computes the norm by a method analogous to hand computation, using FORTRAN 'IF' statements to determine the choice of minerals formed, according to the presence or absence of an element at the current state of computation.

Triangular and tetrahedral data, together with the other indices, are then computed, and the results for each sample printed on a single page of lineprinter output. Triangular and tetrahedral data are stored on scratch drum units for plotting at the end of the run.

The program is listed in Appendix A, and examples of the printout and plots are shown in Figures 1-4.

(c) Treatment of trace element data

The elements F, S, Cl, V, Cr, Co, Ni, Cu, Zn, Rb, Sr, Zr, and Ba may be included in the norm computation if desired. Their treatment is described below.

F and Cl are incorporated into apatite. Any excess F is made into fluorite, and after this, if there is any excess Cl, it is made into halite.

V is combined with Fe_2O_3 .

Co, Ni, and Cu are combined with FeO.

Cr is used to make chromite.

Zn is used to make sphalerite if there is sufficient sulphur, any excess Zn being combined with FeO. Any excess sulphur is used to make pyrite.

Rb is combined with K_2O .

Sr is combined with CaO.

Zr is used to make zircon.

Ba is combined with K_2O .

(d) Input Cards

Job deck structure is given below.

*JOB, chargecode, ident, timelimit (total time in minutes)
 *EQUIP, 1=PL, 2=PL, 3=PL, 4=PL
 *FTN, L, X
 Fortran deck inserted here
 *LOAD
 *RUN, timelimit, printlimit (run time in minutes)
 TRIANGLE (from col.3; if lineprinter plots of triangles required)
 PLOTTRIA (if graph-plotter plots of triangles required)
 TETRAHED (if tetrahedral plots required)

blank card inserted here if trace element cards to be included.

Chemical analysis cards inserted here. Standard silicate analysis card followed by an optional trace element card, for each sample.

7 EOF (7 overpunching 8 in column 1)
 8
 *EOD

Notes

- (i) Total time = run time + 4 minutes.
 Run time = $n/10 + 2$ minutes, where n is the number of samples.
 Print limit = $60n + 500$ lines.
- (ii) On PLOTTRIA card: if an accurate FMA triangle is desired, leave column 12 blank; if the Q-Ab-Or triangle is desired, punch a 1 in column 12.
- (iii) On TETRAHED card: if an FMA-quartz tetrahedron is desired, leave column 12 blank; if a Q-Ab-Or-corundum triangle is required, punch a 1 in column 12.
- (iv) Format of the optional trace element card is similar to the major oxide card.

Columns 1-8 : registered number

Column 9 : fraction letter

Columns 10-11: blank

Columns 12-63: trace element data in fields of four columns each. Values are quoted in integer numbers of ppm, right justified within the field. If values above 9999ppm occur, they are quoted in weight percent of the element, with the decimal point explicitly coded (e.g. 1.23, occupying all 4 columns). Elements are coded in the order F, S, Cl, V, Cr, Co, Ni, Cu, Zn, Rb, Sr, Zr, Ba.

NIGGBART

(a) Purpose

Program NIGGBART computes Niggli values, the Barth 'Standard Cell', the Basis (of the various Niggli norms), and data for plotting the four triangular diagrams, Q-L-M, Q-Kp-Ne, K-Na-Ca, and Fe-Mg-Ca (the last two are not the normal ternary diagrams but represent the element contents in aluminosilicates and in alumina-free silicates respectively). All the computation methods are given in detail by Burri (1964). Optionally the program plots the triangles on the lineprinter and graph plotter.

(b) Program Operation

The structure of the program is very simple, with the Niggli values, Barth Standard Cell, and Niggli Basis computed consecutively for each sample; scratch drum storage is used for retention of triangular diagram data until the end of the job, when triangles are plotted if desired. A listing of the program is given in Appendix B.

(c) Input Cards

Job deck structure is given below.

*JOB, chargecode, ident, timelimit

*EQUIP, 1=PL, 2=PL, 5=60

*FTN, X, L

Fortran deck inserted here

*LOAD

*RUN, timelimit, printlimit

TRIANGLE

(if triangular plots required; start in
col. 3)

Silicate analysis cards inserted here

7 EOF
8

*EOD

Notes

Total time = run time + 2 minutes

Run time = $n/20 + 1$ minute

Print limit = $60n + 250$ lines

ZAVSKY

(a) Purpose

This program computes Zavaritsky parameters (Zavaritsky, 1950, 1964; Coats, 1968) and plots their values on the orthotetrahedral projection proposed by Zavaritsky and now generally adopted in the Soviet petrological literature. The method of calculation is given by Zavaritsky (1964), and Coats (1968) provides a rare example of the use of the method in the English-language literature.

The parameters are divided into four 'principal' numbers and ten 'supplementary' numbers. The principal numbers, a, c, b, and s sum to 100, and have the following significance:

- a is the relative number of alkali atoms combined with aluminium (i.e. in aluminosilicates)
- c is the relative number of calcium atoms combined with aluminium (i.e. in aluminosilicates)
- b is the relative number of all the remaining metal atoms, excluding Silicon and titanium and not combined with aluminium; it includes any aluminium excess over alkalis and calcium or any excess of calcium and alkalis over aluminium.
- s is the relative number of silicon and titanium atoms.

There are ten supplementary numbers (or 'numerical characteristics'):

- f', m', and c' represent the proportions of iron, magnesium, and calcium respectively in simple silicates
- n represents the ratio of sodium atoms to the total number of alkali atoms
- t indicates the content of titanium
- φ represents the amount of ferric iron in simple silicates
- Q indicates the excess (if positive) or deficiency (if negative) of free silica

In rocks with an excess of aluminium over alkalis and calcium, c' is replaced by a value a' which indicates the surplus of alumina over that required for aluminosilicates.

In rocks with an excess of sodium, the value n' is obtained, indicating the sodium excess after formation of aluminosilicates and ferrisilicates (e.g. aegirine). If there is an excess of alkalis over aluminium, the value of c becomes negative, and an additional parameter, $\bar{c}$, indicates the number of excess alkaline atoms.

The principal values a , c , b and s may be plotted in a tetrahedron; each rock composition may be represented by its projections on to two of the triangular facies, and Fig. 5 shows the conventional presentation of this plot as suggested by Zavaritsky. The equilateral triangles are transformed to right-angled isosceles triangles for ease of plotting.

Supplementary characters may also be indicated in the same diagram by vectors constructed from the plotted points x_1 and x_2 .

The vector on point x_1 represents the alkali relationships (Fig. 'a), its length being proportional to total alkali content, and its direction depending on the K/Na ratio.

The vector on x_2 indicates the relationships in the f'm'c' or f'm'a' system, and its construction is illustrated in Fig. 6b. The end of the vector is the point within the appropriate triangle at which the rock composition plots.

(b) Program Operation

For each silicate analysis input, the program computes the Zavaritsky values exactly as directed by Zavaritsky (1964). Scratch drum storage is required to store the values until the end of the job, when the orthotetrahedral diagram is plotted.

(c) Input Cards

Job deck structure is given below.

*JOB, chargecode, timelimit

*EQUIP, 1=PL, 5=60

*FTN, X, L

Fortran deck inserted here

*LOAD

*RUN, timelimit, printlimit

Silicate analysis cards inserted here

7 EOF
8

*EOD

Notes

Total time = run time + 1 minute

Run time = $n/30$ minutes

Print limit = 40n lines

There is no limit to the number n of analyses that can be processed in one run, but the diagram can look very crowded if more than about 20 rocks of similar composition are included.

REFERENCES

- BERRY, L.G. & MASON, B., 1959 - MINERALOGY. San Francisco, Freeman.
- BURRI, C., 1964 - PETROCHEMICAL CALCULATIONS. Jerusalem, Israel Program for Scientific Translations.
- COATS, R.R., 1968 - Basaltic Andesites. In eds. H.H. Hess and A. Poldervaart. BASALTS: THE POLDERVAART TREATISE ON ROCKS OF BASALTIC COMPOSITION, 689-736.
- IRVINE, T.W. & BARAGAR, W.R.A., 1971 - A guide to the chemical classification of the common volcanic rocks. Canad. J. Earth Sci., 8, 523-48.
- KUNO, H., YAMASAKI, K., IIDA, C., & NAGASHIMA, K., 1957 - Differentiation of Hawaiian Magmas, Jap. J. Geol. Geogr., 28, 178-218.
- THORNTON, C.P. & TUTTLE, O.F., 1960 - Chemistry of Igneous Rocks. I: Differentiation Index. Amer. J. Sci., 258, 664-84.
- ZAVARITSKY, A.N., 1950 - VVEDENIE V PETROKHIMIYU IZVERZHENNYKH GORNYKH POROD (Introduction to Petrochemistry of Igneous Rocks) 2nd edn. Moscow, Izdatel'stvo AN SSSR.
- ZAVARITSKY, A.N., 1964 - Outline of the Analysis of Igneous Rocks and the Determination of their Chemical Types (in part). Int. geol. Rev., 6, 1-17.

APPENDIX 1

Listing of program CIPWNORM and the subroutines TRIGDIG, TRIGPLOT, and TETRLOT.

TRIGDIG and TRIGPLOT are used also by program NIGGBART.

```

PROGRAM CIPWNORM
C   TO CALCULATE THE CIPW NORM OF A ROCK FROM A SILICATE ANALYSIS
C   WRITTEN BY W.R. MORGAN
C   REVISED BY S. HENLEY BMR 1971 TO INCLUDE TRACE ELEMENT AND TRIANGULAR
C   DIAGRAM + RATIO DATA. ALL RATIOS ARE IN WEIGHT PERCENT,
C
C
      DIMENSION IELH(28),MINL(49),T(27)
      DIMENSION NTITLE(2)
      INTEGER Z1
      COMMON IJKLMN
      DATA (IELH= 6HSIO2 ,6HTIO2 ,6HAL2O3 ,6HFE2O3 ,6HFEO ,6HMNO ,
1      6HHGO ,6HCAO ,6HNA2O ,6HKK2O ,6HP2O5 ,6HH2O(+),
2      6HH2O(-),6HCU2 ,6HTOTAL ,6HF ,6HS ,6HCL ,
3      6HV ,6HGR ,6HGO ,6HNI ,6HGU ,6HZN ,
4      6HRB ,6HSR ,6HZR ,6HBA )
      DATA (MINL= 8HQWARTZ ,8HAGMITE ,8HGORUNDUM,8HZIRCON ,
1      8HWOLLASTO,8HNITE ,8HORTHOCILA,8HSE ,8HDIOPSIDE,
2      8HWO ,8HALBITE ,8HEN ,8HANORTHIT,8HE ,
3      8HFS ,8HNEPHELIN,8HE ,8HYPERSITH,8HENE ,
4      8HLEUCITE ,8HKALIOPIH,8HLITE ,8HOLIVINE ,8HFO ,
5      8HHALITE ,8HFA ,8HMAGNETIT,8HCHROMITE,8HHEMATITE,
6      8HILMENITE,8HPLAGIOCL,8HASE - AN,8HRUTILE ,8HTITANITE,
7      8HPEROVSKI,8HTE ,8HCOLOUR I,8HNDEX IS ,8HAPATITE ,
8      8HFLOURITE,8HPYRITE ,8HCALGITE ,8HBAKITE ,8HWITHERIT,
9      8HSPHALERI,8H ,8H ,8HTOTAL ,8H )
10  FORMAT (2X,A8,1X,14F4.2/11X,13F4.3)
15  FORMAT (2X,A8,1X,14F4.2/11X,13F4.4)
20  FORMAT (2X,A8,1X,14F4.2)
30  FORMAT (1H1,60X,8HPAGE NO.,16)
40  FORMAT (1H-,5X,*CIPW NORM OF SAMPLE NO.,*,A8)
50  FORMAT (1H-,9X,*SILICATE ANALYSIS*,26X,*FEMIC CONSTITUENTS*,29X,*SA
      LIC CONSTITUENTS*,10X,*OXIDE*,5X,*PERCENT*,11X,*MINERAL*,8X,
      2*PERCENT*,4X,*COMPONENT PERCENT*,16X,*MINERAL*,8X,*PERCENT*)
60  FORMAT (10X,A6,4X,17.2,11X,2A8,F6.2,4X,A8,3X,F7.2,16X,2A8,F6.2)
65  FORMAT (10X,A6,4X,17.4,11X,2A8,F6.2)
80  FORMAT (10X,A6,4X,17.2,11X,2A8,F6.2,38X,2A8,F6.2)
90  FORMAT (10X,A6,4X,17.2,37X,A8,3X,17.2,16X,2A8,F6.2)
100 FORMAT (10X,A6,4X,17.2,71X,2A8,F6.2)
70  FORMAT (38X,2A8,F6.2,38X,2A8,F6.2)
110 FORMAT (//20X,*TRIANGULAR DATA DIAGRAM*,// 7X,*Q = PLAG - OR*,
      15X,*K2O - NA2O - CAO*,
1      5X,*WO = FS = EN*,30X,*PLAGIOCLASE = AN*,10X,F6.2
2      ,1H0,6X,
2      *Q*,F12.2,5X,*K2O*,13.2,5X,*WO*,F10.2,30X,*COLOUR INDEX IS*,
3      31X,F6.2,7X,*PLAG*,F9.2,5X,*NA2O*,F12.2,5X,*FS*,F10.2,7X,*OR*,
4      4F11.2,5X,*CAO*,F13.2,5X,*EN*,F10.2,30X,*CALC. DENSITY*,12X,F6.2)
120 FORMAT (//88X,*SOLIDIFICATION INDEX*,6X,F6.2,7X,*Q = AB = OR*,5X
1      ,*OR = AB = AN*,5X,*F = M = A*,5X,*OL = NE = Q*,13X,*THORN
2      TON - TUTTLE*,88X,*DIFFERENTIATION INDEX*,5X,F6.2)
130 FORMAT (7X,*Q*,F12.2,5X,*OR*,F14.2,5X,*F*,F11.2,5X,*OL*,F10.2,13X,
1      1*PERALKALITY INDEX*,9X,F6.2,7X,*AB*,F11.2,5X,*AB*,F14.2,5X,*M*,
2      2F11.2,5X,*NE*,F10.2,13X,*K2O/NA2O*,18X,F6.2,7X,*OR*,F11.2,5X,*AN*
3      3,F14.2, 5X,*A*,F11.2,5X,*Q*,F11.2,13X,*TOTAL FE AS FEO*,11X,F6.2)
300 FORMAT (2A8)
310 IJKLMN=0
      ITHR=0
      IBLANK=8H
      ICD=14
      ITRIG=8HPLOTTRIA

```

```

TETRA=8HTETRAHED
ITRIA=ITRIG=0
LABQ=8HQUARTZ
LABCO=8HCORUNDUM
LABA=8HALSITE
LABO=8HORTHCLSE
LABP=8HPLAGCLSE
LABAN=8HANORTHTE
LABK=8H K2O
LABN=8H NA2O
LABC=8H CAO
LABW=8H WO
LABF=8H FS
LABE=8H EN
LABI=8H IRON
LABAA=8H ALKALI
LABM=8HMAGNESIA
LABSI=8H SI02
LABAL=8H AL2O3
LABFM=8H FEMICS
ITRIA=8HTRIANGLE
JKL=0
NPAGE=1

```

```

320 CONTINUE

```

```

C READ CHEMICAL DATA FROM CARDS, EITHER 14 OR 27 ELEMENTS

```

```

IF (ICD,EQ,27) 330 ,340

```

```

330 IF (ITHR,EQ,1) 331,332

```

```

331 READ 10,NAME,(T(J),J=1,ICD)

```

```

IF (EOF,60) 1250,350

```

```

332 READ 15,NAME,(T(J),J=1,ICD)

```

```

IF (EOF,60) 1250,350

```

```

340 READ 20 , NAME, (T(J),J=1,ICD)

```

```

IF (EOF,60)1250,350

```

```

350 IF (NAME,EQ,ITRIA)390 ,360

```

```

360 IF (NAME,EQ,ITRIG)400 ,370

```

```

370 IF (NAME,EQ,TETRA) 380,385

```

```

385 IF (NAME,EQ,8HSPECIAL ) 386,420

```

```

386 ITHR=1

```

```

GO TO 410

```

```

380 ITET=1

```

```

IF (T(1),GT,0,0) NOPQ=1

```

```

390 ITRIA=1

```

```

GO TO 410

```

```

400 ITRIG=1

```

```

IF(T(1),GT,0,0) JOAN=1

```

```

GO TO 410

```

```

C

```

```

C

```

```

410 CONTINUE

```

```

GO TO 320

```

```

420 IF (NAME,EQ,IBLANK) 430 ,440

```

```

430 ICD=27

```

```

GO TO 320

```

```

440 CONTINUE

```

```

JKL=JKL+1

```

```

SUM=0,0

```

```

DO 450 I=1,ICD

```

```

IF (I,NE,12,AND,I,NE,13) SUM=SUM+T(I)

```

```

450 CONTINUE

```

```

DO 455 I=1,ICD

```

```
IF (I.EQ.12.OR.I.EQ.13) 455,453
453 T(1)=T(1)*100./SUM
455 CONTINUE
SI=T(1)/60.06
TI=T(2)/79.9
AL=T(3)/101.94
F3=T(4)/159.68
F2=T(5)/71.84
FMN=T(6)/70.93
FMG=T(7)/40.32
CA=T(8)/56.08
ZNA=T(9)/61.99
YK=T(10)/94.19
P=T(11)/141.96
C=T(14)/44.01
TF = T(15)/19.0
TS = T(16)/32.056
TCL = T(17)/35.457
TV = T(18)/50.95
TCR = T(19)/52.01
TFGO=T(20)/58.94
TFNI= T(21)/58.69
TFGU= T(22)/63.54
TFZN= T(23)/65.38
TRB = T(24)/85.48
TSR = T(25)/87.63
TZR = T(26)/91.32
TBA = T(27)/137.36
CA=CA+TSR
FMG=FMG+TFNI
F2=F2+TFGO+FMN+TFGU
YK=YK+TRB
XONA= T(10)/T(9)
PERIND=(YK+ZNA)/AL
F3=F3+TV
PRINT 30 ,NPAGE
NPAGE=NPAGE+1
460 CONTINUE
DO 465, I=1,ICD
465 IF (I.NE.12.AND.I.NE.13) T(I)=T(I)*SUM/100,
POP=0.0
ZIR=CHR=FLU=PYR=SPHAL=HAL=BAR=WITH=0.0
IF(TZR)480,480,470
470 ZIR=TZR*1.5
SI=SI-TZR*0.5
480 IF (TCR) 500,500,490
490 CHR=TCR*2.0
F2=F2-CHR
500 IF(TF)540,540,510
510 IF(TF-P*0.1)530,530,520
520 TF=TF-0.1*P
POP=TF
FLU=TF*1.5
CA=CA-TF*0.5
TF=0.0
GO TO 540
530 TF=0.0
POP=0.0
540 IF(TCL)560,560,550
550 TCL=TCL-POP
```

```
      HAL=TCL*2,0
      ZNA=ZNA-TCL
560 IF (TZN-TS) 570,570,580
570 SPHAL=TZN*2
      TS=TS-TZN
      GO TO 590
580 SPHAL=TS*2
      TZN=TZN-TS
      F2=F2+TZN
590 CONTINUE
600 YK=YK+TBA
610 PYR=TS*1.5
620 TS=0,0
      IF(F2-TI)630,640,640
630 XIL=F2
      TI=TI-F2
      F2=0,
      GO TO 650
640 XIL=TI
      F2=F2-TI
      TI=0,
650 AP=P
      CA=CA-3,33*P
      IF(C-0,)660,660,670
660 CC=0,
      GO TO 680
670 CC=C
      CA=CA-C
680 IF(AL-YK)690,700,700
690 POR=AL
      PM=YK-AL
      AL=0,
      GO TO 710
700 POR=YK
      AL=AL-YK
      PM=0,
710 IF(AL-ZNA)720,720,720
720 I=1
      PAB=ZNA
      AL=AL-ZNA
      IF(AL-CA)740,730,730
730 J=1
      AN=CA
      CO=AL-CA
      RU=TI
      PF=0,
      GO TO 850
740 J=2
      AN=AL
      CA=CA-AL
      CO=0,
750 IF(CA-TI)760,760,770
760 K=1
      PF=CA
      RH=TI-CA
      CA=0,
      GO TO 850
770 K=2
      PF=TI
      RJ=0,
```

```
      CA=CA-TI
      GO TO 850
780 I=2
      J=2
      PAB=ZNA
      AL=0.
      AJ=0.
      CJ=0.
      GO TO 750
790 I=3
      J=2
      PAB=AL
      ZNA=ZNA-AL
      AJ=0.
      CJ=0.
      IF(ZNA-F3)800,810,810
800 L=1
      AG=ZNA
      SJ=0.
      F3=F3-ZNA
      GO TO 820
810 L=2
      AG=F3
      SJ=ZNA-F3
      F3=0.
820 IF(CA-TI)830,830,840
830 K=1
      PF=CA
      RI=TI-CA
      CA=0.
      GO TO 860
840 K=2
      PF=TI
      RI=0.
      CA=CA-TI
      GO TO 860
850 L=1
      AG=0.
      SJ=0.
860 GO TO(870,900),L
870 IF(F2-F3)880,890,890
880 ENT=F2
      HE=F3-F2
      F2=0.
      GO TO 910
890 ENT=F3
      F2=F2-F3
      HE=0.
      GO TO 910
900 ENT=0.
      HE=0.
910 GO TO(920,930),J
920 PEN=FMG
      PFS=F2
      WO=0.
      DWO=0.
      DEN=0.
      DFS=0.
      GO TO 970
930 GO TO(920,940),K
```

```
940 PEN=FMG
    PFS=F2
    XWO=CA
    IF(XWO-(PFS+PEN))950,960,960
950 M=1
    DWO=XWO
    DFS=PFS*DWO/(PFS+PEN)
    DEN=PEN*DWO/(PFS+PEN)
    PFS=PFS-DFS
    PEN=PEN-DEN
    WO=0,
    GO TO 970
960 M=2
    DWO=PEN+PFS
    WO=XWO-DWO
    DEN=PEN
    DFS=PFS
    PEN=0,
    PFS=0,
970 SA=6,*PAB+6,*POR+2,*AN+DWO+DEN+DFS+PEN+PFS+4,*AC+PM+SM*WO+PF
    IF(SI-SA)990,980,980
980 QZ=SI-SA
    AB=PAB
    OR=POR
    EN=PEN
    FS=PFS
    TN=PF
    PF=0,
    AK=0,
    VKA=0,
    XNE=0,
    PLE=0,
    FO=0,
    FA=0,
    GO TO 1130
990 SB=6,*PAB+6,*POR+2,*AN+DWO+DFS+DEN+,5*PEN+,5*PFS+WO+4,*AC+PM+SM
    IF(SI-SB)1010,1000,1000
1000 QZ=0,
    TN=0,
    AB=PAB
    OR=POR
    SL=SI-(6,*AB+6,*OR+2,*AN+DWO+DEN+DFS+4,*AC+PM+SM*WO)
    PHY=PFS+PEN
    OL=2,*PHY-2,*SL
    PHY=PHY-OL
    FO=PEN*OL/(PEN+PFS)
    FA=PFS*OL/(PEN+PFS)
    EN=PEN-FO
    FS=PFS-FA
    AK=0,
    VKA=0,
    XNE=0,
    PLE=0,
    GO TO 1130
1010 SC=6,*POR+2,*AN+DWO+DFS+DEN+,5*PEN+,5*PFS+2,*PAB*WO+4,*AC+SM+PM
    IF(SI-SC)1030,1020,1020
1020 QZ=0,
    TN=0,
    OR=POR
    FO=PEN
```

```

FA=PFS
EN=0,
FS=0,
SV=SI-(6.*OR+2.*AN+DWO+DFS+DEN+.5*FO+.5*FA+WO+4.*AC+SM*PM)
PNE=6.*PAB-SV
XNE=PNE/4,
AB=PAB-XNE
AK=0,
VKA=0,
PLE=0,
GO TO 1130
1030 SD=4.*POR+2.*PAB+2.*AN+DWO+DEN+DFS+.5*PEN+.5*PFS+WO+4.*AC+PM+SM
IF(SI-SD)1050,1040,1040
1040 QZ=0,
TN=0,
XNE=PAB
AB=0,
FO=PEN
FA=PFS
EN=0,
FS=0,
SN=SI-(2.*AN+2.*XNE+DWO+DFS+DEN+WO+.5*FA+.5*FO+SM+PM+4.*AC)
PLE=(6.*POR-SN)/2,
OR=POR-PLE
AK=0,
VKA=0,
GO TO 1130
1050 GO TO(1060,1080),M
1060 SE=4.*POR+2.*PAB+2.*AN+.5*DWO+.5*DFS+.5*DEN+.5*PFS+.5*PEN+4.*AC
SE=SE+SM+PM
IF(SI-SE)1120,1070,1070
1070 QZ=0,
TN=0,
PLE=POR
OR=0,
XNE=PAB
AB=0,
FO=PEN
FA=PFS
EN=0,
FS=0,
SD=SI-(4.*PLE+2.*XNE+2.*AN+4.*AC+.5*FA+.5*FO+SM+PM)
RDI=(2.*SD-(DEN+DFS+DWO))/2,
XOL=(DEN+DFS)-RDI
AK=DWO-RDI
DWO=RDI
XHY=RDI
GFS=DFS*XHY/(DEN+DFS)
GEN=DEN*XHY/(DEN+DFS)
XFA=DFS*XOL/(DEN+DFS)
XFO=DEN*XOL/(DEN+DFS)
DEN=GEN
DFS=GFS
FA=FA+XFA
FO=FO+XFO
VKA=0,
GO TO 1130
1080 SF=4.*POR+2.*PAB+2.*AN+.5*WO+DWO+DFS+DEN+.5*PEN+.5*PFS+4.*AC+SM+PM
IF(SI-SF)1100,1090,1090
1090 SR=4.*POR+2.*PAB+2.*AN+4.*AC+DWO+DFS+DEN+.5*PFS+.5*PEN+WO+SM+PM

```

```

XSI=SR-SI
AK=2,*XSI
WO=WO-AK
QZ=0,
TN=0,
PLE=POR
OR=0,
XNE=PAB
AB=0,
FO=0,
FA=0,
EN=0,
FS=0,
VKA=0,
GO TO 1130
1100 SQ=4,*POR+2,*AN+2,*PAB+.5*WO+.5*DW0+.5*DEN+.5*DFS+.5*PEN+.5*PFS
SQ=SQ+4,*AG+SM+PM
IF (SI-SG) 1120,1110,1110
1110 QZ=0,
TN=0,
OR=0,
PLE=POR
XNE=PAB
AB=0,
EN=0,
FS=0,
FO=0,
FA=0,
SQ=SI-(4,*PLE+2,*XNE+2,*AN+4,*AC+.5*FA+.5*FO+SM+PM)
RDI=(2,*SQ-(DEN+DFS+DW0+WO))/2,
XOL=(DEN+DFS)-RDI
AK=(DW0+WO)-RDI
DW0=RDI
WO=0,
XHY=RDI
GFS=DFS*XHY/(DEN+DFS)
GEN=DEN*XHY/(DEN+DFS)
XFA=DFS*XOL/(DEN+DFS)
XFO=DEN*XOL/(DEN+DFS)
FA=FA+XFA
FO=FO+XFO
DEN=GEN
DFS=GFS
VKA=0,
GO TO 1130
1120 QZ=0,
TN=0,
OR=0,
XNE=PAB
AB=0,
EN=0,
FS=0,
FO=PEN
FA=PFS
AK=DW0+WO
FO=FO+DEN
FA=FA+DFS
WO=0,
DW0=0,
DEN=0,

```

```

DFS=0,
ST=2,*XNE+2,*AN+4,*AC+SM+.5*FA+.5*FO+.5*AK*PM
YSI=SI-ST
PLE=(YSI-2,*POR)/2,
VKA=(4,*POR-YSI)/2,
1130 AQ=T(12)+T(13)
QZ=QZ*60.06
OR=OR*556.49
AB=AB*524.29
AN=AN*278.14
XNE=XNE*284.05
PLE=PLE*436.37
VKA=VKA*316.25
CO=CO*101.94
AG=AG*461.91
WO=WO*116.14
DWO=DWO*116.14
DEN=DEN*100.38
DFS=DFS*131.90
EN=EN*100.38
FS=FS*131.90
AK=(AK/2.)*172.22
FO=(FO/2.)*140.7
FA=(FA/2.)*203.74
EMT=EMT*231.52
HE=HE*159.68
XIL=XIL*151.74
RU=RU*79.90
TN=TN*196.04
PF=PF*135.98
SM=SM*122.05
PM=PM*154.25
AP=AP*336.61
CC=CC*100.09
GHR=GHR*259.7/2,
SPHAL=SPHAL*97.4/2,
ZIR=ZIR*306.5/3,
HAL=HAL*63.45/2,
FLU=FLU*78.1/3,
PYR=PYR*120.0/3,
IF (AN) 1140,1150,1150
1140 AN=0,0
1150 CONTINUE
SUM2=XIL+AP+CC+PM+AN+CO+RU+PF+AC+TN+EMT+AB+HE+WO+EN+FS+DEN+DFS+DWO
SUM2=SUM2+QZ+OR+FO+FA+XNE+PLE+AK+VKA+AQ
DENTY=XIL/4,79+AP/3,1+CC/2,711+AN/2,76+CO/3,98+RU/4,25
1      +PF/3,98+AC/3,55+EMT/5,20+AB/2,62+HE/5,256+WO/3,85
2      +EN/3,18+FS/3,95+DEN/3,18+DFS/3,95+DWO/3,25+QZ/2,65
3      +OR/2,56+FO/3,22+FA/4,39+XNE/2,55+PLE/2,47
4      +VKA/2,59+CHR/5,09+SPHAL/4,096+ZIR/4,65+HAL/2,164
5      +FLU/3,18+PYR/5,01+TN/3,5
C      ALKALI - Q - G TRIANGLE
TOT=T(1)+T(3)+T(9)+T(10)
ZAT=(T(10)+T(9))/TOT*100
ZQZT=T(1)/TOT*100
ZCOT=T(3)/TOT*100
OLNEW=XOLIV+EN*140,7/200,76 +FS*203,74/263,8
QNEW=QZ+(EN/200,76+FS/263,80+AB/131,07)*60,06
XNEW=XNE+AB*142,02/262,14
TOT=OLNEW+QNEW+XNEW

```

```

      OLNEW=OLNEW*100./TOT
      QNEW=QNEW*100./TOT
      XNENEW=XNENEW*100./TOT
      TOT= T(5)+0.9*T(4)+ T(7)+ T(9)+ T(10)
C      FMA DIAGRAM
      TOTFE=T(5)+0.9*T(4)
      FMAF=TOTFE/TOT *100.
      FMAM= T(7)/TOT *100.
      FMAA= (T(9)+T(10))/TOT *100.
      TOT= T(10)+ T(9)+ T(8)
C      K/NA/GA WT OCT
      XKT= T(10)*100.0/TOT
      XNT= T(9)*100.0/TOT
      XCT= T(8)*100.0/TOT
      TOT= QZ+ AB+ OR
C      Q/AB/OR WT PCT
      XQT= QZ *100.0/TOT
      XAT= AB *100.0/TOT
      XOT= OR *100.0/TOT
      TOT= TOT +AN
C      Q/RLAG/OR WT PCT
      XQQT= QZ *100.0/TOT
      XPLT= (AB+AN)*100.0/TOT
      XOOT= OR *100.0/TOT
      TOT= TOT -QZ
C      AB/AN/OR WT PCT
      XABT= AB *100.0/TOT
      XORT= OR *100.0/TOT
      XANT= AN *100.0/TOT
      DIFIND=QZ+ AB+ OR+ XNE+ PLE
      SOLIND= T(7)*100.0/(T(7)+T(5)+T(4)+T(9)+T(10))
      FFFF= T(4)*0.9 +T(5)
      FOFM= FFFF/(FFFF+T(7))
C      WO - FS - EN TRIGDIG
      TOT= WO + FS + EN + DWG + DFB + DEN
      XWOT= (WO+DWG)*100.0/TOT
      XFST= (FS+DFB)*100.0/TOT
      XENT= (EN+DEN)*100.0/TOT
C
C  TRANSFER TRIANGLE DATA TO DRUM UNITS
C
1160 WRITE (21) ZAT,ZCOT
      WRITE (22) FMAF,FMAA
      WRITE (23) XKT,XNT
      WRITE (24) XQT,XAT
      WRITE (25) XQQT,XPLT
      WRITE (26) XORT,XABT
      WRITE (27) XWOT,XENT
      WRITE (30) QNEW,OLNEW
1170 PLAG=100*AN/(AN+AB)
      IF (PLAG) 1180,1190,1190
1180 PLAG=0.0
1190 CONTINUE
      PRINT 40 ,NAME
      SUM2=SUM2+CHR+SPHAL+ZIR+HAL+FLU+PYR
      SUM3=AN+AB+OR+QZ+CO+HAL+AK+VKA+XNE
      SUM3=SUM3+ZIR
      COLIND=1-(SUM3/SUM2)
      DENTY=SUM2/DENTY

```

```

PRINT 50
PRINT 60, IELM(1), T(1), MINL(27), MINL(49), AC
PRINT 100, IELM(2), T(2), MINL(1), MINL(49), QZ
PRINT 80, IELM(3), T(3), MINL(5), MINL(6), WO, MINL(3), MINL(49), CO
PRINT 100, IELM(4), T(4), MINL(4), MINL(49), ZIR
PYROX=DWO+DEN+DFS
PRINT 60, IELM(5), T(5), MINL(9), MINL(49), PYROX, MINL(10), DWO
PRINT 90, IELM(6), T(6), MINL(12), DEN, MINL(7), MINL(8), OR
PRINT 90, IELM(7), T(7), MINL(15), DFS, MINL(11), MINL(49), AB
PRINT 100, IELM(8), T(8), MINL(13), MINL(14), AN
PYROX=EN+FS
PRINT 60, IELM(9), T(9), MINL(18), MINL(19), PYROX, MINL(12), EN
PRINT 90, IELM(10), T(10), MINL(15), FS, MINL(16), MINL(17), XNE
PRINT 100, IELM(11), T(11), MINL(20), MINL(49), PLE
XOLIV=FO+FA
PRINT 60, IELM(12), T(12), MINL(23), MINL(49), XOLIV, MINL(24), FO,
1 MINL(21), MINL(22), VKA
PRINT 90, IELM(13), T(13), MINL(26), FA
PRINT 100, IELM(14), T(14), MINL(25), MINL(49), HAL
PRINT 70, MINL(27), MINL(14), EMT, MINL(28), MINL(49), CHR
PRINT 60, IELM(15), SUM, MINL(29), MINL(49), HE
PRINT 70, MINL(30), MINL(49), XIL, MINL(33), MINL(49), RU
PRINT 65, IELM(16), T(15), MINL(34), MINL(49), TN
PRINT 65, IELM(17), T(16), MINL(35), MINL(36), PF
PRINT 65, IELM(18), T(17), MINL(39), MINL(49), AP
PRINT 65, IELM(19), T(18), MINL(40), MINL(49), FLU
PRINT 65, IELM(20), T(19), MINL(42), MINL(49), GC
PRINT 65, IELM(21), T(20), MINL(41), MINL(49), PYR
PRINT 65, IELM(22), T(21), MINL(45), MINL(36), SPHAL
DO 765 IJK=23,28
JKL=IJK-1
765 PRINT 65, IELM(IJK), T(JKL)
PRINT 110, PLAO, XQOT, XKT, XWOT, COLIND, XPLT, XNT, XFST, XOOT, XGT, XENT,
1 DENTY
PRINT 120, SOLIND, DIFIND
PRINT 130, XQT, XORT, FMAF, OLNEW, PERIND, XAT, XABT, FMAM, XNENEW, XONA,
1 XOT, XANT, FMAA, ONEW, TOTFE
FEMICS=SUM2-SUM3
Z1=2
IF (ITET.EQ,1) 1200,1240
1200 IF (NOPQ.EQ,1) 1210,1220
1210 WRITE (28) QZ,AB,OR,CO
GO TO 1230
1220 WRITE (28) FMAF,FMAA,FMAM,QZ
1230 WRITE (29) FEMICS,OR,AB,AN
1240 GO TO 320
1250 DO 1260 LUN= 21,30
1260 REWIND LUN
IF (ITET.NE,1) GO TO 1280
CALL TETRPLT(LABFM,LABO,LABA,LABAN,29,JKL,2)
IF (NOPQ.EQ,1) GO TO 1270
CALL TETRPLT(LAB1,LABAA,LABM,LABQ,28,JKL,1)
GO TO 1280
1270 CALL TETRPLT(LABQ,LABA,LABO,LABCO,28,JKL,1)
C BEGIN TRIANGLE PLOTTING
1280 IF (IITRIG.NE,1) GO TO 1330
READ 300 , (NTITLE(I),I=1,27)
IF (EOF,60) 1290,1300
1290 NTITLE(1)=NTITLE(2)=8H
1300 CONTINUE

```

```
IF(JOAN,EQ,1) GO TO 1310  
CALL TRIGPLOT (LABI,LABAA,LABM,22,JKL,NTITLE,3)
```

```
GO TO 1320
```

```
1310 CALL TRIGPLOT (LABQ,LABA,LABO,24,JKL,NTITLE,3)
```

```
1320 CALL TRIGPLOT(LABO,LABA,LABAN,26,JKL,NTITLE,4)
```

```
1330 IF (ITRIA,NE,1) GO TO 1340
```

```
CALL TRIGDIG(LABQ,LABA,LABO,24,JKL)
```

```
CALL TRIGDIG(LABO,LABP,LABO,25,JKL)
```

```
CALL TRIGDIG(LABAA,LABAL,LABSI,21,JKL)
```

```
CALL TRIGDIG(LABO,LABA,LABAN,26,JKL)
```

```
CALL TRIGDIG(LABK,LABN,LABC,23,JKL)
```

```
CALL TRIGDIG(LABI,LABAA,LABM,22,JKL)
```

```
CALL TRIGDIG(LABW,LABE,LABF,27,JKL)
```

```
CALL TRIGDIG (2HYZ,2HOL,2HNE,30,JKL)
```

```
1340 CALL EXIT
```

```
END
```

```

SUBROUTINE TRIGDIG (LAB1,LAB2,LAB3,LUN,N)
  DIMENSION LINE (51,101)
  INTEGER SYM(36)
  INTEGER DOT,PLUS,STAR
  INTEGER SPACE
  DATA (DOT=1H.), (PLUS=1H+), (STAR=1H*)
  DATA (SYM=1H1,1H2,1H3,1H4,1H5,1H6,1H7,1H8,1H9,1HA,1HB,1HC,1HD,1HE,
1      1HF,1HG,1HH,1HJ,1HK,1HL,1HM,1HN,1HP,1HQ,1HR,1HS,1HT,1HU,
2      1HV,1HW,1HX,1HY,1HZ,1H-,1H*,1H=)
  SPACE = 1H
  DO 1 I=1,51
  DO 1 J=1,101
C INITIALISE ARRAY LINE
1 LINE(I,J)=1H
  LINE(1,51)=DOT
  DO 2 I=2,51
  J1=52-I
  J2=50+I
  LINE(I,J1)=DOT
2 LINE(I,J2)=DOT
  DO 3 J=1,101,2
3 LINE(51,J)=DOT
  DO 4 I=1,N
  READ (LUN) A,B
  ALEVEL = 51.0 - 0.50 * A + 0.5
  LEVEL=INT(ALEVEL)
  ALONG = 101.5 - 0.505 * A - B
  LONG=INT(ALONG)
  IF(LONG.GT.101.OR.LONG.LE.0.OR.LEVEL.GT.51.OR.
1LEVEL.LE.0) GO TO 35
  LINO=LINE(LEVEL,LONG)
  IF(LINO,EQ,1H ) 34,31
31 IF(LINO,EQ,SYM(36))GO TO 4
  DO 33 J=1,35
  IF (LINO,EQ,SYM(J))32,33
33 CONTINUE
34 J=0
32 J=J+1
  LINE(LEVEL,LONG)=SYM(J)
  GO TO 4
35 PRINT 902,A,B,LONG,LEVEL
4 CONTINUE
  PRINT 899,LAB1,LAB2,LAB3,LAB1
  PRINT 900, ((LINE(I,J),J=1,101),I=1,51)
  PRINT 901, LAB2,LAB3
  REWIND LUN
C
899 FORMAT(1H1,A8,1H-,A8,1H-,A8,3X,*TERNARY DIAGRAM*/1H0,36X,A8)
900 FORMAT(1H ,10X,101A1)
901 FORMAT(1H ,6X,A8,93X,A8)
902 FORMAT(1H ,*PT OUT OF TRIANGLE*,2F8.2,2I4)
  RETURN
  END

```

```

SUBROUTINE TRIGPLOT (LAB1,LAB2,LAB3,LUN,N,NTITLE,IZ)
  DIMENSION ISYM(3)
  DIMENSION NTITLE(2)
  COMMON IJKLMN
  DATA (ISYM=21000112132425368,37364544535261608,007000000000000000B)
900 FORMAT(1H1,*SUBROUTINE TRIGPLOT TEMPORARILY DISABLED, END C)
  1,* FILE, EOF READ ON *,I3,*TH ITERATION, TOTAL NO, OF POINTS*
  2,* SHOULD BE *,I3)
  IFLAG=0
  Q=20./SQRT(3.)
  CALL PLOT(10.,0,2,IZ)
  CALL PLOT(0.,-25.,1,IZ)
  CALL PLOT(0.,0.,3,IZ)
  CALL PLOT(50.,100.,4,IZ)
  CALL PLOT(100.,0.,4,IZ)
  CALL PLOT(0.,0.,4,IZ)
  CALL PLOT(0.0,-5.0,3,IZ)
  CALL TEXT(LAB2,8,2,IZ)
  CALL PLOT(92.0,-5.0,3,IZ)
  CALL TEXT(LAB3,8,2,IZ)
  CALL PLOT(46.0,103.0,3,IZ)
  CALL TEXT(LAB1,8,2,IZ)
  2 DO 1 J=1,N
  8 READ (LUN) B,A
  IF (EOF,LUN) 6,7
  6 PRINT 900, J,N
  IF (IFLAG.EQ.1) GO TO 9
  IFLAG=1
  GO TO 8
  7 IFLAG=0
  Y=B
  X=100,-A-0.5*B
  IF (X.GT.100.0.OR.X.LT.0.0.OR.Y.GT.100.0.OR.Y.LT.0.0) 3,4
  3 PRINT 5, A,B,X,Y,NTITLE(1),NTITLE(2)
  5 FORMAT(1H0,*PLOT OUT OF TRIANGLE*,F8,3,2X,F8,3,4X,F8,3,F8,3,3X,2A8
  1)
  GO TO 1
  4 CALL PLOT(X,Y,3,IZ)
  CALL TEXT(ISYM,1,-1)
  1 CONTINUE
  YPOS=90,
  CALL PLOT(75.,YPOS,3,IZ)
  CALL TEXT(ISYM,1,-1)
  CALL PLOT(80.,YPOS,3,IZ)
  CALL TEXT(NTITLE,16,2,IZ)
  9 REWIND LUN
  RETURN
END

```

```
SUBROUTINE TETRPLUT (L1,L2,L3,L4,LUN,N,Z)
```

```
INTEGER Z
```

```
QQ=20./SQRT(3.)
```

```
CALL PLOT(10.,QQ,2,Z)
```

```
CALL PLOT (0.,-40.,1,Z)
```

```
CALL PLOT (0.,0.,3,Z)
```

```
CALL PLOT (50.,100.,4,Z)
```

```
CALL PLOT (100.,0.,4,Z)
```

```
CALL PLOT (0.,0.,4,Z)
```

```
CALL PLOT (70.,-33.33,4,Z)
```

```
CALL PLOT (100.,0.,4,Z)
```

```
CALL PLOT (70.,-33.33,3,Z)
```

```
CALL PLOT (50.,100.,4,Z)
```

```
CALL PLOT(46.0,103.0,3,Z)
```

```
CALL TEXT(L1,8,2,Z)
```

```
CALL PLOT(0,0,-5,0,3,Z)
```

```
CALL TEXT(L2,8,2,Z)
```

```
CALL PLOT(92,0,-5,0,3,Z)
```

```
CALL TEXT(L3,8,2,Z)
```

```
CALL PLOT(66,0,-38,0,3,Z)
```

```
CALL TEXT(L4,8,2,Z)
```

```
DO 2 I=1,N
```

```
READ (LUN) A,B,C,D
```

```
TOT=A+B+C
```

```
AB=A*100./TOT
```

```
BB=B*100./TOT
```

```
TOT=B+C+D
```

```
DD = D*100./TOT
```

```
BD= B*100./TOT
```

```
TOT=A+B+D
```

```
AL= A*100./TOT
```

```
BL= B*100./TOT
```

```
TOT=A+C+D
```

```
AR=A*100./TOT
```

```
CR=C*100./TOT
```

```
1 YB= AB
```

```
XB =100,-BB*0.5*AB
```

```
XD =100,-BD-DD*0.3
```

```
YD =-DD/3,
```

```
YL =(AL*4,+BL-100,)/3,
```

```
XL = 70,-AL*0.2-BL*0.7
```

```
YR=(AR*4,+CR-100,)/3,
```

```
XR = 70,+CR*0.3-AR*0.2
```

```
C
```

```
TOT=A+B+C+D
```

```
AA =A*100./TOT
```

```
BA =B*100./TOT
```

```
CA =C*100./TOT
```

```
DA=D*100./TOT
```

```
Y=AA-DA/3,
```

```
X=100,-0.3*DA-0.5*AA-BA
```

```
CALL PLOT(XB,YB,3,Z)
```

```
CALL PLOT(X,Y,4,Z)
```

```
CALL PLOT(XL,YL,4,Z)
```

```
CALL PLOT(XD,YD,3,Z)
```

```
CALL PLOT(X,Y,4,Z)
```

```
2 CALL PLOT(XR,YR,4,Z)
```

```
RETURN
```

9.5DAD TETRLOT

04/09/72

END

APPENDIX 2

Listing of program NIGGBART.

```

PROGRAM NIGBAR
DIMENSION T(14), TT(14), TTT(14), NIG(14), BARTH(14), BASIS(16)
DIMENSION WT(14), OX(14), CA(14), NI(14), BAR(14), BAS(16)
REAL NIG
DATA( WT=60.06,79.90,101.94,159.68,71.84,70.93,40.32,56.08,61.89,
  94.19,141.96,18.01,16.18,016.44,01)
DATA(OX=8HSI02 ,8HTI02 ,8HAL203 ,8HFE203 ,8HFE0
1 8HMNO ,8HMG0 ,8HCA0 ,8HNA20 ,8HK20
2 8HP205 ,8HM20(=) ,8HM20(=) ,8HCO2
DATA(CA=8HSI ,8HTI ,8HAL ,8HFE(3) ,8HFE(2)
1 8HMN ,8HMG ,8HCA ,8HNA ,8HK
2 8HP ,8H ,8H ,8H ,8H
DATA(NI=8HSI ,8HAL ,8HFM ,8HC ,8HALK
1 8HTI ,8HP ,8HCO2 ,8HK ,8HMG
2 8HW ,8HAL-ALK=T ,8HT=C ,8HAL-ALK=F)
DATA(BAR=8HSI ,8HTI ,8HAL ,8HFE ,8HMN
1 8HMG ,8HCA ,8HNA ,8HK ,8HP
2 8HC ,8HOXY ,8HQH ,8HCA ,8H
DATA(BAS=8HCP ,8HKP ,8HKS ,8HNE ,8HNS
1 8HCAL ,8HCS ,8HSP ,8HHZ ,8HC
2 8HFS ,8HFD ,8HFA ,8HRU ,8HQ
3 8HCC )
901 FORMAT(1H1, 'CALCULATION OF NIGGLI VALUES, BARTH STANDARD ',
10CELL, NIGGLI BASIS VALUES AND COMPOSITION TRIANGLES FOR ',
20SAMPLE ,A8, '1H, 'SILICATE ANALYSIS', 8X, 'CATION PERCENT',
311X, 'NIGGLI VALUES', 12X, 'BARTH STANDARD CELL', 6X, 'NIGGLI BASIS')
900 FORMAT(2X, A8, 1X, 14F4, 2)
902 FORMAT(1H , 5(A8, F12, 2, 5X))
903 FORMAT(1H , A8, F12, 2, 30X, 3(A8, F12, 2, 5X))
904 FORMAT(1H , 100X, A8, F12, 2)
905 FORMAT(1H0, 'TRIANGULAR DIAGRAMS', 18X, 'Q = L = M')
906 FORMAT(1H , 37X, A2, 18X, F10, 2)
907 FORMAT(1H0, 37X, 'K = NA = CA (BOUND TO AL)')
908 FORMAT(1H0, 37X, 'MG = FE = CA (NOT BOUND TO AL)')
909 FORMAT(1H0, 37X, 'Q = KP = NE')
JKL=IT=SUM=0.0
1 READ(5, 900), ID, TT
IF(EOF, 60) 99, 98
98 IF(ID, EQ, 8HTRIANGLE) 2, 3
2 IT=1
GO TO 1
3 DO 4 I=1, 14
T(I)=TT(I)/WT(I)
4 IF(I, NE, 12, AND, I, NE, 13) SUM=SUM+T(I)
JKL=JKL+1
DO 5 I=1, 14
5 TTT(I)=T(I)=T(I)*100.0/SUM
C
C CALCULATION OF NIGGLI VALUES
C
TEMP=T(5)*2.0+T(4)
TOT=T(3)+TEMP+T(6)+T(7)+T(8)+T(9)+T(10)
F=100.0/TOT
NIG(2)=T(3)*F
NIG(3)=(TEMP+T(5)+T(6)+T(7)+T(8)+T(9)+T(10))*F
NIG(4)=T(8)*F
NIG(5)=(T(9)+T(10))*F
NIG(1)=T(1)*F
NIG(9)=T(10)/(T(9)+T(10))
NIG(6)=T(2)*F

```

```

NIG(10)=T(7)/(TEMP+T(6)+T(7))
NIG(11)=2*T(4)/TEMP
NIG(7)=T(11)*F
NIG(8)=T(14)*F
NIG(12)=NIG(2)-NIG(5)
NIG(13)=NIG(12)-NIG(4)
NIG(14)=NIG(2)+NIG(5)

```

C
C CALCULATION OF BARTH STANDARD CELL
C

```

TTT(4)=T(4)*2,
TTT(3)=T(3)*2,
TTT(9)=T(9)*2,
TTT(10)=T(10)*2,
TTT(11)=T(11)*2,
SUM=100+T(4)+T(3)+T(9)+T(10)+TTT(11)
DO 19 I=1,14
19 T(I)=TTT(I)=TTT(I)*100./SUM
OXY=2+.T(1)+1.5*T(3)+2.*T(2)+1.5*T(4)+T(5)+T(6)+T(7)+T(8)+0.5*T(9)
+0.5*T(10)+2.5*T(11)+2.*T(14)
OXY=OXY*T(12)
CAT=160+100./OXY
OH=2+.T(12)*CAT/100.0
DO 6 I=1,10
J=1
IF(I,GT,4) J=J+1
6 BARTH(I)=T(J)*CAT/100.
BARTH(4)=BARTH(4)+T(5)*CAT/100.
BARTH(11)=T(14)*CAT/100.
BARTH(12)=OXY
BARTH(13)=OH
BARTH(14)=CAT

```

C
C CALCULATION OF NIGGLI BASIS
C

```

BASIS(16)=T(14)
T(8)=T(8)+T(14)
T(14)=0.0
BASIS(1)=T(11)*2.5
T(8)=T(8)+1.5*T(11)
T(11)=0.0
IF (T(10),GT,T(3)) GO TO 7
BASIS(2)=T(10)*3.0
T(1)=T(1)+T(10)
T(3)=T(3)+T(10)
T(10)=0.0
GO TO 8
7 BASIS(2)=T(3)*3.0
T(1)=T(1)+T(3)
T(10)=T(10)+T(3)
T(3)=0.0
BASIS(3)=1.5*T(10)
T(1)=T(1)+0.5*T(10)
T(10)=0.0
GO TO 10
8 IF (T(9),GT,T(3)) GO TO 9
BASIS(4)=3.0*T(9)
T(3)=T(3)+T(9)
T(1)=T(1)+T(9)
T(9)=0.0

```

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```
GO TO 11
9 BASIS(4)=3.0*T(3)
T(9)=T(9)-T(3)
T(1)=T(1)-T(3)
T(3)=0.0
10 BASIS(5)=T(9)*1.5
T(1)=T(1)-0.5*T(9)
T(9)=0.0
GO TO 13
11 TEMP=0.5*T(3)
IF (TEMP,LT,T(8)) GO TO 12
BASIS(6)=3.0*T(8)
T(3)=T(3)-2.0*T(8)
T(8)=0.0
GO TO 14
12 BASIS(6)=1.5*T(3)
T(8)=T(8)-0.5*T(3)
T(3)=0.0
13 BASIS(7)=1.5*T(8)
T(1)=T(1)-0.5*T(8)
T(8)=0.0
GO TO 20
14 TEMP=0.5*T(3)
IF (TEMP,LT,T(7)) GO TO 15
BASIS(8)=3.0*T(7)
T(3)=T(3)-2.0*T(7)
T(7)=0.0
GO TO 16
15 BASIS(8)=1.5*T(3)
T(7)=T(7)-0.5*T(3)
T(3)=0.0
GO TO 20
16 TEMP=0.5*T(3)
IF (TEMP,LT,T(5)) GO TO 17
BASIS(9)=3.0*T(5)
T(3)=T(3)-2.0*T(5)
T(5)=0.0
BASIS(10)=T(3)
T(3)=0.0
GO TO 20
17 BASIS(9)=1.5*T(3)
T(5)=T(5)-0.5*T(3)
T(3)=0.0
20 BASIS(11)=1.5*T(4)
T(1)=T(1)-0.5*T(4)
T(4)=0.0
IF (T(5),LT,0.001,AND,T(7);LT,0.001)GO TO 21
BASIS(12)=1.5*T(7)
T(1)=T(1)-0.5*T(7)
T(7)=0.0
BASIS(13)=1.5*T(5)
T(1)=T(1)-0.5*T(5)
T(5)=0.0
21 BASIS(14)=T(2)
BASIS(15)=T(1)
```

C
C
C

CALCULATION OF TRIANGLES

```
TL=BASIS(2)+BASIS(4)+BASIS(6)+
TM=BASIS(7)+BASIS(12)+BASIS(13)+BASIS(11)+BASIS(5)+BASIS(3)
```

```

1+BASIS(14)+BASIS(1)+BASIS(16)
TQ=BASIS(15)
TOT=TL+TQ+TM
F=100./TOT
TL=TL*F
TM=TM*F
TQ=TQ*F
TOT=BASIS(2)+BASIS(4)+BASIS(6)
F=100./TOT
TK=BASIS(2)*F
TNA=BASIS(4)*F
TCA=BASIS(6)*F
TOT=BASIS(11)+BASIS(12)+BASIS(13)+BASIS(7)
F=100./TOT
TMG=BASIS(12)*F
TFE=(BASIS(11)+BASIS(13))*F
TCS=BASIS(7)*F
TOT=BASIS(15)+BASIS(2)+BASIS(4)
F=100./TOT
TQQ=BASIS(15)*F
TKP=BASIS(2)*F
TNE=BASIS(4)*F
PRINT 901, ID
DO 23 I=1,14
IF(I,EQ,12.OR,I,EQ,13) GO TO 22
PRINT 902,OX(I),TT(I),CA(I),TTT(I),NI(I),NIQ(I),BAR(I),BARTH(I),
1BASIS(I),BASIS(I)
GO TO 23
22 PRINT 903,OX(I),TT(I),NI(I),NIQ(I),BAR(I),BARTH(I),BASIS(I),
1BASIS(I)
23 CONTINUE
PRINT 904,BAS(15),BASIS(15)
PRINT 904,BAS(16),BASIS(16)
PRINT 905
PRINT 906,2HQ ,TQ,2HL ,TL,2HM ,TM
PRINT 907
PRINT 906,2HK ,TK,2HNA,TNA,2HCA,TCA
PRINT 908
PRINT 906,2HMG,TMG,2HFE,TFE,2HCA,TCS
PRINT 909
PRINT 906,2HQ ,TQQ,2HKP,TKP,2HNE,TNE
SUM=0,0

```

```

C
C CHECK FOR TRIANGLE PLOTTING
C AND COPY DATA TO DRUM IF
C REQUIRED
C

```

```

IF (IT,NE,1) GO TO 1
WRITE (21) TQQ,TNE
WRITE (22) TCS,TMG
WRITE(23) TCA,TNA
WRITE(24) TQ,TH
GO TO 1
99 CONTINUE
IF(IT,NE,1) STOP
DO 100 I=21,24
100 REWIND I
CALL TRIGDIG(8HQ ,8HM ,8HL ,24,JKL)
CALL TRIGDIG(8H Q ,8H NE ,8H KP ,21,JKL)
CALL EXIT

```

KF9,34D

END

APPENDIX 3

Listing of program ZAVSKY.

PROGRAM ZAVSKY

C
 C PROGRAM WRITTEN BY S. HENLEY BMR JUNE 1971
 C CALCULATES AND PLOTS ZAVARITSKY NUMBERS
 C REF - INT. GEOL. REV. 1964 P. 1-17
 C

DIMENSION WT(14), CA(14), CROSS(2), ID(2)
 DIMENSION OXIDES(14), CATIONS(14), ZAVS(14), VAL(14), T(14)

REAL NAPR, MPR, N, NPR

DATA (WT=60,06,79,90,101,94,159,68,71,84,70,93,40,32,
 * 56,08,61,994,94,192,141,96,18,016,18,016,44,02)

DATA (OXIDES=6HSIO2, 6HTIO2, 6HAL2O3, 6HFE2O3, 6HFEO,
 * 6HMNO, 6HMO, 6HCAO, 6HNA2O, 6HK2O,
 * 6HP2O5, 6HH2O(+), 6HH2O(-), 6HCO2)

DATA (CATIONS=6HSI, 6HTI, 6HAL, 6HFE(3), 6HFE(2),
 * 6HMN, 6HMG, 6HCA, 6HNA, 6HK,
 * 6HP, 6HH(+), 6HH(-), 6HC)

DATA (ZAVS=4HA, 4HC, 4HB, 4HS, 4H/C, 4HF', 4HM',
 * 4HC', 4HA', 4HN, 4HT, 4HPH', 4HN')

DATA (CROSS=1202052747656240B, 2002700000000000B)

ISUPP = 1

GO TO 70

10 READ (5,901) ID, T

IF (ID(1), EQ, 8HSUPPRESS) 101, 102

101 ISUPP = (-1)

GO TO 10

102 CONTINUE

IF (EOF, 5) 99, 11

11 II = II + 1

C

C CALCULATE CATION PERCENT

C

SUM = 0.0

DO 20 I = 1, 14

CA(I) = T(I) / WT(I)

20 SUM = SUM + CA(I)

DO 21 I = 1, 14

21 CA(I) = CA(I) * 100. / SUM

C

C CALCULATE ZAVARITSKY NUMBERS

C

ALPR = FEPR = CBAR = CAPR = NAPR = 0.0

ALKS = CA(9) + CA(10)

FEO = CA(5) + CA(6)

SS = CA(1) + CA(2)

IF (ALKS, LE, CA(3)) 30, 40

30 AA = ALKS

Z = (CA(3) - ALKS) / 2.

GO TO 50

40 AA = CA(3)

CBAR = ALKS - A

Z = (-CBAR / 2.)

50 IF (Z, LE, CA(8)) 51, 56

51 CC = Z

GO TO 60

56 CC = CA(8)

ALPR = CA(3) - CC - CC - ALKS

60 FEPR = CA(4) + FEO - CBAR

IF (FEPR, LT, 0.0) 61, 62

61 NAPR = CC + FEPR

```
FEPR=0.0
62 CAPR=CA(8)-CC
BB=FEPR+CA(7)+CAPR+ALPR
SUM=AA+BB+CC+SS
SUM=100./SUM
A=AA*SUM
C=CC*SUM
B=BB*SUM
S=SS*SUM
```

```
C
C SUPPLEMENT
C -ARY CHARACTERS
C
```

```
FPR=FEPR*100./BB
MPR=CA(7)*100./BB
CPH=CAPR*100./BB
N=CA(9)*100./AA
TI=CA(2)*100./SS
PHI=CA(4)*100./BB
APR=ALPR*100./BB
NPR=NAPR*100./BB
```

```
C
C PRINT RESULTS
C
```

```
PRINT 900, II, ID
PRINT 903, (OXIDES(I),T(I),CATIONS(I),CA(I),I=1,14)
PRINT 905
VAL(1)=A
VAL(2)=C
VAL(3)=B
VAL(4)=S
VAL(5)=CBAR
VAL(6)=FPR
VAL(7)=MPR
VAL(8)=CPH
VAL(9)=APR
VAL(10)=N
VAL(11)=TI
VAL(12)=PHI
VAL(13)=NPR
PRINT 906, (ZAVS(I),VAL(I),I=1,13)
GO TO 80
```

```
C
C PLOTTING
C
```

```
70 CALL PLOT (-50.,-150.,1)
CALL PLOT (10.,10.,2)
CALL PLOT(-50.,2.,3)
CALL TEXT (1HC,1,2)
CALL TEXT (3H 50,3,2)
CALL PLOT (-50.,0.,3)
CALL PLOT (50.,0.,4)
CALL PLOT (46.0,2.,3)
CALL TEXT (3H50 ,3,2)
CALL TEXT (1HA,1,2)
CALL PLOT (-0,3,2.,3)
CALL TEXT (1HS,1,2)
LA=8HZAVARITS
LB=8HKY NUMBE
LC=8HRS
```

```

      CALL PLUT (-15.,15.,3)
      CALL TEXT (LA,8,3)
      CALL TEXT (LB,8,3)
      CALL TEXT (LC,8,3)
      CALL PLOT (0,0,0,0,3)
      CALL PLOT (0,0,-100,0,4)
      CALL PLOT (-4,0,-100,0,3)
      CALL TEXT (5H100,5,2)
      CALL TEXT (1HB,1,2)
      II=0
      GO TO 10
80  HA=A
      V=(-B)
      IF (CBAR.GT,0,) 81,82
81  HC=CBAR
      GO TO 83
82  HC=(-C)
83  IF (CPR) 831,831,84
831 HA=HA-0,1*APR
      GO TO 85
84  RA=HA-0,1*GPR
85  RB=V-0,1*MPR
      RB2=V-CA(9)
      RC=HC-CA(10)
      ENCODE (3,902,LL) II
      WRITE (2) HA,V,RA,RB,HC,V,RC,RB2,LL,II
      CALL PLOT((HA-0,3),(V-0,4),3)
      CALL TEXT (CROSS,1,-1)
      CALL PLOT((HA-0,8),V,3)
      IF (ISUPP.GT,0) CALL TEXT(LL,3,1)
      CALL PLOT (HA,V,3)
      CALL PLOT (RA,RB,4)
      CALL PLOT((HC-0,3),(V-0,4),3)
      CALL TEXT (CROSS,1,-1)
      CALL PLOT((HC-0,8),V,3)
      IF (ISUPP.GT,0) CALL TEXT (LL,3,1)
      CALL PLOT (HC,V,3)
      CALL PLOT(RC,RB2,4)
      GO TO 10
900 FORMAT (1H1,*ZAVARITSKY NUMBERS CALCULATED FOR SAMPLE*,
      *I3,2X,1H,,2X,A8,A3/1H0,*SILICATE ANALYSIS*,64X,*CATION PERCENT*)
901 FORMAT (A8,A3,14F4,2)
902 FORMAT(I3)
903 FORMAT (1H0/(5X,A6,10X,F10,2,55X,A6,10X,F10,2))
905 FORMAT (1H0,*ZAVARITSKY NUMBERS*)
906 FORMAT (1H0,50X,A4,F16,2)
99  REWIND 2
999 READ (2) X,Y,X1,Y1,A,B,A1,B1,LAB,II
      IF (EOF,2) 998,997
998 CALL EXIT
997 IF (Y+50.) 999,999,150
150 IF (X-25.) 151,999,999
151 IF (A+25.) 999,999,152
152 IF (X1.GT,25,) 153,154
153 Y1=(25.-X)/(X1-X) * (Y1-Y) * Y
      X1=25,
154 IF (Y1.LT,(-50.)) 155,156
155 X1=(-50.-Y)/(Y1-Y) * (X1-X) * X
      A1=(-50.-B)/(B1-B) * (A1-A) * A

```

```
Y1=B1=(-50.)
156 IF (A1.LT.(-25.)) 157,158
157 B1= (-25.-A)/(A1-A) * (B1-B) + B

A1=(-25.)
158 IF (I1.E0.1) 159,160
159 CALL PLOT(-50.,0.,3)
CALL PLOT (-25.,-100.,1)
CALL PLOT (5.,5.,2)
CALL PLOT (-25.,1.,3)
CALL TEXT(4HC 25,4,2)
CALL PLOT(-25.,0.,3)
CALL PLOT(25.,0.,4)
CALL PLOT (23.,1.,3)
CALL TEXT(4H25 A,4,2)
CALL PLOT(-0.15,1.,3)
CALL TEXT(1HS,1,2)
CALL PLOT(0.,0.,3)
CALL PLOT(0.,-50.,4)
CALL PLOT(-1.5,-50.,3)
CALL TEXT(5H50 B,4,2)
160 CALL PLOT((X-0.15),(Y-0.2),3)
CALL TEXT(CROSS,1,-1)
CALL PLOT((X+0.4),Y,3)
ENCODE (3,902,LL) 11
CALL TEXT(LL,3,1)
CALL PLOT(X,Y,3)
CALL PLOT(X1,Y1,4)
CALL PLOT((A-0.15),(B-0.2),3)
CALL TEXT(CROSS,1,-1)
CALL PLOT((A+0.4),B,3)
CALL TEXT(LL,3,1)
CALL PLOT(A,B,3)
CALL PLOT(A1,B1,4)
GO TO 999
END
```

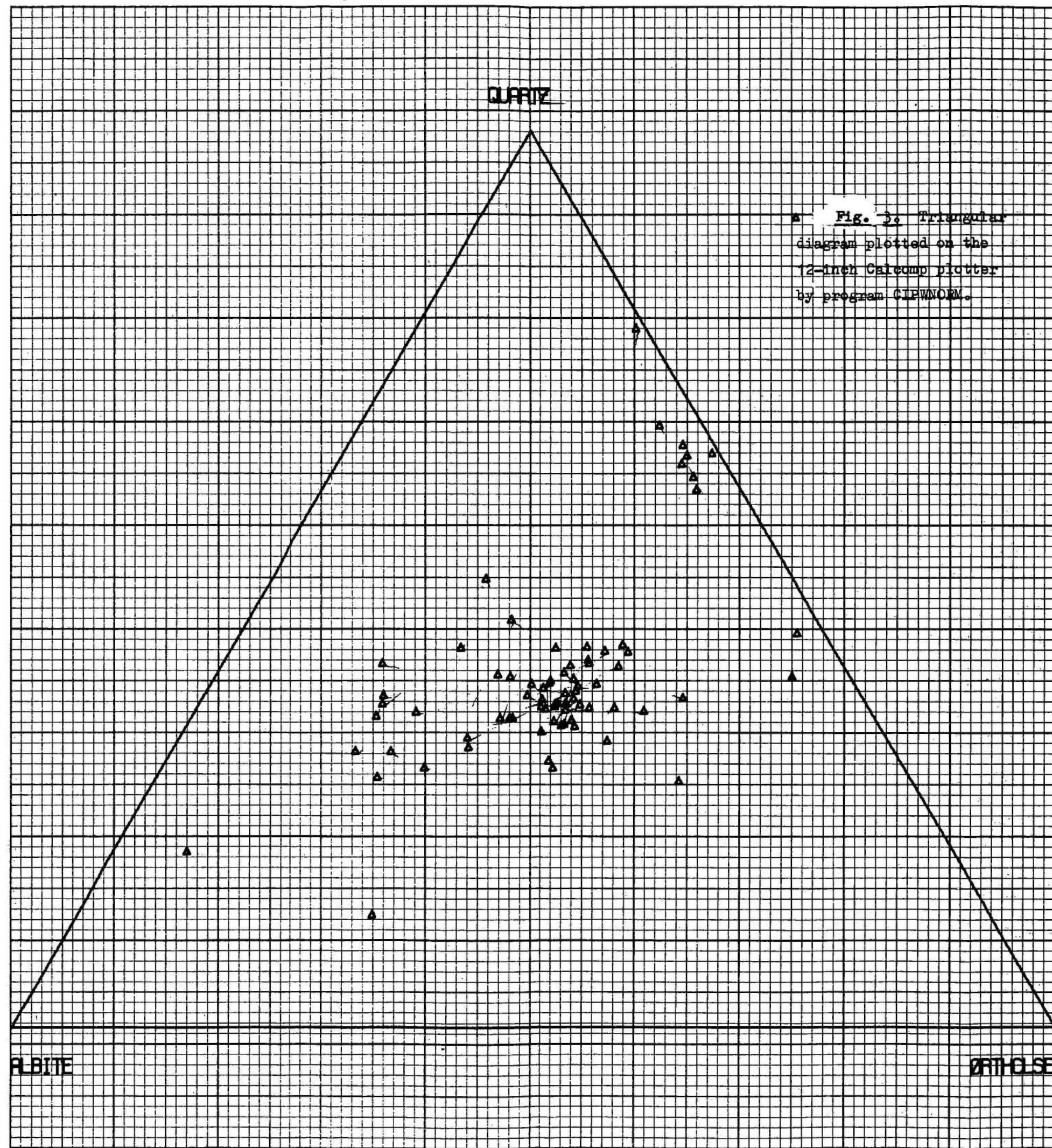
Fig. 1

CIPW NORM OF SAMPLE NO. 69201028

SILICATE ANALYSIS		FEMIC CONSTITUENTS			SALIC CONSTITUENTS	
OXIDE	PERCENT	MINERAL	PERCENT	COMPONENT	PERCENT	MINERAL PERCENT
SiO2	48.16	ACMITE	0.00			
TiO2	1.38					QUARTZ 0.00
Al2O3	13.76	WOLLASTONITE	0.00			CORUNDUM 0.00
Fe2O3	2.67					ZIRCON 0.00
FeO	11.70	DIOPSIDE	24.08	WO	12.14	
MnO	0.23			EN	5.87	ORTHOCLASE 1.56
MgO	6.77			FS	6.07	ALBITE 17.06
CaO	11.58					ANORTHITE 28.23
Na2O	1.99	HYPERSTHENE	20.34	EN	10.00	
K2O	0.26			FS	10.34	NEPHELINE 0.00
P2O5	0.14					LEUCITE 0.00
H2O(+)	0.46	OLIVINE	1.82	FO	0.85	KALIOPHILITE 0.00
H2O(-)	0.00			FA	0.97	
CO2	0.00					HALITE 0.00
		MAGNETITE	3.92			
		CHROMITE	0.00			
TOTAL	98.64	HEMATITE	0.00			
		ILMENITE	2.66			
		RUTILE	0.00			
F	0.0000	TITANITE	0.00			
S	0.0000	PEROVSKITE	0.00			
CL	0.0000	APATITE	0.34			
V	0.0000	FLOURITE	0.00			
CR	0.0000	CALCITE	0.00			
CO	0.0000	PYRITE	0.00			
NI	0.0000	SPHALERITE	0.00			
CU	0.0000					
ZN	0.0000					
RB	0.0000					
SR	0.0000					
ZR	0.0000					
BA	0.0000					

TRIANGULAR DATA DIAGRAM

Q - PLAG - OR		K20 - NA20 - CAO		WO - FS - EN		PLAGIOCLASE - AN		62,33	
Q	0,00	K20	1,88	WO	27,32	COLOUR INDEX IS		0,53	
PLAG	96,68	NA20	14,39	FS	36,94				
OR	3,32	CAO	83,73	EN	35,73	CALC. DENSITY		3,13	
Q - AB - OR		OR - AB - AN		F - M - A		OL - NE - Q		SOLIDIFICATION INDEX	28,94
								THORNTON - TUTTLE	
Q	0,00	OR	3,32	F	60,99	OL	40,09	DIFFERENTIATION INDEX	18,62
AB	91,64	AB	36,42	M	29,28	NE	24,71	PERALKALITY INDEX	0,26
OR	8,36	AN	60,26	A	9,73	Q	35,20	K20/NA20	0,13
								TOTAL FE AS FEO	14,10



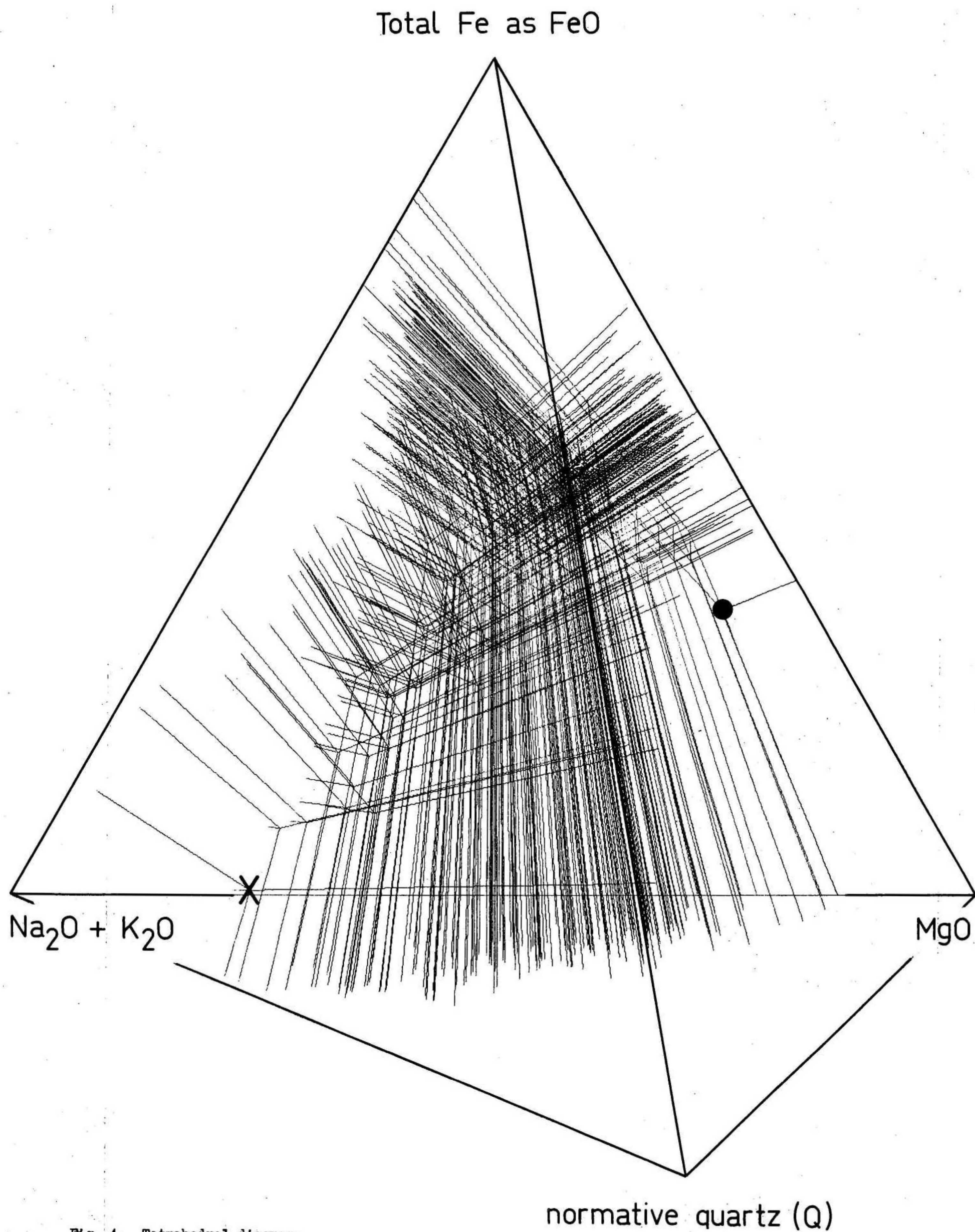


Fig. 4. Tetrahedral diagram
plotted by program CPWNORM.

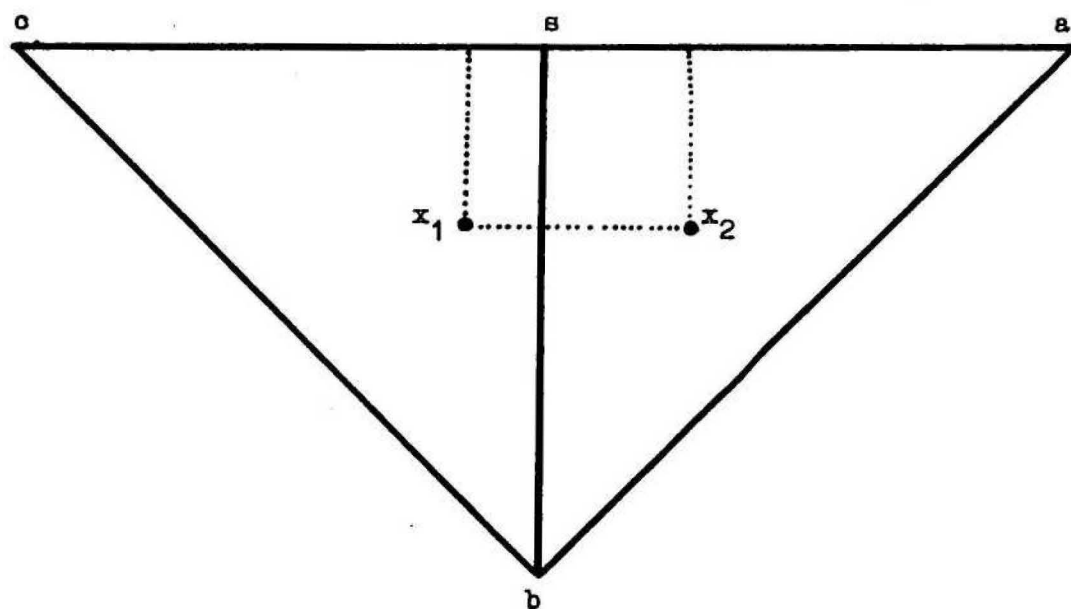
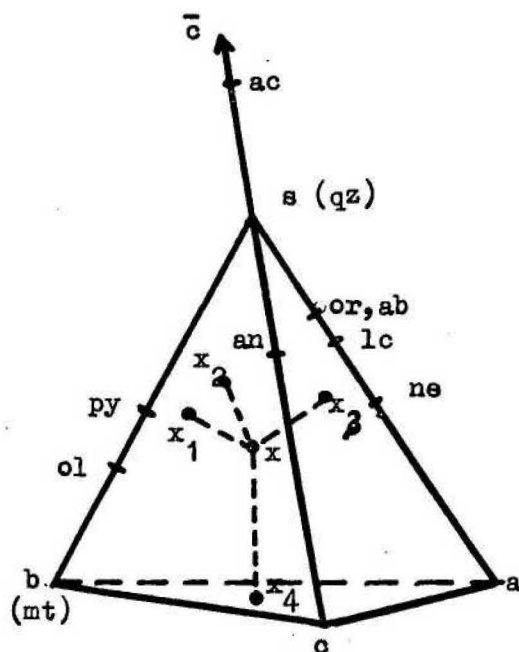


Fig. 5. Method of construction of the orthotetrahedral projection used in plotting the four principal Zavaritsky numbers, a, c, b and s . Point x (upper diagram) within the tetrahedron is projected into planes scb and sab at x_1 and x_2 respectively. The planes are represented by right triangles possessing the common edge sb , and the points are located by measuring ' a ' units along direction sa , ' c ' units along direction sc , and ' b ' units along direction sb .

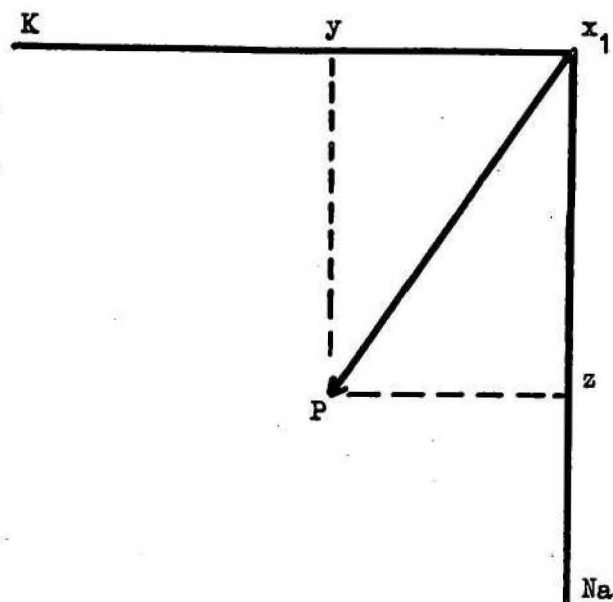


Figure 6a. The method of plotting the alkali vector in the conventional Zavaritsky diagram. Point P is located by measuring a length x_1y proportional to the K content of the rock and a length x_1z proportional to the Na content. Thus the length of x_1P is proportional to the total alkali content and its gradient expresses the K/Na ratio.

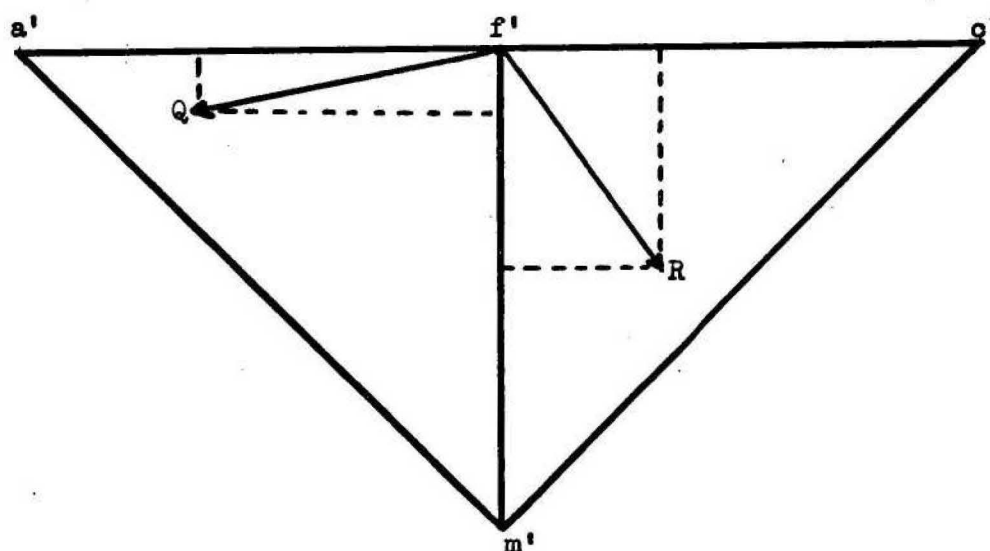


Figure 6b. The method of plotting the $f'm'a'$ or $f'm'o'$ vector in the conventional Zavaritsky diagram. From their definition, $f' + m' + c'$ or $f' + m' + a' = 100$, and thus a point in either system may be directly plotted in a triangular diagram. If, again, we use right triangles, point Q or R may be located by measuring distance m' along $f'm'$ and either distance a' along direction $f'a'$ or c' along $f'o'$. A convenient scale for these triangles is $1/10$ that of the acbs tetrahedron.

ZAVARITSKY NUMBERS

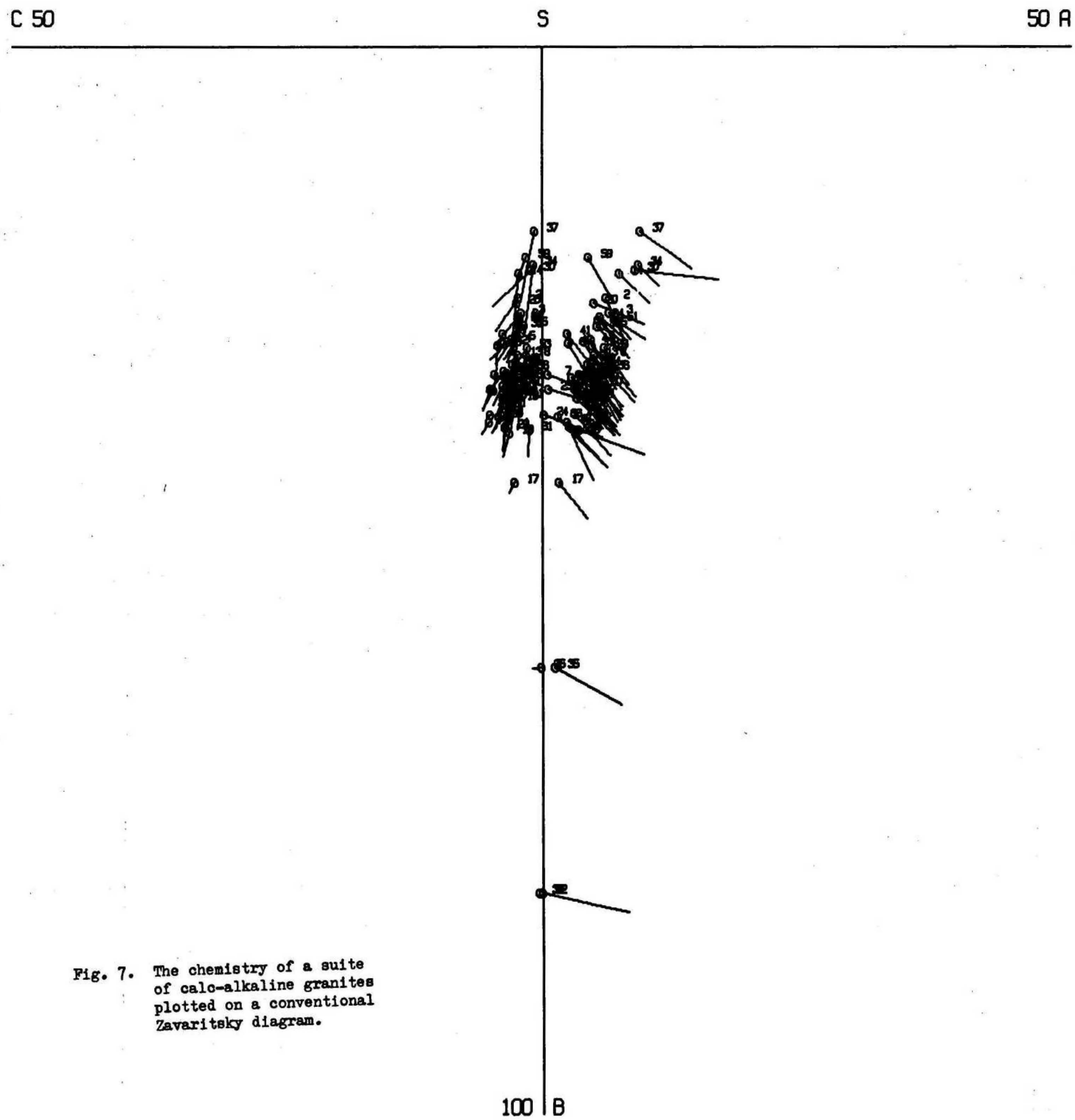


Fig. 7. The chemistry of a suite of calc-alkaline granites plotted on a conventional Zavaritsky diagram.