

1973/31

Copy 3

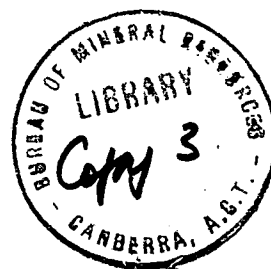
504706
+

DEPARTMENT OF
MINERALS AND ENERGY



BUREAU OF MINERAL RESOURCES, GEOLOGY AND GEOPHYSICS

Record 1973/31



PROGRAM MANYPLOT - COMPUTER CALCULATED INVERSE LAPLACE TRANSFORMS FOR PREDICTION OF CIRCUIT BEHAVIOUR

by

D.W. Kerr

The information contained in this report has been obtained by the Department of Minerals and Energy as part of the policy of the Australian Government to assist in the exploration and development of mineral resources. It may not be published in any form or used in a company prospectus or statement without the permission in writing of the Director, Bureau of Mineral Resources, Geology and Geophysics.

BMR
Record
1973/31
c.3

Record 1973/31

**PROGRAM MANYPLOT - COMPUTER CALCULATED
INVERSE LAPLACE TRANSFORMS FOR PREDICTION
OF CIRCUIT BEHAVIOUR**

by

D.W. Kerr

CONTENTS

	<u>Page</u>
SUMMARY	
1. INTRODUCTION	1
2. THEORY	1
3. PROGRAM MANYPLOT	6
4. FUNCTION LAPLACE	7
5. PROGRAMS MERRYGEN AND MERRY	8
6. OPERATING INSTRUCTIONS	8
7. REFERENCES AND ACKNOWLEDGEMENTS	9
APPENDIX 1 : LISTINGS FROM MANYPLOT, LAPLACE, AND MERRYGEN	
APPENDIX 2 : FLOW CHART ON MANYPLOT AND LAPLACE	
APPENDIX 3 : FLOW CHART OF MERRY	
APPENDIX 4 : SAMPLE PLOTS AND OUTPUT OF MANYPLOT	
APPENDIX 5 : SAMPLE OUTPUT FROM MERRY	

SUMMARY

Programs Manyplot and Merry were written specifically to aid the Design & Development Group in complex circuit analysis of passive and active filter circuits. The use of numerically calculated inverse Laplace transforms allows previously impossible analysis to be carried out rapidly. These programs should be of use in determining accurate response and system curves for magnetotelluric and other geophysical electronic measuring equipment.

1. INTRODUCTION

1.0 In analogue electronics, frequent use is made of the 'pole-zero' method of describing a circuit transfer function by its complex singularities. Specification of these singularities and a gain factor is sufficient to describe the behaviour of a circuit's output in response to any input. The program described here will, given these singularities and a gain factor, calculate amplitude and phase information for sinusoidal input and will calculate system response to a delta function, unit step, or unit ramp function using numerically calculated inverse Laplace transforms.

1.1 The program, called MANYPLOT, produces line printer and drum plotter output of phase and amplitude for sinusoidal inputs. For the other three types of input only line printer outputs are produced, as very large output values may be generated with lightly damped systems. Selection of plotter scale is automatically optimized, and suitable logarithmic intervals are automatically selected for frequency intervals.

1.2 MANYPLOT is usually used as a relocatable binary deck generated from a Fortran source deck. An interactive program (MERRY) is available to pass data to MANYPLOT and control its break-in or execution. MERRY is a binary program generated by the assembly language program MERRYGEN and may be entered from a remote terminal to the CSIRO's CDC 3600 computer in Canberra.

1.3 MANYPLOT should have immediate application as an electronic design aid and perhaps in the field of mechanical engineering.

2. THEORY

2.0 Every linear passive electronic circuit can be reduced to an equivalent circuit of resistors, capacitors, and inductors. (The arguments to be used will also apply to circuits containing active elements). This equivalent circuit may be further reduced by considering capacitors and inductors as reactances, having a certain impedance and associated phase angle. Thus every circuit may be reduced to an equivalent arrangement of resistors and reactances. It is then fairly simple to write down, for such a circuit, the output voltage as a function of any impressed input voltage and of the resistances and reactances in the circuit.

2.1 We may write the generalized reactances as functions of a complex differential operator which we will call 's'. Then the generalized inductive reactance may be written as sL and the generalized capacitive reactance as $1/sC$. Thus the original equivalent circuit mentioned may be expressed

as a function of constants and s . This representation, being equivalent to the original circuit, will of necessity contain all useful information on the system; we can, then, put all knowledge of the circuit's behaviour into the ratio of two polynomials in s . This ratio of polynomials is known as the transfer function for the circuit and may be conventionally written as $H(s)$.

$$\text{i.e. } H(s) = \frac{V_{\text{out}}(s)}{V_{\text{in}}(s)} = \frac{a_n s^n + a_{n-1} s^{n-1} + \dots + a_0}{b_m s^m + b_{m-1} s^{m-1} + \dots + b_0}$$

This ratio of polynomials may be factored into a quotient of products of single-order terms as follows:

$$H(s) = K \cdot \frac{(s-z_0)(s-z_1)(s-z_2)\dots(s-z_n)}{(s-p_0)(s-p_1)(s-p_2)\dots(s-p_m)}$$

where for $s = z_0, z_1, z_2 \dots z_n$, $H(s) = 0$;

these $z_0, z_1, z_2 \dots z_n$ are the zeros of the transfer function $H(s)$

and for $s \rightarrow p_0, p_1, p_2 \dots p_n$, $H(s) \rightarrow \infty$;

these $p_0, p_1, p_2 \dots p_n$ are then the poles of the transfer function.

2.2 Thus our knowledge of the original circuit reduces to a knowledge of the constant 'K' plus the poles and zeros for the circuit. In theory, it is a comparatively simple matter to find K and the poles and zeros of a circuit. It remains for the circuit designer to be able to predict the circuit behaviour from knowledge of K and the poles and zeros; or, knowing that a certain number of poles and zeros gives him the response function he desires, to find the values of the poles and zeros and then work back and synthesize a circuit from them.

2.3 One of the simplest forcing functions used is the sine wave; for this we write $s = j\omega$ ($j = \sqrt{-1}$ and ω = angular frequency in radians per second) and consider the complex function:

$$H(j\omega) = K \cdot \frac{(j\omega - z_0)(j\omega - z_1) \dots (j\omega - z_n)}{(j\omega - p_0)(j\omega - p_1) \dots (j\omega - p_m)} = \frac{V_{out}(j\omega)}{V_{in}(j\omega)}$$

This completely determines the output in terms of the input multiplied by a complex function containing phase and amplitude information. This information may be extracted as phase and amplitude information:

$$\text{for amplitude, } \frac{V_{out}}{V_{in}} = K \cdot \sqrt{\text{Re}^2 + \text{Im}^2} \quad \text{where Re and Im are the respective real and imaginary parts of } H(j\omega)/K.$$

Arctan (Im/Re) gives the desired phase relation from output to input. Thus, all that is necessary for the extraction of the phase and amplitude from the poles and zeros is the finding of the real and imaginary parts of $H(s)$ with $s = j\omega$. This is a tedious job if there are many poles and zeros and if many frequencies ($\omega = 2\pi f$) are to be considered; the task is therefore ideally suited to computer solution. Just how this is done may be seen from the flow chart provided (cf. Chapter 3 and Appendix 2).

2.4 A knowledge of the phase and amplitude response of a circuit to sine wave excitation is unfortunately not enough for the electronics designer. He usually wants to know also how the circuit reacts to ramp-type functions, delta functions (unit impulse functions), and step functions. This is not as easy a problem as that of phase and amplitude. It becomes necessary to introduce the notion of the Laplace Transform, which is a generalization of the Fourier Transform. The Laplace Transform enables transformation from the time domain to the complex frequency domain and back again using the inverse transform. The Laplace Transform is defined as:

$$L(F(t)) = f(s) = \int_0^{\infty} e^{-st} F(t) \cdot dt$$

and the inverse transform may be written:

$$F(t) = L^{-1}(f(s)) = \frac{1}{2\pi j} \int_{\sigma_1 - j\infty}^{\sigma_1 + j\infty} f(s) e^{st} \cdot ds$$

where we assume $F(t) = 0$ if $t < 0$ and $s = \sigma + j\omega$ with $0 < \sigma_1 > \sigma$ for all σ

2.5 In electronics, one is most frequently interested in transformations from the complex frequency (s) domain to the time (t) domain. One is therefore concerned with the inverse transforms of $H(s)$ functions. For polynomials up to third or fourth order, it is reasonably easy to calculate the

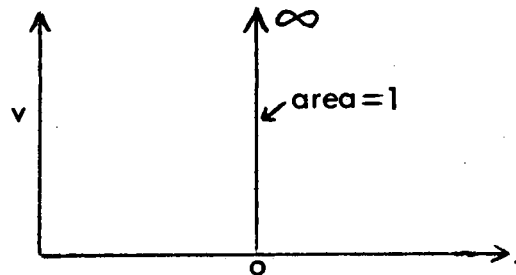
functional form of the inverse transform, but for higher-order ratios of polynomials the task becomes increasingly difficult without machine aid. The program to be described successfully carries out the inverse Laplace Transform for ratios of two polynomials and produces unit impulse, unit step, and unit ramp information from the values of poles and zeros fed into it. The program accepts any combination of up to 24 poles and 24 zeros, which may be either real or complex. There must be more poles than zeros.

2.6 Let us consider $H(S) = \frac{E_{out}(s)}{E_{in}(s)}$ where $E_{out}(s)$ is the Laplace

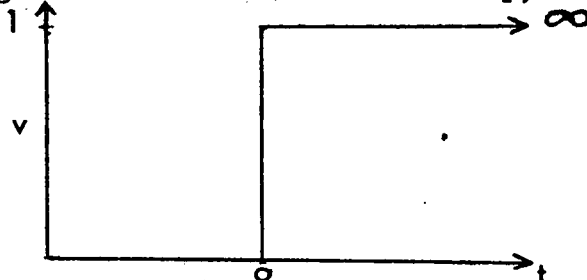
Transform of the output $e_{out}(t)$ and $E_{in}(s)$ is the Laplace Transform of the input $e_{in}(t)$. But if $e_{in}(t)$ is a delta function, $E_{in}(s) = 1$ and thus $H(s) = E_{out}(s)$. Therefore $h(t) = L^{-1} H(S)$ or $e_{out}(t) = L^{-1} H(S)$.

i.e., the impulsive response of the transfer function $H(S)$ is simply the inverse Laplace Transform of the transfer function.

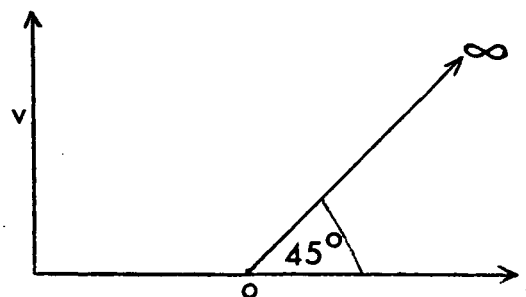
The unit impulse function looks like this:



If we integrate this we obtain the unit step, i.e.:



Integrating the unit step gives the unit ramp function:



2.7 As it stands, the definition of the inverse transform is awkward to use in machine oriented calculations. However, by manipulating the definition, it is possible to derive an expression for polynomial ratios, known as the Heaviside expansion formula. This is:

$$L^{-1} \left[\frac{P(s)}{Q(s)} \right] = \sum_{k=1}^n \frac{P(s_k) e^{s_k t}}{Q'(s_k)}$$

where $P(s)$ and $Q(s)$ are the two polynomials; the roots (and hence the poles) of $Q(s)$ are $s_1, s_2, s_3, \dots, s_n$. $P(s)$ is of degree less than n and the roots of $Q(s)$ are to be all distinct. $Q'(s_k)$ is the derivative of $Q(s)$ with respect to s at the point $s = s_k$.

2.8 It can be seen that for large n , any sort of hand calculations using the above formula would be extremely long and tedious and would rely on a high calculation accuracy from step to step. The problem thus lends itself well to computer calculation. The method of integration of the transfer function for unit step and unit ramp is simple, as integration is equivalent to multiplication by a $1/s$ term or equivalently putting an extra pole into the system at $s = \text{zero}$. This increases the order of polynomial $Q(s)$ by 1.

2.9 There are only two restrictions in the Heaviside expansion formula. Multiple roots of $Q(s)$ are forbidden and the order of $P(s)$ must be less than that of $Q(s)$. The multiple roots problem can be overcome quite simply in computer applications by making identical roots slightly different to machine accuracy (10 figures) but not sufficiently different to affect the desired accuracy of the final result (seldom any more than four to six significant figures). Unfortunately, at this stage, the one remaining restriction - that the order of $P(s)$ be less than that of $Q(s)$ - has not been overcome for the transient analysis part of the program but ramp and step response is slightly less restricted than unit impulse, owing to the addition of the poles at zero.

2.10 Numeric differentiation of polynomial $Q(s)$ cannot easily be carried out with accuracy, so the differentiation is reduced to an algebraic manipulation in the following manner:

$$\text{Consider } Q(s) = (s-a_1)(s-a_2)(s-a_3) \dots (s-a_n)$$

$$\text{Differentiating gives } Q'(s) = -a_1 (s-a_2) \dots (s-a_n) - a_2 (s-a_1)(s-a_3) \dots$$

$$\dots (s-a_n) \text{ etc.}$$

$$\text{i.e. } Q'(s) = \sum_{k=1}^n \left\{ -a_k \prod_{\substack{m=1 \\ m \neq k}}^n (s-a_m) \right\}$$

This then is an exact algebraic expression for the differentiation of $Q(s)$, and has been used in the program.

2.11 As MANYPLOT is completely general, except for the restriction on the order of the zero polynomial (this is only a minor limitation), it would appear that the program could be used for calculating inverse Laplace Transforms of virtually any mathematical function - all functions being reducible to the ratio of two polynomials.

3. PROGRAM MANYPLOT

3.0 MANYPLOT was written in Fortran IV for the CDC 3600 computer. A flow chart may be seen in Appendix 2, and program listings in Appendix 1. Memory requirements for MANYPLOT and LAPLACE are 12 000 words (decimal), and execution times are roughly 30 seconds for a steady-state analysis and between $\frac{1}{2}$ and 2 minutes for a transient analysis, depending upon the number of poles and zeros. MANYPLOT reads its data from a drum document called MANYDRUM, which is lost after MANYPLOT is executed. MANYDRUM is created and saved by MERRY (Chapter 5).

MANYPLOT:

- (a) Reads all necessary data
- (b) Formats all output for printing and/or plotting.
- (c) Performs steady-state analysis as per (2.3) or
- (d) Calls function LAPLACE (Chapter 4) which calculates the inverse Laplace Transforms and integrated transforms as per paragraphs 2.7 and 2.10.

3.1 As Manyplot chooses its own scales etc., all that is required in the form of data is as follows:

Transient Analysis

- (a) Whether transient or steady state
- (b) Poles and zeros
- (c) Gain factor
- (d) Transient time in seconds
- (e) Title for printouts

Steady-state Analysis

- Whether the transient or steady state
- Poles and zeros
- Gain factor
- Start frequency and stop frequency
- Title for plots and printouts

3.2 MANYPLOT can handle any number of poles and zeros. The only restriction lies in the dimensioning of arrays (complex), "Pole" and "Zero". These dimensions are nominally set to 24 each. Present input formatting allows up to 9 poles/zeros.

3.3 Scales. Horizontal scales (i.e. frequency) on the plots are chosen to be 10 inch logarithmic intervals between the stipulated frequency limits. On the phase plot, the most suitable vertical scale in the following range is chosen (the scale is 10 inches high).

- (a) $\pm$ 2000 degrees
- (b) $\pm$ 500 degrees
- (c) $\pm$ 250 degrees
- (d) $\pm$ 100 degrees
- (e) $\pm$ 50 degrees
- (f) $\pm$ 25 degrees
- (g) $\pm$ 5.0 degrees

The amplitude plot has a logarithmic vertical scale labelled from -25 to +25 decibels (10 inches high). This scale (and labelling) extends vertically upwards as far as necessary and moves the phase plot to make sufficient room if the amplitude plot goes above the +25 dB mark. If the amplitude curve attempts to drop below the -25 dB point, backing-off steps of 50 dB are added in as necessary to bring the curve back onto the area of the plot. All amplitude plots are normalized to commence at the +25 dB point, and the normalizing factor is printed on the plot. The title, as defined by the user, is also printed.

4. FUNCTION LAPLACE

4.0 Function LAPLACE is a real in line function called by MANYPLOT for calculating the inverse transform of $H(s)$ as per paragraphs 2.7 and 2.10. The time and the number of integrations required are specified in the call, and gain factor, pole, and zeros are passed in common storage. Appendixes 1 and 2 contain listings and flow charts of LAPLACE.

5. PROGRAM MERRYGEN AND MERRY

5.0 MERRYGEN (Assembly language - Compass) is the generator for the binary program MERRY. MERRY operates in 2000 words of core in CSIRO's DAD console system in the CDC 3600 computer. The program operating in the console system allows interactive creation of a drum document labelled 'MANYDRUM' and will then break-in or execute MANYPLOT as required or delete the drum document with no break-in or execution. Many execution requests may be 'stacked' in the relevant execution list for multiple-job runs. The user can specify a unique title for each executed job for later identification.

5.1 MERRY asks a question, and the user responds by typing a reply. Typically, in 1 to 2 minutes a user can type in all necessary data and break-in or execute MANYPLOT.

5.2 The structure of MERRY can be seen from the flow chart (Appendix 3) and listings (Appendix 1).

5.3 User macro IOC performs I/O transfers between user and MANYDRUM. Subroutines MANY and XFER perform the actual read and writes. Subroutine SWAP initializes index registers needed in the augmented XMIT instruction. Subroutine CRACK decodes numbers typed into the teletype keyboard, and justifies them in binary words.

5.4 MERRY uses less than 600 words of core storage and uses roughly 1 to 2 secs of Central Processor (CPU) time per session.

6. OPERATING INSTRUCTIONS

6.0 The operating instructions pertain to MERRY. Ensure that both MERRY and MANYPLOT are in the Document Region under the user's charge code before starting.

6.1 Reference to Appendix 5 will show what form the interaction with MERRY will take. Lines are terminated by CR/LF. CTRL/BELL deletes the last character. CR and retype to delete a line.

6.2 Appendix 5 shows MERRY to be virtually self-explanatory, but paragraphs 6.3 to 6.5 contain a few pertinent notes on its use.

6.3 In response to 'How many poles' or 'How many zeros', a number from 0 to 9 should be typed in, in column one. (MERRY will accept any number from 0 to 99; MANYPLOT's format will accept only 11 at present).

6.4 At present, the reply to 'MANYPOL' or 'MANYPLOT' will always be 'MANYPLOT'. If a document labelled 'MANYPOL' exists in the document region, MERRY can break-in or execute it.

6.5 In response to 'Type BK or EX else just interrupt', there are three replies:

BK - (1) Break-in MANYPLOT with 1 minute time limit
(cost 2*CPU time) Computer response to this can be either of:

- (a) Break-in request accepted.
- (b) Break-in request rejected. Wait and interrupt i.e. LF.

EX - (2) Put MANYPLOT in execution list EL003 for execution
(cost 1*CPU time)
Computer response to this can be either of:

- (a) Execution request accepted.
- (b) System busy. Wait and interrupt i.e. LF.

LF - (3) Go back to the start and start again from scratch.

6.6 After the computer responds to a BK or EX request, LF terminates the session and gives the cost in seconds (Break-in charges + console program charge).

7. REFERENCES AND ACKNOWLEDGEMENTS

CONTROL DATA CORPORATION, 1966 - CDC 3600 Fortran reference manual No. 60132900.

CONTROL DATA CORPORATION, 1968 - CDC 3600 computer system reference manual No. 60021300.

CSIRO, 1973 - DAD System reference manual.

DRABBLE, J.S. & PUMMERROY, N.R., 1970 - Graph plotting. CSIRO, Div. Computing Res., Tech. Note 35. (unpubl.).

SPIEGEL, M.R., 1965 - THEORY AND PROBLEMS OF LAPLACE TRANSFORMS. N.Y., McGraw Hill.

WALSH, J.B. & MILLER, K.S. 1960 - INTRODUCTORY ELECTRIC CIRCUITS. N.Y. McGraw Hill.

SEERS, K.J. of BMR Canberra provided many of the test cases for proving and testing MANYPLOT.

APPENDIX 1

LISTINGS FROM MANYPLOT, LAPLACE, AND MERRYGEN

```
*DOC ,CCDMR*DA ,MANYPLOT,,, CP00.,1051.,25/01/73
*MESSAGE,EXECUTED FROM DR. NO CARD INPUT OR OUTPUT. PLOT FROM PL.
*EQUIP,61=SV
*EQUIP,61=LP
*EQUIP,60=SV
*DRLOCATE,20.,MANYDRUM
*DFCOPDR,20.,MANYDRUM
*EQUIP,1=PL
*KTN,X,L
```

PROGRAM MANYPLOT

```
C PROGRAM MAY CONTAIN ANY COMBINATION OF UP TO 24 ZEROES AND/OR
C 24 POLES. NUMBER OF ZEROES TO BE GREATER THAN NUMBER OF POLES
C FOR TRANSIENT ANALYSIS.
C POLES OR ZEROES NEED NOT BE COMPLEX CONJUGATES.
C COMPLEX POLE(24),ZERO (24),SUM1,SUM2,S
C REAL LAPLACE, Z00(3)
C DIMENSION HEAD(3),PHASE(250),FREQ2(250),TITLE(5),WRT2(2),WRT4(2)
C 1,WRT6(2),CHAR(2)
C COMMON POLE,ZERO,NZ,NP,FUDGE
C DATA(TYPE=8HTRANSIEN),(HEAD=19HMANYPLOT ANALYSIS. )
C 1,(HERTZ=8HFREQ-HZ.),(DB1=3HDB.),(PHASE4=6HPHASE.)
C 1,(PHASE5=8HDEGREES.),(TOP=8HTITLE - ),(WRT3=8H DB. OR )
C 1,(WRT1=37H25 DB ON THE Y SCALE NORMALISED FROM )
C 1,(WRT5=22H VOLTS. GAIN FACTOR = )
C FACTOR=1.0
C WRITE(61,10)
C 10 FORMAT(24X*MANYPLOT ANALYSIS*/7X*ZEROES*)
C DO 20 K=1,24
C 20 POLE(K)=ZERO(K)=CMPLX(0.,0.)
C READ(20,85)TITLE
C 85 FORMAT(5A8)
C D=DATE(0)
C FUDGE IS THE GAIN FACTOR.
C READ(20,30)FUDGE
C 30 FORMAT(F80.5)
C NZ IS THE NUMBER OF ZEROES.
C READ(20,60)NZ
C DO 40 J=1,NZ
C READ IN REAL/IMAG PARTS OF ZEROES ALTERNATELY.
C READ(20,80)FIRST,FLAST
C 40 ZERO(J)=CMPLX(FIRST,FLAST)
C 50 FORMAT(A8,72X)
C 60 FORMAT(I1)
C READ(20,60)NP
C NP IS THE NUMBER OF POLES.
C DO 70 J=1,NP
C READ IN REAL/IMAG PARTS OF POLES ALTERNATELY.
C READ(20,80)FIRST,FLAST
C 70 POLE(J)=CMPLX(FIRST,FLAST)
C 80 FORMAT(F80.8/F80.8)
C READ(20,50)ANAL
C READ IN TRANSIENT ANALYSIS OR STEADY STATE ANALYSIS.
C IFLAG1=1
C MAKE EQUAL POLES UNEQUAL BY A SMALL AMOUNT.
C DO 90 I=1,NP
C DO 90 J=1,NP
C IFLAG=0
C IF(I.EQ.J)GO TO 90
C IF(POLE(I).EQ.POLE(J))IFLAG=1
C IF(IFLAG.EQ.1)POLE(I)=POLE(I)+(POLE(I)/2E5)*IFLAG1
C IF(IFLAG.EQ.1)POLE(J)=POLE(J)+(POLE(J)/2E5)*(IFLAG1+1)
C IFLAG1=IFLAG1+IFLAG
C 90 CONTINUE
C WRITE(61,100)(ZERO(I),I=1,NZ)
```

100 FORMAT(5X,C(E11.3,E11.3)) -13-

WRITE(61,110)

110 FORMAT(7X*POLES*)

WRITE(61,100)(POLE(I),I=1,NP)

C STATEMENT 300 IS TRANSIENT ANALYSIS START.

IF(TYPE.EQ.ANAL) GO TO 300

C STATEMENT 120 IS STEADY STATE START.

WRITE(61,120)TITLE

120 FORMAT(//6X* STEADY STATE ANALYSIS*///7X5A8//)

WRITE(61,130)

130 FORMAT(//6X*FREQ.HZ*10X*AMPLITUDE*10X*PHASE(DEG.)*8X*DECIBELS*//)

C X= INITIAL FREQUENCY, Z= FINAL FREQUENCY (HZ).

READ(20,140)X,Z

140 FORMAT(F80.5)

Q=Z/X

X1=X

HSCALE=0.1*ALOG10(Q)

CALL PLOT(HSCALE,5.,2)

INKLEX=0

PH2=-10E25

PH3=10E25

CALL PLOT(0.0,50.0,4)

CALL PLOT(0.0,25.0,4)

AXIS=10.0*HSCALE

CALL PLOT(AXIS,25.0,4)

AXIS=AXIS/2.0

CALL PLOT(AXIS,0.0,3)

CALL TEXT(HEAD,19,3)

CALL TEXT(D,8,3)

CALL PLOT(0.0,0.0,3)

CALL TEXT(TOP,8,2)

CALL TEXT(TITLE,40,2)

CALL PLOT(0.0,0.0,3)

VMAX=-10E+25

CALL PLOT(0.0,-50.0,1)

150 W=6.28318*X

PH=0.

SUM1=SUM2=(1.,0.)

X=(1.+ALOG10(Q)/100.)*X

IF(X.GT.Z) GO TO 220

S=CMPLX(0.,W)

IF(NZ.EQ.0) GO TO 170

DO 160 I=1,NZ

RL=S-ZERO(I)

IF(RL.EQ.0.)RL=RL+10E-20

C MAKE ZERO DENOMINATORS NON-ZERO BY A SMALL AMOUNT.

PH=PH+ATAN(AIMAG(S-ZERO(I))/RL)

160 SUM1=SUM1*(S-ZERO(I))

170 DO 180 I=1,NP

IF(NP.EQ.0)GO TO 181

RL=S-POLE(I)

IF(RL.EQ.0.)RL=RL+10E-20

C PH IS PHASE ANGLE.

PH=PH-ATAN(AIMAG(S-POLE(I))/RL)

180 SUM2=SUM2*(S-POLE(I))

181 SUM1=SUM1/SUM2

HW=CABS(SUM1)*FUDGE

C HW IS THE AMPLITUDE

190 CONTINUE

PH=PH*180./3.14159

FREQ=X/(1.+ALOG10(Q)/100.)

DECIBELS=20*ALOG10(HW)

IF(INKLEX.EQ.0)FRUN=DECIBELS

IF(INKLEX.EQ.0)FROD=HW

C AMPLITUDE NORMALISED FOR PLOTTING.

DEWDEC=DECIBELS-FRUN

INKLEX=INKLEX+1

FREQ1=ALOG10(FREQ/X1)

FREQ2(INKLEX)=FREQ1

PHASE(INKLEX)=PH

IF(PH.GT.PH2)PH2=PH

IF(PH.LT.PH3)PH3=PH

C BACKING OFF OF AMPLITUDE PLOT TO STOP PEN GOING OFF SCALE.

200 IF(DEWDEC.LT.-50.)DEWDEC=DEWDEC+50.

IF(DEWDEC.LT.-50.)GO TO 200

CALL PLOT(FREQ1,DEWDEC,4)

WRITE(61,210)FREQ,HW,PH,DECIBELS

210 FORMAT(4X,E12.4,5X,E12.4,7X,E12.4,7X,E12.4)

IF(DEWDEC/5..GT.VMAX)VMAX=DEWDEC/5.

GO TO 150

220 VOT=-45.0

ENCODE(12,225,WRT2)FRUN

ENCODE(12,225,WRT4)FROD

ENCODE(12,225,WRT6)FUDGE

225 FORMAT(E12.4)

IF(PH2**2.GT.PH3**2)PH3=SQRT(PH2**2)

PH3=SQRT(PH3**2)

YSCALE=200.0

C CHOOSE A SUITABLE VERTICAL SCALE FOR PHASE PLOT.

IF(PH3.LE.500.)YSCALE=100.

IF(PH3.LE.250.)YSCALE=50.0

IF(PH3.LE.100.)YSCALE=20.

IF(PH3.LE.50.)YSCALE=10.

IF(PH3.LE.25.)YSCALE=5.

IF(PH3.LE.5.)YSCALE=1.0

CALL PLOT(0.0,0.0,3)

C EXTEND VERTICAL AXIS OF AMPLITUDE PLOT IF NECESSARY.

CALL PLOT(0.0,5.*VMAX,4)

AXIS=-0.4*HSCALE

CALL PLOT(AXIS,-50.0,3)

C EXTEND AMPLITUDE SCALE VERTICALLY AS FAR AS NECESSARY.

IVMAX=55+5*INTF(VMAX)

DO 240 IMP=1,IVMAX,5

IRK=IMP-26

ENCODE(3,230,IHAR)IRK

230 FORMAT(I3)

CALL TEXT(IHAR,3,2)

CALL PLOT(AXIS,VOT,3)

240 VOT=VOT+5.0

CALL PLOT(AXIS,-27.5,3)

CALL TEXT(DB1,3,2)

DO 260 LOO=1,10

C CHOOSE A SUITABLE HORIZONTAL LOGARITHMIC SCALE FOR BOTH PLOTS.

HOS=X1*EXPF(2.30259*FLOATF(LOO)*HSCALE)

ALOO=HSCALE*(FLOATF(LOO)-0.1)

CALL PLOT(ALOO,-26.0,3)

ENCODE(9,250,CHAR)HOS

250 FORMAT(F9.4)

CALL TEXT(CHAR,9,1)

CALL PLOT(ALOO,34.0+5.*VMAX,3)

260 CALL TEXT(CHAR,9,1)

CALL PLOT(HSCALE/10.,-26.0,3)

CALL TEXT(HERTZ,8,1)

CALL PLOT(HSCALE/10.,34.0+5.*VMAX,3)

CALL TEXT(HERTZ,8,1)

CALL PLOT(0.0,0.0,3)

CALL PLOT(0.0,-5.*INTF(VMAX)-60.0,1)

CALL PLOT(0.0,-55.0,3)

CALL TEXT(WRT1,37,2)

CALL TEXT(WRT2,12,2)

CALL TEXT(WRT3,8,2)

CALL TEXT(WRT4,12,2)

```

CALL TEXT(WRT5,22,2)
CALL TEXT(WRT6,12,2)
CALL PLOT(0.0,0.0,3)
CALL PLOT(0.0,-50.0,4)
CALL PLOT(0.0,-25.0,4)
AXIS=10.0*HSCALE
CALL PLOT(AXIS,-25.0,4)
CALL PLOT(0.0,-25.,3)
CALL PLOT(0.0,0.0,1)
CALL PLOT(HSCALE,YSCALE,2)
CALL PLOT(FREQ2(1),PHASE(1),3)
DO 270 N=1,INKLEX
270 CALL PLOT(FREQ2(N),PHASE(N),4)
AXIS=-0.4*HSCALE
CALL PLOT(AXIS,-YSCALE/2.,3)
CALL TEXT(PHASE4,6,1)
CALL PLOT(AXIS,-YSCALE*0.7,3)
CALL TEXT(PHASE5,8,1)
DO 290 I=1,11
QUP=FLOATF(I-6)*YSCALE
IQUP=INTF(QUP)
CALL PLOT(-0.5*HSCALE,QUP,3)
ENCODE(4,280,IHAR)IQUP
280 FORMAT(I4)
290 CALL TEXT(IHAR,4,2)
CALL EXIT
C TRANSIENT ANALYSIS START.
300 T=0.
WRITE(61,310)TITLE
310 FORMAT(/7X* TRANSIENT ANALYSIS*//7X5A8/5X*TIME*12X*UNIT IMPULSE*
18X*UNIT STEP*11X*UNIT RAMP*)
READ(20,320)TIME
C ANALYSIS RUNS FROM TIME ZERO TO NOMINATED TIME.
320 FORMAT(F80.5)
330 DO 340 I=1,3
J=I-1
340 Z00(I)=LAPLACE(T,J)

WRITE(61,350)T,Z00
350 FORMAT(3X,E12.4,4X,3(E12.4,8X))
T=T+TIME/100.
IF(TIME.GT.T)GO TO 330
CALL EXIT
END
REAL FUNCTION LAPLACE(T,ISTEP)
COMPLEX POLE(24),ZERO(24),BOTTOM,FACTOR,DENOM,LAPLACE1
COMMON POLE,ZERO,NZ,NP,FUDGE
C FUNCTION LAPLACE CALCULATES THE REQUIRED INVERSE LAPLACE
C TRANSFORM AND INTEGRATES THIS A SPECIFIED NUMBER OF
C TIMES. ISTEP SPECIFIES THE NUMBER OF ITERATIONS.
INDEX1=INDEX2=0
IF(ISTEP.GE.1)INDEX1=1
IF(ISTEP.EQ.2)INDEX2=1
LAPLACE1=(0.,0.)
NP1=MIN0(NZ,NP)
DO 60 J=1,NP
BOTTOM=(0.,0.)
FACTOR=(1.,0.)
IF(NP1.EQ.0)GO TO 20
DO 10 L=1,NP1
10 FACTOR=FACTOR*(POLE(J)-ZERO(L))
20 DO 50 I=1,NP
DENOM=(1.,0.)
DO 40 K=1,NP
IF(K.EQ.I)GO TO 40
30 DENOM=DENOM*(POLE(J)-POLE(K))

```

40 CONTINUE

50 BOTTOM = BOTTOM+DENOM

60 LAPLACE1=LAPLACE1+(FACTOR/(BOTTOM*POLE(J)**ISTEP))*(CEXP(POLE(J)*T
1)-INDEX1-INDEX2*T*POLE(J))

LAPLACE=LAPLACE1*FUDGE

MULTIPLY THE NORMALISED RESULT BY THE GAIN FACTOR.

C

RETURN

END

SCOPE

*LOAD

*RUN,1,300

(EOF

*EOD

```

*DOC ,CCDMR*DA ,MERRYGEN,,, CP00,,1227,,25/01/73
*EQUIP,40=(,MERRY),SV
*EQUIP,60=SV.61=SV
*EQUIP,61=LP
*DISPLAY
*MAIN,40.30
*COMPASS.L,X=30,R
IDENT MERRY
IOC MACRO A
XMIT,AUG A,WORD
CALL MANY
CALL XFER
ENDM
ENTRY MAIN
COM1 BLOCK 0
COMMON WORD (11B)
TYPE BCD 1,TRANSIEN
HEAD BCD 9, MANYPOLE ANALYSIS CONTROL LOGGED IN. CALLED ON
BCD 9, TYPE YOUR GAIN TERM IN F FORMAT.
BCD 9, HOW MANY ZEROES. (<9) (I FORMAT.)
BCD 9, HOW MANY POLES. (<9) (I FORMAT.)
BCD 9, STEADY STATE OR TRANSIENT.
BCD 9, INITIAL FREQUENCY-HZ. (F FORMAT.)
BCD 9, FINAL FREQUENCY-HZ. (F FORMAT.)
BCD 9, TRANSIENT TIME-SECONDS. (F FORMAT.)
BCD 9, TYPE A NAME FOR THE RUN. (LESS THAN 40 CHARACTERS).
CC BSS 2
CC1 BCD 2,CCDMR*DAMANYPLOT
CC2 BCD 2,CCDMR*DAMANYPOLE
CC3 BCD 2,CCDMR*DAMANYDRUM
EXBK BCD 9, TYPE BK OR EX, ELSE JUST INTERRUPT.
EX BCD 1,EX
BK BCD 1,BK
NUMB BSS 1
COND OCT 0
REAL BCD 9, TYPE REAL PART. (F FORMAT.)
IMAG BCD 9, TYPE IMAGINARY PART. (F FORMAT.)
EXACC BCD 9, EXECUTION REQUEST ACCEPTED.
ACC BCD 9, BREAKIN REQUEST ACCEPTED
NACC BCD 9, BREAKIN REQUEST REJECTED. WAIT AND INTERRUPT.
BUSY BCD 9, SYSTEM BUSY, WAIT AND INTERRUPT
MPLT BCD 9, MANYPOLE OR MANYPLOT.
DEL BCD 9, DRUM DOC DELETED -INTERRUPT AND TRY AGAIN.
MAIN NOP
UBJP START1,6
START1 SLJ START2
CALL REENTER
START2 CALL SWAP1
ISK 0,6
SLJ P0DD
LABEL 25,CC3,,,DR
SAVE 25,
DATE
STA HEAD+6
START3 XMIT,AUG HEAD,WORD
CALL MANY
ENI 1,6
IOC HEAD+110B
IOC HEAD+11B
IOC HEAD+22B
OK CALL CRACK1
LDA WORD
STA NUMB
BEGIN LDA NUMB

```

```

AJP,ZR OUT
RSO NUMB
IOC REAL
IOC IMAG
SLJ BEGIN
OUT LDA COND
AJP,NZ QOD
IOC HEAD+33B
STA COND
SLJ OK
QOD IOC HEAD+44B
LDA WORD
SUB TYPE
AJP,ZR TRANSIEN
IOC HEAD+55B
IOC HEAD+66B
SLJ EXITW
TRANSIEN IOC HEAD+77B
EXITW MARKEF 25,EXITMAIN
ERASE 25,EXITMAIN
IOC MPLT
LDA WORD
SUB CC1+1
AJP,ZR *+4
XMIT CC2,CC
XMIT CC2+1,CC+1
SLJ *+3
XMIT CC1,CC
XMIT CC1+1,CC+1
IOC EXBK
LDA WORD
SUR EX
AJP,ZR EXMANY
LDA WORD
SUB BK
AJP,ZR BKMANY
REWIND 25,EXITMAIN
XMIT,AUG DEL,WORD
CALL MANY
ENI 1,6
ENI 0,6
ENA 0
STA COND
SLJ START2
EXMANY RELEASE 25,*
EXECUTE CC,3,MESSAGE3
IOC EXACC
SLJ EXITMAIN
BKMANY RELEASE 25,*
DBREAK CC
AJP,ZR MESSAGE1
EXITMAIN RELEASE 25,*
DFINISH
PODD ENI 1,6
SLJ START3
MESSAGE1 IOC ACC
SLJ EXITMAIN
MESSAGE2 IOC NACC
SLJ BKMANY
MESSAGE3 IOC BUSY
SLJ EXMANY
END MAIN
IDENT WRITLINE
LIRM WRITE,READ
ENTRY MANY,XFER,REENTER
COM1 RLOCK 0

```

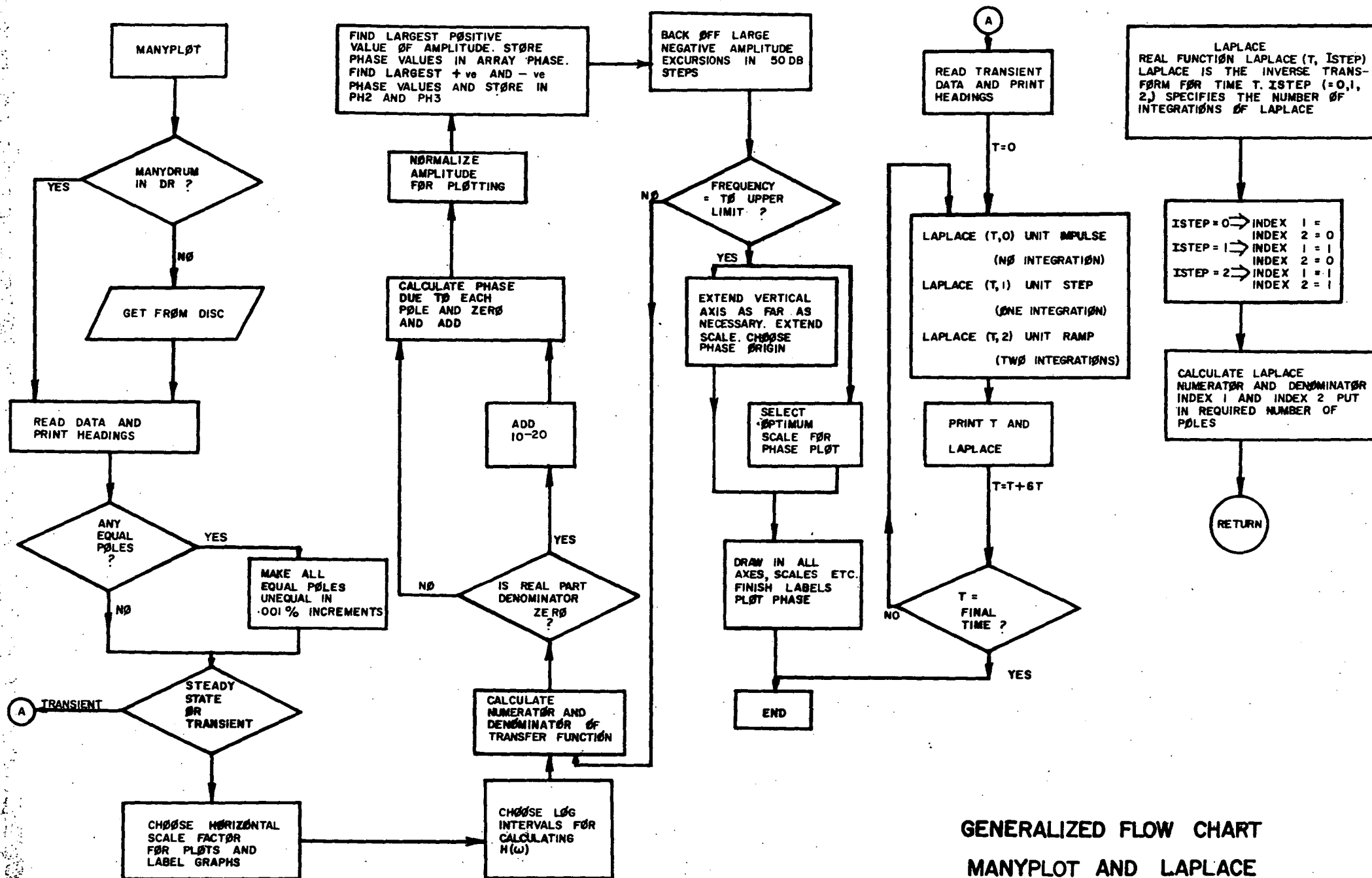
	COMMON ENTK(11B)
BLANK	BCD 9,
ENTK1	BSS 11B
CWD	IOTR ENTK1.11B
REENTER	NOP
MANY	NOP
LINE	CALL SWAP1
	XMIT,AUG ENTK,ENTK1
	WRITE 61,CWD,RET
	CALL SWAP1
	ISK 0,6
	SLJ MEXIT
	SLJ MANY
MEXIT	INI -1,6
	EXIT
11 RET	SLJ MANY
12 XFER	NOP
	CALL SWAP1
	XMIT,AUG BLANK,ENTK1
	READ 60,CWD,REJ
	WRITE 25,CWD,REJ
	CALL SWAP1
	XMIT,AUG ENTK1,ENTK
	CALL SWAP1
REJ	SLJ XFER
	END
	IDENT SWAP
	ENTRY SWAP1
SWAP1	NOP
SET	ENI 9,1
	ENI 0,2
	ENI 1,3
	ENI 0,4
	ENI 1,5
	SLJ SWAP1
	END
	IDENT CRACK
	ENTRY CRACK1
COM1	BLOCK 0
	COMMON X(11B)
LEFT	RSS 1
WHOLE	BSS 1
	OCT 12
CRACK1	NOP
START	LDA X
	ARS,E0 36
	STA WHOLE
	ARS,E0 6
	ALS,E0 6
	STA LEFT
	LDA WHOLE
	SUR LEFT
	STA X
	SUR WHOLE+1
	AJP,MI CRACK2
	LDA LEFT
	ARS,E0 6
	STA X
	SLJ CRACK1
CRACK2	LDA LEFT
	ARS,E0 6
	MUI WHOLE+1
	RAD X
	SLJ CRACK1
	END
	SCOPE

*LOAD,30

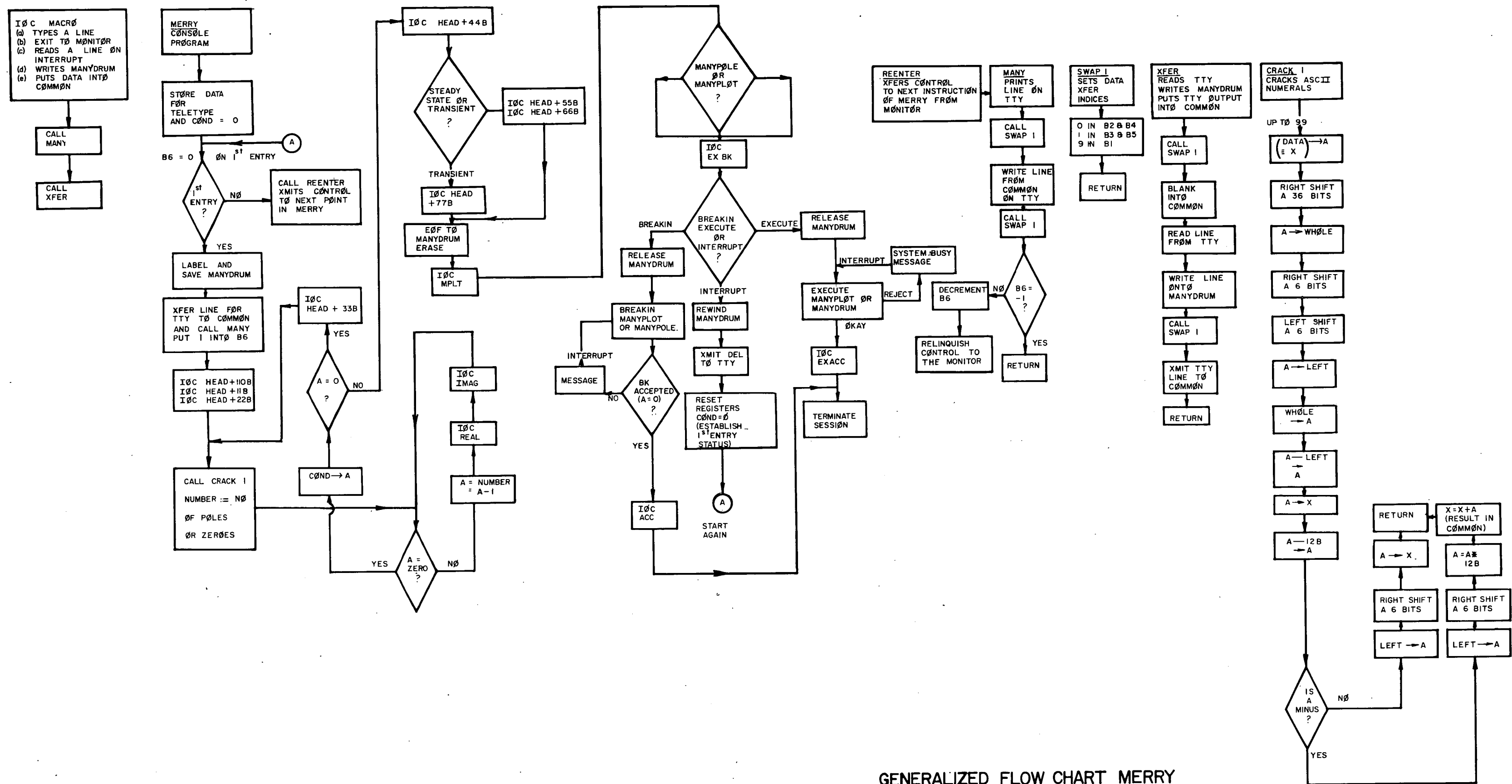
[EOF

*EOD

- 20 -



GENERALIZED FLOW CHART
MANYPLOT AND LAPLACE

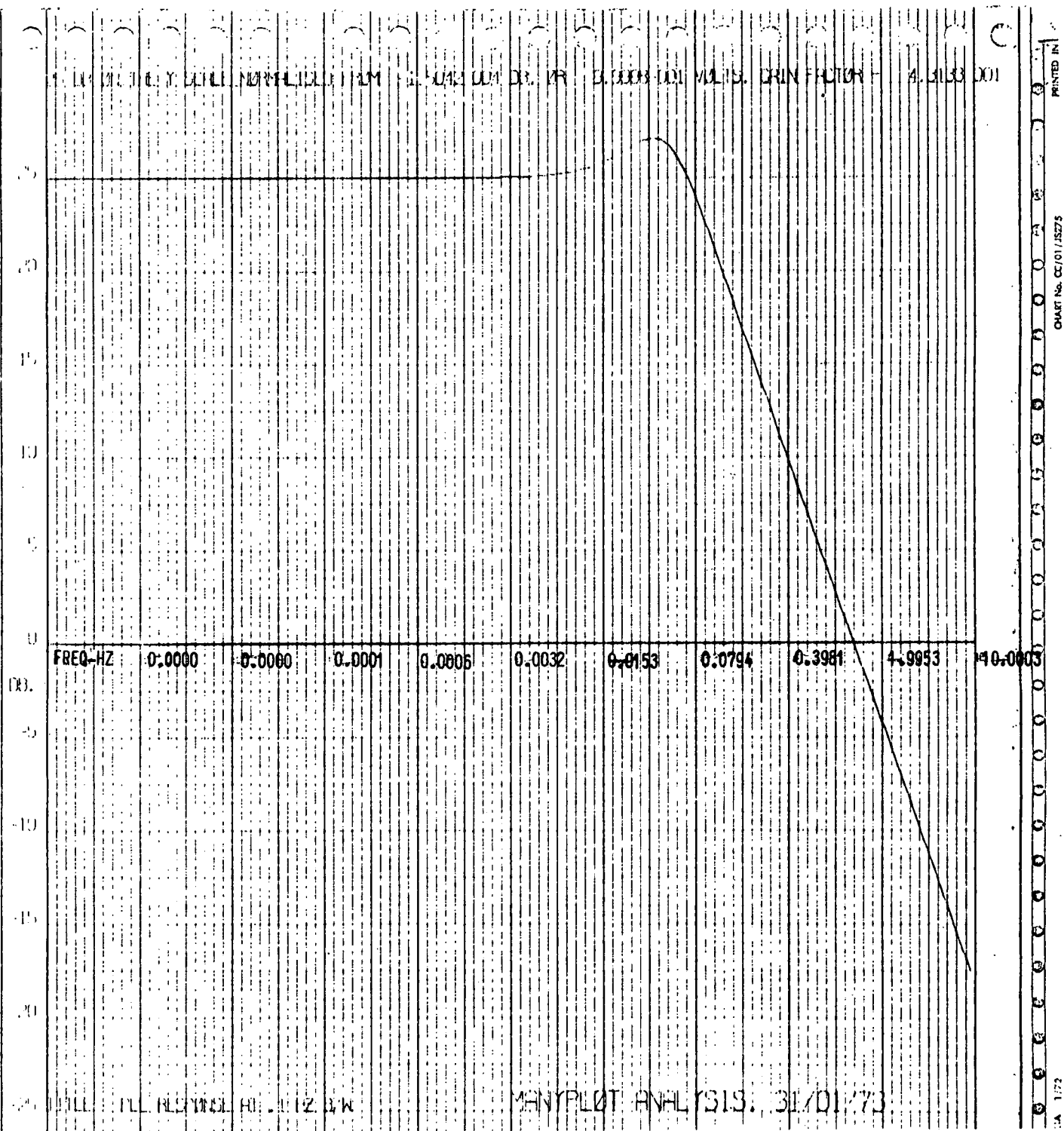


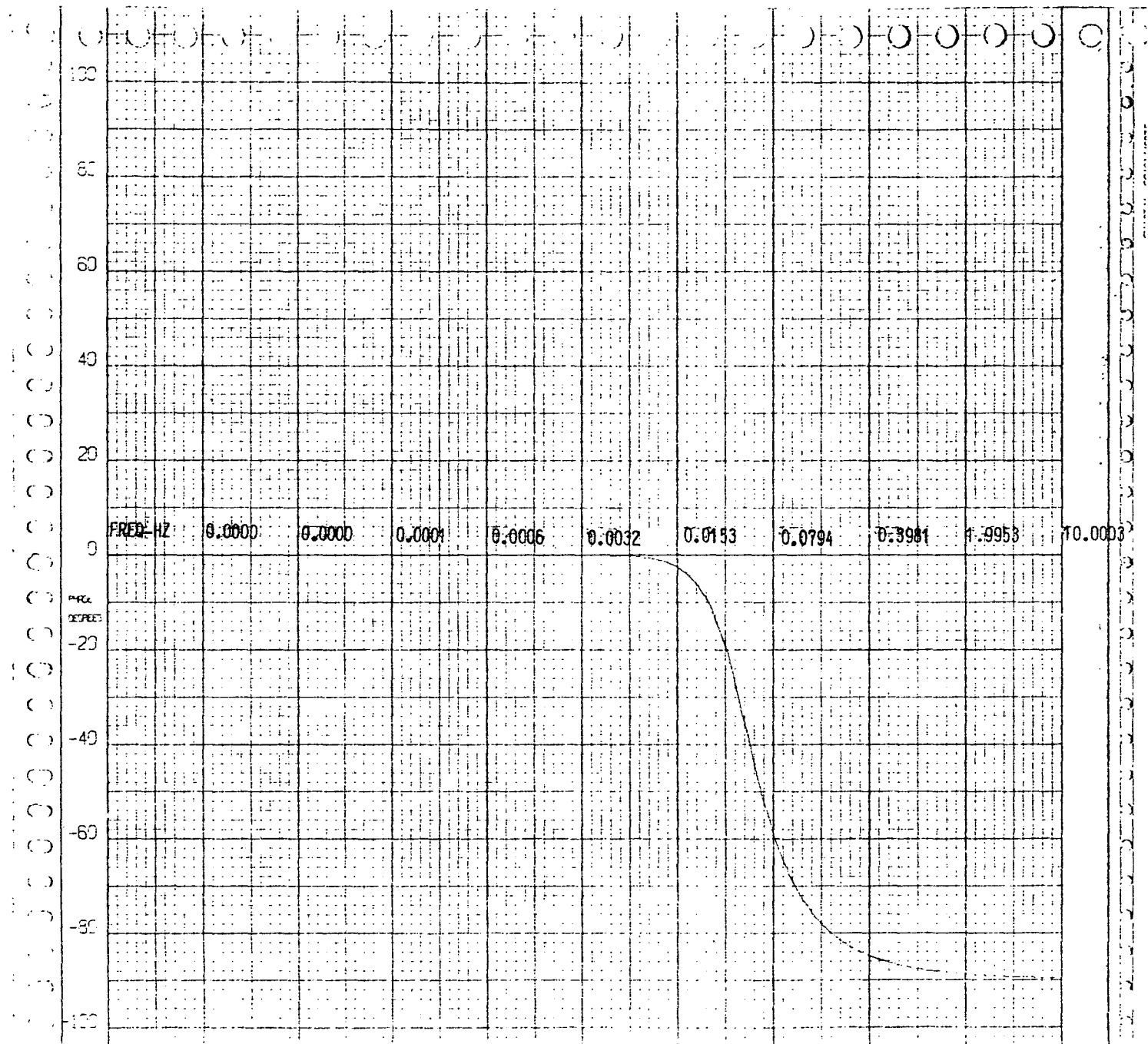
GENERALIZED FLOW CHART MERRY

-21-

APPENDIX 4

SAMPLE PLOTS AND OUTPUT FROM MANYPLOT





MANYPLOT ANALYSIS

ZEROES

-2.157-001 0.000+000

POLES

=2.157-001 2.157-001

=2.157-001 -2.157-001

STEADY STATE ANALYSIS

PLL RESPONSE AT .1 HZ B/W

015411

FREQ,HZ	AMPLITUDE	PHASE(DEG.)	DECIBELS
17.0000-006	9.9998-001	1.3340-008	-1.5042-004
17.0700-006	9.9998-001	1.5842-008	-1.5042-004
17.1449-006	9.9998-001	1.5008-008	-1.5042-004
17.2250-006	9.9998-001	1.6675-008	-1.5042-004
17.3108-006	9.9998-001	1.7509-008	-1.5042-004
17.4026-006	9.9998-001	2.0010-008	-1.5042-004
17.5007-006	9.9998-001	2.1678-008	-1.5042-004
17.6058-006	9.9998-001	2.0844-008	-1.5041-004
17.7182-006	9.9998-001	2.3345-008	-1.5041-004
17.8385-006	9.9998-001	2.5013-008	-1.5041-004
17.9672-006	9.9998-001	2.5013-008	-1.5041-004
27.1049-006	9.9998-001	2.8348-008	-1.5041-004
27.2522-006	9.9998-001	2.9182-008	-1.5040-004
27.4098-006	9.9998-001	3.1683-008	-1.5040-004
27.5785-006	9.9998-001	3.5852-008	-1.5040-004
27.7590-006	9.9998-001	3.5852-008	-1.5040-004
27.9522-006	9.9998-001	3.8353-008	-1.5039-004
37.1588-006	9.9998-001	3.9187-008	-1.5039-004
37.3799-006	9.9998-001	4.4189-008	-1.5038-004
37.6165-006	9.9998-001	4.8358-008	-1.5037-004
37.8697-006	9.9998-001	4.9192-008	-1.5037-004
47.1406-006	9.9998-001	5.1693-008	-1.5036-004
47.4304-006	9.9998-001	5.6696-008	-1.5035-004
47.7405-006	9.9998-001	6.1699-008	-1.5034-004
57.0724-006	9.9998-001	6.5034-008	-1.5033-004
57.4274-006	9.9998-001	6.9202-008	-1.5031-004
57.8074-006	9.9998-001	7.3371-008	-1.5030-004
67.2139-006	9.9998-001	7.9208-008	-1.5028-004
67.6488-006	9.9998-001	8.5878-008	-1.5026-004
77.1143-006	9.9998-001	9.0047-008	-1.5023-004
77.6123-006	9.9998-001	9.6717-008	-1.5021-004
87.1451-006	9.9998-001	1.0422-007	-1.5018-004
87.7153-006	9.9998-001	1.1006-007	-1.5014-004
97.3253-006	9.9998-001	1.1756-007	-1.5010-004
97.9781-006	9.9998-001	1.2757-007	-1.5005-004
17.0677-005	9.9998-001	1.3340-007	-1.5000-004
17.1424-005	9.9998-001	1.4424-007	-1.4994-004
17.2224-005	9.9998-001	1.5091-007	-1.4987-004
17.3079-005	9.9998-001	1.6258-007	-1.4979-004
17.3995-005	9.9998-001	1.7509-007	-1.4969-004
17.4974-005	9.9998-001	1.8593-007	-1.4959-004
17.6023-005	9.9998-001	1.9927-007	-1.4947-004
17.7144-005	9.9998-001	2.1261-007	-1.4933-004
17.8344-005	9.9998-001	2.2595-007	-1.4917-004

005472

1	179628-005	9.9998-001	2.4096-007	-1.4899-004
2	271002-005	9.9998-001	2.5763-007	-1.4879-004
3	272473-005	9.9998-001	2.7514-007	-1.4855-004
4	274046-005	9.9998-001	2.9098-007	-1.4828-004
5	275729-005	9.9998-001	3.1099-007	-1.4797-004
6	277530-005	9.9998-001	3.3100-007	-1.4761-004
7	279457-005	9.9998-001	3.5185-007	-1.4721-004
8	371519-005	9.9998-001	3.7436-007	-1.4674-004
9	373725-005	9.9998-001	3.9604-007	-1.4621-004
10	376086-005	9.9998-001	4.1772-007	-1.4560-004
11	378612-005	9.9998-001	4.4440-007	-1.4490-004
12	471315-005	9.9998-001	4.6858-007	-1.4411-004
13	474207-005	9.9998-001	4.9275-007	-1.4319-004
14	477302-005	9.9998-001	5.1777-007	-1.4215-004
15	570613-005	9.9998-001	5.4278-007	-1.4095-004
16	574156-005	9.9998-001	5.6529-007	-1.3958-004
17	577946-005	9.9998-001	5.8697-007	-1.3801-004
18	672003-005	9.9998-001	6.0948-007	-1.3621-004
19	676343-005	9.9998-001	6.2449-007	-1.3416-004
20	770987-005	9.9998-001	6.3616-007	-1.3180-004
21	775956-005	9.9999-001	6.4200-007	-1.2911-004
22	871273-005	9.9999-001	6.3700-007	-1.2603-004
23	876962-005	9.9999-001	6.2282-007	-1.2249-004
24	973049-005	9.9999-001	5.9447-007	-1.1845-004
25	979563-005	9.9999-001	5.4695-007	-1.1382-004
26	170653-004	9.9999-001	4.7608-007	-1.0852-004
27	171399-004	9.9999-001	3.7686-007	-1.0246-004
28	172197-004	9.9999-001	2.4179-007	-9.5512-005
29	173051-004	9.9999-001	5.9197-008	-8.7561-005
30	173964-004	9.9999-001	-1.8176-007	-7.8458-005
31	174942-004	9.9999-001	-4.9359-007	-6.8037-005
32	175988-004	9.9999-001	-8.9463-007	-5.6106-005
33	177107-004	1.0000+000	-1.4074-006	-4.2447-005
34	178304-004	1.0000+000	-2.0561-006	-2.6810-005
35	179585-004	1.0000+000	-2.8723-006	-8.9066-006
36	270956-004	1.0000+000	-3.8987-006	1.1589-005
37	272423-004	1.0000+000	-5.1852-006	3.5054-005
38	273993-004	1.0000+000	-6.7860-006	6.1919-005
39	275673-004	1.0000+000	-8.7795-006	9.2674-005
40	277470-004	1.0000+000	-1.1252-005	1.2789-004
41	279393-004	1.0000+000	-1.4317-005	1.6820-004
42	371450-004	1.0000+000	-1.8108-005	2.1435-004
43	373652-004	1.0000+000	-2.2794-005	2.6719-004
44	376007-004	1.0000+000	-2.8576-005	3.2768-004
45	378528-004	1.0000+000	-3.5703-005	3.9693-004
46	471225-004	1.0001+000	-4.4486-005	4.7621-004
47	474110-004	1.0001+000	-5.5293-005	5.6698-004
48	477198-004	1.0001+000	-6.8590-005	6.7090-004
49	570502-004	1.0001+000	-8.4941-005	7.8987-004
50	574037-004	1.0001+000	-1.0503-004	9.2607-004
51	577820-004	1.0001+000	-1.2971-004	1.0820-003
52	671867-004	1.0001+000	-1.6002-004	1.2605-003
53	676198-004	1.0002+000	-1.9722-004	1.4649-003
54	770831-004	1.0002+000	-2.4288-004	1.6988-003
55	775790-004	1.0002+000	-2.9890-004	1.9666-003
56	871095-004	1.0003+000	-3.6761-004	2.2732-003
57	876772-004	1.0003+000	-4.5189-004	2.6242-003
58	972846-004	1.0003+000	-5.5524-004	3.0260-003
59	979345-004	1.0004+000	-6.8195-004	3.4859-003
60	170630-003	1.0005+000	-8.3728-004	4.0124-003
	171374-003	1.0005+000	-1.0277-003	4.6150-003
	172170-003	1.0006+000	-1.2611-003	5.3049-003
	173022-003	1.0007+000	-1.5471-003	6.0944-003

1	1.3934-003	1.0008+000	-1.8975-003	6.9981-003
2	1.4909-003	1.0009+000	-2.3269-003	8.0324-003
3	1.5953-003	1.0011+000	-2.8531-003	9.2161-003
4	1.7069-003	1.0012+000	-3.4977-003	1.0571-002
5	1.8264-003	1.0014+000	-4.2873-003	1.2121-002
6	1.9543-003	1.0016+000	-5.2546-003	1.3895-002
7	2.0911-003	1.0018+000	-6.4393-003	1.5924-002
8	2.2374-003	1.0021+000	-7.8903-003	1.8246-002
9	2.3941-003	1.0024+000	-9.6673-003	2.0901-002
10	2.5616-003	1.0028+000	-1.1843-002	2.3939-002
11	2.7410-003	1.0032+000	-1.4508-002	2.7413-002
12	2.9328-003	1.0036+000	-1.7769-002	3.1385-002
13	3.1381-003	1.0041+000	-2.1763-002	3.5925-002
14	3.3578-003	1.0047+000	-2.6650-002	4.1115-002
15	3.5928-003	1.0054+000	-3.2631-002	4.7045-002
16	3.8443-003	1.0062+000	-3.9950-002	5.3819-002
17	4.1134-003	1.0071+000	-4.8903-002	6.1555-002
18	4.4014-003	1.0081+000	-5.9855-002	7.0386-002
19	4.7095-003	1.0093+000	-7.3246-002	8.0463-002
20	5.0391-003	1.0106+000	-8.9618-002	9.1956-002
21	5.3919-003	1.0122+000	-1.0963-001	1.0506-001
22	5.7693-003	1.0139+000	-1.3407-001	1.1998-001
23	6.1732-003	1.0159+000	-1.6392-001	1.3696-001
24	6.6053-003	1.0182+000	-2.0036-001	1.5628-001
25	7.0676-003	1.0207+000	-2.4481-001	1.7824-001
26	7.5624-003	1.0237+000	-2.9902-001	2.0315-001
27	8.0917-003	1.0270+000	-3.6507-001	2.3139-001
28	8.6582-003	1.0308+000	-4.4550-001	2.6335-001
29	9.2642-003	1.0351+000	-5.4333-001	2.9947-001
30	9.9127-003	1.0399+000	-6.6224-001	3.4021-001
31	1.0607-002	1.0454+000	-8.0660-001	3.8604-001
32	1.1349-002	1.0517+000	-9.8162-001	4.3748-001
33	1.2144-002	1.0586+000	-1.1935+000	4.9504-001
34	1.2994-002	1.0665+000	-1.4497+000	5.5922-001
35	1.3903-002	1.0753+000	-1.7587+000	6.3050-001
36	1.4876-002	1.0851+000	-2.1308+000	7.0929-001
37	1.5918-002	1.0960+000	-2.5777+000	7.9589-001
38	1.7032-002	1.1080+000	-3.1131+000	8.9047-001
39	1.8224-002	1.1211+000	-3.7524+000	9.9295-001
40	1.9500-002	1.1354+000	-4.5131+000	1.1030+000
41	2.0865-002	1.1508+000	-5.4147+000	1.2197+000
42	2.2325-002	1.1671+000	-6.4784+000	1.3420+000
43	2.3888-002	1.1841+000	-7.7265+000	1.4677+000
44	2.5560-002	1.2015+000	-9.1820+000	1.5942+000
45	2.7350-002	1.2187+000	-1.0868+001	1.7178+000
46	2.9264-002	1.2350+000	-1.2803+001	1.8337+000
47	3.1313-002	1.2497+000	-1.5005+001	1.9361+000
48	3.3504-002	1.2616+000	-1.7482+001	2.0182+000
49	3.5850-002	1.2694+000	-2.0234+001	2.0721+000
50	3.8359-002	1.2720+000	-2.3247+001	2.0896+000
51	4.1044-002	1.2680+000	-2.6496+001	2.0627+000
52	4.3917-002	1.2566+000	-2.9937+001	1.9840+000
53	4.6992-002	1.2370+000	-3.3516+001	1.8477+000
54	5.0281-002	1.2093+000	-3.7169+001	1.6506+000
55	5.3801-002	1.1738+000	-4.0827+001	1.3917+000
56	5.7567-002	1.1315+000	-4.4426+001	1.0732+000
57	6.1596-002	1.0838+000	-4.7907+001	6.9928-001
58	6.5908-002	1.0323+000	-5.1225+001	2.7590-001
59	7.0522-002	9.7836-001	-5.4346+001	-1.8999-001
60	7.5458-002	9.2350-001	-5.7253+001	-6.9122-001
	8.0740-002	8.6887-001	-5.9938+001	-1.2209+000
	8.6392-002	8.1537-001	-6.2401+001	-1.7729+000
	9.2440-002	7.6366-001	-6.4652+001	-2.3418+000

	978910-002	7.1423-001	-6.6703+001	-2.9232+000
	170583-001	6.6730-001	-6.8567+001	-3.5135+000
	171324-001	6.2302-001	-7.0262+001	-4.1100+000
1	172117-001	5.8141-001	-7.1802+001	-4.7104+000
2	172965-001	5.4243-001	-7.3203+001	-5.3132+000
3	173873-001	5.0599-001	-7.4479+001	-5.9171+000
4	174844-001	4.7199-001	-7.5642+001	-6.5214+000
5	175883-001	4.4028-001	-7.6705+001	-7.1254+000
6	176995-001	4.1074-001	-7.7677+001	-7.7287+000
7	178184-001	3.8321-001	-7.8568+001	-8.3312+000
8	179457-001	3.5758-001	-7.9386+001	-8.9326+000
9	270819-001	3.3370-001	-8.0139+001	-9.5329+000
10	272277-001	3.1145-001	-8.0831+001	-1.0132+001
11	273836-001	2.9073-001	-8.1470+001	-1.0730+001
12	275504-001	2.7141-001	-8.2061+001	-1.1327+001
13	277290-001	2.5341-001	-8.2607+001	-1.1923+001
14	279200-001	2.3663-001	-8.3112+001	-1.2519+001
15	371244-001	2.2098-001	-8.3581+001	-1.3113+001
16	373431-001	2.0638-001	-8.4015+001	-1.3707+001
17	375771-001	1.9276-001	-8.4419+001	-1.4300+001
18	378275-001	1.8005-001	-8.4794+001	-1.4892+001
19	470954-001	1.6819-001	-8.5142+001	-1.5484+001
20	473821-001	1.5712-001	-8.5467+001	-1.6075+001
21	476889-001	1.4679-001	-8.5768+001	-1.6666+001
22	570171-001	1.3714-001	-8.6050+001	-1.7256+001
23	573683-001	1.2814-001	-8.6312+001	-1.7847+001
24	577441-001	1.1972-001	-8.6556+001	-1.8436+001
25	671462-001	1.1187-001	-8.6784+001	-1.9026+001
26	675764-001	1.0453-001	-8.6996+001	-1.9615+001
27	770367-001	9.7673-002	-8.7194+001	-2.0205+001
28	775293-001	9.1270-002	-8.7379+001	-2.0793+001
29	870564-001	8.5288-002	-8.7552+001	-2.1382+001
30	876203-001	7.9699-002	-8.7713+001	-2.1971+001
31	972237-001	7.4478-002	-8.7863+001	-2.2559+001
32	978694-001	6.9599-002	-8.8003+001	-2.3148+001
33	170560+000	6.5041-002	-8.8134+001	-2.3736+001
34	171299+000	6.0782-002	-8.8257+001	-2.4324+001
35	172090+000	5.6803-002	-8.8371+001	-2.4913+001
36	172937+000	5.3084-002	-8.8478+001	-2.5501+001
37	173842+000	4.9609-002	-8.8578+001	-2.6089+001
38	174811+000	4.6362-002	-8.8671+001	-2.6677+001
39	175848+000	4.3327-002	-8.8758+001	-2.7265+001
40	176957+000	4.0491-002	-8.8840+001	-2.7853+001
41	178144+000	3.7841-002	-8.8916+001	-2.8441+001
42	179415+000	3.5365-002	-8.8987+001	-2.9029+001
43	270774+000	3.3051-002	-8.9053+001	-2.9616+001
44	272228+000	3.0888-002	-8.9115+001	-3.0204+001
45	273784+000	2.8867-002	-8.9173+001	-3.0792+001
46	275449+000	2.6978-002	-8.9227+001	-3.1380+001
47	277230+000	2.5213-002	-8.9278+001	-3.1968+001
48	279136+000	2.3563-002	-8.9325+001	-3.2555+001
49	371176+000	2.2021-002	-8.9369+001	-3.3143+001
50	373358+000	2.0581-002	-8.9410+001	-3.3731+001
51	375693+000	1.9234-002	-8.9449+001	-3.4319+001
52	378191+000	1.7976-002	-8.9485+001	-3.4906+001
53	470865+000	1.6800-002	-8.9519+001	-3.5494+001
54	473725+000	1.5701-002	-8.9550+001	-3.6082+001
55	476786+000	1.4673-002	-8.9580+001	-3.6669+001
56	570061+000	1.3713-002	-8.9607+001	-3.7257+001
57	573565+000	1.2816-002	-8.9633+001	-3.7845+001
58	577315+000	1.1978-002	-8.9657+001	-3.8433+001
59	671327+000	1.1194-002	-8.9679+001	-3.9020+001
60	675620+000	1.0462-002	-8.9700+001	-3.9608+001

770213+000	9.7773-003	-8.9720+001	-4.0196+001
775128+000	9.1377-003	-8.9738+001	-4.0783+001
870387+000	8.5399-003	-8.9755+001	-4.1371+001
876014+000	7.9812-003	-8.9771+001	-4.1959+001
972035+000	7.4596-003	-8.9786+001	-4.2546+001

0054175

5

6

7

8

9

10

11

12

13

14

15

16

17

18

19

20

21

22

23

24

25

26

27

28

29

30

31

32

33

34

35

36

37

38

39

40

41

42

43

44

45

46

47

48

49

50

51

52

53

54

55

56

57

58

59

60

MANYPLOT ANALYSIS

ZERJES

=3.833+001 0.000+000

POLES

=3.762+001 3.306+001

=3.762+001 -3.306+001

TRANSIENT ANALYSIS

MNS2 PLL, TRANSIENT ANALYSIS,

TIME	UNIT IMPULSE	UNIT STEP	UNIT RAMP
0.0000+000	7.5237+001	0.0000+000	0.0000+000
1.0000-002	4.6678+001	6.0425-001	3.2596-003
2.0000-002	2.5162+001	9.5732-001	1.1247-002
3.0000-002	1.0679+001	1.1311+000	2.1809-002
4.0000-002	2.0101+000	1.1903+000	3.3488-002
5.0000-002	-2.4220+000	1.1854+000	4.5403-002
6.0000-002	-4.0925+000	1.1510+000	5.7099-002
7.0000-002	-4.1732+000	1.1088+000	6.8399-002
8.0000-002	-3.4908+000	1.0701+000	7.9287-002
9.0000-002	-2.5666+000	1.0398+000	8.9829-002
1.0000-001	-1.6880+000	1.0186+000	1.0011-001
1.1000-001	-9.8255-001	1.0054+000	1.1023-001
1.2000-001	-4.8050-001	9.9825-001	1.2024-001
1.3000-001	-1.6095-001	9.9518-001	1.3021-001
1.4000-001	1.7412-002	9.9456-001	1.4015-001
1.5000-001	9.8462-002	9.9521-001	1.5010-001
1.6000-001	1.1966-001	9.9634-001	1.6006-001
1.7000-001	1.0899-001	9.9750-001	1.7003-001
1.8000-001	8.5149-002	9.9847-001	1.8001-001
1.9000-001	5.9213-002	9.9919-001	1.9000-001
2.0000-001	3.6769-002	9.9967-001	1.9999-001
2.1000-001	1.9845-002	9.9995-001	2.0999-001
2.2000-001	8.4436-003	1.0001+000	2.1999-001
2.3000-001	1.6132-003	1.0001+000	2.2999-001
2.4000-001	-1.8841-003	1.0001+000	2.3999-001
2.5000-001	-3.2070-003	1.0001+000	2.4999-001
2.6000-001	-3.2767-003	1.0001+000	2.5999-001
2.7000-001	-2.7439-003	1.0000+000	2.6999-001
2.8000-001	-2.0191-003	1.0000+000	2.8000-001
2.9000-001	-1.3290-003	1.0000+000	2.9000-001
3.0000-001	-7.7438-004	9.9999-001	2.9999-001
3.1000-001	-3.7932-004	9.9998-001	3.0999-001
3.2000-001	-1.2767-004	9.9998-001	3.1999-001
3.3000-001	1.2960-005	9.9998-001	3.2999-001
3.4000-001	7.6995-005	9.9998-001	3.3999-001
3.5000-001	9.3879-005	9.9998-001	3.4999-001
3.6000-001	8.5629-005	9.9998-001	3.5999-001
3.7000-001	6.6959-005	9.9998-001	3.6999-001
3.8000-001	4.6601-005	9.9998-001	3.7999-001
3.9000-001	2.8963-005	9.9998-001	3.8999-001
4.0000-001	1.5651-005	9.9998-001	3.9999-001
4.1000-001	6.6760-006	9.9998-001	4.0999-001
4.2000-001	1.2941-006	9.9998-001	4.1999-001
4.3000-001	-1.4656-006	9.9998-001	4.2999-001
4.4000-001	-2.5130-006	9.9998-001	4.3999-001
4.5000-001	-2.5728-006	9.9998-001	4.4999-001
4.6000-001	-2.1568-006	9.9998-001	4.5999-001
4.7000-001	-1.5885-006	9.9998-001	4.6999-001
4.8000-001	-1.0464-006	9.9998-001	4.7999-001
4.9000-001	-6.1031-007	9.9998-001	4.8999-001
5.0000-001	-2.9945-007	9.9998-001	4.9999-001

5,1000=001	-1,0126=007	9,9998=001	5,0999=001
5,2000=001	9,6147=009	9,9998=001	5,1999=001
5,3000=001	5,0205=008	9,9998=001	5,2999=001
5,4000=001	7,3652=008	9,9998=001	5,3999=001
5,5000=001	6,7274=008	9,9998=001	5,4999=001
5,6000=001	5,2655=008	9,9998=001	5,5999=001
5,7000=001	3,6676=008	9,9998=001	5,6999=001
5,8000=001	2,2814=008	9,9998=001	5,7999=001
5,9000=001	1,2343=008	9,9998=001	5,8999=001
6,0000=001	5,2783=009	9,9998=001	5,9999=001
6,1000=001	1,0377=009	9,9998=001	6,0999=001
6,2000=001	-1,1398=009	9,9998=001	6,1999=001
6,3000=001	-1,9692=009	9,9998=001	6,2999=001
6,4000=001	-2,0201=009	9,9998=001	6,3999=001
6,5000=001	-1,6953=009	9,9998=001	6,4999=001
6,6000=001	-1,2496=009	9,9998=001	6,5999=001
6,7000=001	-8,2386=010	9,9998=001	6,6999=001
6,8000=001	-4,8100=010	9,9998=001	6,7999=001
6,9000=001	-2,3639=010	9,9998=001	6,8999=001
7,0000=001	-8,0309=011	9,9998=001	6,9999=001
7,1000=001	7,1067=012	9,9998=001	7,0999=001
7,2000=001	4,7074=011	9,9998=001	7,1999=001
7,3000=001	5,7782=011	9,9998=001	7,2999=001
7,4000=001	5,2853=011	9,9998=001	7,3999=001
7,5000=001	4,1406=011	9,9998=001	7,4999=001
7,6000=001	2,8864=011	9,9998=001	7,5999=001
7,7000=001	1,7970=011	9,9998=001	7,6999=001
7,8000=001	9,7347=012	9,9998=001	7,7999=001
7,9000=001	4,1731=012	9,9998=001	7,8999=001
8,0000=001	8,3182=013	9,9998=001	7,9999=001
8,1000=001	-8,8634=013	9,9998=001	8,0999=001
8,2000=001	-1,5430=012	9,9998=001	8,1999=001
8,3000=001	-1,5861=012	9,9998=001	8,2998=001
8,4000=001	-1,3326=012	9,9998=001	8,3998=001
8,5000=001	-9,8307=013	9,9998=001	8,4998=001
8,6000=001	-6,4863=013	9,9998=001	8,5998=001
8,7000=001	-3,7908=013	9,9998=001	8,6998=001
8,8000=001	-1,8661=013	9,9998=001	8,7998=001
8,9000=001	-6,3688=014	9,9998=001	8,8998=001
9,0000=001	5,2310=015	9,9998=001	8,9998=001
9,1000=001	3,6806=014	9,9998=001	9,0998=001
9,2000=001	4,5331=014	9,9998=001	9,1998=001
9,3000=001	4,1523=014	9,9998=001	9,2998=001
9,4000=001	3,2560=014	9,9998=001	9,3998=001
9,5000=001	2,2716=014	9,9998=001	9,4998=001
9,6000=001	1,4155=014	9,9998=001	9,5998=001
9,7000=001	7,6772=015	9,9998=001	9,6998=001
9,8000=001	3,2992=015	9,9998=001	9,7998=001
9,9000=001	6,6656=016	9,9998=001	9,8998=001
1,0000+000	-6,8914=016	9,9998=001	9,9998=001

LUN	TYPE	SECTORS	CHARGE	SERIAL (MT)	LABEL
68	DR	2			
60	DR	7			
20	DR	2			CCDMR*DAMANYPLOT
61	LP	13	6		

JOB,CCDMR*DA,MANYPLOT. END JOB 121326 CPU TIME, 0H 0M 17S

0023121

0023121

7
8
9
10
11
12
13
14
15
16
17
18
19
20
21
22
23
24
25
26
27
28
29
30
31
32
33
34
35
36
37
38
39
40
41
42
43
44
45
46
47
48
49
50
51
52
53
54
55
56
57
58
59
60

-32-

APPENDIX 5

SAMPLE OUTPUT FROM MERRY

-33-

*LG;CCLMF*DA,MERRY

140740 25/01/73

MANYPLOT ANALYSIS CONTROL LOGGED IN. CALLED ON 25/01/73

TYPE A NAME FOR THE RUN. (LESS THAN 40 CHARACTERS).

TEST RUN NUMBER 1

TYPE YOUR GAIN TERM IN F FORMAT.

:12345.875

HOW MANY ZEROS. (<9) (I FORMAT.)

:1

TYPE REAL PART. (F FORMAT.)

:335.768

TYPE IMAGINARY PART. (F FORMAT.)

:-99.7

HOW MANY POLES. (<9) (I FORMAT.)

:2

TYPE REAL PART. (F FORMAT.)

:1.222

TYPE IMAGINARY PART. (F FORMAT.)

:8.975

TYPE REAL PART. (F FORMAT.)

:1.222

TYPE IMAGINARY PART. (F FORMAT.)

:-8.975

STEADY STATE OR TRANSIENT.

:STEADY STATE

INITIAL FREQUENCY-HZ. (F FORMAT.)

:0.001

FINAL FREQUENCY-HZ. (F FORMAT.)

:100.0

MANYPOLE OR MANYPLOT.

:MANYPLOT

TYPE EK OR EX, ELSE JUST INTERRUPT.

:EK

EKJOB 00

BREAKIN REQUEST ACCEPTED

:

CCLMF*DA

MERRY

NORMAL TERM

0 + 2 SEC

:

-34-

```
*LG,CCMISDA,MERRY
141107 25/01/73
MANYPLOT ANALYSIS CONTROL LOGGED IN. CALLED ON 25/01/73
TYPE A NAME FOR THE LOG. (LESS THAN 40 CHARACTERS).
:***TEST RUN NUMBER TWO***
TYPE YOUR GAIN TERM IN F FORMAT.
:054321234.98765
FOR MANY ZEROS. (<9) (I FORMAT.)
:0
FOR MANY POLES. (<9) (I FORMAT.)
:1
TYPE REAL PART. (F FORMAT.)
:2.76
TYPE IMAGINARY PART. (F FORMAT.)
:0.00
STEADY STATE OR TRANSIENT.
:TRANSIENT
TRANSIENT TIME-SECONDS. (F FORMAT.)
:12.78
MANYPOLE OR MANYPLOT.
:MANYPLOT
TYPE EK OR FX, ELSE JUST INTERRUPT.
:FX
EXECUTION REQUEST ACCEPTED.
:
CCMISDA          MERRY          NORMAL TERM          0 + 2 SEC
:
```

-35-

```
*LG,CCIMP*LA,MERRY
141256 25/01/73
MANYPLOT ANALYSIS CONTROL LOGGED IN. CALLED ON 25/01/73
TYPE A NAME FOR THE RUN. (LESS THAN 40 CHARACTERS).
***TEST RUN NUMBER THREE***
TYPE YOUR GAIN TERM IN F FORMAT.
:1.1
HOW MANY ZPOLES. (<9) (I FORMAT.)
:1
TYPE REAL PART. (F FORMAT.)
:7.77
TYPE IMAGINARY PART. (F FORMAT.)
:3.21
HOW MANY POLES. (<9) (I FORMAT.)
:0
STEADY STATE OR TRANSIENT.
:STEADY STATE
INITIAL FREQUENCY-HZ. (F FORMAT.)
:0.23
FINAL FREQUENCY-HZ. (F FORMAT.)
:0.24
MANYPOLE OR MANYPLOT.
:MANYPLOT
TYPE EK OR EX, ELSE JUST INTERRUPT.
:
DRUM LOC DELETED - INTERRUPT AND TRY AGAIN.
:
MANYPLOT ANALYSIS CONTROL LOGGED IN. CALLED ON 25/01/73
TYPE A NAME FOR THE RUN. (LESS THAN 40 CHARACTERS).
:
```

```
CCIMP*LA
:
```

MERRY

NORMAL TERM

0 + 2 SEC

- 36 -

```
*LG,CCLM*LA,MERY
020106 30/01/73
MANYPLOT ANALYSIS CONTROL LOGGED IN. CALLED ON 30/01/73
TYPE A NAME FOR THE RUN. (LESS THAN 40 CHARACTERS).
: *** 2052 PLL RESPONSE. ***
TYPE YOUR GAIN TERM IN F FORMAT.
: 75.237
HOW MANY ZEROS. (<9) (I FORMAT.)
: 1
TYPE REAL PART. (F FORMAT.)
: -33.333
TYPE IMAGINARY PART. (F FORMAT.)
: 0.
HOW MANY POLES. (<9) (I FORMAT.)
: 2
TYPE REAL PART. (F FORMAT.)
: -37.62
TYPE IMAGINARY PART. (F FORMAT.)
: 33.06
TYPE REAL PART. (F FORMAT.)
: -37.62
TYPE IMAGINARY PART. (F FORMAT.)
: -33.06
STEADY STATE OR TRANSIENT.
: STEADY STATE
INITIAL FREQUENCY-HZ. (F FORMAT.)
: .001
FINAL FREQUENCY-HZ. (F FORMAT.)
: 100.
MANYPOLE OR MANYPLOT.
: MANYPLOT
TYPE EK OR EX, ELSE JUST INTERRUPT.
: EK
EKJCE 01
EKJCE 00
EPAKIN REQUEST ACCEPTED
:
CCLM*LA          MERY          NORMAL TERM          86 + 2 SEC
:
```