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GEOLOGICAL INVESTIGATIONS FOR THE GINNINDERRA SEWER TUNNEL
BELCONNEN, A.C.T., 1975

by

P.A. Lang and D.C. Purcell

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SUMMARY

In 1974 the then Department of Housing and Construction requested the Bureau of Mineral Resources to carry out geological design investigations of the proposed Ginninderra sewer tunnel, extending about 5.2 km from Ginninderra Creek southwards to the Lower Molonglo Water Quality Control Centre.

A continuous seismic refraction profile was obtained (and also some cross traverses) along the route, which was mapped at scales of 1:2400 and 1:9600. 14 diamond-drill holes and 9 groundwater observation bores were drilled, by the Department of Housing and Construction and Bureau of Mineral Resources respectively, and several mechanical rock parameters were determined by the Bureau of Mineral Resources.

The tunnels will be driven through an Upper Silurian sequence of acid volcanics, tuffaceous sediments, and a granite porphyry intrusion. Some units in the sequence are gently to moderately folded. Five major faults have been detected, and many small fractured or sheared zones are indicated by airphoto-lineaments and zones of low seismic velocity. Seismic risk to the tunnel, its lining, shafts, or other appurtenant works is very low.

The engineering, geological, and excavation properties of the different rock types have been determined. The rocks to be excavated are generally very hard and strong, and mostly good tunnelling conditions can be expected. Poor tunnelling conditions will generally be confined to faulted, fractured, or sheared zones, and about 16 percent of the tunnel will require support.

Shafts and portals are favourably located with respect to geology, and no serious geotechnical problems are expected.

1. INTRODUCTION

1.1 BACKGROUND

Wastewater from the Ginninderra catchment (i.e., the Belconnen and future Gungahlin development areas) is currently treated at the Belconnen Water Pollution Control Centre (BWPCC). Conventional treatment is followed by lagooning before discharge of effluent to Ginninderra Creek, which flows via the Murrumbidgee River to Burrinjuck Reservoir. The BWPCC has an effective capacity to serve about 70 000 persons; this number is expected to be exceeded in 1977-78, so that the plant must be augmented or wastewater diverted to the Lower Molonglo Water Quality Control Centre (LMWQCC) about 5.3 km away.

An augmented plant at Belconnen would require nutrient removal facilities to avoid stimulating excessive aquatic growths in the receiving waters, and an economic study indicated substantial economies in both capital and operating costs by diverting wastewater to the LMWQCC. A tunnel was preferred to a trench sewer because the shorter tunnel route results in a lower capital cost, and also because construction difficulties and environmental impact are substantially less.

The tunnel will have sufficient capacity to divert future wastewater flows from the neighbouring Gooromon Ponds and Jeir catchments because of the economies of treating all wastewater at the LMWQCC and the small additional cost for a larger tunnel.

1.2 ENGINEERING DETAILS

The Ginninderra sewer tunnel (GST) will join the existing BWPCC near Ginninderra Creek, to the LMWQCC near the confluence of the Molonglo and Murrumbidgee Rivers (Fig. 1).

The design details are shown in Figures 2 and 3.

This scheme will consist of two 2130 mm diameter concrete-lined tunnels about 4240 m and 860 m long, joined at Window Bend by about 150 m of pipe which will be buried in an embankment of spoil excavated from the tunnels. The sewer will fall 8.8 m from RL 523.7 at the base of shaft 1 to RL 514.9 at the outlet portal at LMWQCC - a gradient of 1:600. Two 2600 mm diameter concrete-lined ventilation shafts (shafts 2 and 3) 41 m and 46 m deep will be excavated 4 m west of the centre line of the tunnel at Stn 17+12 and Stn 33+15 (Plate 1).

The GST will be connected to the existing Belconnen trunk sewer by a 210 m section of 1500 mm diameter concrete pipe in an open-cut trench, a tunnel about 148 m long lined with 1350 mm diameter concrete pipes, and a 61 m section of 2130 mm diameter concrete pipe in an open-cut trench.

Two concrete-lined shafts - shaft C and shaft 1 of 2600 mm and 4500 mm diameter, respectively, incorporating vortex drop structures - will drop the sewerage from the Belconnen trunk sewer (RL 555) to the GST (RL 523.7).

The design provides for connection to future sewers from Gooromon Ponds at point E (RL 536) and from Jeir at the bottom of shaft 1 (RL 523.7).

1.3 REQUEST FOR GEOLOGICAL INVESTIGATION

In April 1974 the then Department of Housing and Construction (DHC), who were to design the sewer on behalf of the National Capital Development Commission (NCDC), asked the Bureau of Mineral Resources (BMR) to carry out a feasibility investigation along the proposed route.

In late 1974, NCDC decided that the sewer was to be completed in 1978. DHC then requested BMR to:

- (a) carry out a geological design investigation along the adopted route;
- (b) provide geological information for the design of the tunnel; and
- (c) prepare a report for inclusion in the 'Information for Tenderers' document.

1.4 SCOPE OF INVESTIGATION

During the feasibility stage, geological information was made available to assist in determining:

- (a) the feasibility of constructing a tunnel from BWPCC to the LMWQCC;
- (b) the most practical route and elevation for the tunnel, taking into account cost and environmental aspects; and
- (c) the best positions for the shafts.

During the design stage and for the 'Information for Tenderers' document, information was made available about the geology of the route and the effect it will have on the design and construction of the tunnel, shafts, portals, and the connection from the north end of the tunnel to the existing Belconnen trunk sewer; in particular to predict the effect of geology on:

- (d) choice of tunnelling method

LOCATION MAP
GINNINDERA SEWER TUNNEL
MOLONGLO VALLEY INTERCEPTOR SEWER
LOWER MOLONGLO WATER QUALITY CONTROL CENTRE
CANBERRA A.C.T.



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BWPCC Belconnen Water Pollution Control Centre

Lower Molonglo Water Quality Control Centre

Tunnel

Buried pipeline

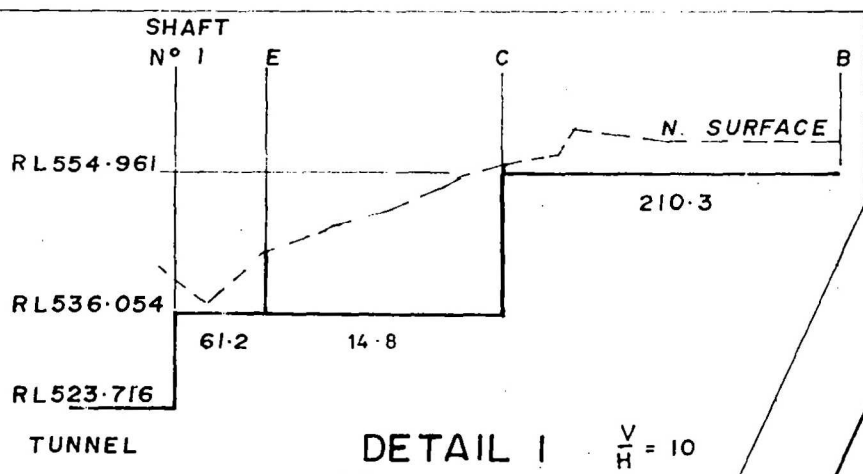
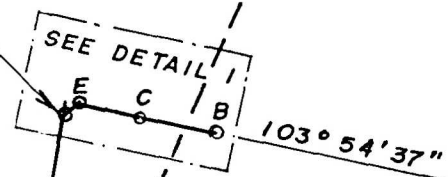
Shaft

GINNINDERRA SEWER TUNNEL DESIGN DETAILS

CHAINAGE 00
COORDS N612801
E199427

FIGURE 2

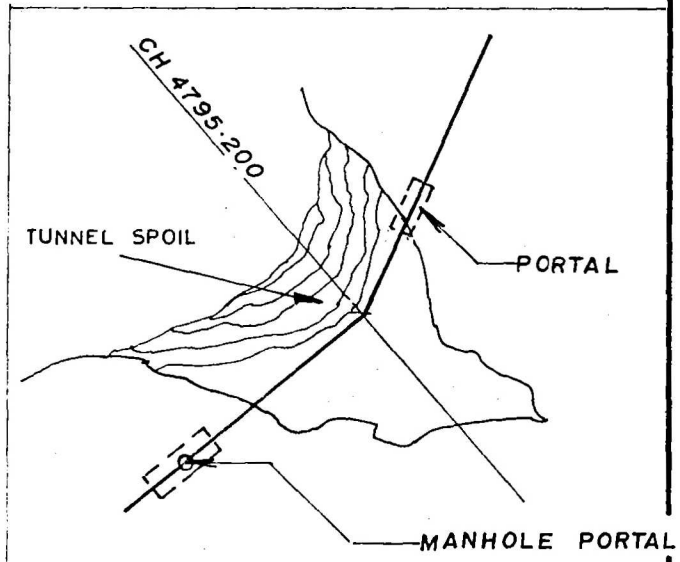
SHAFT N° 1
CHAINAGE 498.711
COORDS N612424
E198948
DEPTH 22.826 m
DIA. 4.500 m
R.L. OF INVERT 523.716



SHAFT N° 2
CHAINAGE 1712.267
COORDS N611225
E198757
DEPTH 40.717 m
DIAMETER 2.600 m
R.L. OF INVERT 521.693

SHAFT N° 3
CHAINAGE 3314.694
COORDS N609751
E198130
DEPTH 46.0 m
DIAMETER 2.600 m
R.L. OF INVERT 519.020

WINDOW BEND - (SEE DETAIL 2).
CHAINAGE 4795.20
COORDS N608388
E197551
R.L. OF INVERT 516.555



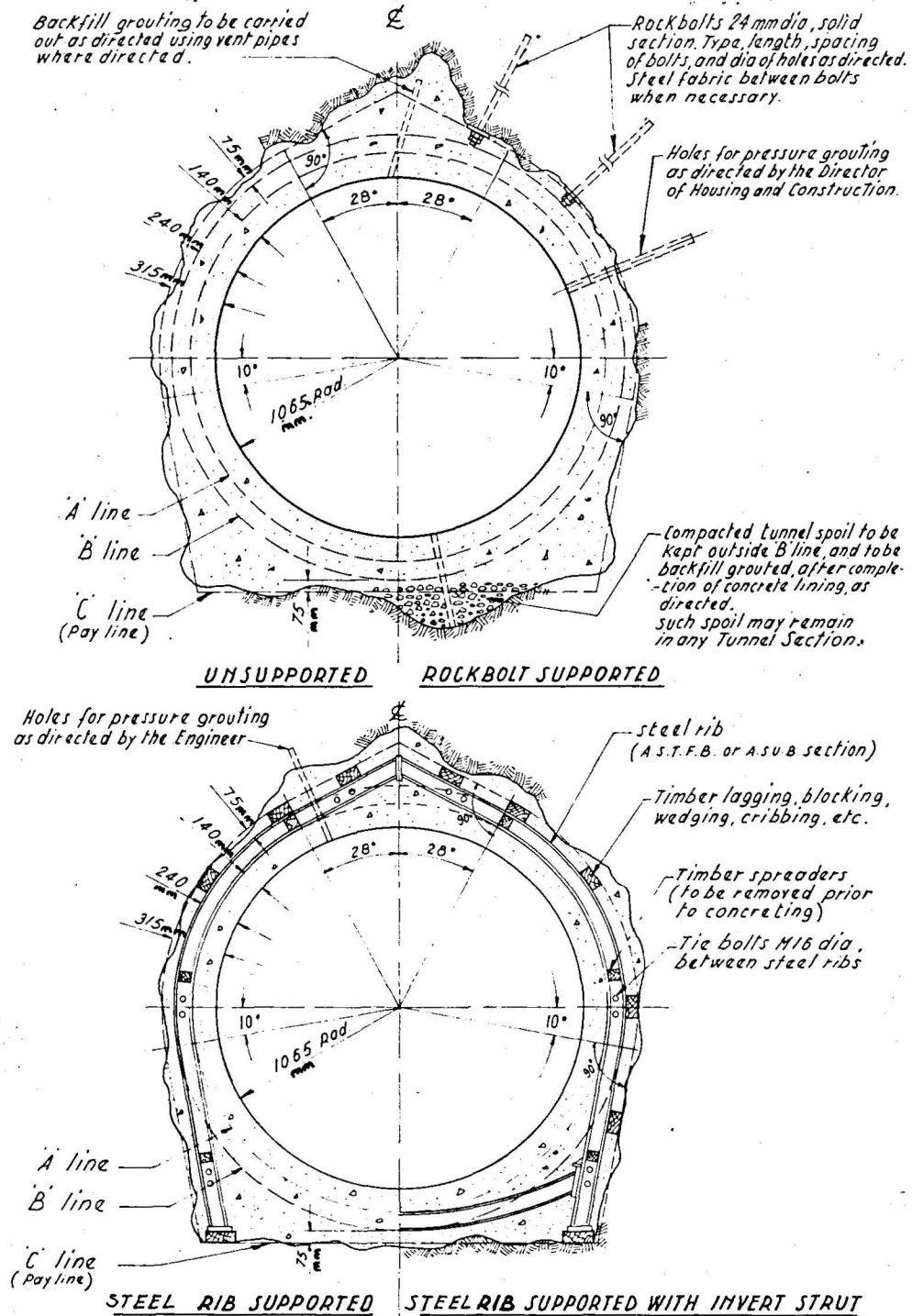
OUTLET PORTAL
CHAINAGE 5788.454
COORDS N607740
E196798
R.L. OF INVERT 514.900

DETAIL 2

GINNINDERRA SEWER TUNNEL

TYPICAL TUNNEL CROSS — SECTIONS

FIGURE 3



SCALE 100 0 500 1000 mm

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- (e) excavation conditions - rate of advance
 - wear rate of drills
 - explosive quantities
- (f) overbreak
- (g) support - type
 - amount
- (h) groundwater inflows - quantities
 - duration of flow
 - effect on excavation rate
 - effect on concrete placement
 - long-term effect on concrete lining.

All these parameters have been studied and this report lists and describes the results of the investigations carried out by the BMR Engineering Geology Subsection for DHC.

2. GENERAL GEOLOGY

2.1 REGIONAL GEOLOGY

The regional geology of the area is described in the Canberra 1:250 000 Geological Series map and explanatory notes (Strusz, 1971), and the area was more recently mapped for the Brindabella Sheet of the 1:100 000 Geological Series (Owen & Wyborn, 1975).

The interpretative solid geology of the proposed tunnel area is shown in Plate 1. The tunnels will be driven through an Upper Silurian sequence of acid volcanics, tuffaceous sediments, and a granite intrusion.*

The rocks are faulted, gently folded, and are tilted about 20°-30° southwest.

2.2 PHYSIOGRAPHY AND WEATHERING

The area south of Stn 40+00 (Plate 1) is generally steep and dissected by tributary creeks of the Murrumbidgee River. Downcutting of the Murrumbidgee River and its tributaries has caused rapid erosion of weathered rock, and a shallow weathering profile remains.

The area north of Stn 40+00 is undulating plateau, with depths of weathered overburden ranging from 10 to 35 m.

* Chemical analyses and petrographic description of rocks samples are set out in Appendix 5.

2.3 GROUNDWATER

The water-table is 0 to 20 m below ground surface (i.e., generally 30 to 45 m above tunnel level) on the plateau area, and 0 to 45 m below ground surface (i.e., 0 to 20 m above tunnel level) in the dissected area.

Permeability of the rock substance in the granites, dacites, and shales are almost zero, and groundwater is contained in open joints and fractures in the rock mass. No large water-filled cavities are present in these rock types. Permeabilities of the rock mass are expected to be less than 30 m/day and generally less than 10 m/day.

Chemical analyses of five water samples from Pine Ridge tunnel are presented in Appendix 6. Water samples from drill holes along the GST tunnel line will be collected and analysed, and results will be available in 1976. See Appendix 1 for investigation methods.

2.4 ROCK TYPES AND STRATIGRAPHY

2.4.1 Purple rhyodacite and green rhyolite

Generally the purple rhyodacite is weathered or partly altered. No fresh samples have been obtained from outcrops, road-cuts, or drill core. It is generally soft and weak, or crumbly. Phenocrysts of quartz, pink feldspar, and epidote are common in a fine-grained purple groundmass. In some places it appears to be a bedded tuff with a sharp contact against the green rhyolite; more commonly it appears to grade upwards into the green rhyolite.

At Pine Ridge Hill (locality C1; Plate 1) the purple rhyodacite appears to grade up through a medium-grained highly weathered and crumbly green rhyolite, into a fine-grained very siliceous green rhyolite at the top.

The relationship of these two rock types to the rocks in the rest of the area is not known, because most of the contacts are either faulted or their nature is not determinable. No definite conformable contacts have been seen. The rocks may be extrusive or intrusive. If intrusive they may be an offshoot of the granite porphyry. If extrusive they probably underlie the volcanics and sediments mapped as the lower part of the Walker Volcanics.

The evidence for an intrusive origin is as follows:

- (a) A dyke of green rhyolite intrudes the upper part of the Walker Volcanics (locality D2; Plate 1); however, the dyke-rock may be younger than the other green rhyolites in the area.
- (b) Near the east end of Pine Ridge tunnel, exposures in creeks and in the Molonglo River show green rhyolite intruding purple dacites (locality D3; Plate 1).
- (c) The irregular contact between the green rhyolite and purple rhyodacite near Window Bend does not appear to be conformable.
- (d) The position of the contact in drill hole GST 16 (Plate 8) did not coincide with its predicted position assuming the beds were conformable (see Appendix 8 for logs of holes, and Appendix 7 for photographs of drill-core).
- (e) Possible intrusive contact against shales near Belconnen Golf Course (locality D5; Plate 1).

The evidence for an extrusive origin is as follows:

- (a) In Pine Ridge tunnel, the green rhyolite is welded and massive at depth and grades up into a coarse agglomerate, then into black shale. The transition zone has blocks of green rhyolite up to 50 cm diameter surrounded by black shale.
- (b) On, and west of Pine Ridge Hill (locality D6; Plate 1), the outcrop pattern suggests the rhyolite is bedded and dips about 20° SW, and is overlain by the shales and tuffaceous sediments (locality G1) in the valley south of Pine Ridge Hill.
- (c) At Belconnen Golf Course (locality D4), the rhyolite crops out to the east of the southwest-dipping Walker Volcanics which suggests that the latter overlies the rhyolite. This would mean that the shales in Pine Ridge tunnel and at locality G1 are within the lower part of the Walker Volcanics.

A chemical analysis of a sample of green rhyolite from a road-cut on Weetangera Road (locality D1), and, for comparison, two analyses from a similar green rhyolite in Tuggeranong tunnel, are tabled in Appendix 5.

2.4.2 Walker Volcanics, lower sequence

A sequence of dacitic welded tuff and agglomerates, pyroclastic flows, and sills and dykes of dacitic composition with interbedded tuffaceous shale, siltstone, and sandstone

comprises the lower part of the Walker Volcanics. In some places there is complete gradation from the welded tuff through to the tuffaceous sandstone. Drill core from GST 7 shows several beds of massive welded tuff grading up into reworked tuffaceous sandstone with scour-and-fill structures near the top of each bed. Intraclasts of contorted shale up to 10 cm thick and 1 m long are incorporated in the tuff in drill core GST 7 and in outcrops to the west of Parkwood Road (locality E2).

Most of the sediments are near the base of the sequence. Above these most of the rock is welded dacitic agglomerate and tuff, and intrusive rock. Most of the extrusive rocks are massive, but in places they show a strong flow-banding/bedding due to flattening of dark grey, fine-grained rock fragments. In some places they grade up through reworked tuff into sandstone lenses.

The intrusive rocks are similar in appearance to the welded tuff, but are massive and slightly coarser-grained. Intrusive contacts against well bedded tuffs and tuffaceous sediments have been seen in several locations (E3 and E4). The intrusions are probably high-level sills and dykes.

The extrusive rocks in hand specimen are similar in appearance to outcrops of extrusive Mount Painter Porphyry* near Coppins Crossing, and have the following features in common.

- (a) both have interbedded sediments
- (b) both contain garnet
- (c) both have a fragmental texture, e.g., contain angular quartz
- (d) both contain biotite which is often fresh
- (e) composition of plagioclase is similar
- (f) both contain rare potash feldspar phenocrysts
- (g) chemical analysis of sample 75840019 is similar to five analyses of Mount Painter Porphyry particularly Rb, Sr, Ba, Zr (see Appendix 5). Sample 75840018 shows some differences; it is an agglomerate and some changes in chemistry probably occurred at the time of eruption.

* The Mount Painter Porphyry was the name given by Öpik (1958) to a porphyritic rock of dacitic composition to the southwest of Canberra that he regarded as a sill. Subsequent mapping to the west of Canberra has indicated that rock with apparent continuity with the Mount Painter Porphyry exhibits primary structures attributable to an extrusive origin.

The lower sequence of the Walker Volcanics is faulted against the upper part of the Walker Volcanics to the south; against purple rhyodacite and green rhyolite to the east; and against Willow Bridge Tuff to the north. It is intruded by a granite porphyry sill (Plate 1).

2.4.3 Walker Volcanics, upper part

The upper part of the Walker Volcanics is at least 1500 m thick (Malcolm, 1954). It is thought to be the same age as the Hawkins Volcanics in the Yass Basin, but the units cannot be correlated lithologically (Wyborn, pers. comm.). It is a sequence of dacitic densely welded pyroclastic flows and tuffs with some lenses of shale and limestone.

In Pine Ridge tunnel the upper part of the Walker Volcanics consists of densely welded pyroclastic flows and tuffs, mostly massive but with some thin-bedded welded tuffs and some thin lenses of water-deposited shales and tuffaceous sandstones. The massive welded rocks grade up into well-bedded crystal tuffs near the west portal of Pine Ridge tunnel; in the LMWQCC, well bedded tuffs are ubiquitous. The general dip is 20° SW, but the tuffs are moderately folded in the LMWQCC area.

The rocks are generally blue-grey to purple, but green-grey rocks are also common. Chemical analyses of five samples collected in Pine Ridge tunnel are presented in Appendix 5. Chemistry of the five samples is fairly similar except for FeO/Fe₂O₃ ratios which are high in the green varieties and low in the purple varieties. Total Fe as FeO ranges from 4 percent to 6 percent; FeO/Fe₂O₃ ranges from 4.3 to 0.45.

The purple colour appears to be due to secondary oxidation which has permeated into the rock from permeable defects in the rock mass. The oxidation is more complete in the more permeable rock (close jointed and fractured) than in the very tight, wide-jointed zones. Calcite veins are common in the blue grey to purple zones, but rare in the green grey zones.

2.4.4 Willow Bridge Tuff (previously Laidlaw Volcanics)

The Willow Bridge Tuff unconformably overlies the Yass Subgroup in the Yass Basin (Link, 1970) and unconformably overlies sediments (thought to be Yass Subgroup), purple rhyodacite and purple rhyolite at Gooramons Ponds (Henderson, 1975). Near the BWPCC, it either unconformably overlies or is faulted against purple rhyodacite and pink rhyolite. The sequence is about 500 m thick 1 km west of Yass (Link, 1971).

In the area of the BWPCC, the Willow Bridge Tuff is a sequence of densely welded pyroclastic flows of dacitic composition. It is generally pale grey with phenocrysts (approximately 25%) of quartz feldspar and biotite up to 5 mm in a fine-grained groundmass; there is a dark grey bed about 70 m thick at the base of the sequence which crops out along the eastern edge near the BWPCC; this bed has fewer phenocrysts and a finer-grained, darker groundmass.

Flow banding/bedding (dip about $35^{\circ}\text{SW}/135^{\circ}$) can be seen in some drill core and in exposures of extremely weathered rock in creek beds (locality J2). Zones of quartz-epidote veining, and pink calcite veining, are seen in GST 2 and 4 and in some outcrops. Where this veining occurs the feldspars and much of the groundmass is stained pink.

2.4.5 Granite porphyry (Ginninderra Porphyry)

This is a sill of granite porphyry which has intruded along the bedding planes of the shales and sandstones within the Walker Volcanics.

Intrusive contacts have been seen in exposures in creeks near the Murrumbidgee River (locality L1) and in drill core from GST 1 and GST 22.

The granite porphyry was probably emplaced in Ludlovian times (Upper Silurian). The granite porphyry is regarded as part of the Ginninderra Porphyry, which intrudes the Willow Bridge Tuff to the west and north.

2.5 STRUCTURE

2.5.1 Folding

Walker Volcanics. Some gentle folding is present in the lower part of the Walker Volcanics; and some strong folding occurs in the shales near the granite porphyry intrusion (location G2). No cleavage is apparent in the shales. The sequence is tilted about 20°SW .

Gentle to moderate folding is present in the upper part of the Walker Volcanics in Pine Ridge tunnel and in the LMWQCC excavations. Most of the upper part of the Walker Volcanics is also tilted about 20°SW .

Willow Bridge Tuff. The Willow Bridge Tuff is a very competent unit. No folding is apparent, and the unit is tilted about 35°SW .

2.5.2 Faults

Seven major faults have been located during the mapping; however, only five of them intersect the GST line (Plates 1 to 5). Many minor fractured or sheared zones are indicated by airphoto-lineaments (Plates 2 to 5). Zones of low bedrock velocity, and defect zones are shown on the seismic profiles (Plates 6 to 8).

The major fault zones range in width from a few metres to several hundred metres; they generally consist of one or more clay-filled crushed and sheared zones from 3 to 30 m wide, with adjacent fractured rock. All the major faults extend beyond the area mapped or are truncated by other major faults.

The upthrown and downthrown sides of the faults have been deduced from stratigraphic relationships and are shown in Plate 1. The faults were active during Silurian and Devonian time, with probably some reactivation during the Late Tertiary to Quaternary Kosciuskan uplift. Significant displacement across the faults is unlikely to have taken place during the last million years.

Some of the faults may still be active (i.e., causing earth tremors), but relative movement along a fault producing a measurable displacement at or near the ground surface would be extremely unlikely and prediction of the site of such a displacement is not possible. See also Seismicity.

Fault 1 crosses the northwest corner of the mapped area and does not intersect the tunnel line (Plate 1). It is roughly parallel to fault 5 and the Winslade Fault, a major fault crossing the Molonglo valley about 6 km to the southeast. It is also subparallel to one of the prominent photo-lineament directions in the area.

In February 1975 an earth tremor of magnitude 3 on the Richter scale originated from an epicentre on this fault at a depth of about 1.6 km. There was no displacement along the fault at the ground surface.

Fault 2 is an east-west-trending fault which crosses the tunnel line near stn 13+00. There is no rock outcrop near the tunnel line from which width or condition of the fault can be estimated. Between the tunnel line and the Murrumbidgee River the fault can be traced on aerial photographs, and appears to divide into several fault zones. Near the Murrumbidgee River the fault can be seen in creeks and in outcrops as sheared and fractured zones up to 100 m wide. Drill holes GST 6 and 8 intersected sections of crushed and sheared granite porphyry. The extent of the fault to the east is not known.

The northside of the fault is thought to be the downthrown block since it contains the Willow Bridge Tuff which is thought to be younger than the lower part of the Walker Volcanics, which occurs south of the fault.

Fault 3 intersects the tunnel at stn 40+20. Where fault 3 is exposed in creek beds to the west of the tunnel line the crushed and sheared zone ranges from 25 to 50 m wide. Where fault 3 crosses the Murrumbidgee River, there is 3 m of sheared and crushed rock with 10 m of strongly fractured rock and up to 100 m of moderately fractured rock on the south side of the fault. The rocks on the north side of the fault have not been affected. Drill hole GST 12 revealed a 3 m wide crushed zone with sheared and fractured rock on the south side.

The south side of the fault is considered to be the downthrown block; this interpretation requires a much smaller displacement than if the south side were the upthrown block. East of the tunnel line, fault 3 may be truncated by fault 6 and probably by fault 5, although fault 3 may diverge and merge with fault 5.

Fault 4 intersects the tunnel line at stn 47+50; it trends southeast, subparallel to the Deakin Fault - a major fault 6 km to the northeast through Belconnen - and to the second major photo-lineament and joint direction in the area. It is truncated at its northwestern end by fault 5, and at the southeastern end, it is possibly truncated by fault 7. Fault 4 is probably a continuation of fault 3 that has been displaced by dextral trans-current movement along fault 5.

Fault 4 is exposed in several places in the creek near Window Bend. The zone of crushed and sheared rock appears to range from less than 1 m to about 15 m wide. Drill hole GST17 revealed that it consists of sheared and crushed shale and volcanic fragments in a heavy clay matrix with 20 m of sheared and fractured rhyolite on the northern side. The condition of the rock on the southern side is probably similar to that on the south side of fault 3, but will not have any effect on the construction of the GST as the rock will be under the spoil heap at Willow Bend.

The fault is an impermeable barrier and has held back water in the fractured rhyolite to the northeast. Drill hole GST17 went through this fault into the fractured rhyolite, and water has flowed from the collar of the hole continuously since it was drilled.

The south side of the fault is considered to be the downthrown block for the same stratigraphic reason that applied to fault 3.

Fault 5 appears to divide into several faults in some areas. The fault zone is about 30 m wide near Pine Ridge homestead (locality Z; Plate 1) but widens out to about 200 m and becomes hard to trace in the upper part of the Walker Volcanics (locality Y; Plate 1). Aerial photographs show the fault continues south of Uriarra Crossing.

Fault 5 is subparallel to Fault 1, to the Winslade Fault, and to the prominent photo-lineament and joint direction (060°) in the area.

Fault 6 is a branch of Fault 5. It was intersected by drill hole GST13; it appears to have been intersected near the surface in GST15, and it must lie between GST14 and GST21 as the rock types in these two holes are on the opposite sides of the fault. The trace of the fault on the ground surface is fairly irregular (Plates 1 and 5).

Where intersected by GST13, the fault zone consisted of 0.5 m of crushed and sheared shale and rhyolite, with about 6 m of sheared and fractured rhyolite on the eastern side. Drill holes GST14 and GST15 revealed that in these areas there is at least 20 m of slicksided, seamy, and fractured rock on each side of the crushed zone.

The wedge between faults 4 and 5 is very complex and appears to be extensively faulted and the detailed structure has not been worked out.

2.5.3 Photo-lineaments

Photo-lineaments are plotted on Plates 2 to 5 (see Investigation Methods, Appendix 1). These probably represent sheared and fractured zones. There are two main directions of lineaments and several random lineaments. The main joint set directions are probably parallel to the main photo-lineament directions.

Photo-lineaments plotted during the design investigation of Tuggeranong tunnel correlated well with defect zones encountered during its construction.

2.5.4 Joints

No detailed joint study has been done in the area. The main joint sets in Pine Ridge tunnel are $90^{\circ}/060^{\circ}$, $90^{\circ}/160^{\circ}$, and a third set parallel to bedding. The sets $90^{\circ}/060^{\circ}$ and $90^{\circ}/160^{\circ}$ are subparallel to the major fault directions (including the Deakin and Winslade faults) and to the most common photo-lineament directions in the area. These will probably be the most common joint sets in the tunnel but joints are controlled by

folding and faulting and vary according to structural domain. Therefore, the main joint sets are likely to vary several times along the tunnel line.

2.6 SEISMICITY

Recorded seismic data for the last 13 years show a number of epicentres within a few kilometres of the tunnel line, indicating the possibility that some of the faults are active (i.e., causing seismic tremors). A tremor of magnitude 3 on the Richter scale originating from an epicentre 1.6 km depth on fault 1 was recorded in February 1975. Data are insufficient to predict either frequency or magnitude of future tremors.

An earthquake producing measurable displacement at the ground surface would be extremely unlikely, and prediction of the site of such a displacement is impossible.

3. ENGINEERING GEOLOGY

3.1 ENGINEERING, GEOLOGICAL AND EXCAVATION PROPERTIES OF THE ROCK TYPES

3.1.1 DACITE: WALKER VOLCANICS, UPPER PART

(Stn 47+60 to 57+88. Drill holes GST17 GST18, GST20, MV7)
(Stn 40+20 to 43+80. Drill holes GST12, GST13, GST14)

Tunnelling conditions in these sections of Ginninderra sewer tunnel are expected to be similar to those encountered in the western 1800 m of Pine Ridge tunnel, which passes through the same rock unit. Within this part of the text, references to Pine Ridge tunnel refer only to the section within 1800 m of its west portal (see note on 'Correlation with Pine Ridge tunnel', Appendix 1).

3.1.1.1 ENGINEERING PROPERTIES OF THE ROCK SUBSTANCE

The methods for determining the mechanical rock parameters, and the results of testing, are set out in Appendix 4.

Most samples tested were of the purple or green varieties of the dacite. The fresh blue grey dacite is expected to give higher values for both UCS and Shore Hardness.

Sample location	UCS (MPa)		Point Load Strength (MPa)					
	No. of samples	Range	Average	Samples successfully tested	Is(50)**		UCS equiv.*	Mean hardness (Shore units)
					Range	Average		
GST 13	-	-	-	6	4.2-9.9	7.0	170	
GST 18	3	96-145	120	7	2.9-7.8	5.1	120	68
GST 20	3	141-255	206	10	4.9-7.5	6.2	150	89
MV 7	3	187-239	213	-	-	-	-	91
Mv 11	4	177-262	222	-	-	-	-	88
Pine Ridge Tunnel	-	-	-	65	4.3-12.0	7.9	200	-

* Values in the 'UCS equivalent' column were obtained from Brock & Branklin (1972).

** Point Load Strength Index; see Appendix 4.

3.1.1.2 TUNNEL SECTION STN 47+60 TO 57+88
(Drill holes GST17, GST18, GST20, MV7)

3.1.1.2.1 Geological properties of the rock mass at tunnel level
(Plate 8)

Weathering. This section of the tunnel will be excavated through fresh dacite, except for about 40 m of moderately weathered to fresh rock near the south portal at Window Bend. The highest-velocity seismic refractor indicates that the base of the zone of weathering is more than 10 m above tunnel crown along 700 m (about 95%) of this section.

Seismic velocities*. Bedrock** velocities range from 3500 to 4400 m/sec, similar to the 3400 to 4800 m/sec for the same rock type in Pine Ridge tunnel.

Defects. No major faults have been detected by surface mapping or seismic refraction along the tunnel line.

In Pine Ridge tunnel, long sections (up to 700 m) of competent rock ($RCN < 4$) are broken by shorter sections (generally 40-100 m, but up to 200 m) of less competent rock ($RCN \geq 4$). In the competent rock (about 75% of Pine Ridge tunnel) joints are mostly spaced 0.3 to 1 m and are slightly open to very tight. There are four main joint sets in Pine Ridge tunnel:

J1	80°/W/170°	Spaced 0.6 - 2 m
J2	90°/060°	" 0.3 - 1 m
J3	20° -40°/N/070° (bedding)	" 0.1 - 0.6 m
J4	80°/S/100°-140°	occur intermittently

The above joints vary in prominence from area to area, and in many places some or all sets are not present. There are many random discontinuous joints, and in some areas joints sets other than those listed above are more prominent.

In competent sections of Pine Ridge tunnel, crushed and sheared zones, generally 0.1 to 0.3 m wide, associated with thin clay seams and close jointed and fractured zones up to 1 m wide, are spaced about 10 to 200 m apart. Most are oriented parallel to J1 or J3.

* Time-distance curves for the seismic profiling are available at BMR for inspection by tenderers.

** The term 'bedrock' as used in this report refers to the deepest seismic refractor detected, and the term 'overburden' refers to the soil, colluvium, and weathered rock above that refractor.

The less competent rock (about 25% of Pine Ridge tunnel) is more closely jointed (0.1-0.3 m), with joints slightly open or with some clay on surfaces. Crushed and sheared zones (less than 2% of Pine Ridge tunnel) are generally 0.3 to 1 m wide, with 3 to 30 m of associated close jointed and/or fractured and seamy rock.

Defects in GST are expected to be similar in width, spacing, and condition to those in Pine Ridge tunnel, except that, along the GST line, joints parallel to bedding dip about $20^{\circ}\text{SW}/130^{\circ}$. Spacing is variable from 10 to 30 cm between the Window Bend south portal and stn 51+00, to greater than 60 cm for most of the rest of the section.

3.1.1.2.2 Groundwater inflows*

Water outflowed from each portal of Pine Ridge tunnel at about $10 \text{ m}^3/\text{hr}$ during excavation. Outflows from this section of the Ginninderra sewer tunnel are expected to be less than those from Pine Ridge tunnel because groundwater in the area has been substantially drained by the deeply incised nearby Murrumbidgee River and its deep tributary creeks. The maximum height of the water-table above tunnel level is about 10 m. The porosity and permeability of this rock mass is expected to be similar to that at Pine Ridge tunnel, so it is unlikely that there is much water stored in the rock above tunnel level.

Based on experience at Pine Ridge tunnel, when water-bearing defects were intersected during excavation, water inflows, generally less than $1 \text{ m}^3/\text{hr}$ but possibly up to $10 \text{ m}^3/\text{hr}$ in a few zones, will enter the tunnel initially but will decrease rapidly after excavation.

3.1.1.2.3 Excavation properties

Effect of engineering properties. The rock is very strong and very hard. Drill penetration is slow and drill wear rate is high. In the hardest blue-grey dacite in Pine Ridge tunnel one drill steel was worn out for about every 5 m of drilling.

In Pine Ridge tunnel the average weight of explosive (AN60 and ANFO in varying proportions) per cubic metre of rock excavated (including overbreak**, which was calculated from concrete quantities) ranged from 2.6 to 3.6 kg/m^3 . However, over-

* Water-pressure test computation sheets are available at BMR for inspection by tenderers (see also Appendix 3).

** The term "overbreak" in this report refers to the depth measured normal to the C-line (see Fig. 3) of the space produced when a block or blocks of rock fall from outside the line of the perimeter drill holes. Predictions of overbreak in this report assume a well designed and loaded drilling pattern suitable for the rock conditions encountered. Overbreak due to poor drilling and blasting procedures cannot be predicted. The overbreak figures quoted do not refer to the average overbreak which could be expected for that particular tunnel section.

break in Pine Ridge tunnel was excessive for such competent rock and much of it is attributed to inaccurate drilling and over-blasting. A neat tunnel profile with less overbreak could be produced in this section of the GST with more accurate drilling and slightly smaller explosive quantities.

Effect of geological properties of the rock mass.

Using the same excavation techniques, overbreak would be slightly greater in GST than in Pine Ridge tunnel because of the prominent joint set J2 (strike 040° to 070° in GST line), which is sub-parallel to the tunnel line.

Joint set $20^{\circ}\text{SW}/130^{\circ}$ (parallel to the bedding) will dip with tunnel drive and should not cause extra overbreak if the tunnel is driven from Window Bend.

Intersection of major joints spaced 0.3 to 1 m will cause blocky ground in areas where the joints are open or clay-coated, and random rock bolts** may be needed to pin some blocks.

The narrow sheared and fractured zones in the competent sections ($\text{RCN} < 4$) will generally not need support. In the less competent sections ($\text{RCN} \geq 4$), low angle shears, seams, and fractured zones will occur at random orientations and will cause some overbreak; some of these defects will need support. Defect zones > 10 m wide will need support irrespective of orientation.

Excluding the portals, 3 percent of the upper part of the Walker Volcanics in Pine Ridge tunnel had steel-set support in irregularly spaced sections 6 to 15 m long. A similar percentage is expected in this section of GST; however, it could be higher if any major defects oriented parallel to the tunnel line run along the tunnel crown for any distance.

In Pine Ridge tunnel the following percentages of each rock condition number were mapped in this section of the Walker Volcanics. See Appendix 2 for definition of Rock Condition Number (RCN).

RCN 2	20%
TCN 3	55%
RCN 4	23%
RCN 5	2%

Similar percentages are expected in this section of GST.

Effect of groundwater inflows. No major groundwater inflows that could significantly slow excavation progress are expected.

** The term 'random rockbolts' is used by tunnel engineers for the placing of rockbolts as required by the rock conditions, as distinct from 'pattern rockbolts' where rockbolts are placed in a regular pattern along a section of tunnel.

Combined effects of all parameters:

- (a) Geologically there is no reason why the excavation rate should differ from that maintained in the same unit in Pine Ridge tunnel.
- (b) The blue grey dacite is very hard, and drill penetration will be slow and drill wear rate high.
- (c) Less overbreak can be expected in this section of GST than in Pine Ridge tunnel if drilling is more accurate and slightly less explosive is used.
- (d) Excluding portals, about 3 percent of this section is expected to need steel-set support.
- (e) No major groundwater inflows which could significantly slow excavation progress are expected.
- (f) Within this section, the percentages of tunnel assigned to each rock condition number are expected to approximate those logged in Pine Ridge tunnel which are set out below.

RCN 2	20%
RCN 3	55%
RCN 4	23%
RCN 5	2%

3.1.1.2.4 Contact, stn 47+50: fault 4 (drill holes GST 17)

The contact between dacite of the upper part of the Walker Volcanics and the green rhyolite is fault 4. This will affect the Window Bend north portal and its engineering significance is described in that section.

3.1.1.3 TUNNEL SECTION STN 40+20 TO 43+80
(Drill holes GST 12, GST 13, GST 24)

3.1.1.3.1 Geological properties of the rock mass at tunnel level
(Plate 8)

Weathering. This section of the tunnel will be in fresh dacite of the upper part of the Walker Volcanics.

Seismic velocities. Seismic velocities of 3600 to 4600 m/sec indicate that the rock mass is fairly tight.

Defects. This part of the tunnel passes through a wedge of rock between faults 3 and 6. Fault 6 runs close to the tunnel line for most of the length of this section and has probably caused some shearing and fracturing in the rock mass. Drill holes GST12 and GST13 reveal that the rock has been partly stressed and sheared, but most defects have been healed with chlorite. Joint spacing is variable from 20 cm to 1 m. Joint surfaces are slickensided and coated with chlorite and are fairly tight. Many small fractured zones from 10 cm to 1 m wide, spaced 30 cm to 5 m, were intersected in drill holes GST12 and GST13. Crushed seams up to 10 cm wide with clay are also common. Most sheared and fractured zones probably strike parallel to fault 6, i.e., at a small angle to the tunnel.

3.1.1.3.2 Groundwater inflows

The water table ranges from 20 to 40 m above tunnel level. Water-pressure test losses in drill holes GST12 and GST13 were up to 10 lugeons, but most were less than 1 lugeon, indicating that permeability of the rock mass is generally fairly low.

Most of this section will be damp, with persistent seepages and drips from some fractured zones. Most open joints and fractured zones will yield₃ initial inflows less than 1 m³/hr, but a few may yield up to 10 m³/hr.

3.1.1.3.3 Excavation properties

Effect of engineering properties: similar to stn 47+60 to 57+88, except that shearing and formation of chlorite throughout the rock has probably reduced the strength of this rock slightly. Drill penetration should be marginally faster and drill wear rate slightly lower.

Effect of geological properties of the rock mass. The variable joint spacing from 20 cm to 1 m will mean that, when blasted, much of the rock mass will break into fragments less than 30 cm diameter, but in some sections some larger blocks will remain.

The fracturing, shearing, and close jointing resulting from the nearby faults will mean that there is more loose ground in this section than in the section from stn 47+60 to 57+88. Many of the crushed, sheared, and fractured zones are expected to be parallel to fault 6 (about 20° to tunnel line) resulting in longer sections of support and more overbreak. About 20 percent of the section from 40+20 to 43+00 is expected to need steel-set support.

In competent rock some blocks generally less than 30 cm will fall out from beyond the C-line. Crushed, sheared, and fractured zones parallel to fault 6 will probably cause up to 1 m overbreak in the east wall and crown in places. Clay-coated defects with dips up to 45° against tunnel drive could cause in excess of 1 m overbreak (rare).

Effect of groundwater inflows. The water inflows expected should not cause any delay in excavation progress. The action of groundwater on the clay-filled defects, especially near fault 6, will reduce the stand-up time of the rockmass.

Combined effects of all parameters:

- (a) Rock condition number is expected to be mainly 3, with some 4 and possibly some 5.
- (b) About 20 percent of the section from stn 40+20 to 42+30 is expected to need steel-set support with timber logging.
- (c) Generally less than 30 cm but in places up to 1 m overbreak in the crown and east wall may result from defects oriented parallel to fault 6. Other unfavourably oriented defects may cause in excess of 1 m overbreak (rare).
- (d) Drill penetration will be slightly faster and drill wear rate slightly lower than section stn 47+60 to 57+88.

3.1.1.3.4 Contact, stn 40+20: fault 3 (Drill hole GST12)

The contact between the upper and lower parts of the Walker Volcanics is fault 3. Drill hole GST12 revealed a 5 m wide crushed zone of soft and weak clayey gravel with fragments less than 2 cm in a sandy clay matrix. On the southern side of the fault the rock is closely jointed and slickensided for 20 m from the fault zone, and to the north of the fault the rock is widely jointed and tight (i.e., little affected by the fault).

3.1.2 GREEN RHYOLITE: STN 46+10 (APPROX.) TO STN 47+45. (DRILL HOLES GST 16, GST 17)

3.1.2.1 Engineering properties of the rock substance

Sample location	UCS (MPa)			Point load strength (MPa)				
	No. of samples	Range	Average	Samples successfully tested	Is(50)		UCS equiv.	Mean hardness (Shore units)
					Range	Average		
GST 16	NOT TESTED			9	6.1-11.4	9.0	220	NOT TESTED
GST 17	3	247-322	283	11	5.9-10.2	8.4	200	96
Road cut D1				9	6.1-11.4	9.8	240	-

3.1.2.2 Geological properties of the rock mass at tunnel level (Plate 8)

Weathering. This section of tunnel will be excavated through fresh green rhyolite.

Seismic velocities. Bedrock velocities range from 3400 to 4400 m/sec. 4400 m/sec probably represents fairly tight rock; 3400 m/sec probably represents closely jointed rock, with joint surfaces partly separated and rock mass moderately loose.

Defects. This section of tunnel will be excavated through rock which is in a wedge between faults 4 and 5. Movement on the two faults during the Siluro-Devonian and Tertiary times has probably broken this wedge of rock into a closely jointed and fractured mass; the movement has probably caused the rock mass to be strained and the joint surfaces to be partly separated. However many of the joints in the drill core from GST 16 and GST 17 have been partly cemented with silica. Where the cementing is incomplete, cavities up to 70 mm but generally less than 5 mm diameter have been formed (drill hole GST 16).

Most of the rock mass is expected to be closely jointed (10-30 cm) and fairly loose with some fractured zones. Areas where joints have been cemented will effectively be wider jointed (30-60 cm) and tight. Clay seams and 'greasy backs' are not expected in the rhyolite although there may be some, especially approaching the contact with the purple rhyodacite.

3.1.2.3 Groundwater inflows

The rock mass is very permeable. Water-pressure test losses in GST 17 were up to 25 lugeons and GST 16 lost all drilling water at one level. GST 17 flowed initially at 1.6 m³/hr and decreased to about 0.5 m³/hr. When GST 17 was drilled, the water-level in GST 16 fell 7 m in one week.

Water is contained in open joints and fractured zones and in the small cavities mentioned above. When these are intersected during excavation, water inflows generally less than 5 m³/hr, but possibly up to 20 m³/hr in a few zones, will enter the tunnel initially.

3.1.2.4 Excavation properties

Effect of engineering properties. The Shore Hardness and the UCS of the green rhyolite are higher than for the dacites in the upper part of the Walker Volcanics. This suggests that drill penetration will be slower and drill wear rate higher.

Explosive quantities per volume will probably be similar to or less than for dacites in the upper part of the Walker Volcanics because the close spacing of joints will offset the higher UCS of the rhyolite.

Effect of geological properties of the rock mass. The closely spaced joints will cause the rock mass to break into fragments generally less than 30 cm diameter when blasted.

Areas where the rock is closely jointed and loose will require steel-set support with timber lagging. About 40 percent of this section is expected to need steel-set support.

In loose sections, overbreak will depend mainly on tunnelling methods (explosive quantities, drilling accuracy), and how quickly support is erected to retain the loose rock.

In the sections where joints are cemented, blocks generally less than 60 cm may fall, in, leaving voids beyond the C-line. Rockbolts may be more efficient and economical than steel sets in supporting rock of this nature.

Effect of groundwater inflows. The water inflows expected should not cause any delay in excavation progress.

This section of tunnel is expected to yield the largest water inflows. Special attention should be given to making a watertight concrete lining in this section. As this section only extends 150 m from the portal some consideration should be given to providing a drain below the tunnel lining.

Combined effect of all parameters:

- (a) Rock condition number will be mostly 4, with some 3.
- (b) About 40 percent of this section is expected to need steel-set support with partial timber lagging.
- (c) Amount of overbreak could vary greatly in this section, but will depend mainly on tunnelling method.
- (d) Advance rate will be slowed by (i) jamming of drill stems in loose rock, and (ii) necessity to erect steel-set support.

3.1.2.5 Contact, stn 46+10 (drill hole GST 16)

The contact between the green rhyolite and purple rhyodacite in the core from GST 16 could be either intrusive or conformably extrusive. No major defect is known to exist at the contact. Water inflows, overbreak and support are not expected to be significantly different at the contact than in the rocks on either side of the contact.

3.1.3 PURPLE RHYODACITE: STN 43+80 TO APPROX. STN 46+10 (DRILL HOLES GST 15, GST 16)

3.1.3.1 Engineering properties of the rock substance

Sample location	UCS (MPa)		Point Load Strength (MPa)			Mean hardness (Shore units)	
	No. of samples	Range Average	Samples successfully tested	Is(50)			UCS equivalent
				Range	Average		
GST 15	3	CORE TOO FRACTURED	NOT TESTED				
GST 16		all samples failed prematurely on joints	6	2.9-6.1	4.6	110	
						78	

The rock was too fractured and seamy to enable samples of required size to be collected for testing although 6 successful point load and three Shore Hardness tests were carried out on GST 16 core.

3.1.3.2 Geological properties of the rock mass at tunnel level (Plate 8)

Weathering. The rockmass at tunnel level is below the zone of weathering, but the rock has been altered by moving groundwaters. Degree of alteration is probably variable; much of the rock is probably equivalent to highly to moderately weathered dacite, with zones of slightly weathered and seams of extremely weathered material.

Seismic velocity. The seismic velocity of 3700 m/sec for this material indicates that although the rock is moderately weak the bulk density is high because there are few voids or open joints; most joints are clay-filled.

Defects. The purple dacite is part of the wedge between faults 4 and 5. Movement of the faults during Siluro-Devonian and Tertiary times has caused the rock mass to be strained and the joint surfaces to be partly separated, allowing water to penetrate the rock mass and cause alteration.

The rock mass is expected to be closely jointed (10-30 cm), with most joints clay-filled. Clay-filled, crushed, sheared, and fractured zones are likely.

3.1.3.3 Groundwater inflows

Water pressure tests in GST 15 and in the purple rhyodacite in GST16 showed negligible water losses. Most of the rock mass is expected to be relatively impermeable because most of the defects are clay-filled.

Any water inflows are expected to be small (probably less than 3 m³/hr). Water will seep and drip from clay-filled fractured and sheared zones.

3.1.3.4 Excavation properties

Effect of engineering properties. The UCS tests of the purple rhyodacite suggests that much of the rock has the strength of highly to moderately weathered rock. Drill penetration will be rapid and drill wear rate low.

Effect of geological properties of the rock mass. Blasting will break the rock into fragments generally less than 20 cm diameter because the rock is weak and closely jointed.

Probably 70-100 percent of this section will need steel-set support with timber lagging. In some places considerable weight may be imposed on the sets, and spacing less than 1 m may be required.

Overbreak will depend mainly on efficiency in installing support. Clay-coated defects with dips up to 45° against tunnel drive could cause several metres of overbreak in a few places. Generally overbreak will be less than 60 cm.

Effect of groundwater inflows. Groundwater inflows are expected to be small. However the action of the groundwater on the clay-filled defects will reduce the stand-up time of the rock mass.

Combined effects of all parameters:

- (a) This is expected to be the most difficult section of the tunnel to excavate and support.
- (b) Rock condition number will be mainly 4, but long sections of 5 are possible.
- (c) Expect 70 to 100 percent steel-set support is expected, which sets spaced less than 1 m in some zones.
- (d) Overbreak will generally be less than 60 cm, but could be in excess of 1 m in some zones where poorly oriented defects occur.
- (e) Advance rate will be slowed by necessity to erect support and sometimes to fill large overbreak with timber lagging. It may be more economical to use hand-held machines for tunnelling some sections.

3.1.3.5 Contact, stn 43+80; faults 5 and 6 (drill hole GST14)

The contact between the purple rhyodacite and the dacite of the upper part of the Walker Volcanics is a fault zone (faults 5 and 6) which probably extends for about 150 m along tunnel line. Drill hole GST14 reveals that the dacite in the fault zone is closely jointed and fractured. Joints are generally spaced less than 10 cm, and are coated with calcite and chlorite and are slickensided. Most joint surfaces are greasy, having from 1 to 10 mm of clay. Clay seams up to 10 cm thick are spaced less than 30 cm in places in GST14.

Rock condition in the tunnel is expected to be 4 to 5.

When blasted the rock will mostly break up into a coarse gravel with few fragments larger than 20 cm diameter.

80 to 100 percent of this section is expected to need steel-set support.

Water inflows are expected to be similar to the remainder of the section from 43+00 to 40+20.

3.1.4 WALKER VOLCANICS, LOWER SEQUENCE

3.1.4.1 DACITE AND TUFFACEOUS SANDSTONE

(Stn 37+30 to 40+20: Drillholes GST 11 and 12)

(Stn 15+20 to 25+00: Drillholes GST 7 and 1)

The rock in these sections consists of dacitic welded tuffs and agglomerates, with sills and dykes of dacitic composition. The northern section (15+20 to 25+00) also contains interbeds of tuffaceous sandstone and some minor shales. The main section of shale in the Walker Volcanics is discussed in the following section.

Samples of reworked tuff give lower strength results than the welded tuff and agglomerates. This accounts for the larger range of values and the lower mean on GST11 and GST 12. UCS of welded tuffs is greater than 200 MPa. UCS of reworked tuff is less than 120 MPa. There is a complete gradation between these rock types, so UCS of the volcanics in this section is expected to range from about 100 to 250 MPa.

3.1.4.1.1 Engineering properties of the rock substance

Sample location	UCS (MPa)			Point load strength (MPa)				
	No. of samples	Range	Average	Samples successfully tested	Is(50)		UCS equivalent	Mean hardness (Shore units)
					Range	Average		
GST7 (reworked tuff)	-	-	-	13	3.2-5.3	4.4	110	
GST7 (welded tuff)	3	203-205	204	11	6.5-15.8	9.8	220	73
GST 11	3	152-164	157	10	4.1-7.4	6.2	150	74
GST 12	3	97-105	102	12	3.4-10.6	7.2	170	70
Locality E1	-	-	-	10	7.1-14.0	10.5	250	

3.1.4.1.2 Geological properties of the rock mass at tunnel level
(Plates 6 and 7)

Weathering. These sections of tunnel will be excavated through fresh rock.

Seismic velocities. Bedrock velocities of 4400 to 5100 m/sec were recorded in this rock type except for 80 m of 3300 to 3400 m/sec between stn 39+40 to 40+20. The higher velocities represent tight rock. The 3300 to 3400 m/sec velocities lie close to fault 3 and probably represent partly fractured and sheared rock.

Defects. Most of the rock mass is expected to be tight. Joints are generally spaced 0.3 to 1 m but are wider in some places and are commonly cemented with calcite. Many joint surfaces are coated with chlorite and slickensided. Flow-banding is apparent in some places but this is not expected to be a weakness. Some narrow fractured and/or sheared and crushed zones can be expected.

In the section from 37+30 to 40+20, GST12 revealed good sound rock and GST11 revealed slightly weaker and more jointed rock with some crushed seams (clayey gravel) generally less than 20 cm wide and spaced 1 to 6 m in the drill core.

3.1.4.1.3 Groundwater inflows

The water-table is about 30 m above tunnel level. Water-pressure test losses in drill holes GST12, GST11, and GST7 were insignificant, which indicates that the permeability of the rock mass is low.

Most of this section will be dry or damp. Most open joints and fractured zones will drip or seep but some will yield initial inflows less than 1 m³/hr. Flows up to 10 m³/hr are possible but unlikely.

3.1.4.1.4 Excavation properties

Effect of engineering properties. The Shore Hardness of this dacite is less (i.e., softer) than the Walker Member dacite. UCS values range from about 100 MPa for the reworked tuffs, up to values similar to those from the dacite of the upper part of the Walker Volcanics (200 MPa) for the densely welded tuffs. Drill penetration, drill wear rate, and explosive quantities for dacites with UCS near 200 MPa will be similar to the dacite in the upper part of the Walker Volcanics; the softer dacite will be more easily and economically excavated.

Effect of geological properties of the rock mass. When blasted, the reworked (softer) dacite is expected to break across the rock fabric more readily than the harder dacite and the dacite in the upper part of the Walker Volcanics. Away from prominent defect zones, joints will be tight and spaced generally 0.3 to 1 m.

About 10-15 percent of the dacite in these tunnel sections is expected to need steel-set support. In most of this rock type overbreak will generally be less than 30 cm beyond C-line; up to 60 cm may occur in blocky zones. Overbreak in sheared or fractured rock will generally be less than 1 m, but may be greater than 1 m (rare).

Effect of groundwater inflows. No major groundwater inflows that could significantly slow excavation are expected.

Combined effects of all parameters:

- (a) Drill penetration and wear rate, and explosive quantities for dacites with UCS near 200 MPa, will be similar to those for the Walker dacite; the softer dacite (reworked tuffs) will be more easily and economically excavated.
- (b) About 10-15 percent of the dacite in these sections is expected to need steel-set support.
- (c) No major groundwater inflows that could significantly slow excavation progress are expected.
- (d) Rock condition will be mostly 2 to 3, with some 4.
- (e) Average excavation rate is expected to be slightly faster than in the Walker dacite.
- (f) Overbreak is expected to be minor along most of this section; a good tunnel profile.

3.1.4.1.5 Contact with granite porphyry, stn 37+30

The contact with the granite porphyry (stn 37+30 approx.) is possibly intrusive or possibly faulted. Drill core from GST24 revealed that the granite porphyry is closely jointed, and joints are strongly slickensided. GST11 revealed that the rock is closely jointed and that there are some crushed seams.

The contact is expected to be closely jointed and fractured. Joints will be strongly slickensided, and coated with chlorite and calcite. There may be some clay seams and zones of clay-coated joints. Parts of the rock mass will be moderately loose.

3.1.4.2 SHALES: STN 25+00 TO 26+20 (DRILL HOLES GST7, GST1)

3.1.4.2.1 Engineering properties of the rock substance

Sample location	UCS (MPa)			Point load strength (MPa)			UCS equiv.	Mean hardness (Shore units)
	No. of samples	Range	Average	Samples successfully tested	Is(50)			
					Range	Average		
GST7	3	>111 - >197	>144	9	1.6-3.7	2.3	55	68
				NOT TESTED				

All UCS samples of shale failed prematurely along an incipient fracture in the test sample.

3.1.4.2.2 Geological properties of the rock mass at tunnel level (Plate 7)

Weathering. The shales at tunnel level are expected to be fresh. However, thin interbeds - beds of tuffaceous sandstone or siltstone - may be decomposed to clay seams in some areas.

Seismic velocities. Bedrock velocities in the sequence of rocks containing the shales are 4200-4400 m/sec, but it is not possible to determine if these velocities are in the shale or in the interbedded dacites since the seismic refraction method cannot pick up a lower velocity below a higher velocity.

No seismic refraction profiling was done in the NSW Electricity Commission Substation (stn 18+20 to 24+20).

Defects. Joint spacing in most of the shale is expected to be tight. However, some tight folding has been seen in surface outcrops; tightly folded shales at tunnel level may be very closely jointed.

GST7 revealed that the bedding planes were very tight and were not a weakness in the rock. However, it is expected that in places the shale will tend to part on the bedding planes. In some places there may be clay seams on bedding planes and in joints. In some places, thin beds (0.1-0.3 m thick) of tuffaceous sandstone or siltstone may be decomposed to clay.

The general dip of the shale is $20^{\circ}\text{W}/160^{\circ}$, but this is likely to be variable owing to small-scale folding.

No major faults or defect zones have been detected, but some may be present where the Electricity Substation prevented investigation.

3.1.4.2.3 Groundwater inflows

The shale is expected to be mostly tight and impermeable. There may be some open joints or fractured zones - especially near contacts - that will yield some initial inflows but these are expected to be generally less than $3 \text{ m}^3/\text{hr}$, although larger inflows are possible.

3.1.4.2.4 Excavation properties

Effect of engineering properties. Drill penetration will be faster and drill wear rate less than in the dacites, and is expected to be about average for hard shale.

Effect of geological properties of the rock mass. The shale will generally fragment into pieces less than 10 cm diameter. Most of the shale will be tight and a good tunnel profile could be produced. In areas where the rock parts easily on bedding planes, 'slabby' conditions may result, producing overbreak generally less than 50 cm. Regular barring-down of flaking slabs will generally be sufficient in these areas but some zones may need rockbolts.

Some badly oriented defects may cause in excess of 1 m overbreak (rare).

Any fractured or sheared zones that dip unfavourably or that are wider than a few metres will need steel-set support. In folded zones with decomposed thin sandstone beds or clay seams on bedding planes, some steel-sets may be required, especially where the dip is against the direction of tunnel drive.

Effect of groundwater inflows. No major groundwater inflows that could significantly slow excavation progress are expected.

Combined effects of all parameters:

- (a) Drill penetration will be fast and drill wear rate low.
- (b) Explosive quantities will be low.
- (c) Rock condition will be mainly 2 to 3, with some 4.
- (d) About 15 percent steel-set support and about 5 percent rock-bolts are expected in the shale.
- (e) Overbreak will be minor in most of the section.
- (f) No groundwater inflows that could significantly slow excavation progress are expected.

3.1.4.2.5 Granite-shale contact between stn 26+00 and 28+00

The contact could cross the tunnel anywhere between stn 26+00 and stn 28+00. It is possible that the contact could follow the tunnel for up to 200 m, but this is considered very unlikely.

Drill hole GST1 revealed that the contact was fractured, open-jointed, and limonite-stained; clay seams are possible. Rock condition at the contact is expected to be 4 to 5. Steel-set support will probably be required if the contact occurs in the tunnel for more than about 3 m.

3.1.4.2.6 Granite contact, stn 15+20 approx.

The contact between the granite porphyry and the lower part of the Walker Volcanics has not been intersected by any drill hole and cannot be seen at the surface. Its exact position, orientation, width, and condition are therefore not known. Rock condition at this contact will probably be similar to conditions at the granite-shale contact.

3.1.5 GRANITE PORPHYRY

(Stn approx. 13+00 to 15+20: Drillholes GST8, GST6)

(Stn approx. 26+20 to 37+30: Drillholes GST1, GST23, GST9,
GST22, GST24)

3.1.5.1 Engineering properties of the rock substance

Sample location		UCS (MPa)		Point load strength (MPa)			Mean hardness (Shore units)	
	No. of samples	Range	Average	Samples successfully tested	Is(50)			UCS equivalent
					Range	Average		
GST23	3	188-263	232	10	5.8-9.7	8.4	200	98
GST9	3	125-237	177	7	5.5-10.1	7.6	180	93
GST24	2	178-201	190	11	2.4-8.4	5.6	130	85

3.1.5.2 Geological properties of the rock mass at tunnel level

Weathering. These sections of the tunnel will be excavated through fresh granite porphyry.

Seismic velocities. Bedrock velocities range from 2000 to 5800 m/sec, but along most of the section range from 4000 to 5000 m/sec. Narrow sections with velocities less than 3000 m/sec, mainly between stns 30+50 and 32+00, coincide with three sets of intersecting photo-lineaments (Plates 4 and 7). These probably represent zones of sheared and fractured rock.

Defects. Most of the rock mass will be tight. Joints are generally spaced 0.3 m to 1 m and often wider. Along most of the section, joints will be tight and often cemented with calcite. There will be some sections where joints are open and not cemented. Photo-lineaments and seismic profile indicate that some fractured and/or sheared and crushed zones can be expected. Most of these will be less than 20 m wide.

3.1.5.3 Groundwater inflows

The water-table is generally 30 to 40 m above tunnel crown. Most of these sections of tunnel will be dry to damp. Most open joints and fractured zones will seep or drip, but some may produce initial inflows less than 3 m³/hr; flows up to 10 m³/hr are possible.

3.1.5.4 Excavation properties

Effect of engineering properties. UCS values are about the same as for the dacite from the upper part of the Walker Volcanics; Shore hardness values of the granite are slightly higher. Unlike the dacites, the granite porphyry does not have the fine-grained siliceous groundmass which is considered responsible for the high wear rate of the drill steels. Balancing these factors it is considered that drill penetration and wear rate will be about the same as for the dacite from the upper part of the Walker Volcanics.

Effect of geological properties of the rock mass. Slightly more explosives may be needed in the granite porphyry than in the dacite from the upper part of the Walker Volcanics because the granite is more widely and tightly jointed.

About 10 percent of the granite porphyry will need steel-set support, and probably most will be confined to individual sections 6 to 20 m long between stns 30+50 and 32+00.

Along most of this section a good tunnel profile could be produced with overbreak generally less than 30 cm beyond the C-line. Where joints are open, blocky conditions may result with generally less than 60 cm of overbreak. Overbreak in sheared or fractured rock will generally be less than 1 m but may be greater than 1 m (rare).

Effect of groundwater inflows. No major groundwater inflows that could significantly slow excavation are expected.

Combined effects of all parameters:

- (a) Excavation rate is expected to be the same as for the dacite in the upper part of the Walker Volcanics.
- (b) Drill penetration and wear rate is expected to be similar to the dacite in the upper part of the Walker Volcanics.
- (c) Rock condition will be mainly 2 to 3, with some 4.
- (d) About 10 percent of this section is expected to require steel-set support.
- (e) Overbreak is expected to be minor over most of this section, resulting in a good tunnel profile.
- (f) No groundwater inflows that could significantly slow excavation progress are expected.

3.1.5.5 Contact, fault 2, stn 13+00 approx.

Fault 2 crosses the tunnel line at about 90°. The exact width, orientation, and condition of the faulted contact is not known. Core recovered from drill holes GST 6 and GST 8 was generally closely jointed, fractured, and sheared. It appears as if fault 2 is comprised of several sheared and fractured zones, separated by zones of harder, less weathered and fractured rock, but nevertheless rock that would require support. Information available suggests that the faulted contact could extend for up to 100 m along tunnel line (stn 13+00 to 14+00) and probably all of this would require steel-set support. Moderate initial water inflows can also be expected (heavy limonite staining of fractures was observed in the core recovered from GST 6 and GST 8).

3.1.6 WILLOW BRIDGE TUFF: STN 1+70 TO 13+00 (DRILLHOLES GST5, GST 3, GST4, GST2)

3.1.6.1 Engineering properties of the rock substance

Sample location	UCS (MPa)			Point load Strength (MPa)			UCS equiv.	Mean hardness (Shore units)
	No. of samples	Range	Average	Samples successfully tested	Is(50)			
					Range	Average		
GST5	3	185-291	245	16	8.7-15.7	11.2	270	100
GST3	2	294-492	393	10	9.5-15.4	12.1	290	102
GST4	2	173-273	223	10	5.8-8.8	7.4	180	98
GST2	-	-	-	21	9.0-11.3	9.9	240	-
Locality J1	-	-	-	10	8.6-16.5	12.6	300	-
Locality K1	-	-	-	10	11.0-14.0	12.9	310	-
Locality K2	-	-	-	10	10.0-13.5	12.0	290	-
Locality K3	-	-	-	6	10.0-16.0	12.3	300	-

3.1.6.2 Geological properties of the rock mass at tunnel level

Weathering. Most of this section is expected to be tunnelled through fresh dacites. The seismic profile (Plate 6) suggests that the zone of weathering may extend down to near tunnel level from stn 8+00 to 9+00; however the correlation of seismic results with drill core indicates that the seismic interpretation may have placed the refractor too deep; if this is so, then the rock at tunnel level will be fresh.

Seismic velocities. Bedrock velocities of 4500-5600 m/sec were recorded for most of this section. Velocities down to 2600 m/sec were recorded between 10+10 and 11+30. The lower velocities probably indicate the presence of zones of fractured and/or sheared and crushed rock.

Defects. Drill holes GST3 and GST5 and the bedrock velocities of 4500-5600 m/sec indicate that the rock mass along most of this section of tunnel will be very tight; joints are expected to be spaced greater than 1 m and tightly closed or cemented with calcite.

Drill holes GST2 and GST4 revealed that in some sections the joint spacing is commonly 10-30 cm, and in some places the rock mass is fractured. Calcite and epidote veins are prolific; as they generally broke during investigation drilling, they would probably break when blasted.

No major faulted zones were detected during investigation drilling, but the seismic and photo lineaments (Plates 2 and 3) indicate that some narrow zones of very closely jointed and/or sheared and crushed rock will probably be intersected. They are expected to be generally less than 5 m wide, but a few may be up to 20 m wide. These zones will have various orientations but the most common ones will probably be near-vertical and strike parallel to the two major photo-lineament directions, i.e., 055° and 145°.

In places there may be joints or narrow sheared and fractured zones parallel to bedding (35°SW/135°).

3.1.6.3 Groundwater inflows

The water-table is about 20-30 m above tunnel level. Water-pressure test losses in drill hole GST3 were zero, and in GST4 and GST5 the results were unreliable. The permeability of most of the rock mass is low.

3.1.6.4 Excavation properties

Effect of engineering properties. This is the hardest and strongest rock type that will be encountered. UCS values range up to 492 MPa and average about 290 MPa. During investigation drilling wear rate of diamond-drill bits was extremely high (some lasting for only 45 cm), and drill penetration extremely slow (1½ hours to drill 70 cm with a new diamond bit). During excavation, drill penetration is expected to be extremely slow, drill wear rate very high, and explosive quantities per cubic metre of rock removed also very high.

Effect of geological properties of the rock mass. The rock hardness and strength and the wide spacing and tightness of joints will require the use of larger quantities of explosive to fragment the rock satisfactorily.

The photo lineaments (Plates 2 & 3) indicate that most of the sheared and fractured zones and the major joints will be vertical and will intersect the tunnel at about 45°. These defects should not require support except for a few that may be more than 3 m wide. About 10 percent of this section is expected to need steel-set support, and this will be mainly in fractured and sheared zones from 6 to 20 m wide.

Joints and fractured zones parallel to bedding, dip with tunnel drive and should not cause much overbreak or require support.

Along most of this section a good tunnel profile could be produced with overbreak generally less than 30 cm. Where joints are open, blocky conditions may result with generally less than 60 cm of overbreak. Overbreak is sheared, and fractured rock will generally be less than 1 m, but may be greater than 1 m (rare) where clay-coated defects are unfavourably oriented.

Effect of groundwater inflows. Most of this section will be dry to damp, with seepages and drips in places. Some open joints and fractured zones will yield initial inflows generally less than 3 m³/hr. Flows in excess of 10 m³/hr are possible but unlikely.

Combined effects of all parameters:

- (a) Excavation rate is expected to be slow.
- (b) Drill penetration will be slow and drill wear rate high.
- (c) Explosive quantities will be high.
- (d) Rock condition will be mainly 2 to 3, with some 4.

- (e) About 10 percent of this section is expected to need steel-set support.
- (f) Overbreak is expected to be minor over most of this section, resulting in good tunnel profile.
- (g) No groundwater inflows that could significantly slow excavation progress are expected.

3.2 PORTALS

3.2.1 WINDOW BEND, NORTH PORTAL: STN 47+40. DRILL HOLE GST 17

3.2.1.1 Suggested portal position

Stn 47+40: this location would avoid the main fault zone of fault 4, which intersects tunnel line between stn 47+60 and stn 47+45.

3.2.1.2 Conditions at portal face

Fresh to fresh stained closely jointed (10-20 cm) and loose green rhyolite will occur from invert to about 3 m above portal crown, and grade into loose variably weathered rock and rubble towards the ground surface, which is 11 m above portal crown. The rock face above portal crown will need to be battered and stabilized with rockbolts and mesh.

In the tunnel, closely jointed and loose ground requiring discontinuous sections of steel-set support with timber lagging can be expected to stn 46+00.

3.2.1.3 Conditions of open cut

The open cut will be in water-saturated loose scree and slopewash overlying fractured and sheared rock; heavy clay will occur in the central section of the fault zone. A low batter slope will be required to restrict slumping especially on the eastern wall of the open cut.

3.2.1.4 Groundwater inflows

Near the portal and for the first 100 m of tunnel, water inflows initially up to 20 m³/hour during excavation, but decreasing to less than 3 m³/hour within a few weeks, can be expected.

3.2.2 WINDOW BEND, SOUTH PORTAL: STN 48+90. DRILLHOLE GST 18

3.2.2.1 Suggested portal position

Stn 48+90

3.2.2.2 Conditions in the open cut

Rock conditions in the open cut should be similar to those in the existing open cut at Pine Ridge west portal if similar excavation procedures are used. Mapping, seismic results, and diamond drilling indicate that there is about 3 m of highly weathered dacite overlying moderately to slightly weathered dacite.

The rock mass is closely jointed. Many joints are coated with 1-10 mm of clay. Some crushed seams and/or weathered seams up to 20 cm thick are expected. The most prominent joint direction is $20^{\circ}\text{S}/110^{\circ} - 130^{\circ}$ (spaced 10-30 cms), which is a favourable orientation for stability in the portal face and the walls of the open cut, but there are probably other joint orientations (spaced generally > 30 cm) that may produce a few unstable blocks of rock; these may need to be bolted or barred down. With the exception of the few unstable blocks mentioned above, near-vertical slopes should be stable in moderately weathered rock below about 4 m if the cut is carefully pre-split.

3.2.2.3 Conditions at the portal

At stn 48+90, the tunnel crown is about 9 m below the surface. The portal will be in moderately to slightly weathered closely jointed dacite with defects as described above.

Rockbolts and mesh will probably be required to stabilize the face above the portal.

In the tunnel, blocky and seamy ground requiring discontinuous sections of steel support with timber lagging can be expected to about stn 49+90.

3.2.2.4 Groundwater inflows

Only minor seepages of groundwater are expected in the open cut and portal areas.

3.2.3 SOUTH PORTAL (LMWQCC): STN 57+55. DRILL HOLE MV7

3.2.3.1 Suggested portal position

Stn 57+55. On geological grounds there is no reason to shift the location of the portal face inwards (northwards) from the existing northeast side of the access road-cut to Pine Ridge tunnel.

3.2.3.2 Conditions in the open cut

If the portal is at stn 57+55 then the only open-cut excavation necessary will be deepening of the existing Pine Ridge access road down to invert level, and removal of rock between the portal and the connection to the LMWQCC.

In the area of the portal the existing cut shows about 2.5 m of extremely to highly weathered dacite overlying moderately to slightly weathered dacite.

There are four prominent sets of continuous joints commonly coated with 1-20 mm of clay:

- | | |
|--|------------------|
| 1. 60° - 70° SW/ 110° - 130° | spaced up to 4 m |
| 2. 80° - 90° S/ 065° - 085° | " " |
| 3. 60° W/ 015° - 045° | " " |
| 4. 20° N/ 070 (bedding) | " 0.3-0.6 m. |

Stability of the portal face and northeast wall of the open cut will be affected by Set 1 which dips out of the rock face. A batter slope of about 60° and some rockbolts will probably be required to stabilize the face.

If the open cut is extended north of stn 57+55 along tunnel line, then joint sets 2, 3, and 4 may cause failure of blocks of rock on the resulting southeast wall of the cut unless the slope is battered or stabilized with rockbolts.

3.2.3.3 Conditions at the portal

At stn 57+55 the tunnel crown is about 11 m below the natural surface. The portal will be in slightly weathered to fresh dacite with defects as described above. Rockbolting of the portal face in a direction normal to joint set 1 should provide a stable portal. Steel mesh may be required above the portal to stabilize any loose rubble.

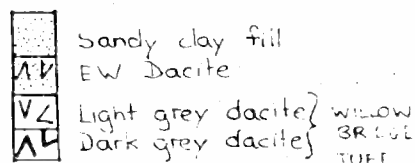
In the tunnel the four joint sets will intersect to form blocks that may fall out of the crown and walls. Steel sets will be required near the portal. Northwards beyond the steel sets, rockbolts will probably be needed to secure some blocks from falling out.

3.2.3.4 Groundwater inflows

Only minor seepages or very small inflows are expected from the portal face and the first 50 m of tunnel.

SHAFT C GEOLOGY (STN 2+90, DRILL HOLE GST. 5)

FIGURE 4



Scale $\frac{V}{H} = 1$ $\frac{2}{1} \frac{1}{0} \frac{2}{1} \frac{4}{1}$

300 Seismic Velocity m/sec
— Seismic refractor

▼ Water level in drill hole
— J Major joint orientation

Note detailed geology shown on log of drill hole GST 5

RL (m)

558 —

556 —

554 —

552 —

550 —

548 —

546 —

554 —

542 —

540 —

538 —

536 —

(Invert)

Seismic
m/sec

400

900

1300

4700

GEOLOGY	EXCAVATION CONDITIONS	PREDICTED SUPPORT	GROUNDWATER INFLOWS
Sandy clay fill	Excavation by large cack-hoe. Any boulders may need to be blasted.	Slopes will need to be battered to about 1:1. Vertical slopes will need steel ring support with continuous timber lagging.	None expected. Some seepages after heavy rain.
EW Dacite (soil properties) Possibly some SW-FS boulders.			
MW-FS Dacite. Some HW seams. Joints mostly dip 30° and 60°, spaced 30-50 cm. Most are limonite stained or slightly weathered. Some are slightly open.	The rock is hard and strong	Probably some support. Random rockbolts and/or rockbolts and mesh may be sufficient.	Probably some seepages and/or minor inflows initially; decreasing after excavation.
Mainly FS Dacite; possibly some EW-HW seams near top. Rock substance very hard and very strong. Joints oriented as above, mostly spaced 30 cm - 2 m. Joint surfaces mostly rough and tight. Some weakly cemented with calcite. Some are open and limonite stained.	No major defects that could cause instability are known. Drill penetration slow. Drill wear rate high. Explosive quantities high.	Probably none necessary, but some random rock bolts possible.	Similar to above but inflows up to 10 m³/hr are possible but unlikely. Some minor inflows near invert may persist throughout construction.

SHAFT 1 GEOLOGY - STN 498-711

Scale $\frac{V}{H} = 1$ 2 0 2 4m

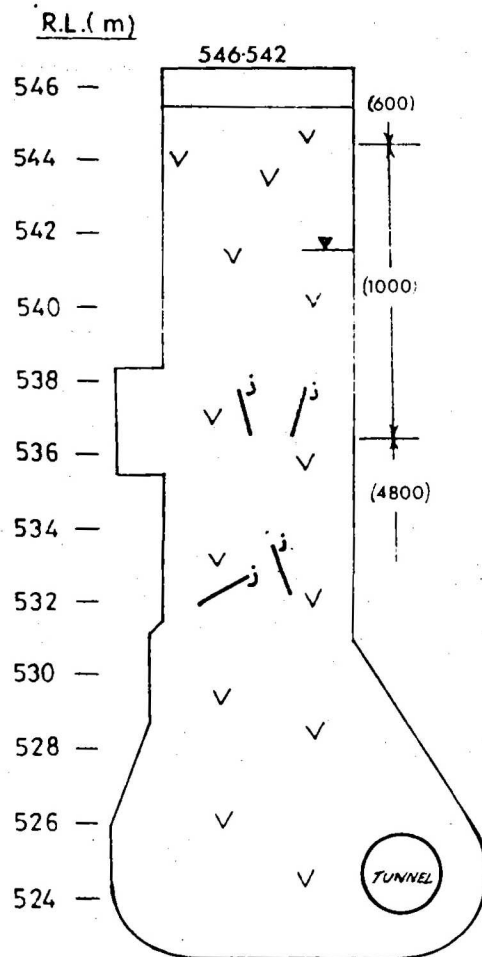
▼ Water table

(300) Seismic velocity (m/s)

— Major joint orientation

— Velocity boundary

NOTE: Detailed geology shown on log of drill hole GST 3



INVERT 523.716

GEOLOGY	SHAFT CONDITIONS	PREDICTED SUPPORT
SOIL		
DACITE Extremely weathered. Water table at 6m below present ground surface.	Rock mass very soft and weak. Easily excavated by backhoe. Minor water inflows possible especially following rain.	Steel rings at 1m. centres with complete timber lagging below top structure.
DACITE - Mainly Fresh stained. Fresh from R.L. 525.5. Light grey with some quartz epidote veins.	Rock mass is very hard and strong. Widely jointed and tight. Weathered seams 7-10cm wide at R.L. 530 and at R.L. 526.5. Minor water seepage only. Shaft - tunnel junction in competent rock.	NO SUPPORT REQUIRED Shaft - tunnel junction should not need support.

SHAFT 2 GEOLOGY - STN 1712-267

Scale $V/H=1$ 2 0 2 4m

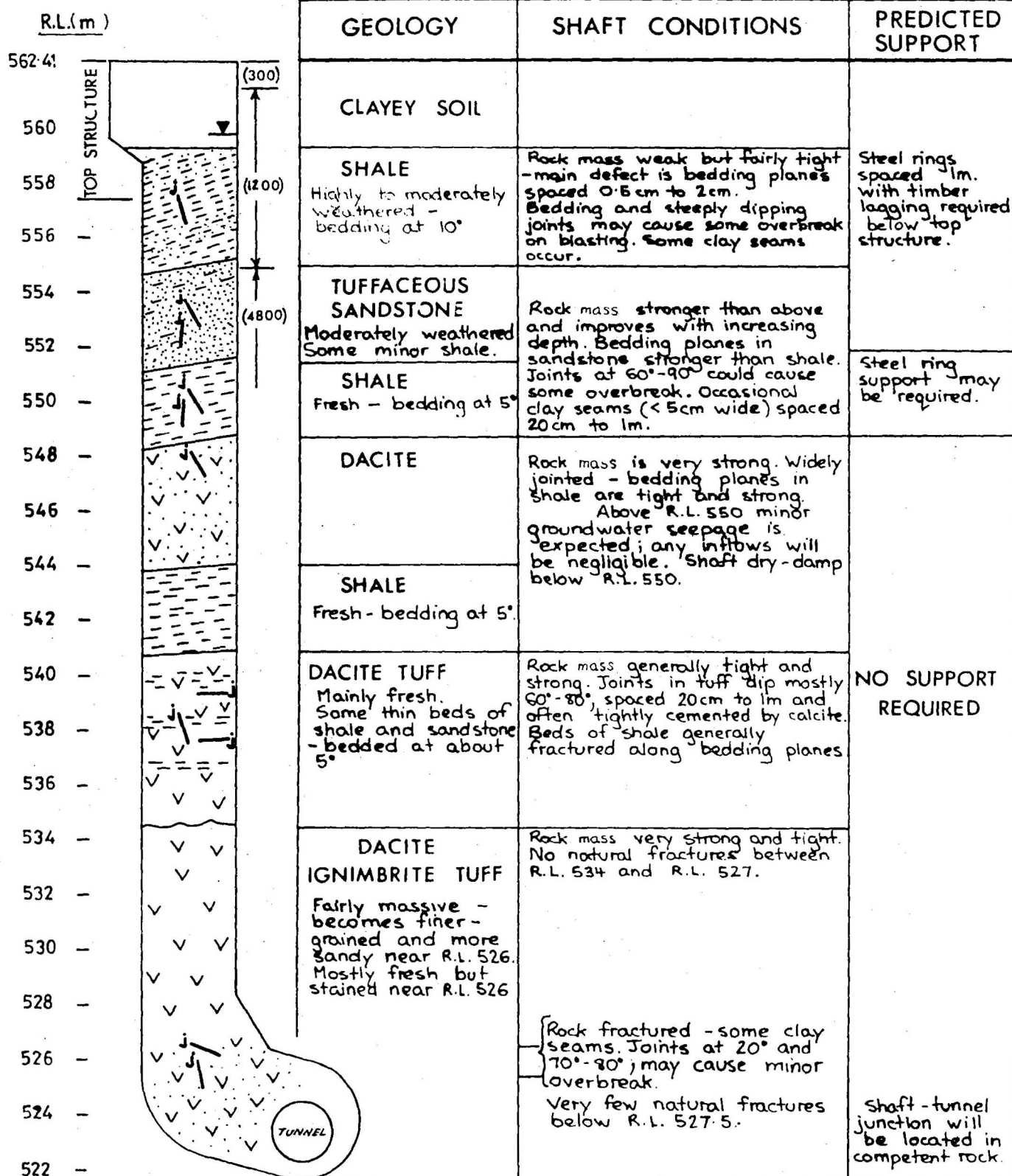
▼ Water table

(300) Seismic velocity (m/s)

— Velocity boundary

— Major joint orientation

NOTE: Detailed geology shown on log of drill hole GST 7



SHAFT 3 GEOLOGY - STN 3314.694

FIGURE 7

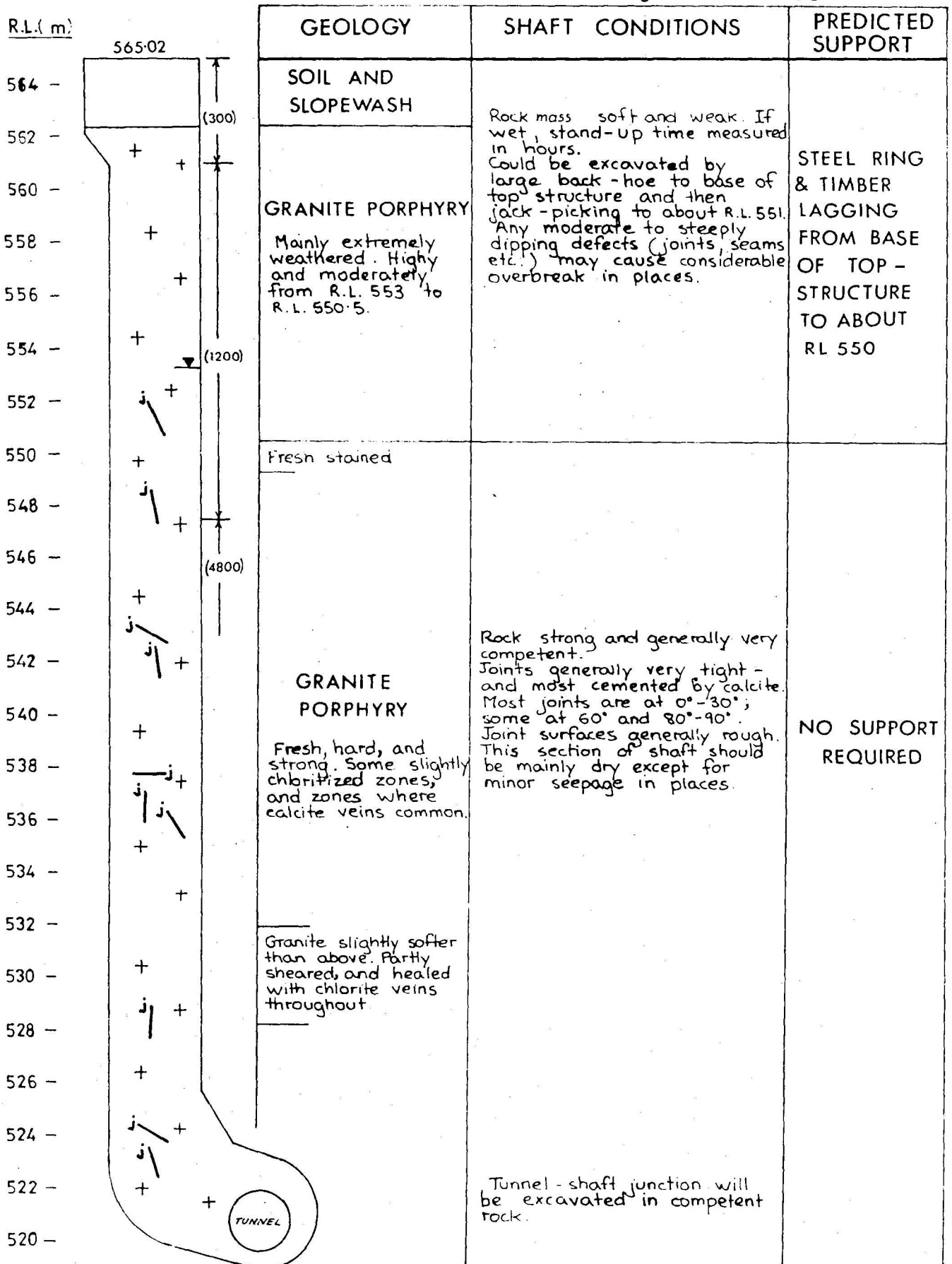
Scale $V/H=1$ 2 0 2 4m

(300) Seismic velocity (m/s)
— Velocity boundary

▼ Water table

— Major joint orientation

NOTE: Detailed geology shown on log of drillhole GST 9



INVERT 519.020

3.3 SHAFTS

3.3.1 SHAFT C: STN 2+90 (DRILL HOLE GST5, FIGURE 4)

3.3.1.1 Geology

4.5 m of sandy clay fill and extremely weathered rock (to RL 553) overlies moderately weathered to fresh-stained dacite with some highly weathered seams to RL 549. Below RL 549 the rock is mainly fresh-stained light to dark grey welded dacite (Willow Bridge Tuff).

3.3.1.2 Excavation conditions

Excavation by mechanical shovel without preblasting should be possible to RL 553; if any fresh boulders are encountered they may need to be blasted.

Below RL 553 the rock is hard and strong. UCS values obtained from GST5 core averaged 245 MPa (range 185 to 291 MPa). UCS values up to 492 MPa have been recorded in the same rock type from nearby drill holes. Average hardness is 100 Shore units. During investigation diamond drilling, drill penetration in the fresh dacite was very slow and drill bit wear rate very high. The same is expected with construction drilling. Explosive quantities will need to be high to fragment the rock satisfactorily.

Minor inflows can be expected below about RL 552, but will rapidly decrease to drips or seepage (which may increase after heavy rain). Below about RL 549, inflows up to 10 m³/hr are possible but will decrease fairly rapidly. Some minor inflows near invert may persist but will not be large enough to significantly slow construction.

3.3.1.3 Shaft support

Above RL 553 vertical slopes will need steel-ring support. Between RL 553 and RL 546, some steel-ring support may be required but rockbolts and mesh may be adequate to hold blocks formed by unfavourably oriented joints (possibly dipping at 30° and 60°). Below RL 549, support should not be required although any unstable blocks will require pinning with rock bolts.

3.3.2 SHAFT 1: STN 4+98.7 (DRILL HOLE GST3, FIGURE 5)

3.3.2.1 Geology

This shaft will be excavated in light grey dacite, which is extremely weathered to RL 537. Below RL 537 the dacite is mainly fresh. For engineering properties of the rock substance see section 3.1.6.1.

3.3.2.2 Excavation conditions

The rock mass is very hard and strong below RL 537, with UCS up to 490 MPa; no prominent defects that would cause excessive overbreak or shaft instability are known to occur.

Above RL 537 the extremely weathered dacite is soft and weak, and water inflows or seepages could result in slumping of the shaft walls unless quickly supported. The rock in this section of shaft would be soft enough to be excavated by a large backhoe.

Some groundwater inflow or seepage can be expected from the sharp contact between weathered and fresh dacite at RL 537. This section may need to be panned before the concrete lining is laid. Groundwater seepage may occur elsewhere from open joints or weathered seams.

3.3.2.3 Shaft support

Steel rings and complete timber lagging will be required from base of top structure to RL 537. Below RL 537, support will not be required unless any steeply dipping seams occur; rockbolts would provide adequate support.

3.3.3 SHAFT 2: STN 17+12.3 (DRILL HOLE GST7, FIGURE 6)

3.3.3.1 Geology

The shaft will be excavated through dacite (60%), shale (30%) and sandstone (10%). About 3 m of clayey soil overlies weathered shale bedrock.

3.3.3.2 Excavation conditions

Shale and sandstone. Bedding planes - the main defects - are nearly horizontal, and little overbreak or instability is expected to result from them. However, where the bedding planes are cut by prominent joints dipping into the shaft, some instability will result; rockbolts may be required to pin back loose blocks.

Dacite. Joints in the dacite are generally tight, and little overbreak or instability is expected.

Minor initial groundwater inflows may occur above about RL 550, but the shaft is expected to be generally dry. Panning groundwater inflows or seepages before concrete is laid may be necessary in places, although this is unlikely.

3.3.3.3 Shaft support

Steel-ring support (spaced 1 m to 1.5 m) with timber lagging is expected from base of top structure to about RL 552 m (10 m below ground surface) and possibly to 548 m. Poorly oriented joints producing unstable blocks of rock may need to be pinned with rockbolts.

3.3.4 SHAFT 3: STN 33+15 (DRILL HOLE GST 9, FIGURE 7)

3.3.4.1 Geology

The shaft will be excavated through granite porphyry; 2.5 m of soil and slopewash overlies weathered bedrock. The granite is fresh below RL 550 (14 m below ground surface).

3.3.4.2 Excavation conditions

The rock mass is soft and weak to RL 550. The shaft walls may become unstable in areas of groundwater seepage and along unfavourably oriented joints or clay seams. The rock is expected to become progressively harder and stronger below about RL 553.

Below about RL 550 the granite is essentially fresh and the contact with the weathered rock above is sharp. Shaft stability in the fresh granite will depend on the orientation and frequency of clay-coated joints and seams; no major defects are known to occur and no major wall instability is therefore expected. Overbreak is expected to be negligible in fresh rock.

The shaft will be damp below about RL 553. Any water inflow will be small and will be mainly confined to the weathering contact at RL 550. Panning water inflows or seepages before concrete is laid may only be necessary near RL 550. Water inflows through contraction cracks in the concrete lining should be confined to the crack closest to RL 550.

3.3.4.3 Shaft support

Steel-ring support will be required from base of top structure to about RL 551 (11 m). Support is not expected to be required below RL 551; however, if any unfavourably oriented defect occurs, rockbolts may be required to pin back the defect.

3.4 CONNECTION, SHAFT 1 TO EXISTING BELCONNEN TRUNK SEWER

3.4.1 OPEN-CUT EXCAVATION: STN 0+79 TO 2+90 (SHAFT C)

400-1100 m/sec material (probably extremely to highly weathered dacite) extends from the surface to below the bottom of the excavation along most this section; this can probably be excavated by a large backhoe without preblasting. However, the seismic profile indicates that 1500 m/sec material (probably moderately weathered dacite) extends above invert between stn 1+90 and 2+40, and some blasting or jack-picking will be necessary. Boulders of fresh dacite (generally less than 1 m but up to 3 m in diameter) surrounded by extremely weathered dacite occur in the area; if encountered in the trench they may have to be blasted or jack-picked.

Groundwater inflows. No water inflows are expected.

3.4.2 TUNNEL: STN 2+90 (SHAFT C) TO AT LEAST STN 3+30

At stn 3+30 the tunnel crown is 16 m below ground surface. From stn 2+90 to at least stn 3+30 the rock at tunnel level is expected to be slightly weathered to fresh stained welded dacite. It is extremely strong (UCS av. 290 MPa)* and very hard to drill (abrasive and resistant to penetration).

The rock mass is expected to be strong and fairly tight. Joints mostly dipping about 30° and generally spaced 0.3 m to 1 m are rough and tight, and sometimes with up to 5 mm of flaky pink calcite cement (weak). The refractor between the 800 m/sec and 4700 m/sec layers (probably extremely to highly weathered and slightly weathered to fresh dacite respectively) is shown (Plate 6) to cross the tunnel at stn 3+30. However seismic-drill hole correlations (see Plates 6-8) show that the seismic interpretation may have placed the refractor too deep; if this is so the tunnel could be continued in hard rock (4700 m/sec) beyond stn 3+30.

Support. Steel-set support will probably be needed from the selected portal to stn 3+20.

Groundwater inflows. Water-pressure tests in drill hole GST 5 showed large water losses, but results are thought to be unreliable. There are probably some open joints and weathered seams, but any water inflows are expected to be less than 5 m³/hr and of short duration.

* An approximate value obtained from 9 UCS tests and Point Load tests on rock from drill holes GST 3, 4, and 5, and from Point Load tests on cubes from surface outcrops. Maximum value was UCS 492 MPa from GST 3. See Appendix 4 for results.

3.4.3 OPEN CUT OR TUNNEL: STN 3+30 TO 4+38

The contractor has the option whether to open-cut or tunnel this section.

The seismic profile shows that 800 to 1200 m/sec material (probably extremely to moderately weathered dacite) extends from the surface to below invert level in this section. However, as noted previously, the bedrock refractor may be shallower than this interpretation shows.

Excavation Alternative. The excavation will be at least 9 m and up to 18 m deep depending on the position of the tunnel portal. Most of the excavation will be in extremely to highly weathered dacite which can be excavated by bulldozer and ripper without blasting. If the bedrock refractor is shallower than shown in Plate 6, then some blasting will be needed in the bottom of the trench along at least part of this section. There may be some large boulders of fresh dacite sitting in extremely weathered dacite; these may need to be blasted. The excavation will need to be battered or shored to prevent collapse.

Tunnelling Alternative. The portal crown will be at least 7 m (at stn 4+38) and up to 16 m (at stn 3+30) below the surface. This section of the tunnel will be mainly in extremely to moderately weathered rock. There may be some slightly weathered to fresh rock encountered if the bedrock refractor is shallower than shown in Plate 6. Steel-set support with timber lagging will be required throughout. Any areas of saturated extremely weathered rock will need continuous timber lagging.

Groundwater inflows. Some water is expected to drain into the tunnel or open cut through open joints and/or weathered seams and especially from the interface between extremely weathered and fresh rock. If any open joints are connected to Ginninderra Creek, these inflows could become large especially if 'piping' has developed in the extremely weathered dacite.

3.4.4 OPEN CUT EXCAVATION: STN 4+38 TO 4+99

Plate 6 shows that material of up to 1200 m/sec velocity (probably extremely to moderately weathered dacite) extends from the surface to invert level. However, drill hole GST 3 entered fresh rock 1 m above invert level, which suggests that the refractor is shallower than marked on the profile.

Most of the rock can probably be excavated by bulldozer with ripper, but some blasting will be necessary near invert.

Battered or supported slopes will be necessary.

Groundwater inflows. As for stn 3+30 to 4+38.

4. CONCLUSIONS AND RECOMMENDATIONS

4.1 CONCLUSIONS

1. Geologically, construction of the tunnel is feasible.
2. The tunnel will be driven through dacite, rhyodacite, and rhyolite units (67%), granite porphyry (25%) and tuffaceous sediments (8%). (Percentages are approximate.)
3. Most of the rock excavated will be fresh. Weathered rock will occur at portals, top sections of shafts, most of the section connecting this tunnel to the existing Belconnel Trunk sewer (stn 0+79 to stn 5+00) and in wide defect (faults, etc.) zones.
4. Unconfined compressive strengths for the acid volcanic units mostly range from 200 to 300 MPa (but up to 400 MPa); granite about 200 MPa; and shales 145 MPa. Shore hardness values were between 70 and 100 (average about 90) for the acid volcanics and the granite; value for the shale was about 68.
5. The contact between different rock types is generally a defect zone. Deterioration in rock condition, increased water inflows, overbreak and support requirements can generally be expected.
6. Five major faults have been detected and many small fractured or sheared zones are indicated by airphoto-lineaments and zones of low seismic velocity. Four of the major faults occur between stns. 40+00 and 48+00, and generally poor tunnelling conditions are expected in this section.
7. All rock units along the route are jointed. Joint spacing will generally be in the range 0.3 to 1 m.
8. Overbreak will generally be less than 50 cm beyond C-line, although overbreak in excess of 1 m can be expected in and near some wide defect zones or in blocky and seamy ground.
9. Tunnelling condition will generally be very good in the dacites of the Walker Volcanics, granite porphyry, tuffaceous sediments, and the Willow Bridge Tuff. Just north of the Window Bend area (stn 40+00 to 44+00), the green rhyolite, purple rhyodacite, and that section of dacite of the Walker Volcanics, will generally yield poor tunnelling conditions, mainly because several major fault zones are present.

10. From the outlet portal (stn 57+88) to shaft 1 (stn 5+00), about 16 percent of the tunnel (850 m) will need to be supported with steel sets and timber lagging during construction (see also 'Recommendations').
11. No large underground cavities containing large quantities of groundwater are expected in the area. Water inflows ranging from seepage to inflows not exceeding 20 m³/hr can be expected. Very few inflows in excess of 5 m³/hr are expected and most will be less than 1 m³/hr; most will be reduced to dripping a few weeks after excavation. Some water will continue to enter the tunnel from open defects mostly near invert level. In areas of shallow cover some defects will seep or drip again after heavy rain.
12. An earthquake producing measurable displacement at the ground surface is unlikely. Seismic risk to the tunnel, its lining, shafts, or other appurtenant works is low.
13. Owing to the variability of the rock units encountered, the extreme strength and hardness of the rock material, and the presence of at least five major fault zones, the use of a tunnel boring machine is not considered practical.
14. At Window Bend, the north portal open cut will be located in fault zone material, soil, and slopewash; the portal face will be in loose green rhyolite. The south portal at Window Bend and the south portal (LMWQCC) will be located in generally sound rock with no known major defects.
15. No known major defects occur at any of the shaft sites. Shafts 1 and C will be located in dacite, shaft 2 in interbedded sediments and dacite, and shaft 3 in granite porphyry.
16. The open-cut excavation, stns 0+79 to 2+90 (shaft C), will mostly be in extremely to highly weathered dacite.
17. The tunnel section between stns 2+90 and 3+30 will probably not need steel-set support.
18. The section from stn 3+30 to 5+00 will be located mainly in extremely weathered to moderately weathered dacite, although fresh rock may occur between invert and springline in some places.

4.2 RECOMMENDATIONS

1. A permanent drain should be installed at Window Bend north portal near tunnel invert. (The purpose of this drain is to release groundwater from the highly permeable open jointed green rhyolite that occurs behind fault 4, which acts as an impermeable groundwater barrier. Drill hole GST 17 penetrated the green rhyolite behind the fault zone and is flowing at a constant rate of 1200 to 1400 l/hr.)
2. Total groundwater outflows from the tunnel (and shafts) should be measured accurately, using appropriate automatic recorders, and an accurate record should be kept of all groundwater inflows into the tunnel, including initial inflow quantity, location of flow and duration. (Such records will help in locating areas requiring panning before concrete is laid.)
3. Greater use of rockbolts (instead of steel sets) should be made, particularly in blocky ground or slabby ground associated with shallow dipping sediments.
4. The lining of invert and walls up to only maximum design flow should be considered for sections of tunnel where the standard (specified full 360°) concrete lining could be dispensed with. The sections for consideration are:
 - (a) Essentially self-supporting and free of steel-set support, but including areas of rockbolt, gunite, or shotcrete support. (Narrow sections, such as fault zones, within essentially self-supporting sections may require steel support and full lining, but these cannot be predicted accurately.)
 - (b) Essentially dry sections of tunnel that never produced water inflows even when first excavated. (Narrow sections, such as narrow faults, etc., as described above, may need to be grouted to reduce water inflows to an acceptable level.)

<u>Tunnel Sections</u>	<u>Length (m)</u>
Stn 5+00 to 8+00	300
Stn 9+00 to 10+00	100
Stn 10+30 to 13+00	270
Stn 14+00 to 25+60	1160
Stn 26+50 to 42+30	1580
Stn 50+00 to 57+00	<u>700</u>
<u>TOTAL</u>	4110 (80% of tunnel between 5+00 and 57+88)

5. ACKNOWLEDGEMENTS

The geological investigations were carried out in co-operation with officers of the Department of Construction (DC, formerly part of the Department of Housing and Construction), Canberra. The diamond drilling was carried out by DC drilling crews based at the Fyshwick Materials Testing Laboratory in Canberra.

The BMR Engineering Geophysics group carried out the seismic refraction survey of the tunnel route. Mechanical properties of rock samples from surface outcrops and drill core were determined by N. Wise (Engineering Geology) and M. Idnurm (Rock Testing Group, Geophysical Branch). The petrographic descriptions were done by C. Gardner (Geological Branch).

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APPENDIX 1

INVESTIGATION METHODS

Correlation with Pine Ridge tunnel

The information obtained during construction of the nearby Pine Ridge tunnel has been used as an aid in assessing conditions in the GST. Pine Ridge tunnel and its portals were photographed and geologically mapped at a scale of 1:240; geochemical, petrographic, and water samples were collected and tested, and the results studied; groundwater inflows were measured; observation bores monitored; overbreak calculated from concrete quantities; explosive quantities, drilling pattern, advance rate, support, and overbreak were correlated; and all the results were correlated with the predictions made from mapping, seismic refraction profiling, and diamond drilling during the design investigation for that tunnel.

Airphoto-interpretation

Airphoto-interpretation of photos taken from 760 m (1968 black and white), 427 m (1968 colour), and 214 m (1973 colour) was done by P. Lang throughout the investigations.

Geological mapping

Geological mapping at a scale of 1:2400 and 1:9600 was carried out by P. Lang and field hand D. Broome between April 1974 and September 1975. The maps were reduced to 1:2500 and 1:10 000 respectively, and metric coordinates added (see Plates 1 to 5).

Geophysical methods

A continuous seismic refraction profile was obtained by the BMR Engineering Geophysics Group (Taylor, 1975) along most of the route from stn 00+50 (on the preliminary tunnel line) to stn 55+20. The traverse consisted of 53 spreads, and fieldwork was done in November and December 1974.

The following sections were omitted:

- (a) from stn 18+20 to stn 24+20 (Belconnen Electricity substation)
- (b) from stn 41+60 to stn 42+30
- (c) from stn 47+70 to stn 47+95
- (d) stn 55+20 to stn 57+88 because of its proximity to the Pine Ridge tunnel operations.

During March 1975, eight additional traverses were done to investigate the altered route at the north end (stn 4+99 to stn 17+12), the connection from shaft 1 to the existing Belconnen trunk sewer (stn 0+79 to stn 4+99), and to further investigate the faulted zone from stn 40+00 to stn 45+00.

Each spread was 88 m long, with 23 geophones spaced 4 m and with a reciprocal geophone 60 m from each end of the spread. Five shots were fired for each spread at -

geophone 1	-60 m
geophone 1	- 2 m
geophone 12	+ 2m
geophone 23	+ 2 m
geophone 23	+60 m

Time-distance curves were made available at BMR for inspection by Tenderers.

Drilling

From April to October 1975, 15 diamond-drill holes totalling 665 m were drilled by DHC using three drill rigs. NMLC triple-tube core barrels with split inner tube were used. Water-pressure testing was done on each hole. Geological logs of drill core showing water-pressure testing results are in Appendix 8. Water-pressure test computation sheets are available at BMR for inspection by Tenderers.

From December 1974 to October 1975, nine 125 mm diameter observation bores were drilled by BMR. The holes were partly cored but were not water-pressure tested. Geological logs of drill core are in Appendix 8.

Locations of drill holes are plotted in Plates 1 to 5, and summary logs are plotted on the profiles (Plates 6 to 8).

Drill core is stored at the Department of Construction Core Shed at Kingston, A.C.T. Photographs of the drillcore comprise Appendix 7.

Rock testing

Several mechanical rock parameters were determined by BMR. Point load induced tensile strength tests were carried out on rock samples collected from surface outcrops at seven localities (see Plates 2 and 3 for sample locations), and from 35 localities in Pine Ridge tunnel within 1800 m of the west portal.

The parameters measured on drill core were uniaxial compressive strength, specific gravity, modulus of elasticity, Poisson's ratio, Shore hardness, compressional velocity, and point load induced tensile strength. Detailed results are in Appendix 4.

Petrology

Petrographic descriptions and chemical analyses were done on rocks from drill core and surface outcrops (see Appendix 5).

Water analyses

Water samples from drill holes and from Pine Ridge tunnel were analysed for components aggressive to concrete lining (see Appendix 6).

APPENDIX 2

GLOSSARY OF TERMS

ROCK CONDITION NUMBERS

1. Descriptions of the Rock Condition Numbers (RCN) have been modified here by one of us (D.C.P.) after Terzaghi (1946) and Deere, Merritt, & Coon (1969) to suite geological conditions actually encountered in tunnelling operations carried out in the A.C.T. since 1971. To date these tunnels have passed mainly through acid volcanics and sedimentary rocks derived from them.

2. The predicted support requirements for each RCN should only be used as a guide, as very narrow but poorly oriented defects in an otherwise long section of competent rock (e.g., RCN 2) may require 2 or 3 steel sets or a few rockbolts for stabilization. The predictions of support assume an excavated tunnel diameter of up to 4 m.

3. It should also be noted that RCN 7 and 8 have not been recorded to date in the A.C.T.

ROCK CONDITION

NUMBER

DESCRIPTION OF THE ROCK MASS

1. HARD INTACT ROCK: Rock massive, very hard and very strong, with no significant joints or other defects. Breaks across sound rock when blasted. No support necessary.
2. HARD WIDELY JOINTED ROCK: As above, but may be foliated or bedded with a fairly high resistance to separation of surfaces. Prominent continuous joints spaced 1-3 m are tight; joints usually not continuous for more than a few metres. No support required.
3. MASSIVE, MODERATELY JOINTED: Rock mostly hard and strong. Continuous joints generally spaced 0.5 m - 1 m are usually fairly tight, but some water seepage along joints may occur. Rock may be partly blocky in places, and generally breaks along joint surfaces when blasted. Steel or rockbolt supports generally not required in 3 m diameter tunnel; in a 4 m tunnel, some rockbolts may be required where blocky or poorly oriented defects cross the tunnel.

4. MASSIVE, MODERATELY JOINTED, SEAMY: As above but defect surfaces generally clay-coated and loose. Clay seams and sheared or fractured rock with clay common. Rock may be moderately weathered or altered and soft in parts. Steel-set support (1-1.3 m spacing) sometimes required in tunnels up to 3 m diameter; more often in 4 m tunnel. Rockbolts may be preferable in places.
5. CLOSELY JOINTED AND SEAMY: Closely jointed, seamy, and fractured rock; joints and fractures are loose and open (where not clay-filled), and may result in large water inflows into the excavation; includes highly and extremely weathered (or altered) rock. May exert considerable weight on steel-set supports; steel supports spaced at 1 m (or less) with heavy timber lagging. Rockbolts not usually effective.
6. SEAMY AND CRUSHED ROCK: Includes unconsolidated sand, slopewash, etc. Refers to fault zone material (gouge) or shattered rock where clay and gravel sized fragments makes up the greater percentage of the material mass. If water content is high, these materials may run or flow and exert significant side pressures. Stand-up time near zero. Rockbolting not effective. Steel sets <0.5 m centres, invert struts, and possibly linear plates. Shotcrete or gunite often effective in containing running ground.
7. SQUEEZING GROUND: Slow movement of rock into the tunnel without perceptible volume increase (rock with clay minerals with low swelling characteristics).
8. SWELLING GROUND: Material expands in volume upon exposure to water (e.g. montmorillonite clay, serpentine, anhydrite, etc.).

DEGREES OF ROCK WEATHERING

FRESH	: No discolouration or loss in strength.
FRESH STAINED	: Limonitic staining along fractures; rock otherwise fresh and shows no loss of strength.
SLIGHTLY WEATHERED	: Rock is slightly discoloured, but not noticeably lower in strength than the fresh rock.
MODERATELY WEATHERED	: Rock is discoloured and noticeably weakened; N-size (54 mm) drill core generally cannot be broken by hand across the rock fabric.

- HIGHLY WEATHERED : Rock is discoloured and weakened; N-size (54 mm) drill can generally be broken by hand across the rock fabric.
- EXTREMELY WEATHERED : Rock is decomposed to soil, but the original rock fabric is mostly preserved.

ROCK SUBSTANCE

This is defined as intact, effectively (for engineering purposes) homogenous rock. Repeated mechanical tests on the material would give acceptable coefficients of variations (e.g., uniform results).

ROCK MASS

Rock mass is a body of material which is not effectively homogenous, that is, the rock substance is crossed by natural defects such as joints, faults, seams etc.

SHEARED ROCK

Consists of rock intersected by close (< 1 cm), slightly curving intersecting fracture planes; the fracture surface may be smooth, polished, slickensided, or coated with clay.

CRUSHED ROCK

Consists of rock which is mechanically disintegrated but not obviously chemically decomposed.

FRACTURED ROCK

Consists of rock which is intensively jointed in several directions. Fracture surfaces are often clay-coated.

FAULTED ROCK

Faults can be sheared, crushed, or fractured rock, and where relative displacement of rock can be seen. Unless evidence for faulting is quite definite the term should not be used.

JOINT SPACING

- Very close - joints spaced < 5 cm
- Close - joints spaced 5 cm to 30 cm
- Moderately close - joints spaced 30 cm to 1 m
- Wide - joints spaced 1 m to 3 m
- Very wide - joints spaced > 3 m

JOINT APERTURE

This describes the amount of separation of the joint surfaces. Joints may be open or tight. If two joint faces fit perfectly it is probable that the joint in the rock mass was tight (or closed). However, if they do not fit it probably means that the joint was open; or possibly filled with clay that has been washed away during drilling.

BEDDING

Laminated	-	< 10 mm thick
Thinly bedded	-	10 mm to 100 mm thick
Thickly bedded	-	> 100 mm thick

GRAINSIZE

Coarse-grained	-	1 mm to 4 mm in diameter
Medium-grained	-	$\frac{1}{2}$ mm to 1 mm in diameter
Fine-grained	-	< $\frac{1}{2}$ mm in diameter.

ROCK QUALITY DESIGNATION (RQD)

RQD is the ratio (expressed as a percentage) of length of core recovered to the total length of core run, counting only those pieces of hard and sound rock 10 cm in length or longer.

APPENDIX 3

DRILL HOLE WATER-PRESSURE TESTS

Water-pressure tests were carried out on NMLC diamond-drill holes along the route. Standard test procedures were used.

Permeabilities have been calculated for each test section and have been plotted on the geological logs (Appendix 3) in lugeon units. The lugeon is defined as:

'the rate of loss of water from a drill hole 46 to 76 mm diameter, of 1 litre per minute per metre of drill hole at a pressure of 10 bars, the test being applied for ten minutes over a test length of 2 metres.'

Computation sheets for every test carried out are not presented here but can be examined at the Bureau of Mineral Resources.

APPENDIX 4

MECHANICAL PROPERTIES OF ROCK SAMPLES

Appendix 4 describes the measurement of mechanical properties of NMLC and Treifus 2½" drill core samples from the proposed tunnel line. Point Load Strengths were determined by N. Wise of the BMR Engineering Geology Section. The other measurements were carried out by M. Idnurm and R. Eaton of the Rock Measurements Group.

The rocks tested were dacites, rhyodacites, granite, rhyolite, and shales. All samples were classified as fresh rock.

MEASUREMENT TECHNIQUES

Elastic properties

The elastic properties are measured on drill core samples 10 to 13 cm long in a laboratory-dry condition.

Compressional sound velocity. The compressional sound velocities were determined from the transmission times of a sound pulse using a Cawkell ultrasonic instrument type UCT2. The pulse consisted of a damped sine wave of frequency 150 kHz.

Modulus of Elasticity and Poisson's Ratio. The Modulus of Elasticity and Poisson's ratio were calculated from the compressional velocity and the resonance frequency of the drill core sample. A Cawkell instrument type SCT4 was used for the resonance measurements. The elastic moduli consequently represent the dynamic rather than the static values. The experimental errors in the velocity are estimated to be within 5 percent, and in the elastic moduli within 15 percent.

The elastic properties, specific gravity, and hardness of the drill core samples are shown in Table A together with the drill log data. The gaps in the table denote lack of reliable elastic property data owing to high sonic attenuation.

Hardness

The hardnesses were determined by the Shore scleroscope, which measures the height of rebound of a diamond-tipped weight from a flat test surface. A total of 64 readings was obtained from the end faces of each sample, and the average of these was taken as the Shore Hardness. The samples were tested in a laboratory-dry condition.

Table B lists for comparison the values of Shore Hardness for several common rock types. This table is compiled from

the information given in the US Bureau of Mines report on their Investigation No. 4727.

Uniaxial compressive strength (UCS)

The length to diameter ratio of the samples for the compressive strength tests was 2:1. The specimen ends were surface-ground to a flatness within $25\mu\text{m}$ (highest to lowest point). The ends were parallel within $\frac{1}{2}^\circ$. No lubricant was used on the end faces. The samples were tested in a laboratory-dry condition. A Baldwin testing machine Model 400 CT was used. The loading rate was $500\text{ KN/m}^2/\text{sec}$.

Table C lists the uniaxial compression test results. The samples tested represent the least jointed sections of the drill core. Defect free samples were not available from some of the drill cores. Where the failure occurred prematurely on pre-existing fracture planes only the lower limit of uniaxial compressive strength is given. The shale samples were tested normal to their bedding planes.

Point Load Strength Index: $I_s(50)$

The Point Load Strength (PLS) test was devised as a quick means of determining the rock strength. The tests were carried out using a technique developed by Brock & Franklin (1972).

Where possible at least 10 tests were carried out on a sample 'unit'. A 'unit' is a sample of rock considered on inspection to have uniform strength. In some cases it was not always possible to obtain 10 suitable rock samples.

Failure of a sample was considered satisfactory if it occurred across the rock substance. Where failure occurred along fractures, joints, or bedding planes, the results were discounted.

Tests of shale samples were carried out perpendicular to the bedding planes. The length of the drill core shale samples tested was roughly equal to the diameter.

Drill-core samples and surface samples were tested in a laboratory-dry condition.

Drillcore samples

Tests were carried out on core samples having a length to diameter ratio greater than 1.4. The samples were tested through a core diameter at a distance 0.7 diameter between the contact point of the platen and the nearest free end.

All tests were carried out in the field using core samples taken from the boxed drill core.

The PLS test results for the drill core are included in Table D.

Surface samples

The PLS test results for surface samples from GST and tunnel samples from Pine Ridge tunnel are included in Tables E and F. The samples tested were the form of irregular lumps collected from surface outcrops and from the tunnel-walls. With one exception the testing procedures have followed those recommended by Brock & Franklin (1972). The exception is in the shape factor for which the lower limit has been reduced from 1.0 to 0.9. This should not introduce any serious errors and has enabled a large number of samples to be retained, which would have otherwise been unsuitable for the tests.

The following should be noted about the tests:

1. The test samples were roughly cubical in shape with an average edge length of 6 cm. The final trimming to produce the cubical shape was done with a diamond-disc saw.
2. The shape factor ranged from 0.9 to 1.3.

Correlation of Point Load Strength Index, $Is(50)$, with Uniaxial Compressive Strength (UCS).

From the $Is(50)$ a corresponding UCS can be predicted from the correlation curve of Brock & Franklin (op. cit.). The correlation is:

$$UCS \approx 24 Is(50)$$

A comparison between $Is(50)$ and UCS has been carried out by M. Idnurm of the BMR Rock Measurements Group. The correlation coefficient between $Is(50)$ and UCS found here was 0.84, which compares with values of 0.88 obtained by Brock & Franklin, and 0.95 obtained by D'Andrea et al. (1965).

The results obtained by M. Idnurm agree reasonably well with those of Brock & Franklin at low and intermediate compressive strengths, but deviate at high strengths. For example the average $Is(50)$ for fresh dacite from Pine Ridge tunnel is 7.9 MPa, and the corresponding UCS predicted from the correlation curve of Brock & Franklin is 190 MPa; however, measurements by M. Idnurm indicate a UCS of 210 MPa. These results indicate a possible non-linear relationship between $Is(50)$ and UCS at high stress levels, and departures from the Brock & Franklin curve start from about 160 MPa.

TABLE A. GENERAL RESULTS OF ROCK TESTS

Drill hole	Depth (m)	Geological description	Sample no.	Specific gravity	Compressional velocity (m/s)	Modulus of elasticity (E) (10^3 MN/m^2)	Poissons Ratio (r)	Hardness (Shore units)
GST. 3	17.90	Dacite	75/529	2.67	5660	76	0.22	-
GST. 3	24.70	"	75/530	2.65	5560	72	0.23	-
GST. 3	35.60	"	75/531	2.64	4420	45	0.24	-
GST. 3	17.95	"	75/532		Shore Hardness test only			102
GST. 3	24.65	"	75/533		Shore Hardness test only			102
GST. 3	19.80	"	75/534		Shore Hardness test only			101
GST. 4	29.10	Dacite	75/535	2.68	5930	81	0.25	-
GST. 4	29.30	"	75/536	2.65	5650	74	0.24	-
GST. 4	32.40	"	75/537	2.66	5750	77	0.24	-
GST. 4	29.30	"	75/538		Shore Hardness test only			100
GST. 4	32.05	"	75/539		Shore Hardness test only			98
GST. 4	32.30	"	75/540		Shore Hardness test only			96
GST. 5	12.50	Dacite	75/541	2.66	5490	67	0.26	-
GST. 5	12.60	"	75/542	2.65	5740	65	0.31	-
GST. 5	12.80	"	75/543	2.67	5630	73	0.24	-
GST. 5	12.45	"	75/544		Shore Hardness test only			102
GST. 5	12.70	"	75/545		Shore Hardness test only			101
GST. 5	12.87	"	75/546		Shore Hardness test only			96
GST. 7	19.10	Shale	75/547	2.68	4400	-	-	-
GST. 7	19.63	"	75/548	2.68	4650	-	-	-
GST. 7	19.95	"	75/549	2.68	5020	-	-	-
GST. 7	19.05	"	75/550		Shore Hardness test only			72
GST. 7	19.50	"	75/551		Shore Hardness test only			64
GST. 7	19.80	"	75/552		Shore Hardness test only			67
GST. 7	35.76	Dacite	75/553	2.61	3850	-	-	-
GST. 7	39.70	"	75/554	2.63	4790	52	0.25	-
GST. 7	40.35	"	75/555	2.65	3900	-	-	-
GST. 7	35.85	"	75/556		Shore Hardness test only			81
GST. 7	40.40	"	75/557		Shore Hardness test only			68
GST. 7	59.80	"	75/558		Shore Hardness test only			71
GST. 9	44.10	Granite	75/487	2.68	5770	71	0.29	-
GST. 9	45.90	"	75/488	2.67	5720	71	0.28	-
GST. 9	46.50	"	75/489	2.68	5650	60	0.33	-
GST. 9	44.50	"	75/491		Shore Hardness test only			91
GST. 9	46.00	"	75/490		Shore Hardness test only			92
GST. 9	47.50	"	75/492		Shore Hardness test only			97
GST. 11	31.80	Dacite	75/493	2.71	5070	61	0.24	-
GST. 11	38.60	"	75/494	2.74	5450	67	0.27	-
GST. 11	58.20	"	75/495	2.69	5500	70	0.25	-
GST. 11	31.68	"	75/496		Shore Hardness test only			71
GST. 11	38.65	"	75/497		Shore Hardness test only			75
GST. 11	58.05	"	75/498		Shore Hardness test only			75
GST. 12	70.30	Dacite	75/499	2.70	5330	59	0.30	-
GST. 12	71.50	"	75/500	2.67	5580	69	0.27	-
GST. 12	71.60	"	75/501	2.67	5310	59	0.29	-
GST. 12	70.20	"	75/502		Shore Hardness test only			71
GST. 12	71.42	"	75/503		Shore Hardness test only			82
GST. 12	77.70	"	75/504		Shore Hardness test only			57

TABLE A. (contd.)

Drill hole	Depth (m)	Geological description	Sample no.	Specific gravity	Compressional velocity (m/s)	Modulus of elasticity (E) (10^3 MN/m^2)	Poissons Ratio (ν)	Hardness (Shore units)
GST. 16	37.30	Rhyodacite	75/559	2.63	4560	49	0.22	-
GST. 16	37.40	"	75/560	2.61	5030	61	0.20	-
GST. 16	39.50	"	75/561	2.58	4600	45	0.26	-
GST. 16	27.45	"	75/562		Shore Hardness test only			90
GST. 16	37.20	"	75/563		Shore Hardness test only			81
GST. 16	39.60	"	75/564		Shore Hardness test only			63
GST. 17	20.00	Rhyolite	75/505	2.74	5710	75	0.26	-
GST. 17	21.80	"	75/506	2.66	5680	73	0.28	-
GST. 17	21.80	"	75/507	2.60	5560	62	0.30	-
GST. 17	20.10	"	75/508		Shore Hardness test only			98
GST. 17	20.14	"	75/509		Shore Hardness test only			93
GST. 17	21.92	"	75/510		Shore Hardness test only			97
GST. 18	18.60	Dacite	75/565	2.70	4540	42	0.31	-
GST. 18	18.70	"	75/566	2.70	4740	49	0.28	-
GST. 18	18.90	"	75/567	2.71	4390	-	-	-
GST. 18	18.50	"	75/568		Shore Hardness test only			63
GST. 18	18.75	"	75/569		Shore Hardness test only			69
GST. 18	18.85	"	75/570		Shore Hardness test only			71
GST. 20	56.60	Dacite	75/511	2.72	4600	40	0.33	-
GST. 20	57.80	"	75/512	2.68	5650	70	0.27	-
GST. 20	58.00	"	75/513	2.69	5520	68	0.26	-
GST. 20	57.61	"	75/515		Shore Hardness test only			90
GST. 20	58.00	"	75/514		Shore Hardness test only			89
GST. 20	60.00	"	75/516		Shore Hardness test only			87
GST. 23	48.50	Granite	75/517	2.68	5880	75	0.28	-
GST. 23	59.90	"	75/518	2.68	5840	75	0.27	-
GST. 23	61.30	"	75/519	2.68	5870	76	0.27	-
GST. 23	48.35	"	75/520		Shore Hardness test only			100
GST. 23	59.90	"	75/521		Shore Hardness test only			97
GST. 23	61.35	"	75/522		Shore Hardness test only			97
GST. 24	43.90	Granite	75/523	2.66	5600	67	0.28	-
GST. 24	44.10	"	75/524	2.66	5600	67	0.28	-
GST. 24	34.10	"	75/525	2.67	5440	65	0.27	-
GST. 24	43.60	"	75/526		Shore Hardness test only			82
GST. 24	43.90	"	75/527		Shore Hardness test only			87
GST. 24	43.64	"	75/528		Shore Hardness test only			86
MV 7	11.9	Dacite	71/229	2.67	5660	70	0.28	99
MV 7	18.8	"	71/230	2.70	5450	66	0.28	89
MV 7	19.2	"	71/231	2.68	5600	69	0.28	90
MV 7	19.5	"	71/232	2.68	5500	67	0.28	86
MV 11	33.6	"	71/233	2.67	5850	75	0.28	96
MV 11	34.5	"	71/234	2.68	5640	64	0.31	93
MV 11	35.6	"	71/235	2.69	5630	69	0.23	94
MV 11	48.5	"	71/236	2.69	4250	32	0.36	69

TABLE B. SHORE HARDNESS RANGE IN COMMON ROCK TYPES*

Rock type	Shore Hardness	No. of localities of sample collection
Granite	90 - 100	5
Basalt	69 - 84	1
Quartzite	81 (one value only)	1
Limestone	27 - 66	4
Sandstone	31 - 65	3
Shale	34 - 58	2

* From US Bureau of Mines Report on Investigation 4727

TABLE C. UNIAXIAL COMPRESSIVE STRENGTHS (UCS)

Drill hole	Depth (m)	Diam (cm)	Geological description	Sample no.	Compressive strength MPa	Mode of failure
GST. 3	17.90	5.2	Dacite	75/529	294	Fractured into numerous small pieces
GST. 3	24.70	5.2	"	75/530	492	Longitudinal failure through length
GST. 3	35.60	5.2	"	75/531	> 110	Premature failure through joint plane
GST. 4	29.10	5.2	Dacite	75/535	>101	Premature failure through joint plane
GST. 4	29.30	5.2	"	75/536	273	Fracture into numerous small pieces
GST. 4	32.40	5.2	"	75/537	173	Longitudinal failure through length
GST. 5	12.50	5.2	Dacite	75/541	291	Fracture into numerous small pieces
GST. 5	12.60	5.2	"	75/524	258	Fracture into numerous small pieces
GST. 5	12.80	5.2	"	75/543	234	Longitudinal failure through lengths
GST. 7	19.10	5.2	Shale	75/547	> 245	Premature failure through joint plane
GST. 7	19.63	5.2	"	75/548	>124	Premature failure through joint plane
GST. 7	19.95	5.2	"	75/549	>197	Premature failure through joint plane
GST. 7	35.76	5.2	Dacite	75/553	203	Conical
GST. 7	39.70	5.2	"	75/554	204	Fracture into numerous small pieces
GST. 7	40.35	5.2	"	75/555	205	Conical
GST. 9	44.10	5.2	Granite	75/487	170	Fracture into numerous small pieces
GST. 9	45.90	5.2	"	75/488	237	Fracture into numerous small pieces
GST. 9	46.50	5.2	"	75/489	125	Longitudinal failure through length
GST. 11	31.80	5.2	Dacite	75/493	154	Fracture into numerous small pieces
GST. 11	38.60	5.2	"	75/494	152	Fracture into numerous small pieces
GST. 11	58.20	5.2	"	75/495	164	Fracture into numerous small pieces
GST. 12	70.30	5.2	Dacite	75/499	104	Semiconical failure
GST. 12	71.50	5.2	"	75/500	97	Semiconical failure
GST. 12	71.60	5.2	"	75/501	105	Longitudinal failure through length
GST. 16	37.30	5.2	Rhyodacite	75/559	> 52	Premature failure through joint plane
GST. 16	37.40	5.2	"	75/560	> 39	Premature failure through joint plane
GST. 16	39.50	5.2	"	75/561	> 38	Premature failure through joint plane
GST. 17	20.00	5.2	Rhyolite	75/505	279	Fracture into numerous small pieces
GST. 17	21.80	5.2	"	75/506	322	Fracture into numerous small pieces
GST. 17	21.80	5.2	"	75/507	247	Conical
GST. 18	18.60	5.2	Dacite	75/565	145	Longitudinal failure through length
GST. 18	18.70	5.2	"	75/566	119	Longitudinal failure through length
GST. 18	18.90	5.2	"	75/567	96	Conical
GST. 20	56.60	6.3	Dacite	75/511	141	Conical
GST. 20	57.80	6.3	"	75/512	255	Longitudinal failure through length
GST. 20	58.00	6.3	"	75/513	223	Longitudinal failure through length
GST. 23	48.50	6.3	Granite	75/517	188	Longitudinal failure through length
GST. 23	59.90	6.3	"	75/518	246	Fracture into numerous small pieces
GST. 23	61.30	6.3	"	75/519	263	Fracture into numerous small pieces
GST. 24	43.90	6.3	Granite	75/523	178	Longitudinal failure through length
GST. 24	44.10	6.3	"	75/524	201	Fracture into numerous small pieces
GST. 24	34.10	6.3	"	75/525	> 110	Premature failure through joint plane
MV 7	11.8	5.2	Dacite	71/229	239	Not available
MV 7	18.8	5.2	"	71/230	214	Not available
MV 7	19.2	5.2	"	71/231	187	Not available
MV 7	19.5	5.2	"	71/232	-	Not available
MV 11	33.6	5.2	"	71/233	257	Not available
MV 11	34.8	5.2	"	71/234	262	Not available
MV 11	48.5	5.2	"	71/235	192	Not available
			"	71/236	177	Not available

TABLE D. POINT LOAD STRENGTH TESTS ON DRILL CORE

Hole no.	Depth approx. (m)	No. samples tested	Formation	No. successful tests	Mean $I_a(50)$ MPa	Standard deviation	Geological description
GST. 2	43.0	9	Willow Bridge Tuff	7	9.8	0.85)FR - Dacite, light grey to dark grey to pink with zones of alteration.
	56.0	11		10	9.9	1.01	
	60.0	7		5	9.4	0.94	
GST. 3	17.0	10	Walker Volcanics Lower Sequence	10	12.1	1.65	FS - Dacite, light grey
GST. 4	28.0	10		10	7.4	1.06	FS - Dacite, pale grey
GST. 5	10.0	10		7	11.2	1.78)FS - Dacite, welded, mostly pale grey
	20.0	10		9	11.1	3.08	
GST. 7	10.0	10	Walker Volcanics Lower Sequence	8	7.3	1.44	FR - Dacite, crystal tuff arenite
	16.0	3		3	2.4	0.93	Black shale intraclasts
	19.0	2		2	2.6	0.02	FR - Black shale
	25.0	4		4	2.2	0.21	Black shale intraclasts
	28.0	10		8	7.9	3.92	FR - Dacite tuff
	36.0	11		8	4.3	0.95	FR - Dacite ignimbrite tuff, med. grey
GST. 8	15.0	10	Ginninderra Porphyry	8	1.5	0.67	MW-FS Granite porphyry, light grey
	20.0	18		8	6.1	2.00)FR - Granite porphyry light grey
	30.0	14		3	8.4	3.24	
GST. 9	35.0	8	Ginninderra Porphyry	4	2.9	1.46	FR - Granite porphyry, but slightly altered and chloritized.
	44.0	14		7	7.6	2.22	FR - Granite porphyry
GST. 11	30.0	14	Walker Volcanics Lower Sequence	6	6.3	0.82	FR - Dacite ignimbrite tuff
	44.0	11		4	6.0	1.10	FR - Dacite ignimbrite tuff
GST. 12	38.0	10	Walker Volcanics Upper Sequence	4	5.1	0.82	FS - FR Dacite, mostly sheared but healed with chlorite and limonite
	72.0	10		8	7.2	2.51	FR - Dacite ignimbrite tuff
GST. 13	63.0	10	Walker Volcanics Upper Sequence	6	7.0	1.91	FR - Dacite
	80.0	14		5	4.1	0.95)FR - Rhyolite, green mottled
	82.0	9		3	2.0	0.54	
GST. 14	23.0	10	Walker Volcanics Upper Sequence	2	6.4	0.10)FR - Rhyolite, purple with chlorite veins throughout
	32.0	8		3	4.5	0.62	
GST. 16	20.0	10	Green rhyolite	7	6.5	1.32	SW-FS Rhyolite, pale green
	24.0	10	Purple rhyodacite	9	9.1	1.67	SW-FS Rhyolite, blue green
	37.0	12	Green rhyolite	6	4.6	1.00	FS - Rhyodacite, purple
GST. 17	20.0	15	Green rhyolite	11	8.4	1.07	FR - Rhyolite, green
GST. 18	19.0	10	Walker Volcanics Upper Sequence	7	5.1	2.00	FR - Dacite, welded, stained purple
GST. 20	55.0	13	Ginninderra Porphyry	10	6.2	0.94	FR - Dacite, blue grey
GST. 23	46.0	10	Ginninderra Porphyry	10	8.4	1.19)FR - Granite porphyry pale grey
	60.0	11		6	7.9	0.93	
GST. 24	28.0	12	Ginninderra Porphyry	10	5.6	1.79	FS - FR Granite porphyry green grey

TABLE E. POINT LOAD STRENGTH TESTS ON SURFACE SAMPLES

Map locality and thin-section numbers	Grid position	No. samples tested	Mean Is(50) MPa	Standard deviation	Geological description
J1 75360026	198750 E 612590 N	10	12.6	2.34	Light grey dacite, SW - FR
74360060	199180 E 612710 N	10	12.9	0.92	Dark grey dacite, FS - FR
74360061	199210 E 612100 N	10	12.0	1.07	Dark grey dacite, FS- FR
K3 75360023	199177 E 612310 N	6	12.3	2.44	Dark grey dacite, SW - FS
75360021	199940 E 612340 N	9	9.8	2.16	Purple dacite, SW
E1	196710 E 610390 N	10	10.5	1.83	Dacite agglomerate, SW - FS
D1 75360031	198810 E 608690 N	9	9.8	1.85	Green rhyolite, SW- FS

TABLE F. PINE RIDGE TUNNEL POINT LOAD STRENGTH TESTS

All samples consisted of fresh dacite containing cemented fractures.

Location chainage (ft)	No. of samples	Mean Is(50) MPa
200 (w)	4	7.8
300 (w)	3	8.4
400 (w)	2	8.0
500 (w)	3	8.2
600 (w)	3	6.7
700 (w)	2	9.0
800 (w)	2	10.7
900 (w)	3	8.5
1000 (w)	2	8.1
1100 (w)	2	5.9
1200 (w)	2	7.3
1300 (w)	3	8.3
1400 (w)	3	7.4
1500 (w)	2	9.6
1600 (w)	2	7.5
1700 (w)	3	7.1
1800 (w)	2	7.1
1900 (w)	3	5.9
2000 (w)	3	8.0
2100 (w)	3	7.3
2200 (w)	3	8.9
2300 (w)	2	7.1
2400 (w)	2	8.0
2500 (w)	2	7.3
2600 (w)	2	6.4
2700(w)	3	10.4
		<u>Mean 7.9</u>

APPENDIX 5
PETROLOGY

THIN SECTION DESCRIPTIONS
(by C. Gardner)

SUMMARY

All the samples described are porphyritic dacites (62-68% SiO_2) or rhyolites (SiO_2 68%) with between 30 and 50 percent phenocrysts. These generally include unbroken phenocrysts, fragments of broken phenocrysts (fragmentation is a distinctive feature of these rocks), and microphenocrysts. Quartz is the dominant porphyritic mineral in all of the samples, in terms of abundance and grain size; it occurs as rounded or hexagonal embayed crystals and always shows complete extinction.

Plagioclase (albite-?andesine) is always present, usually as subhedral, partly sericitized, irregularly twinned, zoned laths. Euhedral microphenocrysts of magnetite also occur in all the samples.

Mafic phenocrysts were originally biotite + hornblende + clinopyroxene, orthopyroxene was found in one sample. In almost all the samples, the mafics have been completely altered, usually to chlorite + opaque oxides or sericite. Calcite, tremolite, sphene are also common alteration products. Low-grade greenschist metamorphism is inferred from these alteration products.

The groundmass is usually composed of quartz, plagioclase, K-feldspar, chlorite, sericite, and opaque oxides in many stages of devitrification. Strong flow-banding is evident in some samples, the flow enveloping deformed biotite pseudomorphs.

Accessories include apatite, zircon, and epidote.

THIN SECTION DESCRIPTIONS

Purple rhyodacite

(No. 75360021)

Phenocrysts: (35%) Most of these are clear (i.e., not undulose) quartz, up to 5 mm, cracked but not displaced. Sericitized albite and biotite partly replaced by chlorite + opaques make up the remainder of the phenocrysts. Microphenocrysts of biotite, chlorite, opaques and magnetite occur. (3%)

Groundmass: Partly devitrified quartz-feldspar-opaques. Feldspar is clouded with inclusions of opaque oxides.

Green rhyolite

(No. 75360031)

Extensively altered. Large areas of the matrix are recrystallized - these may be of sedimentary origin. Quartz phenocrysts (20%) cracked but not displaced, and feldspars (10%) sericitized. Rare original biotite and hornblende has been replaced by opaques + sericite or opaques + chlorite.

Groundmass is poorly crystalline.

Accessory zircon, magnetite microphenocrysts.

Walker Volcanics, lower sequence (Dacite)

(No. 74360064)

Phenocrysts: (60%) composed of rounded fragments of clear quartz, sericitized subhedral feldspar, and pseudomorphs after biotite and hornblende. The pseudomorphs are aggregates of quartz-calcite-tremolite-epidote, calcite-chlorite, or Fe-rich chlorite. Former biotite laths are deformed.

Groundmass: is structureless cryptocrystalline quartz-chlorite-plagioclase-K-feldspar.

Accessory: zircon, sphene, opaques.

(No. 74360065)

?Phenocrysts: (60%) Comprised of fragmented irregularly-shaped but well-rounded quartz, dense enough that they are just touching, and partly sericitized untwinned sodic plagioclase. As for 0064, mafic phenocrysts have been altered (low-grade greenschist metamorphism) to aggregates of Fe-poor chlorite, Fe-poor chlorite-sphene, and calcite-qtz-sphene. Some of the sphene occurs as radially-grown spheres.

Groundmass: structureless cryptocrystalline quartz-Fe-rich chlorite-albite-calcite.

(No. 75360028)

Possibly sedimentary as quartz phenocrysts are generally not embayed, although some are angular. However, texture is similar to that of rhyodacites already described. Feldspar phenocrysts are replaced by sericite, clay or calcite; mafics (biotite, hornblende) replaced by colourless chlorite + opaques.

Groundmass consists of quartz, clay, calcite, sericite.

(No. 75360030)

Probably sedimentary. Sub-angular quartz fragments occur in all sizes from micro-crystalline matrix to 1.5 mm (40%) and feldspar fragments comprise 25 percent of rock. Matrix consists of quartz clay-feldspar-calcite-opaques-chlorite no structure observed (sed. or volcanic).

Willow Bridge rhyolite (dark grey)

(No. 74360060)

This sample (like most of those described) is comprised of distinct phenocryst and groundmass phases, each making up about 50 percent of the total rock.

Phenocrysts: i) clear, sometimes strained, quartz, 30 percent of total rock, from .05 mm (microphenocrysts) to 5 mm, mostly fragmented as well as embayed. Original crystal faces are either rounded or hexagonal (indicating high temperature origin).

ii) sericitized anhedral plagioclase (15%), smaller than quartz (indicating relatively deep level of derivation), also fragmented.

iii) sericite and chlorite (+ opaques) pseudomorphs after biotite. Strongly deformed - probably during solidification of groundmass, as the contortions parallel the groundmass flow structure.

iv) rare CPX.

Groundmass: Cryptocrystalline partly devitrified Qtz, Kspar, plag. Well-defined flow structure.

Accessory. Apatite, magnetite, zircon, goethite.

Willow Bridge dacite (dark grey and near base of unit)

(No. 74360061)

Similar to 0060 except (i) phenocrysts comprise 35 percent instead of 50 percent of total rock, (ii) groundmass is fully devitrified, consequently flow pattern in the groundmass has been destroyed; deformed former biotite laths indicate that flow structure did originally exist.

Willow Bridge dacite (dark grey)

(No. 75360022) As for 74360061. Phenocrysts: (50%) fragmented phenocrysts and microphenocrysts, plagioclase, oscillatory zoned, twinned.

Groundmass: very dark, due to density of opaques, only incipient devitrification; flow structure evident.

(No. 75360023) As for 75360022. Biotite (now chlorite or sericite, + opaques) is strongly deformed and is strung out to narrow elongate laths concordant with the excellent groundmass flow structure; also crenulated.

NOTE: the chlorite replacing biotite is an intermediate biotite to chlorite alteration product, having higher birefringence than chlorite (same order of birefringence as sericite). Magnetite and apatite are accessory.

(No. 75360024) Porphyritic dacite (as for 0023)

(No. 75360025) Mineralogy as for 0023, 0024. Phenocrysts, fragmented phenocrysts and microphenocrysts comprise 50% of rock. Biotite is unaltered and undeformed, i.e. red-brown phenocrysts.

Willow Bridge dacite (light grey)

(No. 75360026) As for 0025. Phenocrysts: Nearly all fragmented. Biotite quite fresh, dark brown-pale green. Plagioclase shows good twinning and zoning (Ano - 10). No K-feldspar phenocrysts. Magnetite phenocrysts abundant.

Fresh orthophyroxene phenocrysts occur rarely and carry zircon inclusions.

Groundmass: Completely devitrified, quartz-albite-K-feldspar-chlorite.

(No. 75360027) Phenocrysts: Fragmented phenocrysts and microphenocrysts make up 50 percent of rock. They include embayed, generally rounded, non-undulose quartz, up to 5 mm diameter; smaller subhedral partly sericitized twinned plagioclase, zoned Ano - 10; strongly deformed chlorite + opaque pseudomorphs after biotite, chlorite pseudomorphs after hornblende.

Groundmass: devitrified crytocrystalline, no flow structure remaining.

Willow Bridge rhyolite (light grey)

(No. 74360069)

Phenocrysts: Comprise 40 percent of total rock. Most of these are qtz, clear, highly fragmented, all with sharp angular edges. Both plagioclase (albite-twinning) and potash feldspar (microcline-twinning) occur. Some K-feldspar phenocrysts are altered to qtz-sericite. Biotite microphenocrysts (8%) are altered to opaques + epidote, and carry abundant zircon inclusions.

Groundmass: is devitrified, rarely recrystallized.

Granite Porphyry

(No. 74360062, 63)

Similar mineralogy to 0060, 61 except for higher proportion of mafics in 0062, 63.

Phenocrysts. As for 0061 except quartz and plagioclase are both commonly 4 mm (indicating shallower level of commencement of crystallization than for 0061). Plagioclase is twinned, euhedral, composition not determinable because of sericitization.

Mafic phenocrysts (biotite, clinopyroxene) are pseudomorphed by quartz-chlorite + calcite, sphene-chlorite-opaque oxide or sericite aggregates.

Groundmass. (50% of total rock) Fine-grained; probably recrystallized volcanic groundmass.

(No. 75360029)

Phenocrysts: (40%) Large, embayed quartz, heavily corroded feldspars (to sericite, calcite, clay, dusted with opaques). Mafics altered to epidote or colourless chlorite + opaques. Calcite abundant in groundmass; associated with this calcite are abundant tiny (.05 mm) euhedral magnetites.

This rock seems to have partly sedimentary content.

TABLE G. CHEMICAL ANALYSES

	Green Rhyolite			Mount Painter Porphyry					Walker Volcanics Lower sequence	
	Tuggeranong tunnel		CST area	Mount Painter area					CST area	
Location (1:100 000 series)	Sta. 244+15	Sta. 246+35	811883 D1	878953	877952	958866	944872	938864	800000 E2	803018 E1
Registration No.	75840014	75840015	73840101	74840003	74840004	74840085	74840086	74840088	75840018	75840019
SiO ₂	71.84	72.99	80.25	68.40	67.15	65.65	66.52	65.03	68.00	66.70
TiO ₂	0.22	0.23	.22	.57	.54	.59	.57	.58	0.46	0.59
Al ₂ O ₃	12.93	13.33	10.74	13.89	13.74	14.13	14.06	13.88	10.78	14.00
Fe ₂ O ₃	1.39	0.53	.28	.81	.98	.30	.40	.46	1.16	0.26
FeO	0.55	0.90	.07	4.47	4.34	4.52	4.20	4.62	5.09	4.55
MnO	0.04	0.03	.01	.06	.09	.10	.07	.10	0.13	0.13
MgO	0.59	0.49	.23	2.92	3.09	3.09	2.80	2.80	4.01	2.65
CaO	2.49	1.73	.03	2.09	2.39	1.74	1.52	2.06	2.35	2.54
Na ₂ O	0.75	1.12	.52	1.73	1.82	2.10	1.92	1.38	1.08	2.58
K ₂ O	4.12	3.78	5.94	3.38	2.81	3.86	4.27	4.67	1.52	2.78
P ₂ O ₅	0.06	0.06	.05	.11	.11	.09	.07	.07	0.10	0.11
H ₂ O ⁺	2.23	2.47	.87	2.41	2.69	2.75	2.44	2.78	3.43	2.39
H ₂ O ⁻	0.47	0.51	.15	.11	.13	.13	.08	.10	0.23	0.11
CO ₂	1.95	1.80	.05	.05	.05	.75	.40	1.40	0.45	0.25
Cu	20	14	8	28	66	30	22	30	34	36
Zn	45	50	52	104	84	114	71	104	110	98
Co	2	3	6	20	16	2	4	2	6	2
Ni	2	14	2	24	20	22	36	28	22	16
Cr	15	15	25	75	80	85	80	85	75	75
V	35	50	5	135	130	145	170	180	170	140
Ba	620	540	530	580	500	620	640	640	380	540
Ce	80	100	40	80	70	60	80	80	100	110
La	40	60	30	40	60	50	60	60	40	50
Pb	36	34	30	14	20	12	6	12	36	34
Rb	240	210	260	150	130	170	160	200	75	135
Sr	50	100	50	130	130	100	80	44	110	160
Th	18	18	16	16	16	12	14	16	12	14
U	6	8	6	4	4	4	4	4	4	6
Zr	115	125	145	190	185	175	175	195	100	200
Nb	10	10	4	4	8	4	4	6	10	10
Y	30	30	20	20	20	25	25	30	25	25

TABLE G. (contd.)

	Walker Member (Purcell, in prep.)					Willow Bridge Tuff				
	Pine Ridge tunnel					North of Ginninderra Creek				
Location (1:100 000 series)	Stn. 23+70	Stn. 50+00	Stn. 26+50	Stn. 45+00	Stn. 45+00	759104	773123	757133	739214	803221
Registration No.	73840487	73840488	73840489	73840490	73840491	73840438	73840438	73840440	73840446	73840449
SiO ₂	67.78	68.42	67.84	65.86	66.80	67.98	69.63	7.193	69.88	67.80
TiO ₂	.54	.51	.55	.62	.55	.51	.46	.31	.41	.50
Al ₂ O ₃	13.95	12.86	14.10	14.37	13.68	14.04	14.67	14.00	14.04	15.18
Fe ₂ O ₃	2.12	2.58	.87	3.62	3.32	1.39	1.53	.15	1.05	1.25
FeO	2.08	3.73	4.06	1.63	1.63	2.35	1.98	1.73	2.14	2.44
MnO	-	.09		.08	.09	.04	.04	.03	.05	.05
MgO	1.70	1.63	1.92	1.70	1.46	1.43	1.30	.52	1.27	1.37
CaO	1.73	.41	.32	1.44	1.83	3.81	3.05	.73	3.10	3.70
Na ₂ O	2.33	.72	1.27	1.22	1.38	2.48	2.52	4.00	2.66	2.80
K ₂ O	3.55	5.46	6.43	6.46	5.88	2.85	3.29	4.49	3.16	2.97
P ₂ O ₅	.11	.11	.14	.13	.12	.11	.10	.04	.08	.10
H ₂ O+	2.53	2.22	2.17	2.02	2.07	1.26	1.41	.87	1.22	1.54
H ₂ O-	.33	.26	.19	.22	.15	.16	.09	.13	.10	.10
CO ₂	.90	.05	.05	.55	1.05	.05	.10	.05	.05	.05
Cu	14	8	6	6	12	18	20	44	24	22
Zn	56	55	53	50	58	59	45	56	50	74
Co	6	8	8	6	6	10	18	2	4	2
Ni	20	15	20	18	18	10	13	10	13	18
Cr	65	60	50	55	85	30	30	20	30	30
V	130	110	140	150	150	83	80	38	85	100
Ba	450	1180	1020	1330	1310	600	660	700	640	620
Ce	70	60	60	70	70	70	80	70	80	80
La	40	40	40	40	30	40	60	50	50	50
Pb	105	6	10	14	1150	14	14	4	22	18
Rb	250	240	230	310	280	110	125	180	120	120
Sr	95	40	45	60	50	195	185	190	180	220
Th	16	16	16	12	18	14	14	22	14	16
U	4	6	6	4	4	4	4	4	4	6
Zr	180	160	180	170	190	200	200	220	180	210
Nb	5	5	5	10	10	5	5	5	5	5
Y	30	30	30	30	25	25	30	30	25	25

TABLE G. (contd.)

	Willow Bridge Tuff								
	North of Ginninderra Creek								Dark grey near B.W.P.C.C.
Location (1:100 000 series)	783105	780130	822120	814153	802187	785160	738111	724107	822027 K3
Registration No.	73840455	73840457	73840458	73840460	73840463	73840464	73840465	73840470	73840020
SiO ₂	70.42	69.33	74.92	68.80	67.98	67.91	68.09	68.61	72.01
TiO ₂	.41	.46	.16	.53	.47	.49	.52	.48	0.31
Al ₂ O ₃	14.32	14.43	12.92	15.40	14.99	14.31	15.05	14.61	13.34
Fe ₂ O ₃	1.06	1.32	.89	1.44	1.11	1.19	1.41	1.21	0.85
FeO	2.14	2.11	.81	2.40	2.44	2.46	2.46	2.29	1.49
MnO	.05	.05	.05	.06	.06	.06	.06	.06	0.03
MgO	1.19	1.23	.55	1.49	1.51	1.73	1.57	1.72	0.95
CaO	3.49	3.66	.83	4.13	3.65	2.77	2.96	1.15	2.17
Na ₂ O	2.48	2.54	2.82	2.64	2.56	2.92	3.02	4.18	2.79
K ₂ O	3.01	3.03	5.09	2.94	3.03	3.20	3.27	3.48	3.93
P ₂ O ₅	.09	.10	.04	.11	.11	.10	.11	.09	0.12
H ₂ O ⁺	1.09	1.35	.78	1.13	1.27	1.45	1.53	1.42	1.04
H ₂ O ⁻	.11	.11	.18	.11	.11	.17	.19	.22	0.04
CO ₂	.05	.05	.05	.05	.05	.05	.05	.10	0.05
Cu	20	22	14	22	22	20	20	14	24
Zn	46	56	30	63	46	53	66	43	35
Co	10	14	4	4	2	10	10	8	2
Ni	13	18	13	15	15	18	15	18	12
Cr	20	20	10	25	25	20	23	25	20
V	85	98	40	113	98	100	100	100	35
Ba	580	600	400	620	620	620	620	580	680
Ca	90	90	90	80	80	70	80	80	130
La	40	40	60	50	40	50	50	30	70
Pb	20	18	24	14	18	26	16	10	46
Rb	120	130	230	120	120	120	130	110	155
Sr	190	190	85	210	200	200	190	155	170
Th	14	16	18	10	14	14	12	16	22
U	4	4	4	4	4	4	4	4	4
Zr	170	180	95	200	200	200	200	190	140
Nb	5	5	5	5	5	5	5	5	10
Y	25	25	80	25	25	30	25	25	25

APPENDIX 6
GROUNDWATER DATA

Conductivity and pH of water samples from GST bores.

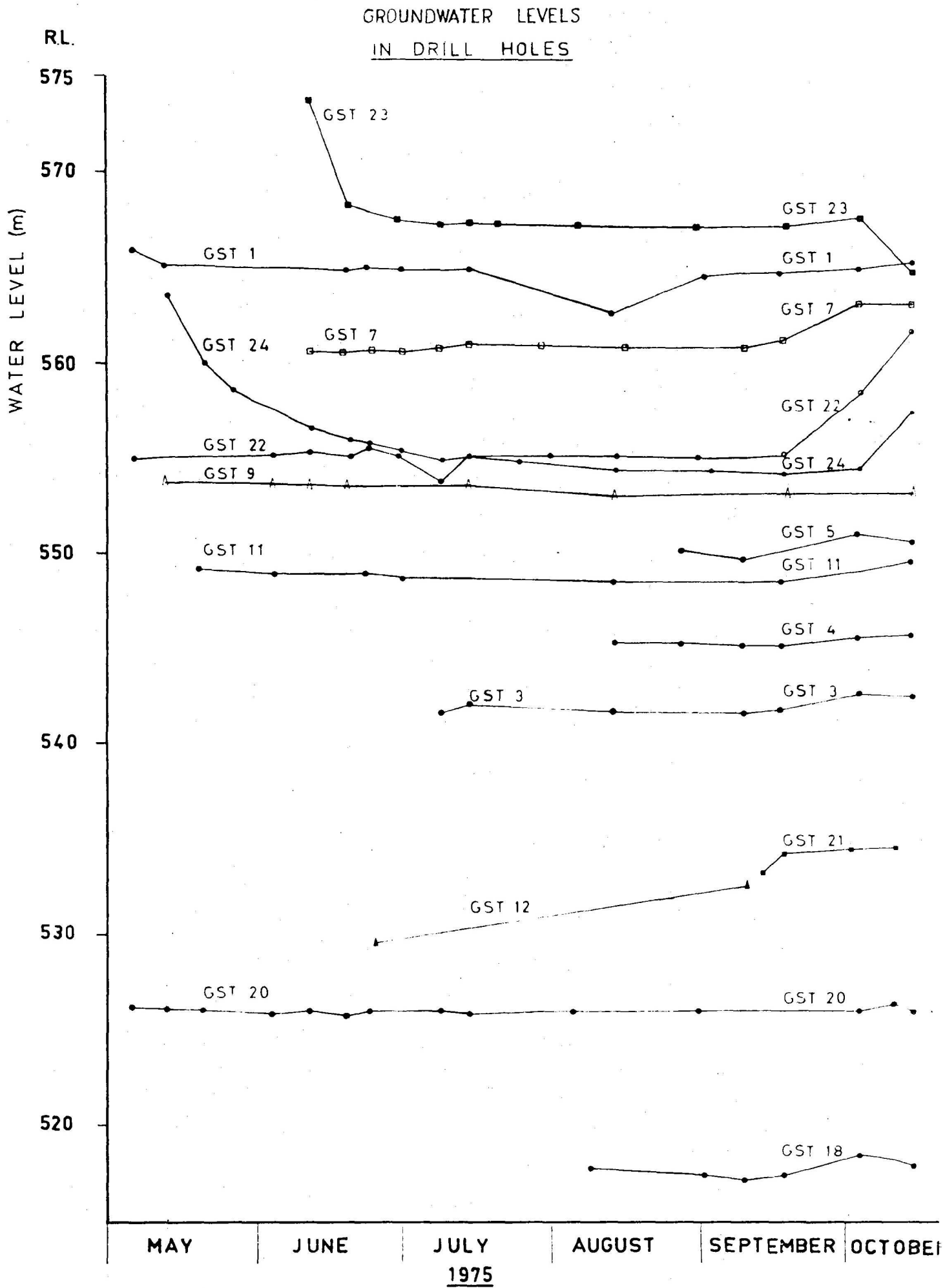
Date of sampling 14/10/75

		Specific Conductance cm^{-1}	pH
GST	3	367	6.4
	4	550	6.0
	5	550	6.5
	7	1520	6.2
	17	608	5.8

Date of sampling 11/11/75

GST	17	688	5.9
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FIGURE A



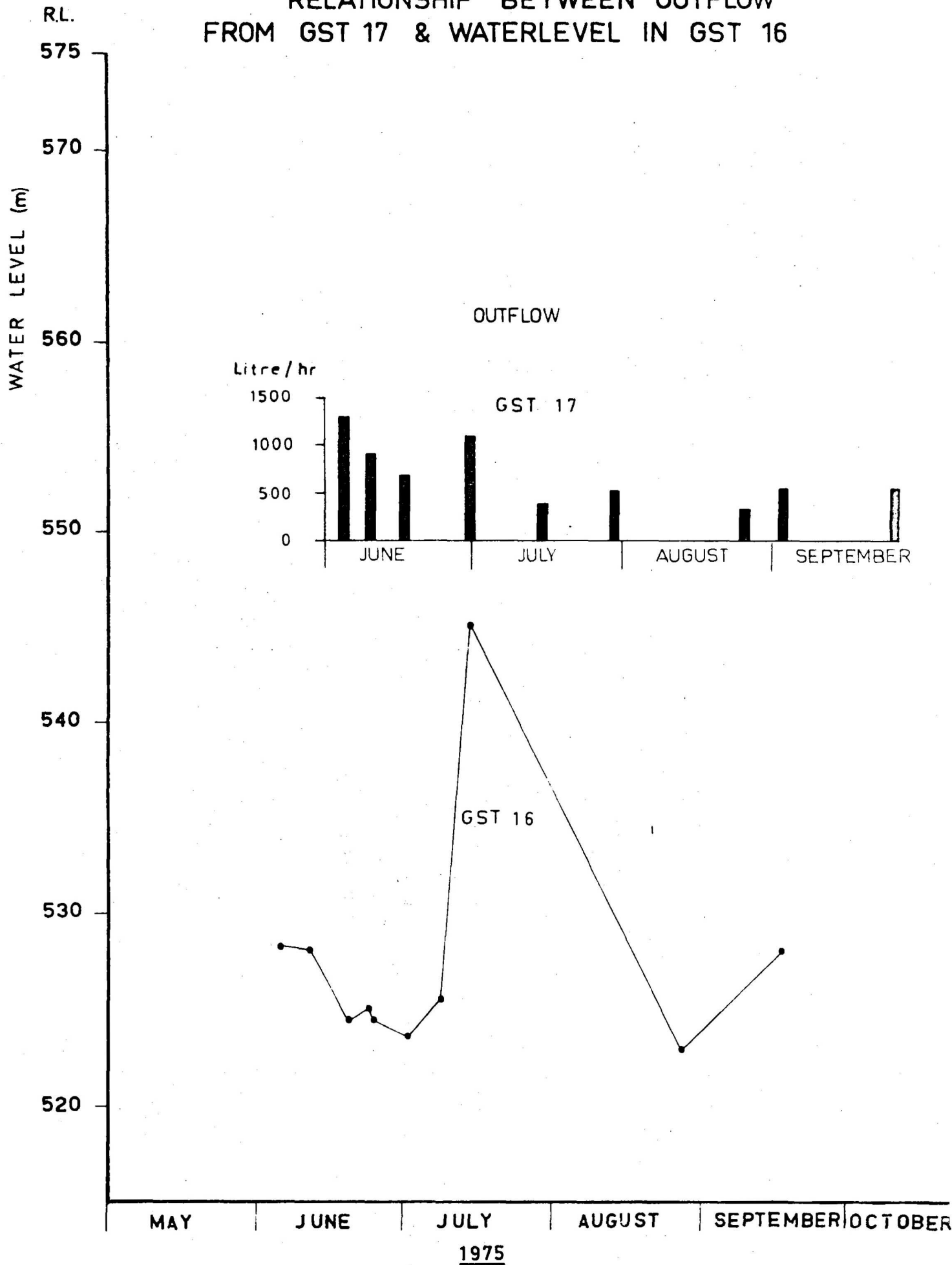
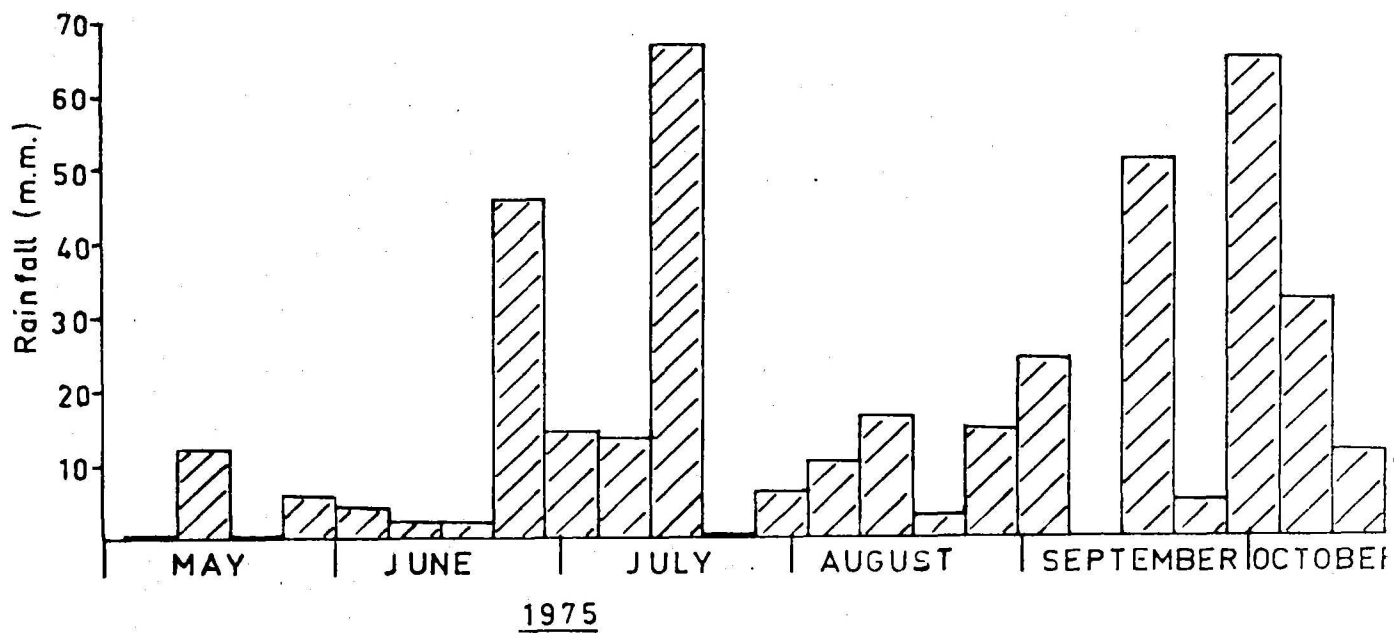
RELATIONSHIP BETWEEN OUTFLOW
FROM GST 17 & WATERLEVEL IN GST 16

FIGURE C

RAINFALL RECORDINGS FOR GST AREA

* Data taken from Bureau of Meteorology Report:
Year 1975; Station 070059; Belconnen (Weetangera);
Lat. 35°15'S, Long. 149°3'E; Elevation 624.7 m.

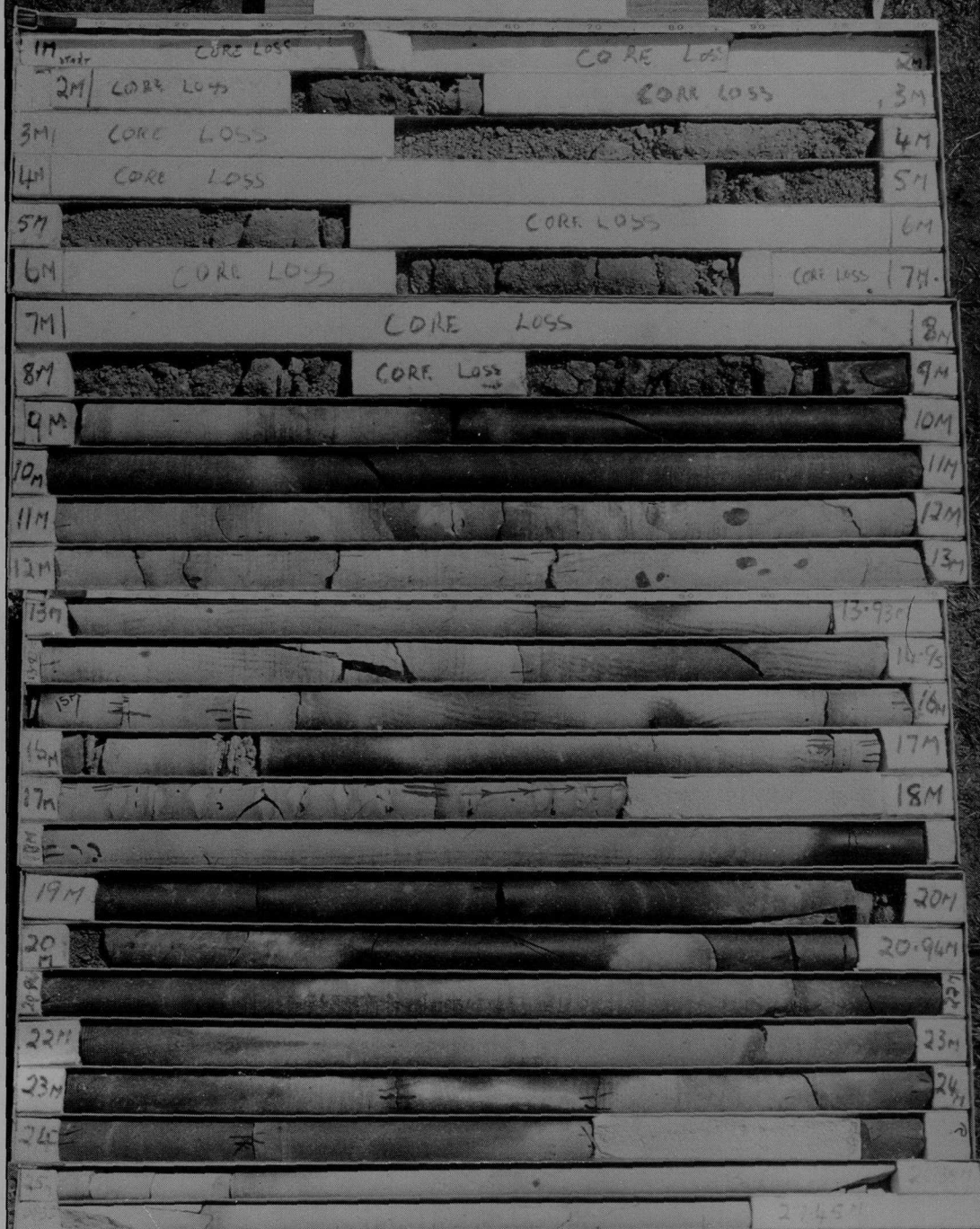
-81-

APPENDIX 7

DRILL CORE PHOTOGRAPHS

GINNINDERRA SEWER TUNNEL

GST 3

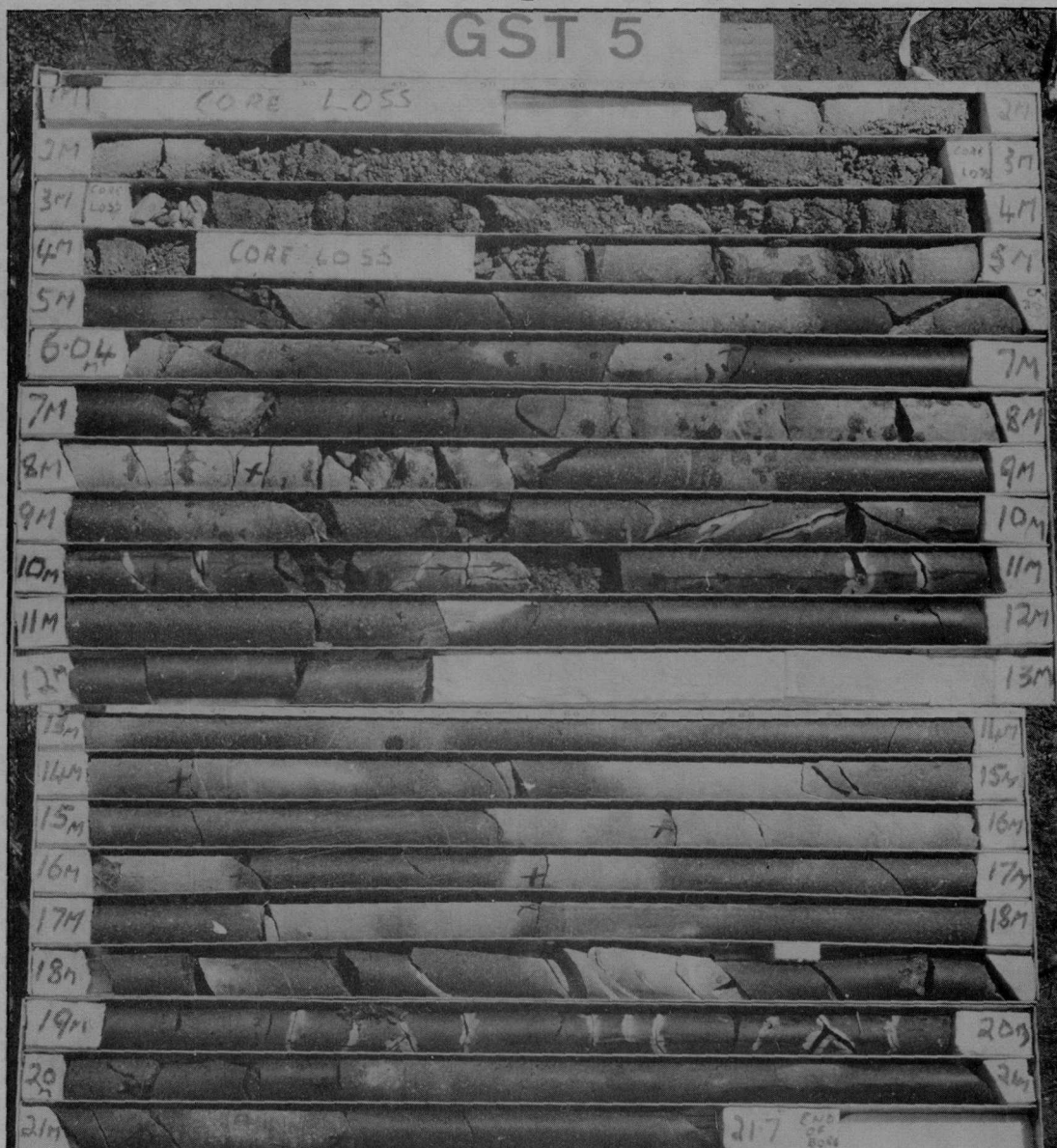


GINNINDERRA SEWER TUNNEL

GST 4



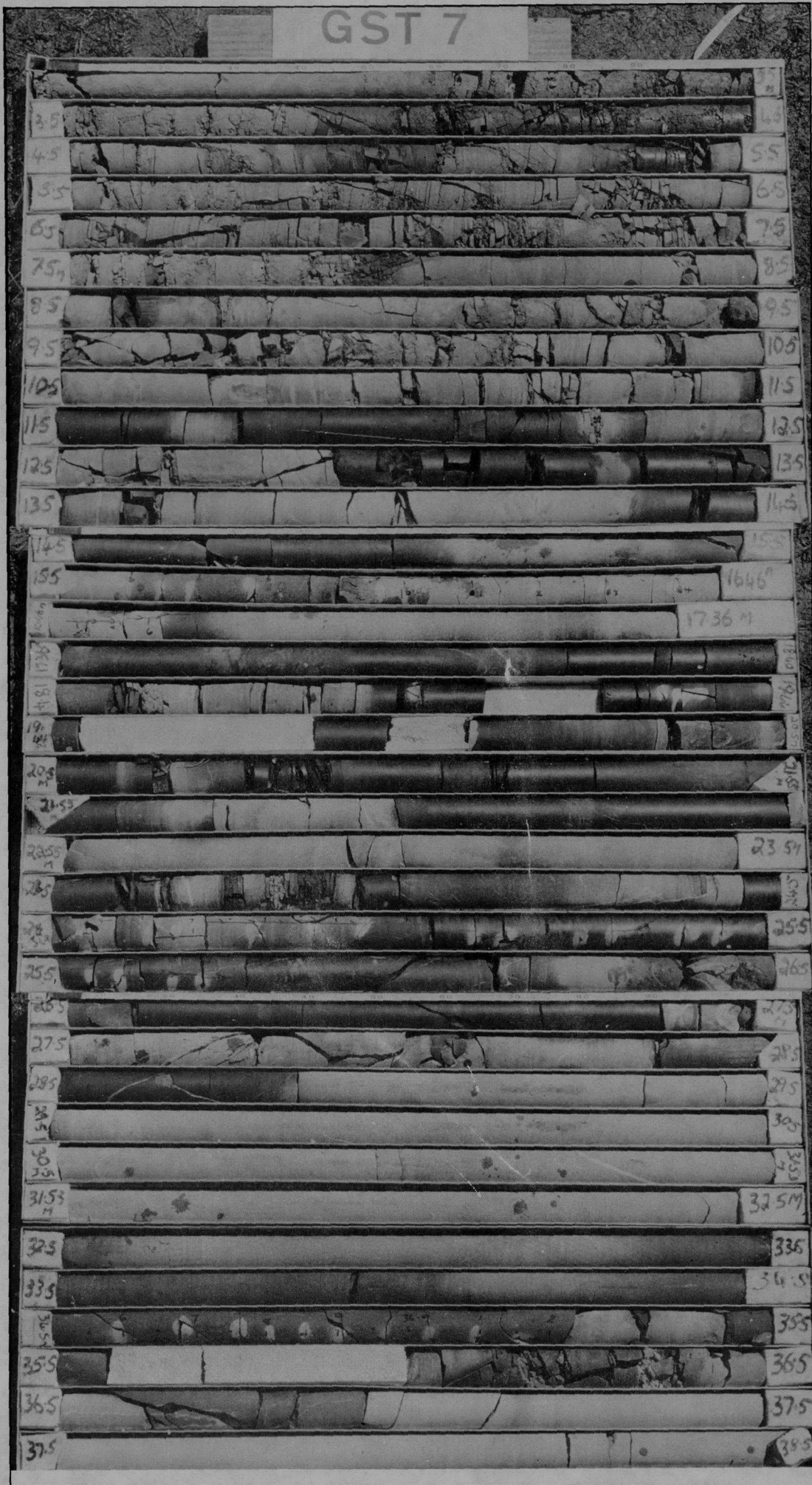
GST 5



GINNINDERRA SEWER TUNNEL GST 6

9M	ROCK ROLLED	CORE LOSS	10M
10M			11M
11M		CORE LOSS	12M
12M		CORE LOSS	13M
13M	CORE LOSS		14M
14M			15M
15M	CORE LOSS		16M
16M			17M
17M			18M
18M			19M
19M			20M
20M			21M
21M			22M
22M			23M
23M			24M
24M		CORE LOSS	25M
25M	CORE LOSS		26M
26M	CORE LOSS		27M
27M			28M
28M		CORE LOSS	29M
29M		CORE LOSS	30M
30M	CORE LOSS		31M
31M	CORE LOSS		32M
32M	CORE LOSS	MATERIAL AS ABOVE FROM BORE WASHINGS	33M

GST 7



GINNINDERRA SEWER TUNNEL

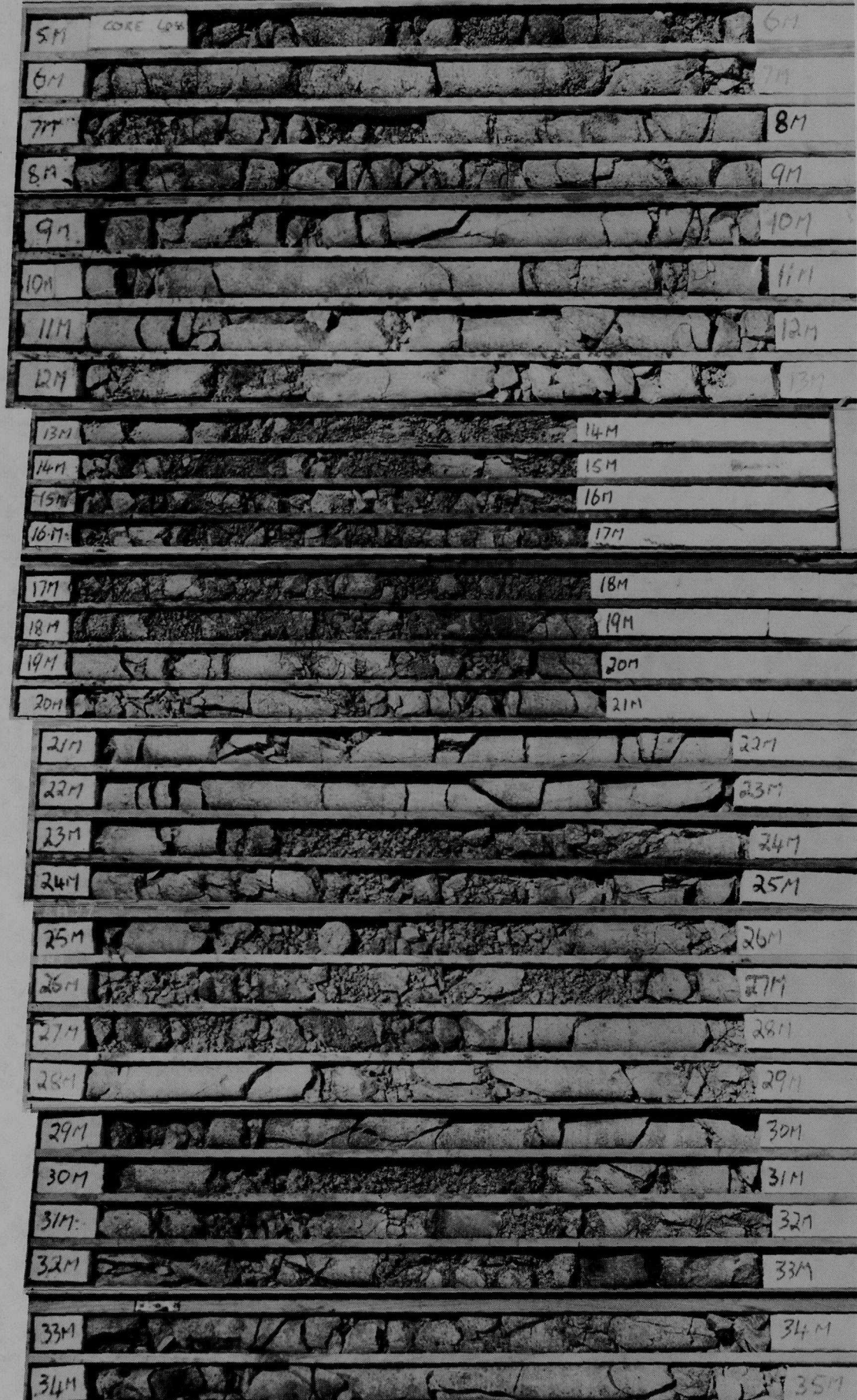


GINNINDERRA

SEWER

TUNNEL

GST8



GINNINDERRA SEWER TUNNEL



GINNINDERRA SEWER TUNNEL



GINNINDERRA SEWER TUNNEL



GINNINDERRA SEWER TUNNEL



GINNINDERRA SEWER TUNNEL

GST 12



GINNINDERRA SEWER TUNNEL

GST 12

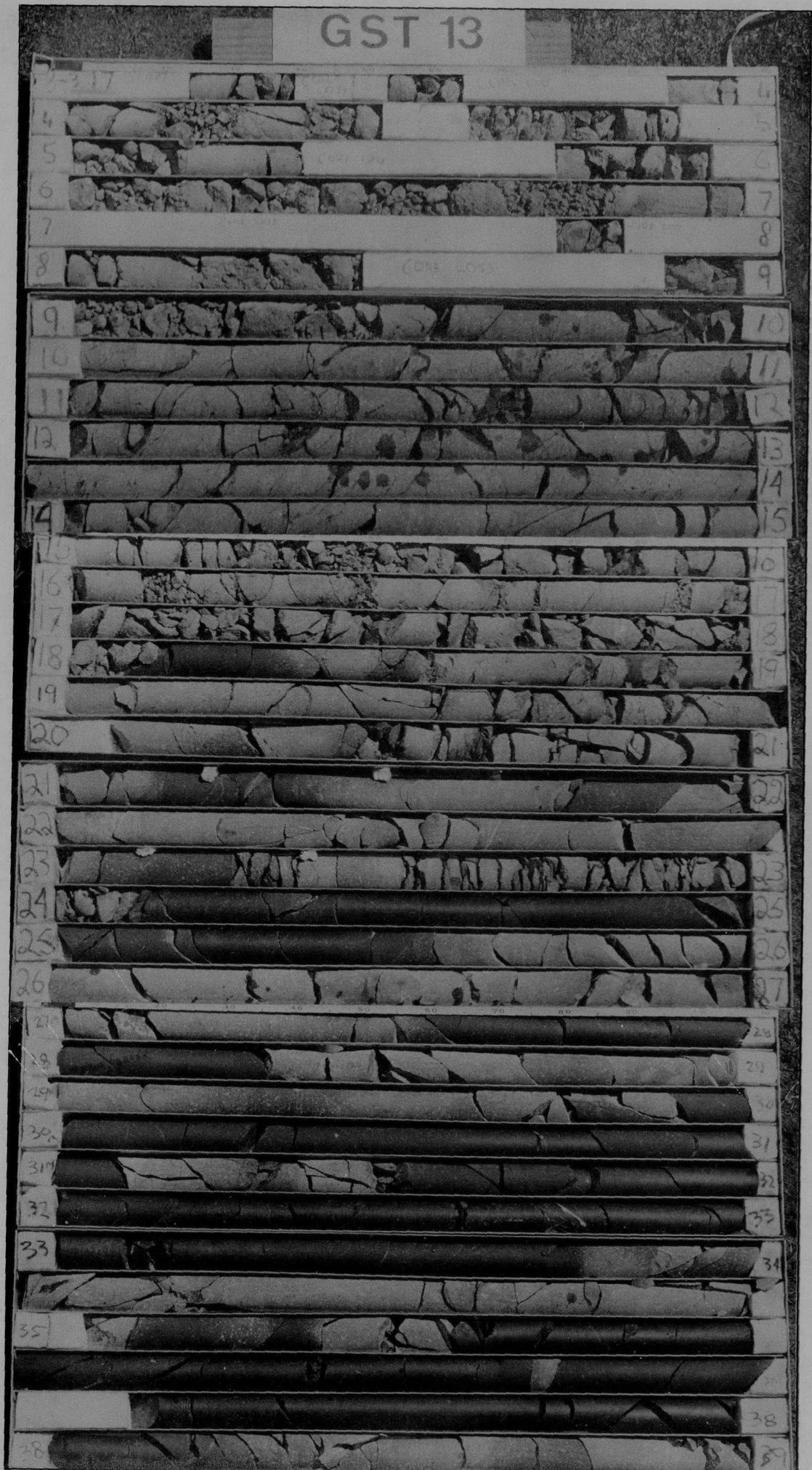


GST 12



GINNINDERRA SEWER TUNNEL

GST 13



GINNINDERRA SEWER TUNNEL

GST 13



GINNINDERRA SEWER TUNNEL

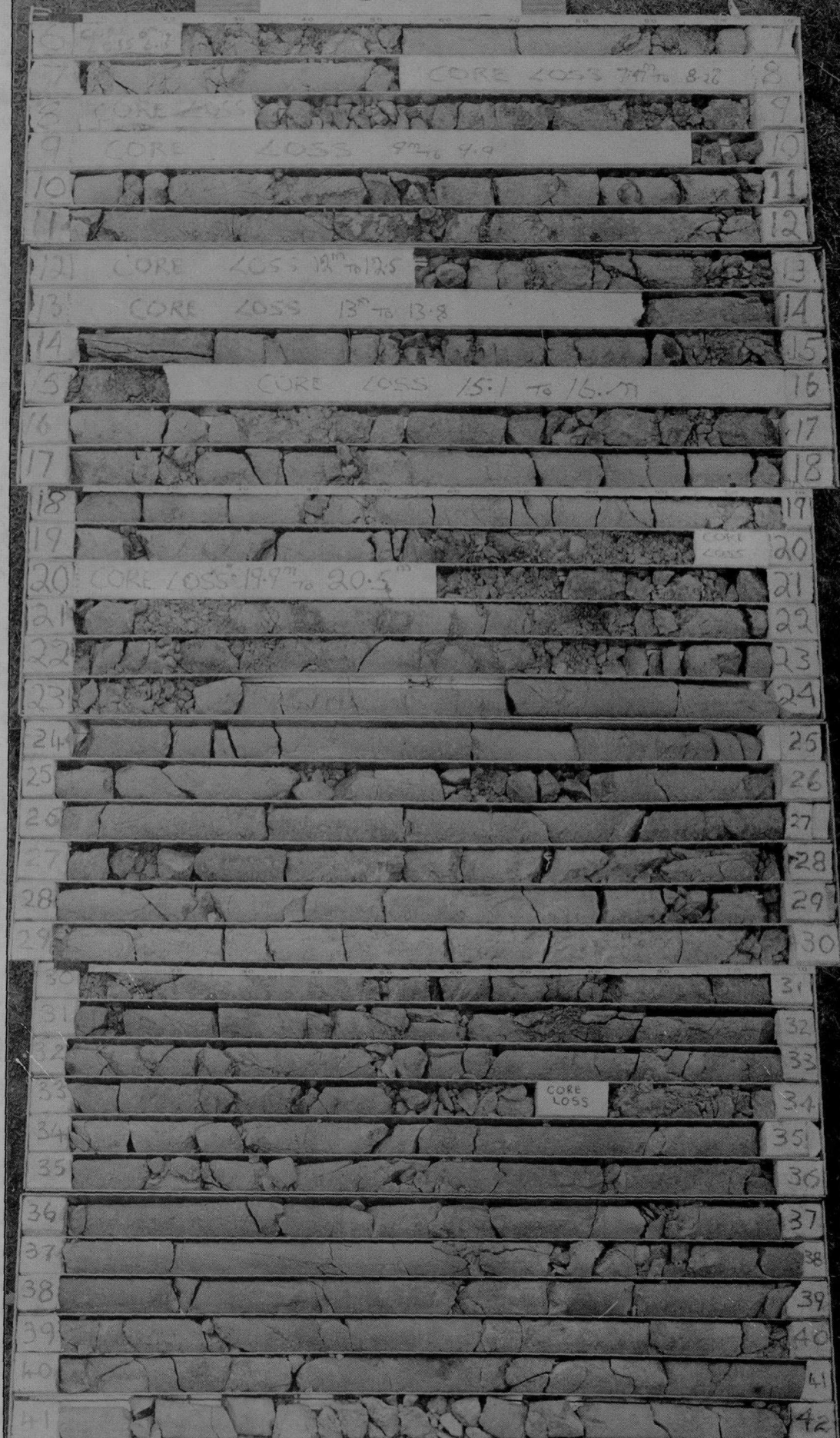
GST 13



GST 14



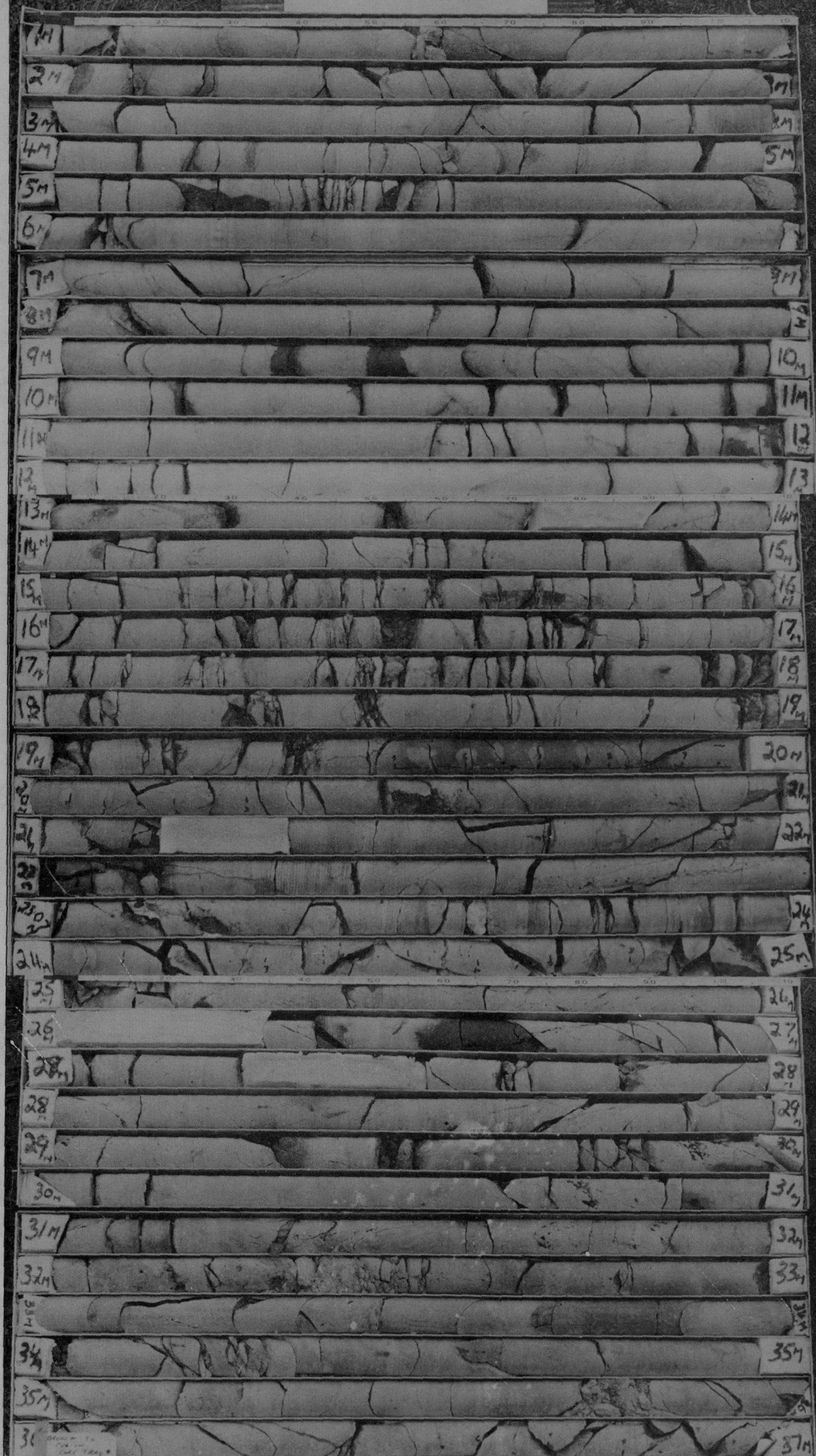
GST 15



GST 15



GST 16



GST 16

37		38
38		39
39		40
40		41
41		42
42		43
43		44
44		45
45		46
46		47
47		48
48		49
49		50
50		51
51		52
52		53
53	53.15M	END OF BORE

GST 17



GST 18

0m	Roller - ROLL TO 0.5M	1M
1M		2M
2M		3M
3M		4M
4M		5M
5M		6M
6M		7M
7M		8M
8M		9M
9M		10M
10M		11M
11M		12M
12M		13M
13M		14M
14M		15M
15M		16M
16M		17M
17M		18M
18M		19M
19M		20M
1995	20.7M END OF BOFF	

APPENDIX 8

GEOLOGICAL LOGS OF DIAMOND-DRILL HOLES

GEOLOGICAL LOG OF DRILL HOLE

SHEET 1 of 4

Rock Type and Degree of Weathering	Description Lithology, colour, strength, etc	Core Graphic Log	Loss and % core recovery	Defect Log	Fracture Log	RQD	Defect spacing Intercept Angle 30 60 90	Structures Joints, veins, seams, faults, etc	Water Level	Water Pressure Test Losses (Lugeons) *
NOT CORED										
			4.57							
NO CORE			25%							
EW Granite Porphyry	Yellow brown clayey sand to sandy clay.		7.01			N/A 0		SOIL PROPERTIES		
NO CORE			40%							
EW Granite Porphyry	Yellow brown clayey sand.		9.14			N/A 0		SOIL PROPERTIES	22/1/75	
NO CORE			35%						5/5/75	
EW Granite Porphyry	Yellow brown clayey sand.		11.58			N/A 0		SOIL PROPERTIES		
NO CORE			50%							
EW Granite Porphyry	Yellow brown clayey sand.		13.11			N/A 0		SOIL PROPERTIES		
NO CORE			10%							
HW	Yellow grey brown HW granite, qtz, feldspar + biotite. Phenocrysts up to 4mm. Weak, soft.		16.15			N/A 0				
NO CORE			0%							
			19.20							
			15%							

Drill type MAYHEW 1000
Feed HYDRAULIC
Core barrel type TREIFUS
HQ WIRE LINE
Driller L. KEAST (BMR)
Commenced 6/12/74
Completed 14/1/75
Logged by P.A. LANG
Vertical scale 1cm = 1m

Checked by D.C.R.

Notes

Fracture Log — Number of fractures per 25 cm of core. Zones of core loss blacked in. Healing and Joint Planes — Angles are measured relative to a plane normal to the core axis.

Defect spacing — or spacing of natural defects (shears, joints, fractures) occurring at specified intercept angle range.

Water Level Measurements — ∇ Level when hole in progress at specified depth.
 ∇ Level in completed hole on specified date.



EW-HW GRANITE PORPHYRY



NO CORE

N/A NOT APPLICABLE

Water Pressure Tests

* values in lugeons should be read in conjunction with computation sheets. Test sections are indicated by blacked in strips.

Core Photograph Negative No
Depth (m) Black & White Colour

155/A16/1467 1 of 4

SHEET 2 OF 4

[illegible]

ANGLE FROM HORIZONTAL (θ) 0 DIRECTION -
COORDINATES 198417E 612416N R.L. OF COLLAR 573.9m

SHEET 4 OF 4

[illegible]

Drill type MAYHEW 1000

Feed HYDRAULIC

Core barrel type TREIFUS

HQ. WIRE LINE

Driller L. KEAST (BMR)

Commenced 6/12/74

Completed 14/1/75

Logged by P A LANG

Vertical scale 1 cm = 1 m

Notes

Fracture Log — Number of fractures per 25 cm of core. Zones of core loss blacked in
Bedding and Joint Planes — Angles are measured relative to a plane normal to the core axis

Defect spacing - av spacing of natural defects (shears, joints, fractures) occurring at specified intercept angle range

Water Level Measurements - 1 Level when hole in progress at specified depth
2 Level in completed hole on specified date

Water Pressure Tests

* Values in lugeons should be read in conjunction with computation sheets. Test sections are indicated by blocked in strips.

Core Photograph Negative No		
Depth (m)	Black & White	Colour

SEE PREVIOUS

Checked by DCP

155/A16/1467 4 of 4

BUREAU OF MINERAL RESOURCES,
GEOLOGY & GEOPHYSICS

GEOLOGICAL LOG OF DRILL HOLE

PROJECT GINNINDERRA SEWER TUNNEL*

LOCATION At station 9+97m. on centre line of old alignment of
tunnel at northend, 800m. north of Parkwood Road, A.C.T.
ANGLE FROM HORIZONTAL (°) 90 DIRECTION
COORDINATES 199039E 6118811 R.L. OF COLLAR 5635m.

HOLE NO. G.S.T.

2.

CANBERRA 101

SHEET 1 OF 3

Drilling Information				Rock Substance		Rock Mass Defects						
Method	Casing	Water	Pressure test * (lugeons)	Lift & % core recovery	Depth (metres)	Graphic log & core loss	Substance description rock type: grain characteristics colour, structure, minor components.	Weathering	Strength Is (50) (MPa)	Defect spacing (cm)	Defect description thickness, type, inclination, planarity, roughness, coating, strength. Particular General	Rock condition No
DIAMOND DRILLING WITH BQ CORE LA. NO.	NOT RECORDED	30/1	NOT TESTED	NOT CORED	1	NOT CORED	DACITE Light grey, very hard, very strong. Quartz phenocrysts up to 3mm., pink feldspar phenocrysts. Calcite and epidote veins common.	MW to SW	0.3 0.5 0.003 0.001 0.002	0.003 0.001 0.002	Core fragmented most breaks (70%) at 30°-45°. 10% at 80°-90°. 20% at 0-30°.	2
					2							
					3							
					4							
					5							
					6							
					7							
					8							
					9							
					10							
					11							
					12							
					13							
					14							
					15							
					16							
					17							
					18							
					19							
100%	100%	100%	100%									
Joint, tight. Planar and rough to smooth. Cemented with pink calcite (cement moderately strong). Calcite and epidote veins up to 1 cm. (strong).												3

Drill type Gemco
Feed Hydraulic
Core barrel type BQ L 1/2
with WIRE LINE
Driller G. Brandon (BMA)
Commenced 20-11-74
Completed 12-2-75
Logged by P. Lang
Vertical scale 1cm=1m

Weathering
Fr — Fresh
SW — Slightly weathered
MW — Moderately weathered
HW — Highly weathered
EW — Extremely weathered

Notes:

Bedding & Joint Planes — Angles are measured relative to a plane normal to the core axis.
* Water Pressure Tests — Values in lugeons should be read in conjunction with computation sheets. Test sections are indicated by blacked in strips.

Water

10 Oct. '73 water level date shown
Water inflow
Partial drilling water loss
Complete drilling water loss

Core Photograph Negative No.

Depth (m) Black & White Colour

155/116/1468 1 of 3

GEOLOGICAL LOG OF DRILL HOLE

PROJECT GINNINDERRA SEWER TUNNEL

LOCATION ~~at station 131~~ line of old alignment of

tunnel at north end 800m north of Packwood Rd. A.C.T.

ANGLE FROM HORIZONTAL (°) 90 DIRECTION

COORDINATES 199039E 11885N R.L. OF COLLAR 5535.61

HOLE NO GST

2

CANBERRA 109

SHEET 2 OF 3

Drilling Information				Rock Substance		Rock Mass Defects			Rock condition No.			
Method	Casing	Water	Pressure test * (lugeons)	Lift & % core recovery	Depth (metres)	Graphic log & core loss	Substance description rock type: grain characteristics colour, structure, minor components.	Weathering		Strength Is (50) (MPa)	Defect spacing (cm)	Defect description thickness, type, inclination, planarity, roughness, coating, strength. Particular General
DIAMOND DRILLING - WIRELINE WITH DOUBLE TUBE BQ CORE BARREL (1 7/16")												Joints very tight. Planar and rough to smooth. Joints generally cemented with pink to yellow calcite. Cement moderately strong. Calcite and epidote veins up to 1 cm wide spaced 10 cm to 2 m. Rock would tend to break along these veins and cemented joints when blasted.
TESTED				100%	21	✓✓✓✓✓	DACITE Light grey, very hard, very strong. Pink calcite & green epidote veins from 2mm to 2cm wide, spaced 30cm to 2 m.	FR	0.03 0			

Drill type Gemco
Feed Hydraulic
Core barrel type BQ 1 7/16"
Casing WIRE LINE
Driller G. Brandon (BMR)
Commenced 20-11-74
Completed 19-2-75
Logged by P. Lang
Vertical scale 1cm = 1m

Weathering

Fr - Fresh

SW - Slightly weathered

MW - Moderately weathered

HW - Highly weathered

EW - Extremely weathered

Notes:

Bedding & Joint Planes - Angles are measured relative to a plane normal to the core axis.

* Water Pressure Tests - Values in lugeons should be read in conjunction with computation sheets. Test sections are indicated by blocked in strips.

Water

10 Oct. '73 water level date shown

Water inflow

Partial drilling water loss

Complete drilling water loss

Core Photograph Negative No.

Depth (m) Black & White Colour

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155/416/1468 2 of 3

BUREAU OF MINERAL RESOURCES,
GEOLOGY & GEOPHYSICS

GEOLOGICAL LOG OF DRILL HOLE

PROJECT GUNNINDERRA SEWER TUNNEL

LOCATION At station 9+91 m on centre line of old alignment of
tunnel at northern end of 300 m north of Backwood Road A.C.T.

ANGLE FROM HORIZONTAL (°) 30

COORDINATES 199039E 61885N

DIRECTION R.L. OF COLLAR 563.5m

HOLE NO. GSI

2

CANDERRA 101

SHEET 3 OF 3

Drilling Information				Rock Substance		Rock Mass Defects			
Method	Casing	Water	Pressure test * (lugeons)	Depth (metres)	Substance description rock type: grain characteristics colour, structure, minor components.	Weathering	Strength Is (50) (MPa)	Defect spacing (cm)	Defect description thickness, type, inclination, planarity, roughness, coating, strength. Particular General
							0.03 0.1 0.3 1.0 3.0 10.0	0.03 0.1 0.3 1.0 3.0 10.0	
DIAMOND DRILLING WITH BQ 1 1/2" WIRELINE SCALE TYPE CORE BARREL.				90%		Mainly Fr. Some SW in places.			Clay seams on joints up to 1 cm. thick.
				41	DACITE Light grey to dark grey to pink. Probably bedded ignimbrite with cone of alteration.				
				98%					
				42					
				100%					
				43					
				93%					
				44					
				93%	Light grey and pink with epidote calcite veins.	FR			
				85%					
				45					
				100%	-Dark grey	Mainly Fr, but with zones of alteration.			Rock hard Joints tight
				46	-Medium grey altered				
				47	-Pink				
					-Medium grey altered				
				75%					
				48					
				97%					
				50					
				51					
				97%	-Medium grey altered				
				52	-Pink altered				
				100%					
				53					
				100%					
				54					
				100%					
				55	Light grey Dacite				
				100%					
				56					
				100%					
				57					
				100%					
				58					
				100%					
				59					
				100%					

Drill type GEMCO
Feed Hydraulic
Core barrel type BQ 1 1/2"
WIRELINE
Driller G. Branton (BMR)
Commenced 26-11-74
Completed 19-2-75
Logged by F. Lang
Vertical scale 1 cm = 1 m

Weathering

Fr - Fresh
SW - Slightly weathered
MW - Moderately weathered
HW - Highly weathered
EW - Extremely weathered

Notes:

Bedding & Joint Planes - Angles are measured relative to a plane normal to the core axis.
* Water Pressure Tests - Values in lugeons should be read in conjunction with computation sheets. Test sections are indicated by blocked in strips.

Water

10 Oct. '73 water level date shown
Water inflow
Partial drilling water loss
Complete drilling water loss

Core Photograph Negative No.

Depth (m) Black & White Colour

155/418/1-168 3-68

GEOLOGICAL LOG OF DRILL HOLE

ANGLE FROM HORIZONTAL (θ) 30° DIRECTION

COORDINATES E198948 N612424

- - - - -
_ DIRECTION

COORDINATES E198948 N612424 B.L. OF COLLAR 547.1 m

SHEET 1 OF 2

Drilling Information				Rock Substance		Rock Mass Defects						
Method	Casing	Water	Pressure test * (lugeons)	% core recovery	Depth (metres)	Substance description rock type: grain characteristics colour, structure, minor components	RQD	Weathering	Strength Is (50) (MPa)	Defect spacing (cm)	Defect description thickness, type, inclination, planarity, roughness, coating, strength.	Rock condition No.
Rock Rolled											Particular	General
												</

Drill type MOLE
Feed Hydraulic
Core barrel type NMC with
fracture tube & split inner
Driller B. Harte (DHC)
Commenced 10/6/75
Completed 4/7/75
Logged by P. A. LANG
Vertical scale 1cm=1m

Weathering
Fr — Fresh
SW — Slightly weathered
MW — Moderately weathered
HW — Highly weathered
EW — Extremely weathered

Notes :

* **Water Pressure Tests**—Values in lugons should be read in conjunction with computation sheets. Test sections are indicated by blacked in strips.

Water

10 Oct. '73 water level date shown

Water inflow

Partial drilling water loss

Complete drilling water loss

Core Photograph Negative No.

Depth (m)	Black & White	Colour
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CPM (n)	Black & White	Color
100	100	100
200	200	200
300	300	300
400	400	400
500	500	500
600	600	600
700	700	700
800	800	800
900	900	900
1000	1000	1000

1557A16/1469 - 1 of 2 -

PROJECT GINNINDERRA SEWER TUNNEL
LOCATION At inlet drop shaft at station 4+99 on
centre line of tunnel
ANGLE FROM HORIZONTAL (θ) 90° DIRECTION —
COORDINATES E198948 N612424 R.L. OF COLLAR

SHEET 2 OF 2

ANGLE FROM HORIZONTAL (θ) 90°
COORDINATES E198948 N612424

DIRECTION -
R.L. OF COLLAR 547.1 m

TUNNEL

Weathering

Fr — Fresh

SW — Slightly weathered

MW — Moderately weathered

HW — Highly weathered

EW — Extremely weathered

Notes:

Bedding & Joint Planes — Angles are measured relative to a plane normal to the core axis.

* Water Pressure Tests — Values in lugeons should be read in conjunction with computation sheets. Test sections are indicated by blacked in strips.

Water	
10	Oct. '73 water level date shown
	Water inflow
	Partial drilling water loss
	Complete drilling water loss

Core	Photograph	Negative	No
Depth (m)	Black & White	Colour	

1551A1611469 2 of 2

GEOLOGICAL LOG OF DRILL HOLE

ANGLE FROM HORIZONTAL (θ) 90° DIRECTION -
COORDINATES E198916 N612225 R.L. OF COLLAR 556.8m

SHEET 1 OF 2

[illegible]





Drill type MOLE
Feed Hydraulic
Core barrel type NMLC with
triple tube split inner
Driller B. Harte (LHC)
Commenced 7/7/75
Completed 10/7/75
Logged by P.A. LANG
Vertical scale 1cm \equiv 1m

Weathering
Fr — Fresh
SW — Slightly weathered
MW — Moderately weathered
HW — Highly weathered
EW — Extremely weathered

Notes:

Bedding & Joint Planes — Angles are measured relative to a plane normal to the core axis.

* Water Pressure Tests — Values in lugeons should be read in conjunction with computation sheets. Test sections are indicated by blacked in strips.

Water	
	10 Oct. '73 water level date shown
	Water inflow
	Partial drilling water loss
	Complete drilling water loss

[illegible]

1557A161470 1of2

GEOLOGICAL LOG OF DRILL HOLE

ANGLE FROM HORIZONTAL (θ) 90°
COORDINATES E 198916 N 612225

DIRECTION

R.L. OF COLLAR 556.8m

SHEET 2 OF 2

Drilling Information				Rock Substance		Rock Mass Defects								
Method	Casing	Water	Pressure test * (lugeons)	Lift & % core recovery	Depth (metres)	Graphic log & core loss	Substance description rock type: grain characteristics colour, structure, minor components.	RQD	Weathering	Strength is (50) (MPa)	Defect spacing (cm)	Defect description thickness, type, inclination, planarity, roughness, coating, strength.		Rock condition No
NMLC														

The rock mass is generally close jointed and moderately tight. Defects are mainly joints at 30°, 45°, 60° & 90°, and some minor fracture zones up to 20m wide at 70°-90°. Most joints are tight and weakly cemented with calcite & epidote. Some joints are fractured with calcite and epidote & some clay. Many quartz-epidote & calcite epidote veins (generally mod. strong).

3

TUNNEL

Drill type MOLE

Feed Hydraulic

Core barrel type NMLC with

Imple tube & split inner

Driller B. Harte (DHC)

Commenced 7/7/75

Completed 16/7/75

Logged by P.A. LANG

Vertical scale km=1m

Weathering

Fr - Fresh

SW - Slightly weathered

MW - Moderately weathered

HW - Highly weathered

EW - Extremely weathered

Notes:

Bedding & Joint Planes - Angles are measured relative to a plane normal to the core axis.

* Water Pressure Tests - Values in lugeons should be read in conjunction with computation sheets. Test sections are indicated by blacked in strips.

Water

10 Oct. 73 water level date shown

Water inflow

Partial drilling water loss

Complete drilling water loss

Core Photograph Negative No

Depth (m) Black & White Colour

155/116/1470 20f2

GEOLOGICAL LOG OF DRILL HOLE

ANGLE FROM HORIZONTAL (°) 90
COORDINATES E199140 N612425DIRECTION
R.L. OF COLLAR 557.2 m

SHEET 1 OF 2

Drilling Information				Rock Substance				Rock Mass Defects						
Method	Casing	Water	Pressure test * (lugeons)	Lift & % core recovery	Depth (metres)	Graphic log & core loss	Substance description rock type: grain characteristics colour, structure, minor components	RQD	Weathering	Strength is (50) (MPa)	Defect spacing (cm)	Defect description thickness, type, inclination, planarity, roughness, coating, strength. Particular General		Rock condition No.
Rock Rotted				Not Cored	1	Not Cored	SANDY CLAY FILL		Soil					
				50	2	Loss		0				SOIL PROPERTIES Easily excavatable by mechanical shovel or by back-hoe.		5
				-90	3			0	EW					
				-90	4			0						
				-90	5	Loss		0						
				25	6			0						
				100	7			60	HW to HW			1cm HW seam at 60° with limonite staining.		
				100	8		Welded DACITE ignimbrite tuff or flow with banding in places. Mostly pale grey, but some narrow bands of dark grey. Quartz phenocrysts up to 7mm in light grey zones, smaller in dark zones. Pink feldspar in zones of quartz-epidote veining. Rock is extremely hard and extremely strong.	80	SW to FS			3 joints at 60°-70° spaced 10cm with calcite & limonite. These joints are perp to a joint set (spaced 15-40cm) which is parallel to flow. Banding is parallel to		

NOT TESTED

8

Unreliable results. W.P.T. show values
ranging from 13 - 30 lugeonsSOIL PROPERTIES
Easily excavatable by
mechanical shovel or
by back-hoe.

1 cm HW seam at
60° with limonite
staining.
3 joints at 60°-70° spaced
10 cm with calcite &
limonite. These joints
are perp to a 30° joint set
(spaced 15-40 cm), which
is parallel to flow banding.
10 cm HW seam between
joints at 30° and 60°.
2 joint sets at 30° each
spaced 15 cm + 1 at
60° spaced 30° cm.
Core close jointed.

2 limonite stained
joints at 60° spaced 10 cm.
2 limonite stained
joints at 0° & 60°.
14 cm EW seam
clayey sand, dip
approx. 45°.

Joints at approx. 30°
parallel to banding,
limonite stained,
spaced 20 cm.

3 joints at 30°-45° spaced
2 cm with 1 mm clay,
calcite.
2 joints at 80° spaced
1 cm with calcite & limonite.

Pink calcite veins at 45°-60°
not parallel to banding

Joints at 30° parallel to
banding spaced 30 cm
with 1-2 mm calcite.

Generally sound rock but with some
weathered seams.
2 prominent joint sets above 7.5 m. 1 at 30°
parallel to banding spaced 15-40 cm and one
at 60° perp to banding spaced 10-30 cm. Below
7.5 m another joint set at 30° not parallel to
banding. Joints are mostly slightly open,
limonite stained or weathered.

Vertical slopes will need steel ring
Probably no support required but possibly a few random rock bolts
Possibly some rock bolts & mesh in place support with full timber lagging.

Drill type MQLC

Feed Hydraulic

Core barrel type NMLC with

triple tube & split inner

Driller B. Harle (DHC)

Commenced 9/8/75

Completed 20/8/75

Logged by PALANG

Vertical scale 1 cm = 1 m

Weathering

Fr - Fresh

SW - Slightly weathered

MW - Moderately weathered

HW - Highly weathered

EW - Extremely weathered

Notes:

Bedding & Joint Planes - Angles are measured relative to a plane normal to the core axis.

* Water Pressure Tests - Values in lugeons should be read in conjunction with computation
sheets. Test sections are indicated by blacked in strips.

Water

10 Oct. '73 water level date shown

Water inflow

Partial drilling water loss

Complete drilling water loss

Core Photograph Negative No.

Depth (m) Black & White Colour

155/A161/1471 10/2

GEOLOGICAL LOG OF DRILL HOLE

PROJECT GINNINDERRA SEWER TUNNEL
LOCATION At chainage 210.311 (shaft site) on connection to
existing Belconnen Sewer near Belconnen Pollution Control
ANGLE FROM HORIZONTAL (°) 90 DIRECTION ---
COORDINATES E 199140 N 612425 R.L. OF COLLAR 557.2m

HOLE NO. GST
Centre. 5

SHEET 2 OF 2

Drilling Information					Rock Substance				Rock Mass Defects					
Method	Casing	Water	Pressure test * (lugeons)	Lift & % core recovery	Depth (metres)	Graphic log & core loss	Substance description rock type: grain characteristics colour, structure, minor components	RQD	Weathering	Strength Is (50) (MPa) 0-30-60 000-100	Defect spacing (cm) 0-100 100-200 200-300 300-400 400-500	Defect description thickness, type, inclination, planarity, roughness, coating, strength Particular General		Rock Condition No
NMLC			SEE ABOVE	100	21		DACITE as above. Light to medium grey becoming darker below 20.7m. Some pink feldspar below 21m banding at approx. 30-35°.	100	FS				Rockmass is very strong. Joints mostly at about 30° (not parallel to banding). Spaced 1m. above 21m, spaced 10-30 cm below 21m. Surfaces generally rough & tight with 1-2mm calcite.	2-3
				100				100						
				100	22		END OF HOLE 21.7m	95						
				100										

Drill type MOLE
Feed Hydraulic
Core barrel type NMLC with
triple tube & split inner
Driller B:Harte (DHC)
Commenced 9/8/75
Completed 20/8/75
Logged by PALANG
Vertical scale 1m = 1m

Weathering
Fr — Fresh
SW — Slightly weathered
MW — Moderately weathered
HW — Highly weathered
EW — Extremely weathered

Notes:

Bedding & Joint Planes — Angles are measured relative to a plane normal to the core axis.

* Water Pressure Tests—Values in lugeons should be read in conjunction with computation sheets. Test sections are indicated by blocked in strips.

Water

10 Oct. '73 water level data shown

Water inflow

Partial drilling water loss

Complete drilling water loss

Core Photograph Negative No.

Depth (m)	Black & White	Colour
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155/16/1471 20/2

GEOLOGICAL LOG OF DRILL HOLE

Drilling Information							Rock Substance		Rock Mass Defects						
Method	Drilling rate	Casing	Water	Pressure test * (lugcons)	Lift & % core recovery	Depth (metres)	Graphic log & core loss	Substance description rock type: grain characteristics colour, structure, minor components	Weathering	Point load strength 100 IS(50)(MPa)	Defect spacing (cm)	R.O.D.	Defect description thickness, type, inclination, planarity, roughness, coating, strength. Particular General	Rock condition No (interpretive)	
ROCK ROLLED			water flowing from hole-slits			1		NOT CORED							
				2											
				3											
				4											
				5											
				6											
				7											
				8											
				9											
	NMLC				NOT TESTED				9.5	loss	GRANITE PORPHYRY Light blue-gray where fresh	HW and MW			0
		95	10	+											
		100	11	+		loss									
		80	12	+		loss									
		95	13	+											
		100	14	+											
		80	15	+		loss									
		100	16	+											
		80	17	+											
		100	18	+											
		80	19	+											
		100	20	+											
										</					

Drill type CRAELIUSFeed HYDRAULICCore barrel type NMLC

Triple tube

Driller DHC

Commenced

Completed

Logged by D.C. PurcellVertical scale 1cm: 1m

Weathering

Fr - Fresh

SW - Slightly weathered

MW - Moderately weathered

HW - Highly weathered

EW - Extremely weathered

Notes

Bedding & Joint Planes - Angles are measured relative to a plane normal to the core axis.

* Water Pressure Tests - Values in lugcons should be read in conjunction with computation sheets.

Water

10 Oct. '73 water level date shown

Water inflow

Partial drilling water loss

Complete drilling water loss

Core Photograph Negative No.

Depth (m) Black & White Colour

155/416/493 1 of 2

GEOLOGICAL LOG OF DRILL HOLE

Drilling Information						Rock Substance		Rock Mass Defects																		
Method	Drilling rate	Casing	Water	Pressure test * (lugesons)	Lift & % core recovery	Depth (metres)	Graphic log & core loss	Substance description rock type grain characteristics colour, structure, minor components	Weathering	Point load strength (MPa) 0.3 1.0 3.0 10.0 150 (MPa)	Defect spacing (cm) 0-20 20-50 50-100 100-300	R O D	Defect description thickness, type, inclination, planarity, roughness, coating, strength Particular General	Rock condition No (interpretive)												
NMLC	Water flowing from hole stops				100	20	+	GRANITE PORPHYRY	SW and MW			20	As above. Heavy limonite staining above 24m. Rock closely jointed and fractured. Calcite vein Below 24m the rock is tighter and the joints are mostly slickensided Rock mass weak.	4 to 5												
					100	21	+		FRS			0														
					100	22	+					30														
					160	23	+					FR			0											
					100	24	+								10											
					40	25	+									0										
					0	26	Loss										?									
					95	27	+											As above. Some fractures appear drill-induced. Rock mass remains weak.								
					90	28	+												5							
					80	29	Loss																			
					80	30	+																			
					0	31	Loss																			
					70	32	+																			
					10	33	+																			
					This section of core obtained from bare washings. Therefore no structure obtained.																					
					END OF HOLE 33.0m																					
					Note: Tunnel crown not reached with this hole.																					

Drill type CRAELIUS
Feed HYDRAULIC
Core barrel type NMLC
Triple tube
Driller DHC (Harte)
Commenced
Completed
Logged by D. Russell
Vertical scale 1cm: 1m

Weathering

Fr - Fresh
SW - Slightly weathered
MW - Moderately weathered
HW - Highly weathered
EW - Extremely weathered

Notes

Bedding & Joint Planes - Angles are measured relative to a plane normal to the core axis

* Water Pressure Tests - Values in lugesons should be read in conjunction with computation sheets.

Water

10 Oct '73 water level date shown
Water inflow
Partial drilling water loss
Complete drilling water loss

Core Photograph Negative No

Depth (m) Black & White Colour

GEOLOGICAL LOG OF DRILL HOLE

Drilling Information				Rock Substance				Rock Mass Defects					
Method	Casing	Water	Pressure test * (lugesons)	Lift & % core recovery	Depth (metres)	Graphic log	Substance description * rock type: grain characteristics colour, structure, minor components.	RQD	Weathering	Strength is (50) (MPa)	Defect spacing (cm)	Defect description thickness, type, inclination, planarity, roughness, coating, strength. Particular General	Rock condition No.
Rock Rolled													

Drill type MOLE
Feed Hydraulic
Core barrel type NMLC
Triple tube & split inner tube
Driller Bill Harte (D.H.C.)
Commenced 21/5/75
Completed 7/6/75
Logged by P. Long
Vertical scale 1cm = 1m

Weathering

Fr - Fresh
SW - Slightly weathered
MW - Moderately weathered
HW - Highly weathered
EW - Extremely weathered

Notes:

Bedding & Joint Planes - Angles are measured relative to a plane normal to the core axis.
* Water Pressure Tests - Values in lugesons should be read in conjunction with computation sheets. Test sections are indicated by blocked in strips.

Water

10 Oct. '73 water level date shown
Water inflow
Partial drilling water loss
Complete drilling water loss

Core Photograph Negative No

Depth (m) Black & White Colour

155/161/1472 10r3**

BUREAU OF MINERAL RESOURCES,
GEOLOGY & GEOPHYSICS

PROJECT GINNINDERRA SEWER TUNNEL

LOCATION At SHAFT 2, 4m west of centre line of Tunnel at

Station 17+12

ANGLE FROM HORIZONTAL (°)

COORDINATES E198,757; N611,225

DIRECTION

R.L. OF COLLAR 56.0m

HOLE NO GST

7

SHEET 2 OF 3

GEOLOGICAL LOG OF DRILL HOLE

Drilling Information				Rock Substance				Rock Mass Defects									
Method	Casing	Water	Pressure test * (lugeons)	Lift & % core recovery	Depth (metres)	Graphic log & core loss	Substance description rock type: grain characteristics colour, structure, minor components	RQD	Weathering	Strength Is (50) (MPa)	Defect spacing (cm)	Defect description thickness, type, inclination, planarity, roughness, coating, strength. Particular General	Rock condition No.				
TUNNEL	NMLC		0	100	21	✓✓✓✓	SHALE as above	85	FR	0.0-0.1 0.0-0.1 0.0-0.1 0.0-0.1	0.0-0.1 0.0-0.1 0.0-0.1 0.0-0.1	shale fractured along bedding planes (horizontal) Probably mostly drill induced in tuff.	3				
				100	22	✓✓✓✓	mainly DACITE TUFF Some thin beds of shale a poorly sorted sandstone, some intra clasts of shale dip. approx 5°	50									
				100	23	✓✓✓✓		88									
				100	24	✓✓✓✓		97									
				100	25	✓✓✓✓		80	FS	0.0-0.1 0.0-0.1 0.0-0.1 0.0-0.1	0.0-0.1 0.0-0.1 0.0-0.1 0.0-0.1	Shale fractured along bedding planes (horizontal)	3				
				100	26	✓✓✓✓	shale + sandstone bands and contorted shale bands + intraclasts	95									
				100	27	✓✓✓✓		60	FR	0.0-0.1 0.0-0.1 0.0-0.1 0.0-0.1 0.0-0.1 0.0-0.1 0.0-0.1 0.0-0.1	0.0-0.1 0.0-0.1 0.0-0.1 0.0-0.1 0.0-0.1 0.0-0.1 0.0-0.1 0.0-0.1	fractures at 60°-80°	Rockmass is tight. Generally defects spaced 20cm - 1m, but narrow bands of shale are loosely fractured along bedding planes (horizontal). Natural fractures in tuff are generally 60-80° + strongly cemented & calcite	1			
				100	28	✓✓✓✓		95									
				100	29	✓✓✓✓	DACITE IGNIMBRITE TUFF Medium grey. Massive, becoming finer towards top (probably top of a flow?)	100									
				100	30	✓✓✓✓		100									
				100	31	✓✓✓✓		100									
				100	32	✓✓✓✓		100									
				100	33	✓✓✓✓		100									
			NOT TESTED	100	34	✓✓✓✓		100					No natural fractures. Core broken at end of each run and to fit into core box.	1			
				100	35	✓✓✓✓		100									
			0	100	36	✓✓✓✓		50	FS	0.0-0.1 0.0-0.1 0.0-0.1 0.0-0.1 0.0-0.1 0.0-0.1 0.0-0.1 0.0-0.1	0.0-0.1 0.0-0.1 0.0-0.1 0.0-0.1 0.0-0.1 0.0-0.1 0.0-0.1 0.0-0.1	Rock is fractured with calcite + clay seams up to 3 cms. Joints at 20° spaced 10-30 cms. & clay. Joints at 70°-80° & limonite staining.	3				
				100	37	✓✓✓✓	TUFF (as above) becoming finer grained + more sandy towards 36m. (probably top of a flow?)	97									
				100	38	✓✓✓✓		10	FR				Very few natural fractures. Most fractures drill-induced. Sticks of core 30 cm - 2m.	1-2			
				100	39	✓✓✓✓	fine grained band.	10									
				100	40	✓✓✓✓						fractures probably drill induced					

Drill type MOLE
Feed Hydraulic
Core barrel type NMLC
triple tube & split inner tube
Driller Bill Harte (D.H.C.)
Commenced 29/5/75
Completed 7/6/75
Logged by P Lang
Vertical scale 1 cm = 1 m

Weathering
Fr - Fresh
SW - Slightly weathered
MW - Moderately weathered
HW - Highly weathered
EW - Extremely weathered

Notes:
Bedding & Joint Planes - Angles are measured relative to a plane normal to the core axis.
* Water Pressure Tests - Values in lugeons should be read in conjunction with computation sheets. Test sections are indicated by blacked in strips.

Water
10 Oct. '73 water level date shown
Water inflow
Partial drilling water loss
Complete drilling water loss

Core Photograph Negative No.
Depth (m) Black & White Colour

155/116/1472 20/3

BUREAU OF MINERAL RESOURCES,
GEOLOGY & GEOPHYSICS

GEOLOGICAL LOG OF DRILL HOLE

PROJECT GINNINDERRA SEWER TUNNEL

LOCATION At SHAFT 2, 4m west of centre line of Tunnel at station 17+12

ANGLE FROM HORIZONTAL (θ) 90°

COORDINATES E 198,757, N 611,225

DIRECTION

R.L. OF COLLAR 563.0m

HOLE NO GST 7

SHEET 3 OF 3

Drilling Information				Rock Substance				Rock Mass Defects						
Method	Casing	Water	Pressure test * (lugeons)	Lift & % core recovery	Depth (metres)	Graphic log & core loss	Substance description rock type: grain characteristics colour, structure, minor components	RQD	Weathering	Strength Is (50) (MPa)	Defect spacing (cm)	Defect description thickness, type, inclination, planarity, roughness, coating, strength. Particular General	Rock condition No.	
NMLC			0	100	41	✓✓	DACITE IGNIMBRITE TUFF Very hard. Very strong.	100	FR			Vertical Joint wavy & irregular strong limonite staining. Some calcite. Rockmass is strong & tight Vertical joints strongly stained with limonite. Calcite veins up to 5mm thick at 60°. Most fractures are horizontal (probably drill induced.)	2	
		100		42	✓✓	75		FS						3
				43	✓✓✓✓	TUFFACEOUS SANDSTONE (Tuff arenite) Pale grey. Fine to medium grained. Very hard. Very strong.	66	SW-FS						2
		100		44	✓✓✓✓									
				45		END OF HOLE 44.30m								

Drill type MOLE
Feed Hydraulic
Core barrel type NMLC
multiple tube & split inner tube
Driller Bill Harte (D.H.C.)
Commenced 29/5/75
Completed 7/6/75
Logged by P. Lang
Vertical scale 1cm = 1m

Weathering
Fr — Fresh
SW — Slightly weathered
MW — Moderately weathered
HW — Highly weathered
EW — Extremely weathered

Notes:
Bedding & Joint Planes — Angles are measured relative to a plane normal to the core axis.
* Water Pressure Tests — Values in lugeons should be read in conjunction with computation sheets. Test sections are indicated by blacked in strips.

Water

10 Oct. '73 water level date shown
Water inflow
Partial drilling water loss
Complete drilling water loss

Core Photograph Negative No.
Depth (m) Black & White Colour

155/A16/1472 30P3

GEOLOGICAL LOG OF DRILL HOLE

ANGLE FROM HORIZONTAL (°) 90°
CO-ORDINATES E 198816 N 611613DIRECTION —
R L OF COLLAR 554.2 m

SHEET 1 OF 2

Drilling Information						Rock Substance		Rock Mass Defects											
Method	Drilling rate	Casing	Water	Pressure test + (lugans)	Lift B % core recovery	Depth (metres)	Substance description rock type grain characteristics colour, structure, main components	Weathering	Point load strength (N/mm ²)	Defect spacing (cm)	RQD	Defect description thickness, type, inclination, frequency, roughness, coating, strength Particular General	Block core recovery						
ROCK ROLLED						1	NOT CORED												
						2													
						3													
						4													
						5													
						NMLC					60	GRANITE PORPHYRY Light blue-grey where fresh	HW to CW				0	Rock closely jointed and joints often crushed; clay on some joint surfaces. Most joint surfaces limonite and manganese stained.	
											75						20		
											100								
											80		0						
											80		0						
											95		0						
											80		20						
											100		30						
											100		10						
											95		10						
											95			Mainly HW - some MW pieces			0	Rock crushed and sheared between 13m and 19m. Rock mass weak, some clay-limonite stained. Zone probably at about 45° from horizontal	5 10 6
											100								
											95								
											100								
											95								
100																			
95								Closely jointed, broken in parts	4										
100																			
95																			
80																			
100																			

Drill type MOLE
Feed HYDRAULIC
Core barrel type NMLC
Triple tube
Driller DHC (Harte)
Completed
Logged by D.C. Purcell
Vertical scale 1 cm : 1 m

Weathering
FW - Fresh
SW - Slightly weathered
MW - Moderately weathered
HW - Highly weathered
EW - Extremely weathered

Notes

Bedding & Joint Planes — Angles are measured relative to a plane normal to the core axis
* Water Pressure Tests — values in lugans should be read in conjunction with computation sheets

Water

100% (100%) water level rise shown
Water inflow
Partial drilling water loss
Complete drilling water loss

Core Photograph Negative to
Depth (m) Block B White

155/416/1494 1 of 2

BUREAU OF MINERAL RESOURCES,
GEOLOGY & GEOPHYSICS
GEOLOGICAL LOG OF DRILL HOLE

PROJECT **GINNINDERRA SEWER TUNNEL**
LOCATION **ON TUNNEL C/L AT STN. 13+20**
ANGLE FROM HORIZONTAL (°) **90°** DIRECTION **—**
COORDINATES **E 198816 N 611613** R.L. OF COLLAR **554.2**

HOLE NO. **GST 8**
SHEET **2** OF **2**

Drilling Information						Rock Substance		Rock Mass Defects						
Method	Drilling rate	Casing	Water	Pressure test * (lugons)	Lift & % core recovery	Depth (metres)	Substance description rock type grain characteristics colour, structure, minor components	Weathering	Point load strength 0.3 1.0 3.0 10.0 15.0 (MPa)	Defect spacing (cm)	R Q D	Defect description thickness, type, inclination, planarity, roughness, coating, strength Particular General	Rock condition No (Interpretive)	
NMLC					95	21	GRANITE PORPHYRY	MW and SW			10	Rock fairly hard and tight to about 23.3m	4	
					100	22		SW			30			
					90	23				40				
					100	24								
					75	25				0	About 80% of this section of core sheared and crushed. Sections of hard intact rock up to 0.3m long separate sections of sheared and crushed rock Direction of shearing not known but dips at about 40° Heavy limonite staining in places; minor clay on defect surfaces	5 to 6		
					60	26								
					65	27				15				
					80	28				25				
					100	29				30	closely jointed, but otherwise fairly sound. Joints gen. sp. 10cm			
					100	30				10				
					70	31	TUNNEL	HW. SW where rock intact				Crushed and sheared 30.2 to 32.75m; stained, some clay. From 32.75 to 35.0m rock is closely jointed and fractured Rock mass weak. Individual pieces of intact core between defects are hard and strong.	4 to 5	
					95	32					0			
					95	33								
					100	34								
					100	35					25			
								END OF HOLE 35.0m						

Drill type **MOLE**
Feed **HYDRAULIC**
Core barrel type **NMLC**
Triple tube
Driller **DHC (Harte)**
Commenced
Completed
Logged by **D.C. Purcell**
Vertical scale **1cm: 1m**

Weathering
Fr - Fresh
SW - Slightly weathered
MW - Moderately weathered
HW - Highly weathered
EW - Extremely weathered

Notes
Bedding & Joint Planes - Angles are measured relative to a plane normal to the core axis
* Water Pressure Tests - Values in lugans should be read in conjunction with computation sheets

Water
10 Oct '73 water level date shown
Water inflow
Excess drilling water loss
Complete drilling water loss

Core Photograph Negative No
Depth (m) Black & White Colour

155/16/1494 2 of 2

GEOLOGICAL LOG OF DRILL HOLE

Drilling Information				Rock Substance				Rock Mass Defects					
Method	Casing	Water	Pressure test * (lugesons)	Lift & % core recovery	Depth (metres)	Graphic log & core loss	Substance description rock type: grain characteristics colour, structure, minor components.	RQD	Weathering	Strength Is (50) (MPa)	Defect spacing (cm)	Defect description thickness, type, inclination, planarity, roughness, coating, strength Particular General	Rock condition No.
ROCK ROLLER and BORE FLUSHING	NMLC	3/6	NOT TESTED	NOT CORED	1		Not cored slope wash		EW	0 0 0 0 0 0 0 0 0 0	5 10 100 100 300	NOT CORED	4-5
					2								
					3								
					4								
					5								
					6		Not cored granite porphyry soft, weak.						
					7								
					8								
					9								
					10								
					11	loss		0	EW	0	3 10 100 100 300	3cm. clay seam. Clay seams up to 2mm. Slightly sheared at 60° to 70°, healed with clay. Weak. Limonite staining & thin veneer of clay on joints. Close jointed & seamy. Many fractures healed with epidote	Rock mass weathered and soft.
					12	loss	GRANITE PORPHYRY Soft and weak. Clayey sand. Brown with white feldspar.	0					
					13	+		0					
					14	+		0	EW to HW	0	3 10 100 100 300	1mm. clay seam on 80° joint. Rock close jointed. Calcite on faces, no clay.	Quality of rock improves below 1m. Fairly tight joint. Starts up to 40 cm. Many healed with calcite (strong). Clay veneer on some joints.
					15	+		0					
					16	+		0	FR	60 0 0	3 10 100 100 300		3
					17	+		60					
					18	+		0					
					19	+		0					

Drill type MOLE
Feed Hydraulic
Core barrel type NMLC, triple
tube and split inner tube
Driller J. Morgan (DHC)
Commenced 10.4.75
Completed 21.4.75
Logged by P. Lang
Vertical scale 1 cm = 1 m

Weathering

Fr - Fresh

SW - Slightly weathered

MW - Moderately weathered

HW - Highly weathered

EW - Extremely weathered

Notes:

Bedding & Joint Planes - Angles are measured relative to a plane normal to the core axis.

* Water Pressure Tests - Values in lugosons should be read in conjunction with computation sheets. Test sections are indicated by blacked in strips.

Water

10 Oct. '73 water level date shown

Water inflow

Partial drilling water loss

Complete drilling water loss

Core Photograph Negative No.

Depth (m) Black & White Colour

155/A16/1473 10F3

BUREAU OF MINERAL RESOURCES,
GEOLOGY & GEOPHYSICS

PROJECT GINNINDERRA SEWER TUNNEL

LOCATION At centre of proposed shaft 13, 4.26m west of
centre line of tunnel at station 33+15.24m.

HOLE NO GSI

GEOLOGICAL LOG OF DRILL HOLE

ANGLE FROM HORIZONTAL (°) 90
COORDINATES 198130E 609750N

DIRECTION

R.L. OF COLLAR 565m

SHEET 2 OF 3

Drilling Information				Rock Substance				Rock Mass Defects					
Method	Casing	Water	Pressure test # (lugeons)	Lift & % core recovery	Depth (metres)	Graphic log & core loss	Substance description rock type: grain characteristics colour, structure, minor components	RQD	Weathering	Strength Is (50) (MPa)	Defect spacing (cm)	Defect description thickness, type, inclination, planarity, roughness, coating, strength Particular General	Rock condition No.
NMLC			0	100%	21	+	GRANITE PORPHYRY Pale pinkish, green grey, very Hard, & very strong.	30	FR	0.0-0.00 0.00-0.00 0.00-0.00 0.00-0.00	0.00-0.00 0.00-0.00 0.00-0.00 0.00-0.00	Vertical joints with thin veneer of clay. 1m. of rock fractured with joints at 80° & 30° some clay on joint surfaces. Some narrow fractured zones with clay. Rock mass moderately tight to very tight. Most joints 80°-90°. Joints cemented with calcite and chlorite. Cement moderately strong. Joints planar to wavy and rough and tight.	3 -4 2-3
				100%	22	+		10					
				100%	23	+		20					
				100%	24	+		50					
				100%	25	+		65					
				100%	26	+		93					
				100%	27	+		75					
				100%	28	+		25					
				100%	29	+		75					
				100%	30	+		75					
NX			0	100%	31	+	GRANITE PORPHYRY Green. Hard and strong. Softer than above. Easier to drill Sheared and healed with chlorite veins throughout.	75	FR but slightly altered and chloritized	0.0-0.00 0.00-0.00 0.00-0.00 0.00-0.00	0.00-0.00 0.00-0.00 0.00-0.00 0.00-0.00	Core ground and broken by drill. Core ground and broken by drill. Vertical fractures with calcite (weak).	2-3
				100%	32	+		75					
				100%	33	+		30					
				100%	34	+		90					
				100%	35	+		75					
NMLC			0	100%	36	+	GRANITE PORPHYRY Mainly very hard and very strong. Some slightly chloritized zones and some zones with many calcite veins.	90	FR	0.0-0.00 0.00-0.00 0.00-0.00 0.00-0.00	0.00-0.00 0.00-0.00 0.00-0.00 0.00-0.00	Some clay, calcite & pyrite on joints. Rock mass very tight & strong. Joint surfaces rough. Most cemented with calcite.	2-3
				100%	37	+		75					
				100%	38	+		75					
				100%	39	+		100					

Drill type Mole	Weathering	Water	Core Photograph Negative No.
Feed Hydraulic	Fr - Fresh	10 Oct. '73 water level date shown	Depth (m) Black & White Colour
Core barrel type NMLC with triple tube-split inner	SW - Slightly weathered	Water inflow	
Driller Wheally (DHC)	MW - Moderately weathered	Partial drilling water loss	
Commenced 11-4-75	HV - Highly weathered	Complete drilling water loss	
Completed 21-4-75	EW - Extremely weathered		
Logged by E. Lang	Notes:		
Vertical scale 1cm = 1m	Bedding & Joint Planes - Angles are measured relative to a plane normal to the core axis.		
	* Water Pressure Tests - Values in lugeons should be read in conjunction with computation sheets. Test sections are indicated by blacked in strips.		

155/116/1473 2 of 3

BUREAU OF MINERAL RESOURCES,
GEOLOGY & GEOPHYSICS

GEOLOGICAL LOG OF DRILL HOLE

PROJECT GINNINDERRA SEWER TUNNEL

LOCATION At centre of proposed shaft 3. 426m west of
tunnel at station 33+15.24m

ANGLE FROM HORIZONTAL (°) 90

COORDINATES 198130E 609750N

DIRECTION

R.L. OF COLLAR 565m

HOLE NO. 351
9

SHEET 3 OF 3

Drilling Information				Rock Substance		Rock Mass Defects							
Method	Casing	Water	Pressure test * (lugeons)	Lift & % core recovery	Depth (metres)	Graphic log & core loss	Substance description rock type: grain characteristics colour, structure, minor components.	RQD	Weathering	Strength Is (50) (MPa)	Defect spacing (cm)	Defect description thickness, type, inclination, planarity, roughness, coating, strength. Particular General	Rock condition No.
NMLC			0	100%	41	+	GRANITE PORPHYRY Mainly very hard and very strong. Some zones with chlorite and calcite veins moderately hard & strong.	80	FR	0.3 0.5 1.0 2.0 5.0 10.0 20.0 50.0 100.0 200.0 300.0	0.3 0.5 1.0 2.0 5.0 10.0 20.0 50.0 100.0 200.0 300.0	Rock mass mostly very strong and very tight. Some close jointed and fractured zones up to 30cm. wide. Joints cemented with calcite (moderately strong) no clay. Joint surfaces rough, most joints at 0-30° some at 60-90°. Rock closely jointed and fractured with calcite on joints. Cement moderately weak. Some limonite staining on joints.	2-3
			100%	42	+	100							
			100%	43	+	90							
			100%	44	+	85							
			100%	45	+	100							
			100%	46	+	35							
			100%	47	+	100							
			100%	48	+	100							
END OF HOLE 49m.													

Drill type Mole
Feed Hydraulic
Core barrel type NMLC with
Triple tube & split inner
Driller B. Hart (DHC)
Commenced 10-4-75
Completed 21-4-75
Logged by P. Lang
Vertical scale 1cm = 1m

Weathering

Fr — Fresh
SW — Slightly weathered
MW — Moderately weathered
HW — Highly weathered
EW — Extremely weathered

Notes:

Bedding & Joint Planes — Angles are measured relative to a plane normal to the core axis.
* Water Pressure Tests — Values in lugeons should be read in conjunction with computation sheets. Test sections are indicated by blacked in strips.

Water

10 Oct. '73 water level date shown
Water inflow
Partial drilling water loss
Complete drilling water loss

Core Photograph Negative No.

Depth (m) Black & White Colour

155/146/1473 3013

GEOLOGICAL LOG OF DRILL HOLE

Drilling Information				Rock Substance		Rock Mass Defects																	
Method	Casing	Water	Pressure test * (lugeons)	Lift & % core recovery	Depth (metres)	Graphic log & core loss	Substance description rock type: grain characteristics colour, structure, minor components	R.Q.D.	Weathering	Strength Is (50) (MPa)	Defect spacing (cm)	Defect description thickness, type, inclination, planarity, roughness, coating, strength	Particular	General	Rock condition No.								
NMLC				100			DACITE IGIMBRITE TUFF with flow banding	55	MW	03-1000 00-1000 000-1000	000-1000 000-1000 000-1000		Vertical fractures spaced 0-5cm with limonite & clay clay veneer on joint clay seams from 1cm to 5cm wide clayey gravel (GC) to clayey sand (SC) seams at 0-30° Drill induced fractures 5cm wide crushed seam with clay (GC) Rockmass mod. tight. Limonite & thin veneer of clay on most joints. A few crushed seams with clay. 2-5cm wide, spaced 8cm-3m. Generally 50cm-3m joints at 30°, 45°, 90° spaced 10-30cm. Surfaces rough & irregular.	3-4									
		100	21	✓✓	45																		
						22		✓✓															
					100	23		✓✓															
					100																		
					98	24		✓✓															
						25		✓✓															
					100																		
					100	26		✓✓															
						27		✓✓															
					100																		
						28		✓✓															
					100	29		✓✓															
					100	30		✓✓															
						31		✓✓															
					100	32		✓✓															
						33		✓✓															
					100	34		✓✓															
						35		✓✓															
					100	36		✓✓															
						37		✓✓															
					100	38		✓✓															
					100	39		✓✓															
				100	40	✓✓																	

Drill type Mole	Weathering	Water	Core Photograph Negative No
Feed Hydraulic	Fr - Fresh	10 Oct. '73 water level date shown	Depth (m)
Core barrel type NMLC	SW - Slightly weathered	Water inflow	Black & White
Tripple tube with split inner tube	MW - Moderately weathered	Partial drilling water loss	Colour
Driller Bill Harte (D.H.C.)	HW - Highly weathered	Complete drilling water loss	
Commenced 24/4/75	EW - Extremely weathered		
Completed 27/5/75	Notes:		
Logged by P. Lang	Bedding & Joint Planes - Angles are measured relative to a plane normal to the core axis.		
Vertical scale 1 cm = 1 m	* Water Pressure Tests - Values in lugeons should be read in conjunction with computation sheets. Test sections are indicated by blacked in strips.		

BUREAU OF MINERAL RESOURCES,
GEOLOGY & GEOPHYSICS

GEOLOGICAL LOG OF DRILL HOLE

PROJECT GINNINDERRA SEWER TUNNEL

LOCATION near Strathgairn Homestead Belconnen A.C.T.

On tunnel line at station 37+80 m

ANGLE FROM HORIZONTAL (°) 90° DIRECTION

COORDINATES E 197,995 N 604,322 R.L. OF COLLAR 563.8 m

HOLE NO. GST.

11

SHEET 3 OF 3

Drilling Information				Rock Substance		Rock Mass Defects							
Method	Casing	Water	Pressure test * (lugeons)	Lift & % core recovery	Depth (metres)	Graphic log & core loss	Substance description rock type: grain characteristics colour, structure, minor components.	Weathering	Strength Is (50) (MPa)	Defect spacing (cm)	Defect description thickness, type, inclination, planarity, roughness, coating, strength. Particular General	Rock condition No.	
TUNNEL NMLC			0	100			DACITE IGNIMBRITE TUFF with flow banding.	FR	0.3 0.3-3 0.00-100 100		Fractured & jts at 60° & Ca + clay on jts continuous stick of core but with vertical fracture, calcite, chl. & clay. fractured zone & crushed seams & clay vertical joint wavy & irregular & chlorite & calcite Vertical joint same as above - 10cm crushed seam GC } core fractured by joints at 45°-60° & 90° Ca, Chl, Clay core generally fractured at 0-30°. Joints at 30°-45° with calcite and chlorite. Joints at 60° with calcite chlorite and clay slickensided. - 10cm crushed seam with chlorite & calcite - 5cm crushed seam with chlorite & calcite	3-4	
				41	vv	60							
				100		80							
				42	vv								
				100		40							
				43	vv								
				100		40							
				44	vv								
				100		70							
				45	vv								
			100		10								
			46	vv									
			100		80								
			47	vv									
			100		70								
			48	vv									
			100		20								
			49	vv									
			100		70								
			NOT TESTED	100		20	fine grained siliceous green sandstone contacts tight (intrusive?) dip 10-20°						
100		70		DACITE IGNIMBRITE TUFF									
				50			End of hole 52.40m					3	
				51	vv								
				52	vv								
				53									
				54									
				55									
				56									
				57									
				58									
				59									
				60									

Drill type Mole
Feed Hydraulic
Core barrel type NMLC
triple tube with split inner tube
Driller Bill Harte (D.H.C.)
Commenced 24/4/75
Completed 27/5/75
Logged by P. Lang
Vertical scale 1 cm = 1 m

Weathering
Fr — Fresh
SW — Slightly weathered
MW — Moderately weathered
HW — Highly weathered
EW — Extremely weathered

Notes:

Bedding & Joint Planes — Angles are measured relative to a plane normal to the core axis.
* Water Pressure Tests — Values in lugeons should be read in conjunction with computation sheets. Test sections are indicated by blocked in strips.

Water

10 Oct. '73 water level date shown
Water inflow
Partial drilling water loss
Complete drilling water loss

Core Photograph Negative No.

Depth (m) Black & White Colour

155/A16/1474 30/3

GEOLOGICAL LOG OF DRILL HOLE

ANGLE FROM HORIZONTAL (°) 45° DIRECTION 023° grid
COORDINATES E 199,784 N 609,070 R.L. OF COLLAR 570.8

SHEET 1 OF 5

Drilling Information				Rock Substance				Rock Mass Defects					
Method	Casing	Water	Pressure test * (lugeons)	Lift & % core recovery	Depth (metres)	Graphic log & core loss	Substance description rock type: grain characteristics colour, structure, minor components.	RQD	Weathering	Strength Is (50) (MPa)	Defect spacing (cm)	Defect description thickness, type, inclination, planarity, roughness, coating, strength. Particular General	Rock condition No.
Rock Rolled							Top soil						
					1								
					2								
					3								
				100	4	V	DACITE blue gray to green-gray when fresh. qtz phenocrysts up 2mm	0	Mostly HW but with narrow seams of SW and blocks of SW between large joint blocks				
				100	5	V		40					
				100	6	V		50				crushed seams 1-2cm spaced 10cm	
				100	7	V		45					
				100	8	V		40					
				50	9	V	Core loss	0				5cm sandy clay seam.	
				100	10	V		20		SW			
				100	11	V		15		HW & SW seams			
				100	12	V							
				100	13	V		20				3cm crushed seam	
				100	14	V					25cm crushed seam (GC)		
				100	15	V		25					
				100	16	V		45			10cm crushed seam (GC)		
				100	17	V		20			30cm crushed seam (GC)		
				100	18	V							
				100	19	V		50			crushed seams & clay up to 3cm wide (GC)		
				20			35						

NOT TESTED

11/9/75

24/4/75

Rock is sheared at 60°. Holed with limonite, clay & gravel (GW). Much limonite staining. Some clay in some seams. Most fractures at 45-60°. Joint surfaces rough & thick limonite coating.

Rockmass is very close jointed (9-20cm) & fractured. Crushed seams from 5-20cm thick spaced approx. 1m consist mainly of sand & gravel (GW). Much limonite staining.

Rockmass very close jointed, close jointed, much clayey sand (SW). Sheared.

Rockmass very close jointed (generally <10cm) & sandy, most joints at 45°. Some at 90°. Most joints have clay veneer or clay seam up to 1cm thick. All joints limonite stained & incipient joints throughout rockmass have limonite staining & cement.

4

4 - 5

4

Drill type Fox
Feed Hydraulic
Core barrel type NMLC
triple tube split inner tube
Driller Derreck Whalley, T. Stok
Commenced 3/5/75
Completed 18/6/75
Logged by P. Lang
Vertical scale 1cm = 1m

Weathering
Fr — Fresh
SW — Slightly weathered
MW — Moderately weathered
HW — Highly weathered
EW — Extremely weathered

Notes:
Bedding & Joint Planes — Angles are measured relative to a plane normal to the core axis.
* Water Pressure Tests — Values in lugeons should be read in conjunction with computation sheets. Test sections are indicated by blacked in strips.

Water
10 Oct. '73 water level date shown
Water inflow
Partial drilling water loss
Complete drilling water loss

Core Photograph Negative No.
Depth (m) Black & White Colour

155/A16/14.75 1 of 5

GEOLOGICAL LOG OF DRILL HOLE

Drilling Information				Rock Substance				Rock Mass Defects					
Method	Casing	Water	Pressure test * (lugeons)	Lift & % core recovery	Depth (metres)	Graphic log & core loss	Substance description rock type: grain characteristics colour, structure, minor components.	RQD	Weathering	Strength Is (50) (MPa)	Defect spacing (cm)	Defect description thickness, type, inclination, planarity, roughness, coating, strength. Particular General	Rock condition No.
NMLC			NOT TESTED	100	21	V	DACITE mostly sheared but healed with chlorite & limonite.	35	Mostly SW-Fs. Some HW seams along jts.	03 000-1000 000-			

Drill type Fox
Feed Hydraulic
Core barrel type NMLC
Tripple tube & split inner tube
Driller Derreck Whitley, I. Stork
Commenced 3/5/75
Completed 18/6/75
Logged by P. Lang
Vertical scale 1cm = 1m

Weathering

Fr — Fresh
SW — Slightly weathered
MW — Moderately weathered
HW — Highly weathered
EW — Extremely weathered

Notes:

Banding & Joint Planes — Angles are measured relative to a plane normal to the core axis.
* Water Pressure Tests — Values in lugeons should be read in conjunction with computation sheets. Test sections are indicated by blacked in strips.

Water

10 Oct. '73 water level date shown
Water inflow
Partial drilling water loss
Complete drilling water loss

Core Photograph Negative No.

Depth (m) Black & White Colour

155/A16/1475 2075

GEOLOGICAL LOG OF DRILL HOLE

Drilling Information				Rock Substance			Rock Mass Defects														
Method	Casing	Water	Pressure test * (lugeons)	Lift & % core recovery	Depth (metres)	Graphic log & core loss	Substance description rock type: grain characteristics colour, structure, minor components.	RQD.	Weathering	Strength Is (50) (MPa)	Defect spacing (cm)	Defect description thickness, type, inclination, planarity, roughness, coating, strength.	Rock condition No.								
N.M.L.C.			0	100			DACITE	95	FR	03 01-30 000-200 000-300 10-0	000-100 100-200 200-300 300-400	Particular General	Rock condition No.								
				41	V	Sheared & healed with chlorite. Red stained quartz phenocrysts. Becoming finer grained towards bottom. Hard & strong.	90														
				100	42	V		45													
				100	43		FAULT ZONE														
				90?	44		Rock is strongly sheared. Very weak & soft. Much clay & chlorite.	0													
				90?	45		Dacite ignimbrite tuff below 43.5m. Also	0													
				100	46		strongly sheared with clay & chlorite.	10													
				100	47	VV	DACITE IGNIMBRITE TUFF	8													
				100	48	VV	medium grey														
				100	49	VV	Very hard, very strong	0													
				100	50	VV		35													
				100	51	VV		40													
				100	52	VV		25													
				100	53	VV		30													
				100	54	VV		55													
				100	55	VV		40													
				100	56	VV		40													
				100	57	VV		40													
				100	58	VV		40													
				100	59	VV		25													
100	60																				

Drill type Fox
Feed Hydraulic
Core barrel type N.M.L.C.
triple tube & split tube
Driller D. Wheally, T. Stark
Commenced 3/5/75
Completed 18/6/75
Logged by P. Lang
Vertical scale 1 cm = 1 m

Weathering

Fr - Fresh
SW - Slightly weathered
MW - Moderately weathered
HW - Highly weathered
EW - Extremely weathered

Notes:

Bedding & Joint Planes - Angles are measured relative to a plane normal to the core axis.
* Water Pressure Tests - Values in lugeons should be read in conjunction with computation sheets. Test sections are indicated by blocked in strips.

Water

10 Oct. '73 water level date shown
Water inflow
Partial drilling water loss
Complete drilling water loss

Core Photograph Negative No

Depth (m) Black & White Colour

155/16/1475 3 of 5

BUREAU OF MINERAL RESOURCES,
GEOLOGY & GEOPHYSICSPROJECT GLINNINDERBA SEWER TUNNEL
LOCATION At station 40+50 on centre line of tunnel

HOLE NO. _____

GST 121

GEOLOGICAL LOG OF DRILL HOLE

ANGLE FROM HORIZONTAL (°) 45° DIRECTION 023° grid
COORDINATES E 199784 N 609070 R.L. OF COLLAR 570.8SHEET 4 OF 5

Drilling Information				Rock Substance				Rock Mass Defects							
Method	Casing	Water	Pressure test * (lugeons)	Lift & % core recovery	Depth (metres)	Graphic log	Substance description rock type: grain characteristics colour, structure, minor components.	RQD	Weathering	Strength Is (50) (MPa) 000-100 100-200 200-300	Defect spacing (cm) 000-100 100-200 200-300	Defect description thickness, type, inclination, planarity, roughness, coating, strength Particular General	Rock condition No.		
TUNNEL	NMLC		0	100			DACITE IGNIMBRITE TUFF	25	FR			10cm crushed seam & clayey sand (SC)	4		
				100	61	✓✓	Bedding and/or flow banding	65				5cm fractured.			
					62	✓✓	Very hard, very strong	45							
				100	63	✓✓	Bedding planes are not a weakness.								
					64	✓✓		50				10cm fractured & some clay.			
				100	65	✓✓		75							
					66	✓✓									
				100	67	✓✓		75				5cm fractured			
					68	✓✓						5cm fractured at 60°			
				100	69	✓✓		90				Joint at 60° & clay (// to bedding)			
					70	✓✓	banding dips approx. 8°-10° west.	95							
					71	✓✓									
				100	72	✓✓		80							
					73	✓✓		100							
				100	74	✓✓		75							
					75	✓✓									
				100	76	✓✓		100							
					77	✓✓		75							
				100	78	✓✓									
					79	✓✓		55				1cm thick calcite vein at 70°			
				100	80	✓✓						1cm thick calcite vein at 60°			
Rockmass strong & light. Many drill induced fractures. This rock breaks more easily across the rock fabric than the granite. Should break up to pieces from 10-30cm across when blasted. Several sticks of core 30-70cms long. Natural defects are joints generally spaced 30cm-1m, but up to 2m. In places spaced 7-10cms. Most natural joints are at 60-70° or 30-45° to core. Joint surfaces are generally cemented with calcite usually less than 1mm thick. Many joints are slickensided.															
As above but core more closely jointed due to 2 intersecting joint sets at 45° to core and one wavy joint at 80°-90° to core. Also calcite veins up to 1cm thick.													3		

Drill type Fox
Feed Hydraulic
Core barrel type NMLC
trapped tube split over tube
Driller D. Whately, C. Steek
Commenced 3/5/75
Completed 18/6/75
Logged by P. Lang
Vertical scale 1cm = 1m

Weathering

Fr — Fresh
SW — Slightly weathered
MW — Moderately weathered
HW — Highly weathered
EW — Extremely weathered

Notes:

Bedding & Joint Planes — Angles are measured relative to a plane normal to the core axis.
* Water Pressure Tests — Values in lugeons should be read in conjunction with computation sheets. Test sections are indicated by blocked in strips.

Water

10 Oct. '73 water level date shown
Water inflow
Partial drilling water loss
Complete drilling water loss

Core Photograph Negative No.

Depth (m) Black & White Colour

155/A16/1475 4 of 5

HOLE NO. . . .
GST 12
SHEET 5 OF 5

ANGLE FROM HORIZONTAL (θ) 45° DIRECTION 023° grid
COORDINATES E199,784 N609,070 R.L. OF COLLAR 570.8

SHEET 1 OF 5

NOT TESTED

Core Photograph Negative No.		
Depth (m)	Black & White	Colour
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100		

Rock mass is close to very close jointed with some fractured zones. 1-5m. Some crushed seams with chlorite clay & sandy clay up to 10cm thick spaced 30cm-5m. Most joints at 30° (2 sets) and 60°. Rock mass riddled with cavities, up to 2mm (these are partly healed fractures where calcite cement may have been dissolved out, leaving cavities). All joint surfaces down to 18m have a thin laminar staining. Some chlorite & chlorite clay below 18m.

ANGLE FROM HORIZONTAL (θ) 38° DIRECTION 125° grid
 COORDINATES E 197719 N 608906 R.L. OF COLLAR 546.5m

SHEET 2 OF 5

Drill type <u>FOX</u>	Weathering	Water	Core Photograph Negative No.
Feed <u>Hydraulic</u>	Fr — Fresh	10 Oct. '73 water level date shown	Depth (m) Black & White Colour
Core barrel type <u>NML with triple tube split joint</u>	SW — Slightly weathered	Water inflow	-----
Driller <u>J. Morgan (CHC)</u>	MW — Moderately weathered	Partial drilling water loss	-----
Commenced <u>23/6/75</u>	HW — Highly weathered	Complete drilling water loss	-----
Completed <u>3/7/75</u>	EW — Extremely weathered	Notes:	-----
Logged by <u>E. A. LANG</u>	Bedding & Joint Planes — Angles are measured relative to a plane normal to the core axis.		-----
Vertical scale <u>1cm = 1m</u>	* Water Pressure Tests — Values in lugeons should be read in conjunction with computation sheets. Test sections are indicated by blocked in strips.		-----
			<u>155/16/1478-2055</u>

GEOLOGICAL LOG OF DRILL HOLE

ANGLE FROM HORIZONTAL (°) 38°

DIRECTION 125 grid

COORDINATES E 197,719 N 608,906

R.L. OF COLLAR 546.5m

SHEET 3 OF 5

Drilling Information				Rock Substance		Rock Mass Defects											
Method	Casing	Water	Pressure test * (lugeons)	Lift & % core recovery	Depth (metres)	Graphic log & core loss	Substance description rock type: grain characteristics colour, structure, minor components.	RQD	Weathering	Strength Is (50) (MPa)	Defect spacing (cm)	Defect description thickness, type, inclination, planarity, roughness, coating, strength. Particular General	Rock condition No.				
NMLC				100	41	✓	DACITE With quartz phenocrysts up to 3mm. Blue grey when fresh. Stained purple by hydrothermally deposited haematite in some zones. Green grey due to epidote near fault.	70	FR			Rock mass is close jointed but fairly tight. Joints are generally spaced 3-20 cm, and oriented at 30° (2 sets), & 80°-90°. Surfaces are mostly slickensided with chlorite and calcite. A few have a thin veneer of clay. A few crushed seams with chlorite and clay (generally <1cm thick) orientated at 45° and 85-90°. Many thin calcite veins (strong).					
				100	42	✓		80									
					100	43		✓					60			1cm crushed seam with chlorite & clay	
					100	44		✓					65			30cm of crushed seams with chlorite & clay.	
					100	45		✓					40			Near vertical joint, planar and smooth. Slickensided with chlorite, calcite and a thin veneer of clay	
					100	46		✓					50				
					100	47		✓					50				
					100	48		✓					50				
					100	49		✓					50				
					100	50		✓					60			2 vertical joints spaced 1cm. Slickensided with chlorite and clay.	
					100	51		✓					50			1cm crushed seam with chlorite & clay.	
					100	52		✓					80				
					100	53		✓					40				
					100	54		✓					40				
					100	55		✓					50				
					100	56		✓					40				
					100	57		✓					40				
					100	58		✓					50				
					100	59		✓					30			2 crushed seams < 5cm thick with chlorite.	

Drill type FOX
Feed Hydraulic
Core barrel type NMLC with triple tube & split inner
Driller J. Morgan (DHC)
Commenced 23/6/75
Completed 9/7/75
Logged by R. LANG
Vertical scale 1cm = 1m

Weathering

Fr — Fresh
SW — Slightly weathered
MW — Moderately weathered
HW — Highly weathered
EW — Extremely weathered

Notes:

Bedding & Joint Planes — Angles are measured relative to a plane normal to the core axis.
* Water Pressure Tests — Values in lugeons should be read in conjunction with computation sheets. Test sections are indicated by blacked in strips.

Water

10 Oct. '73 water level date shown
Water inflow
Partial drilling water loss
Complete drilling water loss

Core Photograph Negative No.

Depth (m) Black & White Colour

155/A16/1476 30/5

GEOLOGICAL LOG OF DRILL HOLE

ANGLE FROM HORIZONTAL (θ) 38° DIRECTION 125° grid
COORDINATES E 197719 N 608906 R.L. OF COLLAR 546.5m

SHEET 4 OF 5

Drilling Information				Rock Substance				Rock Mass Defects														
Method	Casing	Water	Pressure test * (lugeons)	Lift & % core recovery	Depth (metres)	Graphic log & core loss	Substance description rock type: grain characteristics colour, structure, minor components.	RQD	Weathering	Strength Is (50) (MPa)	Defect spacing (cm)	Defect description thickness, type, inclination, planarity, roughness, coating, strength. Particular General	Rock condition No.									
NMLC				1-2	100	V	DACITE With quartz phenocrysts up to 3cm. Green due to epidote. Partly sheared in places and healed with epidote and calcite.	30	FR	0.03 0.1 0.3 0.5 1.0 2.0 3.0 5.0 10.0 20.0 30.0 50.0	0.03 0.1 0.3 0.5 1.0 2.0 3.0 5.0 10.0 20.0 30.0 50.0	Rock is crushed & fractured with 2 joint sets at 60° with chlorite. Joints spaced 0°-30° spaced 1-3 cm.	3									
					61	V		80						2 joint sets at 30° each spaced 8 cm.								
					100	V		62							50	5cm crushed seam with chlorite.						
					63	V		64							40		2cm & 5cm crushed seam with chlorite					
					100	V		65							35			Sheared shale				
					66	V		67							35				Sheared & crushed rhyolite			
					100	V		68							20					50cm crushed and sheared.		
					69	V		70							30						Crushed seams. 1-10cm thick with chlorite & some clay.	
					100	V		71							40							SEE BELOW
					72	V		73							15							
					100	V	74	60														
					75	V	76	85														
					100	V	77															
					78	V	79															
					100	V	80															
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296	V	297																				
298	V	299																				
300	V	301																				
302	V	303																				
304	V	305																				
306	V	307																				
308	V	309																				
310	V	311																				
312	V	313																				
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316	V	317																				
318	V	319																				
320	V	321																				
322	V	323																				
324	V	325																				
326	V	327																				
328	V	329																				
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332	V	333																				
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360	V	361																				
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378	V	379																				
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382	V	383																				
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388	V	389																				
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416	V	417																				
418	V	419																				
420	V	421																				
422	V	423																				
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426	V	427																				
428	V	429																				
430	V	431																				
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434	V	435																				
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456	V	457																				
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464	V	465																				
466	V	467																				
468	V	469																				
470	V	471																				
472	V	473																				
474	V	475																				
476	V	477																				
478	V	479																				
480	V	481																				
482	V	483																				
484	V	485																				
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492	V	493																				
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502	V	503																				
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526	V	527																				
528	V	529																				
530	V	531																				
532	V	533																				
534	V	535																				
536	V	537																				
538	V	539																				
540	V	541																				
542	V	543																				
544	V	545																				
546	V	547																				
548	V	549																				
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558	V	559																				
560	V	561																				
562	V	563																				
564	V	565																				
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568	V	569																				
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572	V	573																				
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616	V	617																				
618	V	619																				
620	V	621																				
622	V	623																				
624	V	625																				
626	V	627																				
628	V	629																				
630	V	631																				
632	V	633																				
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672	V	673																				
674	V	675																				
676	V	677																				
678	V	679																				
680	V	681																				
682	V	683																				
684	V	685																				
686	V	687																				
688	V																					

Drill type FOX
Feed Hydraulic
Core barrel type NMLC with
triple tube & split
Driller J. Morgan (DHC)
Commenced 23/6/75
Completed 9/7/75
Logged by E.A. LANG
Vertical scale 1cm=1m

Weathering

Fr - Fresh
SW - Slightly weathered
MW - Moderately weathered
HW - Highly weathered
EW - Extremely weathered

Notes:

Bedding & Joint Planes - Angles are measured relative to a plane normal to the core axis.

* Water Pressure Tests - Values in lugeons should be read in conjunction with computation sheets. Test sections are indicated by blacked in strips.

Water

10 Oct '73 water level date shown
Water inflow
Partial drilling water loss
Complete drilling water loss

Core Photograph Negative No.

Depth (m) Black & White Colour

155/116/1476 4 of 5

HOLE NO GST
13

SHEET 5 OF 5

Drilling Information					Rock Substance				Rock Mass Defects					
Method	Casing	Water	Pressure test * (lugeons)	Lith & % core recovery	Depth (metres)	Graphic log B core loss	Substance description rock type: grain characteristics colour, structure, minor components	RQD	Weathering	Strength Is (50) (MPa)	Defect spacing (cm)	Defect description thickness, type, inclination, planarity, roughness, coating, strength. Particular General		Rock condition No.
NMLC			0	100	81		RHYOLITE Green mottled. Silicious with black chlorite.	85	FR				Rock mass is close jointed but moderately tight. 2 joint sets at 30° spaced 10cm + 1 set at 65° + random joints. Surfaces slickensided with chlorite.	3
		100		82	60									
		100		83	75									
		100		84										
		100		85	65									
							END OF HOLE 85.45m							

Depth (m)	Black & White	Colour
10	100	100
20	100	100
30	100	100
40	100	100
50	100	100
60	100	100
70	100	100
80	100	100
90	100	100
100	100	100

155/16/1476 5015

HOLE NO. GST
14

SHEET 1 OF 3

Drill type <u>CRAELIUS</u>	<u>Weathering</u>	<u>Water</u>	Core Photograph Negative No.
Feed <u>Hydraulic</u>	Fr — Fresh	10 Oct. '73 water level date shown	Depth (m) Black & White Colour
Core barrel type <u>NPUC with triple tube & split inner</u>	SW — Slightly weathered	Water inflow	
Driller <u>D.Wheatly (DHC)</u>	MW — Moderately weathered	Partial drilling water loss	
Commenced <u>24/6/75</u>	HW — Highly weathered	Complete drilling water loss	
Completed <u>27/7/75</u>	EW — Extremely weathered	Notes:	
Logged by <u>PALANG</u>		Bedding & Joint Planes — Angles are measured relative to a plane normal to the core axis.	
Vertical scale <u>1cm=1m</u>		* Water Pressure Tests — Values in lugeons should be read in conjunction with computation sheets. Test sections are indicated by blacked in strips.	
			<u>155A161477 Inf 3</u>

GEOLOGICAL LOG OF DRILL HOLE

ANGLE FROM HORIZONTAL (°) 30°

DIRECTION 124° (grid)

COORDINATES E197698.8 N606805.7

R.L. OF COLLAR 534.9m

SHEET 2 OF 3

Drilling Information				Rock Substance		Rock Mass Defects									
Method	Casing	Water	Pressure test * (lugeons)	Lift & % core recovery	Depth (metres)	Graphic log & core loss	Substance description rock type: grain characteristics colour, structure, minor components.	RQD	Weathering	Strength Is (50) (MPa)	Defect spacing (cm)	Defect description thickness, type, inclination, planarity, roughness, coating, strength.		Rock condition No.	
										0.03 0.1 0.3 0.5 1.0 2.0 5.0 10.0 20.0 50.0 100.0	0.03 0.1 0.3 0.5 1.0 2.0 5.0 10.0 20.0 50.0 100.0	Particular	General		
NIMLC			NOT TESTED	100	21	V	DACITE Mostly stained. Purple with dark green (chlorite) veins throughout. Hard. Moderately strong.	40	FR					Rock mass is close jointed and in places fractured (15%) with many defect surfaces greasy &/or slickensided. In close jointed zones joints are generally spaced 3-10 cm and oriented at 30° (2 sets) and 60°-90° to core. Surfaces are strongly slickensided with chlorite and calcite. Many are greasy with a thin coating of clay. In fractured zones spacing is < 1mm to 2 cm. Surfaces are strongly slickensided with chlorite & greasy.	3-4
				100	22	V		10							4
				100	23	V		35							3-4
				100	24	V		60							
				100	25	V		35							
			O	100	26	V		10							4
				100	27	V		15							
				100	28	V		30							
			O	100	29	V		35							5
				100	30	V		0							
				100	31	V		15							
			O	100	32	V		30							4-5
				100	33	V		25							
				100	34	V		15							
			A	100	35	V		40							
				100	36	V									
				100	37	V									
				100	38	V		15							
				100	39	V		40							

Drill type CRAELIUS

Feed Hydraulic

Core barrel type NMLC

Triple tube split barrel

Driller D. Wheatly (DHC)

Commenced 24/6/75

Completed 7/7/75

Logged by E.A. LANG

Vertical scale 1cm=1m

Weathering

Fr — Fresh

SW — Slightly weathered

MW — Moderately weathered

HW — Highly weathered

EW — Extremely weathered

Notes:

Bedding & Joint Planes — Angles are measured relative to a plane normal to the core axis.

* Water Pressure Tests — Values in lugeons should be read in conjunction with computation sheets. Test sections are indicated by blocked in strips.

Water

10 Oct. '73 water level date shown

Water inflow

Partial drilling water loss

Complete drilling water loss

Core Photograph Negative No.

Depth (m) Black & White Colour

155/A16/1477 2 of 3

GEOLOGICAL LOG OF DRILL HOLE

Drilling Information					Rock Substance			Rock Mass Defects					
Method	Casing	Water	Pressure test * (lugeons)	Lift & % core recovery	Depth (metres)	Graphic log & core loss	Substance description rock type: grain characteristics colour, structure, minor components.	RQD	Weathering	Strength Is (50) (MPa)	Defect spacing (cm)	Defect description thickness, type, inclination, planarity, roughness, coating, strength. Particular General	Rock condition No
NMLC			<1	100	41	V	DACITE Purple	55	FR	0.3 0.1-3 0.003-100 0.001-100	2.0 1.0 0.5 0.3 0.1	Rock mass is close jointed and inplaces fractured. Joints are coated with chlorite (weak) and some thin veneer of clay. Some crushed seams up to 10 cm thick.	4
					42	V		35					
		100		43	V								
							END OF HOLE 43.25m						

Drill type CRAELIUS
Feed Hydraulic
Core barrel type NMLC with
triple tube & split inner
Driller D. Wheatly (DHC)
Commenced 24/6/75
Completed 7/7/75
Logged by BALANG
Vertical scale 1cm = 1m

Weathering

Fr — Fresh
SW — Slightly weathered
MW — Moderately weathered
HW — Highly weathered
EW — Extremely weathered

Notes:

Bedding & Joint Planes — Angles are measured relative to a plane normal to the core axis.
* Water Pressure Tests — Values in lugeons should be read in conjunction with computation sheets. Test sections are indicated by blacked in strips.

Water

10 Oct. '73 water level date shown
Water inflow
Partial drilling water loss
Complete drilling water loss

Core Photograph Negative No.

Depth (m) Black & White Colour

155/AIG/1477 3 of 3

GEOLOGICAL LOG OF DRILL HOLE

ANGLE FROM HORIZONTAL (°) 30°

DIRECTION 138° gr. d

COORDINATES E 197662 N 608745

R.L. OF COLLAR 543m

SHEET 1 OF 3

Drilling Information				Rock Substance				Rock Mass Defects														
Method	Casing	Water	Pressure test * (lugeons)	Lift & % core recovery	Depth (metres)	Graphic log & core loss	Substance description rock type: grain characteristics colour, structure, minor components	Weathering	Strength Is (50) (MPa)	Defect spacing (cm)	Defect description thickness, type, Inclination, planarity, roughness, coating, strength. Particular General	Rock condition No.										
Rock Rolled					1	NOT CORED	NOT CORED				NOT CORED											
					2																	
NMLC			NOT TESTED		3	NOT CORED	NOT CORED															
					4																	
					5																	
					6																	
					7								80	SS	FAULT BRECCIA Partly healed & cemented, partly loose and fractured or held together with heavy fat clay. Rock fragments are mostly Walker member Dacite above 16m. with increasing proportion of purple rhyodacite towards 16m.	20	some EW seams.			Faulted rock. Sheared and fractured. Healed in places. Loose or held together with heavy clay in other places. Many clay seams up to 30cm thick. Fractured zones with clay up to 1m. thick.	5	
					8								35	loss		0						
					9								35	SS		0						
					10								100	SS		45						
					11								45	loss		0						
					12								45	SS		7						
					13								100	SS		0						
					14								25	loss		10						
					15								95	SS		20						
					16								100	SS		40						MW
					17								98	SS	15	HW	Fractured to gravel size.	5				
					18																	
					19																	
					20																	
					21																	
					22																	
23																						
24																						
25																						

Drill type CRAELIUS

Feed Hydraulic

Core barrel type NMLC with

triplicate split barrel

Driller D. Wheatly (DHC)

Commenced R. White 11-7-75

Completed 11-8-75

Logged by PALANG

Vertical scale 1cm=1m

Weathering

Fr — Fresh

SW — Slightly weathered

MW — Moderately weathered

HW — Highly weathered

EW — Extremely weathered

Notes:

Bedding & Joint Planes — Angles are measured relative to a plane normal to the core axis.

* Water Pressure Tests — Values in lugeons should be read in conjunction with computation sheets. Test sections are indicated by blacked in strips.

Water

10 Oct. '73 water level date shown

Water inflow

Partial drilling water loss

Complete drilling water loss





Core Photograph Negative No.

Depth (m) Black & White Colour

155[A16]1478 1053

HOLE NO. GSI
15

SHEET 2 OF 3

Drill type <u>CRAELIUS</u> -----	<u>Weathering</u>	<u>Water</u>	Core Photograph Negative No.
Feed <u>Hydraulic</u> -----	Fr — Fresh	 10 Oct. '73 water level data shown	Depth (m)
Core barrel type <u>HC LC with</u>	SW — Slightly weathered	 Water inflow	Black & White
<u>triple tube & split inner</u>	MW — Moderately weathered	 Partial drilling water loss	Colour
Driller <u>D. Wheatly (DHC)</u>	HW — Highly weathered	 Complete drilling water loss	
<u>R. White</u>	EW — Extremely weathered		
Commenced <u>11-7-75</u>	Notes:		
Completed <u>11-8-75</u>	Bedding & Joint Planes — Angles are measured relative to a plane normal to the core axis.		
Logged by <u>F. ALANG</u>	* Water Pressure Tests — Values in lugeons should be read in conjunction with computation		
Vertical scale <u>1cm = 1m</u>	sheets. Test sections are indicated by blacked in strips.		
			<u>1551A1611478 2 of 3</u>

GEOLOGICAL LOG OF DRILL HOLE

ANGLE FROM HORIZONTAL (θ) 30° DIRECTION 138° gr d
COORDINATES E 197662 N 608745 R.L. OF COLLAR 543m

SHEET 3 OF 3

Drilling Information					Rock Substance		Rock Mass Defects				
Method	Casing	Water	Pressure test * (lugeons)	Lift & % core recovery	Depth (metres)	Substance description rock type: grain characteristics colour, structure, minor components.	Weathering	Strength Is (50) (MPa)	Defect spacing (cm)	Defect description thickness, type, inclination, planarity, roughness, coating, strength Particular General	Rock condition No.
TUNNEL NMLC			0	100	41	Purple RHYODACITE Partly altered. Moderately strong. Fairly soft to drill.	FR	03-1000 000-1000 m 000-1000	m 000-1000 m 000-1000 m 000-1000	40cm gravelly clay 30cm gravelly clay 50cm fractured with clay. Gravelly clay. Fractured Fractured Near 90° fracture zone with clay. 2m of core. 10cm clay seam	Rock mass is generally close jointed (10-15cm) and in places fractured. Joints are generally coated with 1-5mm of clay. Fractured zones generally 60-90° to core and up to 2m of core is affected in each zone. Fractured zones have much clay. Crushed seams up to 30cm thick spaced > 1m. Rock mass is close jointed (generally 10-15cm). Many joints have a veneer of clay. Some clay seams up to 10cm thick (rare). Most joints at 30° some at 80°.
				95	42						
				100	43						
				100	44						
				100	45						
				100	46						
				100	47						
				100	48						
				100	49						
				100	50						
				100	51						
				100	52						
				100	53						
				100	54						
				100	55						
				100	56						
				100	57						
				100	58						
				100	59						
				END OF HOLE 59.38m							

Drill type CRAELIUS
Feed Hydraulic
Core barrel type NMLC with
tube & air line
Driller D. Whealy (DHC)
R. White
Commenced 11-7-75
Completed 11-8-75
Logged by P. LANG
Vertical scale 1cm = 1m

Weathering
Fr - Fresh
SW - Slightly weathered
MW - Moderately weathered
HW - Highly weathered
EW - Extremely weathered

Notes:
Bedding & Joint Planes - Angles are measured relative to a plane normal to the core axis.
* Water Pressure Tests - Values in lugeons should be read in conjunction with computation sheets. Test sections are indicated by blacked in strips.

Water

10 Oct. '73 water level date shown
Water inflow
Partial drilling water loss
Complete drilling water loss

Core Photograph Negative No.
Depth (m) Black & White Colour

155/A16/1478 3 of 3

GEOLOGICAL LOG OF DRILL HOLE

ANGLE FROM HORIZONTAL (°) 90°

DIRECTION

COORDINATES 197629E

608565N

R.L. OF COLLAR 569.0m

SHEET 1 OF 2

Drilling Information				Rock Substance				Rock Mass Defects						
Method	Casing	Water	Pressure test * (lugeons)	Lift & % core recovery	Depth (metres)	Graphic log & core loss	Substance description rock type: grain characteristics colour, structure, minor components	RQD	Weathering	Strength Is (50) (MPa)	Defect spacing (cm)	Defect description thickness, type, inclination, planarity, roughness, coating, strength.		Rock condition No.
Rock Rotted	NIL			NOT CORED						0.03 0.1 0.3 0.5 1.0 3.0 10.0	0.03 0.1 0.3 0.5 1.0 3.0 10.0	Particular	General	
NOT TESTED														
				100	1		RHYOLITE Pale green. Silicious with quartz phenocrysts. Hard, strong.	60	MW			10cm sandy clay joint filling. 2cm sandy clay joint filling. 2cm sandy clay joint filling. } all at 30°		2 joints sets : 0°-30° , 45°-60° and random joints. Thin veneer of sandy clay on joints for 10cm. 20cm of horizontal fractures spaced 2mm - 2cm. 10cm with clay and limonite infilling on joints 1cm with clay and limonite 2cm yellow clay and limonite 2 joint sets : 30°-45° , 45°-60° in opposite directions and random joints. Rock mass moderately strong. Joints heavily stained with limonite but tight. Some joints cemented with limonite. (moderately strong) did not break during drilling but may open up during blasting. Joints spaced generally 10-40cm. Some joints are crushed and partly sheared with clay.
				100	2			60	SW					
				100	3			60						
				100	4			50						
				100	5			90						
				100	6			80	SW to FS					
				100	7			75						
				100	8			80						
				100	9			70						
				100	10			80						
				100	11			70						
				100	12			80						
				100	13			93						
				100	14			43	MW to SW					
				100	15			50						
				100	16			75						
				100	17			35	FS					
				100	18									
				100	19									

NOT TESTED

RHYOLITE
Pale green. Silicious with
quartz phenocrysts.
Hard, strong.10cm sandy clay joint filling.
2cm sandy clay joint filling.
2cm sandy clay joint filling.
all at 30°

Thin veneer of sandy clay on joints for 10cm.

20cm of horizontal fractures spaced 2mm - 2cm.
10cm with clay and limonite infilling on joints.
1cm with clay and limonite

2cm yellow clay and limonite

2 joint sets: 0°-30°, 45°-60° and random joints.
2 joint sets: 30°-45°, 45°-60° in opposite directions and random joints.
Rock mass moderately strong. Joints heavily stained with limonite but tight. Some joints cemented with limonite. (moderately strong) did not break during drilling but may open up during blasting. Joints spaced generally 10-40cm. Some joints are crushed and partly sheared with clay.

Rock close jointed, and fractured (many fractures are drill induced). Defects are joints and fractures spaced often < 7cm, but up to 40cm, with sandy zones generally less than 5cm wide spaced from 20-50cm. Mostly horizontal. Probably need support.

Drill type MLE
Feed Hydraulic
Core barrel type NMLC with
triple tube & split inner
Driller B.Harte (DHC)
Commenced 13/5/75
Completed 26/5/75
Logged by P.A.LANG
Vertical scale 1cm = 1m

Weathering

Fr - Fresh
SW - Slightly weathered
MW - Moderately weathered
HW - Highly weathered
EW - Extremely weathered

Notes:

Bedding & Joint Planes - Angles are measured relative to a plane normal to the core axis.

* Water Pressure Tests - Values in lugeons should be read in conjunction with computation sheets. Test sections are indicated by blacked in strips.

Water

10 Oct. '73 water level date shown
Water inflow
Partial drilling water loss
Complete drilling water loss

Core Photograph Negative No.

Depth (m) Black & White Colour

155/A16/1479 70r3

DIRECTION

R.L. OF COLLAR 5690m

SHEET 2 OF 3

Drill type MOLE	<u>Weathering</u>	<u>Water</u>	Core Photograph Negative No.
Feed Hydraulic	Fr — Fresh	IO Oct. '73 water level date shown	Depth (m)
Core barrel type NMUC with triple tube & split inner	SW — Slightly weathered	Water inflow	Black & White
Driller B.Harte (DHC)	MW — Moderately weathered	Partial drilling water loss	Colour
Commenced 13/5/75	HV — Highly weathered	Complete drilling water loss	
Completed 26/5/75	EW — Extremely weathered		
Logged by P.A.LANG	Notes:		
Vertical scale 1cm=1m	Bedding & Joint Planes — Angles are measured relative to a plane normal to the core axis.		
	* Water Pressure Tests — Values in lugeons should be read in conjunction with computation sheets. Test sections are indicated by blacked in strips.		
			153/108/1479-2083

GEOLOGICAL LOG OF DRILL HOLE

ANGLE FROM HORIZONTAL (°) 90° DIRECTION -
COORDINATES 197629E 608565N R.L. OF COLLAR 569.0 mSHEET 3 OF 3

Drilling Information				Rock Substance			Rock Mass Defects								
Method	Casing	Water	Pressure test * (lugeons)	Lift & % core recovery	Depth (metres)	Graphic log & core loss	Substance description rock type: grain characteristics colour, structure, minor components.	Weathering	Strength Is (50) (MPa)	Defect spacing (cm)	Defect description thickness, type, inclination, planarity, roughness, coating, strength. Particular General	Rock condition No.			
NMLC		11/6/75	0	100	41	✕	RHYODACITE Purple Moderately soft, weak.	FS altered	0.03 0.03 0.03 0.03 0.03 0.03 0.03	0.03 0.03 0.03 0.03 0.03 0.03 0.03	Rock mass is very seamy, weak. Defects are all joints all clay coated & crushed seams with clay. Joints spaced 10-30 cm, commonly 1-15 cm. Crushed sandy clay seams often spaced 5-10 cm. Support very likely.	5			
				100	42	✕									
				100	43	✕									
				100	44	✕									
				100	45	✕									
				100	46	✕									
				100	47	✕									
		18/6/75	0	100	48	✕	RHYOLITE Purplish green. Moderately soft, weak. Rock is partly sheared & healed with epidote.	FR altered	60 85	Rock mass weak. Core broken into lengths 10-30cm. Rock sheared and healed with epidote & clay. Clay veneer on joints. No crushed seams. Incipient healed fractures at 80-90°. Many incipient fractures would break during blasting.	4				
				100	49	✕									
				100	50	✕	RHYODACITE Purple. Moderately soft, weak. Rock is sheared & healed with epidote and clay veins.			55	clay seams 3-7cm wide.	20cm thick clay seam dip 30-45°.	Rock mass very seamy. Clay seams & crushed sandy clay seams 5-20cm wide, spaced 15-20cm. Rock mass riddled with incipient fractures cemented with clay. Support likely.	5	
				100	51	✕									
				100	52	✕									
				100	53	✕									
															END OF HOLE 53.15m

Drill type MOLE
Feed Hydraulic
Core barrel type NMLC with triple tube & split inner
Driller B.Harte (DHC)
Commenced 13/5/75
Completed 26/5/75
Logged by PA LANG
Vertical scale 1:1000

Weathering

Fr — Fresh
SW — Slightly weathered
MW — Moderately weathered
HW — Highly weathered
EW — Extremely weathered

Notes:

Bedding & Joint Planes — Angles are measured relative to a plane normal to the core axis.
* Water Pressure Tests — Values in lugeons should be read in conjunction with computation sheets. Test sections are indicated by blacked in strips.

Water

10 Oct. '73 water level date shown
Water inflow
Partial drilling water loss
Complete drilling water loss

Core Photograph Negative No.

Depth (m) Black & White Colour

155/116/1479 30f3

ANGLE FROM HORIZONTAL (θ) 30° DIRECTION 025 grid
COORDINATES E197569 N608429 R.L. OF COLLAR 522.2m

SHEET 1 OF 2

NOT TESTED

Depth (m)	Black & White	Colour
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SHEET 1 OF 2

Drill type MCLE	Weathering	Water	Core Photograph Negative No.
Feed Hydraulic	Fr — Fresh	10 Oct. '73 water level date shown	Depth (m) Black & White Colour
Core barrel type MML with splitter	SW — Slightly weathered	Water inflow	— — — — —
Driller B.Hartiz (DHC)	MW — Moderately weathered	Partial drilling water loss	— — — — —
Commenced 29/7/75	HW — Highly weathered	Complete drilling water loss	— — — — —
Completed 2/8/75	EW — Extremely weathered		— — — — —
Logged by PALANG	Notes:		— — — — —
Vertical scale 1cm = 1m	Bedding & Joint Planes — Angles are measured relative to a plane normal to the core axis.		— — — — —
	* Water Pressure Tests — Values in lugeons should be read in conjunction with computation sheets. Test sections are indicated by blacked in strips.		— — — — —
			1557A16T148J 1 of 2

GEOLOGICAL LOG OF DRILL HOLE

ANGLE FROM HORIZONTAL (θ) 90 DIRECTION —
COORDINATES E197471.5 N608319.7 R.L. OF COLLAR 529m.

SHEET 2 OF 2

Drilling Information					Rock Substance				Rock Mass Defects				
Method	Casing	Water	Pressure test * (lugeons)	Lift & % core recovery	Depth (metres)	Graphic log & core loss	Substance description rock type: grain characteristics colour, structure, minor components.	RQD	Weathering	Strength Is (50) (MPa)	Defect spacing (cm)	Defect description thickness, type, inclination, planarity, roughness, coating, strength. Particular General	Rock condition No.
NM-C			3-4	100	21	V	DACITE as above	40	FR	0.03 0.05 0.07 0.10 0.15 0.20 0.25 0.30 0.35 0.40 0.45 0.50 0.55 0.60 0.65 0.70 0.75 0.80 0.85 0.90 0.95 1.00 1.05 1.10 1.15 1.20 1.25 1.30 1.35 1.40 1.45 1.50 1.55 1.60 1.65 1.70 1.75 1.80 1.85 1.90 1.95 2.00 2.05 2.10 2.15 2.20 2.25 2.30 2.35 2.40 2.45 2.50 2.55 2.60 2.65 2.70 2.75 2.80 2.85 2.90 2.95 3.00 3.05 3.10 3.15 3.20 3.25 3.30 3.35 3.40 3.45 3.50 3.55 3.60 3.65 3.70 3.75 3.80 3.85 3.90 3.95 4.00 4.05 4.10 4.15 4.20 4.25 4.30 4.35 4.40 4.45 4.50 4.55 4.60 4.65 4.70 4.75 4.80 4.85 4.90 4.95 5.00 5.05 5.10 5.15 5.20 5.25 5.30 5.35 5.40 5.45 5.50 5.55 5.60 5.65 5.70 5.75 5.80 5.85 5.90 5.95 6.00 6.05 6.10 6.15 6.20 6.25 6.30 6.35 6.40 6.45 6.50 6.55 6.60 6.65 6.70 6.75 6.80 6.85 6.90 6.95 7.00 7.05 7.10 7.15 7.20 7.25 7.30 7.35 7.40 7.45 7.50 7.55 7.60 7.65 7.70 7.75 7.80 7.85 7.90 7.95 8.00 8.05 8.10 8.15 8.20 8.25 8.30 8.35 8.40 8.45 8.50 8.55 8.60 8.65 8.70 8.75 8.80 8.85 8.90 8.95 9.00 9.05 9.10 9.15 9.20 9.25 9.30 9.35 9.40 9.45 9.50 9.55 9.60 9.65 9.70 9.75 9.80 9.85 9.90 9.95 10.00 10.05 10.10 10.15 10.20 10.25 10.30 10.35 10.40 10.45 10.50 10.55 10.60 10.65 10.70 10.75 10.80 10.85 10.90 10.95 11.00 11.05 11.10 11.15 11.20 11.25 11.30 11.35 11.40 11.45 11.50 11.55 11.60 11.65 11.70 11.75 11.80 11.85 11.90 11.95 12.00 12.05 12.10 12.15 12.20 12.25 12.30 12.35 12.40 12.45 12.50 12.55 12.60 12.65 12.70 12.75 12.80 12.85 12.90 12.95 13.00 13.05 13.10 13.15 13.20 13.25 13.30 13.35 13.40 13.45 13.50 13.55 13.60 13.65 13.70 13.75 13.80 13.85 13.90 13.95 14.00 14.05 14.10 14.15 14.20 14.25 14.30 14.35 14.40 14.45 14.50 14.55 14.60 14.65 14.70 14.75 14.80 14.85 14.90 14.95 15.00 15.05 15.10 15.15 15.20 15.25 15.30 15.35 15.40 15.45 15.50 15.55 15.60 15.65 15.70 15.75 15.80 15.85 15.90 15.95 16.00 16.05 16.10 16.15 16.20 16.25 16.30 16.35 16.40 16.45 16.50 16.55 16.60 16.65 16.70 16.75 16.80 16.85 16.90 16.95 17.00 17.05 17.10 17.15 17.20 17.25 17.30 17.35 17.40 17.45 17.50 17.55 17.60 17.65 17.70 17.75 17.80 17.85 17.90 17.95 18.00 18.05 18.10 18.15 18.20 18.25 18.30 18.35 18.40 18.45 18.50 18.55 18.60 18.65 18.70 18.75 18.80 18.85 18.90 18.95 19.00 19.05 19.10 19.15 19.20 19.25 19.30 19.35 19.40 19.45 19.50 19.55 19.60 19.65 19.70 19.75 19.80 19.85 19.90 19.95 20.00 20.05 20.10 20.15 20.20 20.25 20.30 20.35 20.40 20.45 20.50 20.55 20.60 20.65 20.70 20.75 20.80 20.85 20.90 20.95 21.00 21.05 21.10 21.15 21.20 21.25 21.30 21.35 21.40 21.45 21.50 21.55 21.60 21.65 21.70 21.75 21.80 21.85 21.90 21.95 22.00 22.05 22.10 22.15 22.20 22.25 22.30 22.35 22.40 22.45 22.50 22.55 22.60 22.65 22.70 22.75 22.80 22.85 22.90 22.95 23.00 23.05 23.10 23.15 23.20 23.25 23.30 23.35 23.40 23.45 23.50 23.55 23.60 23.65 23.70 23.75 23.80 23.85 23.90 23.95 24.00 24.05 24.10 24.15 24.20 24.25 24.30 24.35 24.40 24.45 24.50 24.55 24.60 24.65 24.70 24.75 24.80 24.85 24.90 24.95 25.00 25.05 25.10 25.15 25.20 25.25 25.30 25.35 25.40 25.45 25.50 25.55 25.60 25.65 25.70 25.75 25.80 25.85 25.90 25.95 26.00 26.05 26.10 26.15 26.20 26.25 26.30 26.35 26.40 26.45 26.50 26.55 26.60 26.65 26.70 26.75 26.80 26.85 26.90 26.95 27.00 27.05 27.10 27.15 27.20 27.25 27.30 27.35 27.40 27.45 27.50 27.55 27.60 27.65 27.70 27.75 27.80 27.85 27.90 27.95 28.00 28.05 28.10 28.15 28.20 28.25 28.30 28.35 28.40 28.45 28.50 28.55 28.60 28.65 28.70 28.75 28.80 28.85 28.90 28.95 29.00 29.05 29.10 29.15 29.20 29.25 29.30 29.35 29.40 29.45 29.50 29.55 29.60 29.65 29.70 29.75 29.80 29.85 29.90 29.95 30.00 30.05 30.10 30.15 30.20 30.25 30.30 30.35 30.40 30.45 30.50 30.55 30.60 30.65 30.70 30.75 30.80 30.85 30.90 30.95 31.00 31.05 31.10 31.15 31.20 31.25 31.30 31.35 31.40 31.45 31.50 31.55 31.60 31.65 31.70 31.75 31.80 31.85 31.90 31.95 32.00 32.05 32.10 32.15 32.20 32.25 32.30 32.35 32.40 32.45 32.50 32.55 32.60 32.65 32.70 32.75 32.80 32.85 32.90 32.95 33.00 33.05 33.10 33.15 33.20 33.25 33.30 33.35 33.40 33.45 33.50 33.55 33.60 33.65 33.70 33.75 33.80 33.85 33.90 33.95 34.00 34.05 34.10 34.15 34.20 34.25 34.30 34.35 34.40 34.45 34.50 34.55 34.60 34.65 34.70 34.75 34.80 34.85 34.90 34.95 35.00 35.05 35.10 35.15 35.20 35.25 35.30 35.35 35.40 35.45 35.50 35.55 35.60 35.65 35.70 35.75 35.80 35.85 35.90 35.95 36.00 36.05 36.10 36.15 36.20 36.25 36.30 36.35 36.40 36.45 36.50 36.55 36.60 36.65 36.70 36.75 36.80 36.85 36.90 36.95 37.00 37.05 37.10 37.15 37.20 37.25 37.30 37.35 37.40 37.45 37.50 37.55 37.60 37.65 37.70 37.75 37.80 37.85 37.90 37.95 38.00 38.05 38.10 38.15 38.20 38.25 38.30 38.35 38.40 38.45 38.50 38.55 38.60 38.65 38.70 38.75 38.80 38.85 38.90 38.95 39.00 39.05 39.10 39.15 39.20 39.25 39.30 39.35 39.40 39.45 39.50 39.55 39.60 39.65 39.70 39.75 39.80 39.85 39.90 39.95 40.00 40.05 40.10 40.15 40.20 40.25 40.30 40.35 40.40 40.45 40.50 40.55 40.60 40.65 40.70 40.75 40.80 40.85 40.90 40.95 41.00 41.05 41.10 41.15 41.20 41.25 41.30 41.35 41.40 41.45 41.50 41.55 41.60 41.65 41.70 41.75 41.80 41.85 41.90 41.95 42.00 42.05 42.10 42.15 42.20 42.25 42.30 42.35 42.40 42.45 42.50 42.55 42.60 42.65 42.70 42.75 42.80 42.85 42.90 42.95 43.00 43.05 43.10 43.15 43.20 43.25 43.30 43.35 43.40 43.45 43.50 43.55 43.60 43.65 43.70 43.75 43.80 43.85 43.90 43.95 44.00 44.05 44.10 44.15 44.20 44.25 44.30 44.35 44.40 44.45 44.50 44.55 44.60 44.65 44.70 44.75 44.80 44.85 44.90 44.95 45.00 45.05 45.10 45.15 45.20 45.25 45.30 45.35 45.40 45.45 45.50 45.55 45.60 45.65 45.70 45.75 45.80 45.85 45.90 45.95 46.00 46.05 46.10 46.15 46.20 46.25 46.30 46.35 46.40 46.45 46.50 46.55 46.60 46.65 46.70 46.75 46.80 46.85 46.90 46.95 47.00 47.05 47.10 47.15 47.20 47.25 47.30 47.35 47.40 47.45 47.50 47.55 47.60 47.65 47.70 47.75 47.80 47.85 47.90 47.95 48.00 48.05 48.10 48.15 48.20 48.25 48.30 48.35 48.40 48.45 48.50 48.55 48.60 48.65 48.70 48.75 48.80 48.85 48.90 48.95 49.00 49.05 49.10 49.15 49.20 49.25 49.30 49.35 49.40 49.45 49.50 49.55 49.60 49.65 49.70 49.75 49.80 49.85 49.90 49.95 50.00 50.05 50.10 50.15 50.20 50.25 50.30 50.35 50.40 50.45 50.50 50.55 50.60 50.65 50.70 50.75 50.80 50.85 50.90 50.95 51.00 51.05 51.10 51.15 51.20 51.25 51.30 51.35 51.40 51.45 51.50 51.55 51.60 51.65 51.70 51.75 51.80 51.85 51.90 51.95 52.00 52.05 52.10 52.15 52.20 52.25 52.30 52.35 52.40 52.45 52.50 52.55 52.60 52.65 52.70 52.75 52.80 52.85 52.90 52.95 53.00 53.05 53.10 53.15 53.20 53.25 53.30 53.35 53.40 53.45 53.50 53.55 53.60 53.65 53.70 53.75 53.80 53.85 53.90 53.95 54.00 54.05 54.10 54.15 54.20 54.25 54.30 54.35 54.40 54.45 54.50 54.55 54.60 54.65 54.70 54.75 54.80 54.85 54.90 54.95 55.00 55.05 55.10 55.15 55.20 55.25 55.30 55.35 55.40 55.45 55.50 55.55 55.60 55.65 55.70 55.75 55.80 55.85 55.90 55.95 56.00 56.05 56.10 56.15 56.20 56.25 56.30 56.35 56.40 56.45 56.50 56.55 56.60 56.65 56.70 56.75 56.80 56.85 56.90 56.95 57.00 57.05 57.10 57.15 57.20 57.25 57.30 57.35 57.40 57.45 57.50 57.55 57.60 57.65 57.70 57.75 57.80 57.85 57.90 57.95 58.00 58.05 58.10 58.15 58.20 58.25 58.30 58.35 58.40 58.45 58.50 58.55 58.60 58.65 58.70 58.75 58.80 58.85 58.90 58.95 59.00 59.05 59.10 59.15 59.20 59.25 59.30 59.35 59.40 59.45 59.50 59.55 59.60 59.65 59.70 59.75 59.80 59.85 59.90 59.95 60.00 60.05 60.10 60.15 60.20 60.25 60.30 60.35 60.40 60.45 60.50 60.55 60.60 60.65 60.70 60.75 60.80 60.85 60.90 60.95 61.00 61.05 61.10 61.15 61.20 61.25 61.30 61.35 61.40 61.45 61.50 61.55 61.60 61.65 61.70 61.75 61.80 61.85 61.90 61.95 62.00 62.05 62.10 62.15 62.20 62.25 62.30 62.35 62.40 62.45 62.50 62.55 62.60 62.65 62.70 62.75 62.80 62.85 62.90 62.95 63.00 63.05 63.10 63.15 63.20 63.25 63.30 63.35 63.40 63.45 63.50 63.55 63.60 63.65 63.70 63.75 63.80 63.85 63.90 63.95 64.00 64.05 64.10 64.15 64.20 64.25 64.30 64.35 64.40 64.45 64.50 64.55 64.60 64.65 64.70 64.75 64.80 64.85 64.90 64.95 65.00 65.05 65.10 65.15 65.20 65.25 65.30 65.35 65.40 65.45 65.50 65.55 65.60 65.65 65.70 65.75 65.80 65.85 65.90 65.95 66.00 66.05 66.10 66.15 66.20 66.25 66.30 66.35 66.40 66.45 66.50 66.55 66.60 66.65 66.70 66.75 66.80 66.85 66.90 66.95 67.00 67.05 67.10 67.15 67.20 67.25 67.30 67.35 67.40 67.45 67.50 67.55 67.60 67.65 67.70 67.75 67.80 67.85 67.90 67.95 68.00 68.05 68.10 68.15 68.20 68.25 68.30 68.35 68.40 68.45 68.50 68.55 68.60 68.65 68.70 68.75 68.80 68.85 68.90 68.95 69.00 69.05 69.10 69.15 69.20 69.25 69.30 69.35 69.40 69.45 69.50 69.55 69.60 69.65 69.70 69.75 69.80 69.85 69.90 69.95 70.00 70.05 70.10 70.15 70.20 70.25 70.30 70.35 70.40 70.45 70.50 70.55 70.60 70.65 70.70 70.75 70.80 70.85 70.90 70.95 71.00 71.05 71.10 71.15 71.20 71.25 71.30 71.35 71.40 71.45 71.50 71.55 71.60 71.65 71.70 71.75 71.80 71.85 71.90 71.95 72.00 72.05 72.10 72.15 72.20 72.25 72.30 72.35 72.40 72.45 72.50 72.55 72.60 72.65 72.70 72.75 72.80 72.85 72.90 72.95 73.00 73.05 73.10 73.15 73.20 73.25 73.30 73.35 73.40 73.45 73.50 73.55 73.60 73.65 73.70 73.75 73.80 73.85 73.90 73.95 74.00 74.05 74.10 74.15 74.20 74.25 74.30 74.35 74.40 74.45 74.50 74.55 74.60 74.65 74.70 74.75 74.80 74.85 74.90 74.95 75.00 75.05 75.10 75.15 75.20 75.25 75.30 75.35 75.40 75.45 75.50 75.55 75.60 75.65 75.70 75.75 75.80 75.85 75.90 75.95 76.00 76.05 76.10 76.15 76.20 76.25 76.30 76.35 76.40 76.45 76.50 76.55 76.60 76.65 76.70 76.75 76.80 76.85 76.90 76.95 77.00 77.05 77.10 77.15 77.20 77.25 77.30 77.35 77.40 77.45 77.50 77.55 77.60 77.65 77.70 77.75 77.80 77.85 77.90 77.95 78.00 78.05 78.10 78.15 78.20 78.25 78.30 78.35 78.40 78.45 78.50 78.55 78.60 78.65 78.70 78.75 78.80 78.85 78.90 78.95 79.00 79.05 79.10 79.15 79.20 79.25 79.30 79.35 79.40 79.45 79.50 79.55 79.60 79.65 79.70 79.75 79.80 79.85 79.90 79.95 80.00 80.05 80.10 80.15 80.20 80.25 80.30 80.35 80.40 80.45 80.50 80.55 80.60 80.65 80.70 80.75 80.80 80.85 80.90 80.95 81.00 81.05 81.10 81.15 81.20 81.25 81.30 81.35 81.40 81.45 81.50 81.55 81.60 81.65 81.70 81.75 81.80 81.85 81.90 81.95 82.00 82.05 82.10 82.15 82.20 82.25 82.30 82.35 82.40 82.45 82.50 82.55 82.60 82.65 82.70 82.75 82.80 82.85 82.90 82.95 83.00 83.05 83.10 83.15 83.20 83.25 83.30 83.35 83.40 83.45 83.50 83.55 83.60 83.65 83.70 83.75 83.80 83.85 83.90 83.95 84.00 84.05 84.10 84.15 84.20 84.25 84.30 84.35 84.40 84.45 84.50 84.55 84.60 84.65 84.70 84.75 84.80 84.85 84.90 84.95 85.00 85.05 85.10 85.15 85.20 85.25 85.30 85.35 85.40 85.45 85.50 85.55 85.60 85.65 85.70 85.75 85.80 85.85 85.90 85.95 86.00 86.05 86.10 86.15 86.20 86.25 86.30 86.35 86.40 86.45 86.50 86.55 86.60 86.65 86.70 86.75 86.80 86.85 86.90 86.95 87.00 87.05 87.10 87.15 87.20 87.25 87.30 87.35 87.40 87.45 87.50 87.55 87.60 87.65 87.70 87.75 87.80 			

Drill type MOLE
Feed Hydraulic
Core barrel type NML with
triple tube & split inner
Driller B. Harte (DHC)
Commenced 29/7/75
Completed 2/8/75
Logged by P. A. LANG
Vertical scale km = 1m

Weathering

Fr — Fresh
SW — Slightly weathered
MW — Moderately weathered
HW — Highly weathered
EW — Extremely weathered

Notes:
Bedding & Joint Planes — Angles are measured relative to a plane normal to the core axis.
* Water Pressure Tests — Values in lugeons should be read in conjunction with computation sheets. Test sections are indicated by blacked in strips.

Water

10	Oct. '73	water level date shown
		Water inflow
		Partial drilling water loss
		Complete drilling water loss

Core Photograph Negative No.

[illegible]

$1557A1611481^{-2}of2$

BUREAU OF MINERAL RESOURCES,
GEOLOGY & GEOPHYSICS

PROJECT GINNINDERRA SEWER TUNNEL
LOCATION 20m east of tunnel line at station 52+00

OBS BORE
HOLE NO. GST
20
CANBERRA 135
SHEET 1 OF 2

GEOLOGICAL LOG OF DRILL HOLE

ANGLE FROM HORIZONTAL (θ) 90° DIRECTION ---
COORDINATES E 137260 N 608100 R.L. OF COLLAR 572m

Drilling Information				Rock Substance		Rock Mass Defects						
Method	Casing	Water	Pressure test * (lugeons)	Lift & % core recovery	Depth (metres)	Graphic log & core loss	Substance description rock type: grain characteristics colour, structure, minor components.	Weathering	Strength Is (50) (MPa)	Defect spacing (cm)	Defect description thickness, type, inclination, planarity, roughness, coating, strength. Particular General	Rock condition No.
Rock Rolled — chips collected at 0.5m intervals.			NOT TESTED	NOT CORED	2	NOT CORED	DACITE Blue grey when fresh. Commonly stained purple. Very hard, very strong.	FR	0.3 0.1 0.05 0.01 0.005 0.001 0.0005 0.0001 0.00005 0.00001 0.000005 0.000001 0.0000005 0.0000001 0.00000005 0.00000001 0.000000005 0.000000001 0.0000000005 0.0000000001	0.0005 0.0001 0.00005 0.00001 0.000005 0.000001 0.0000005 0.0000001 0.00000005 0.00000001 0.000000005 0.000000001 0.0000000005 0.0000000001 0.00000000005 0.00000000001 0.000000000005 0.000000000001	Rock mass very strong. Joints tight.	Mainly 2-3
					4							
					6							
					8							
					10							
					12							
					14							
					16							
					18							
					20							
					22							
					24							
					26							
					28							
					30							
					32							
					34							
					36							
					38							
					40							

Drill type MEYHEW
Feed Hydraulic
Core barrel type NOT CORED
Driller Shanahan (BMR)
Commenced 19/3/75
Completed 10/4/75
Logged by R.A. LANG
Vertical scale 1cm = 2m

Weathering

Fr — Fresh

SW — Slightly weathered

MW — Moderately weathered

HW — Highly weathered

EW — Extremely weathered

Notes:

Bedding & Joint Planes — Angles are measured relative to a plane normal to the core axis.

* Water Pressure Tests — Values in lugeons should be read in conjunction with computation sheets. Test sections are indicated by blacked in strips.

Water

10 Oct. '73 water level date shown

Water inflow

Partial drilling water loss

Complete drilling water loss

Core Photograph Negative No.

Depth (m) Black & White Colour

GEOLOGICAL LOG OF DRILL HOLE

ANGLE FROM HORIZONTAL (°) 0
COORDINATES 157260E 608000N
DIRECTION
R.L. OF COLLAR 572m

SHEET 2 OF 2

Drilling Information				Rock Substance		Rock Mass Defects							
Method	Casing	Water	Pressure test * (lugeons)	Lift & % core recovery	Depth (metres)	Graphic log & core loss	Substance description rock type: grain characteristics colour, structure, minor components.	Weathering	Strength Is (50) (MPa)	Defect spacing (cm)	Defect description thickness, type, inclination, planarity, roughness, coating, strength. Particular General		Rock condition No.
TREIFUS 2 1/2" triple tube split jointer with split inner tube & DIAMOND BIT		9/2/75			41								
					42								
					43								
					44								
					45								
					46								
					47								
					48								
					49								
					50								
				100%	51	V	BLUE GREY JACITE - with red stained quartz phenocrysts and green inclusions up to 2cm (epidote?)					Thin veneer of clay on some joints - joints rough - Rock mass fairly tight.	3
				100%	52	V	Very hard, very strong.						
				100%	53	V							
				100%	54	V		FR			Drill core fragmented by shaking drill rig	Some clay seams of clay on joints. Joints rough.	3
				100%	55	V					1cm. clay seam		
				100%	56	V							
					57	V							
				100%	58	V							
					59	V							
				100%	60-10m.	V							
												Rock mass is very strong. Joints strongly cemented with calcite. Sticks of core up to 1.5m. long. Most joints at 30°, one at 90°. Joints rough.	2

Drill type Meyhew
Feed Hydraulic
Core barrel type TREIFUS 2 1/2" triple tube - split jointer
Driller J. Shanahan (BM)
Commenced 19-3-75
Completed 10-4-75
Logged by P. Lang
Vertical scale 1cm=1m

Weathering

Fr - Fresh
SW - Slightly weathered
MW - Moderately weathered
HW - Highly weathered
EW - Extremely weathered

Notes:

Bedding & Joint Planes - Angles are measured relative to a plane normal to the core axis.
* Water Pressure Tests - Values in lugeons should be read in conjunction with computation sheets. Test sections are indicated by blacked in strips.

Water

10 Oct. '73 water level date shown
Water inflow
Partial drilling water loss
Complete drilling water loss

Core Photograph Negative No.

Depth (m) Black & White Colour

155/A16/1482 2 of 2

GEOLOGICAL LOG OF DRILL HOLE

ANGLE FROM HORIZONTAL (θ) 90°
COORDINATES E 197749 N 608790DIRECTION
R.L. OF COLLAR 540m

SHEET 1 OF 2

Drilling Information				Rock Substance		Rock Mass Defects									
Method	Casing	Water	Pressure test * (lugeons)	Lift & % core recovery	Depth (metres)	Graphic log & core loss	Substance description rock type: grain characteristics colour, structure, minor components	RQD	Weathering	Strength Is (50) (MPa)	Defect spacing (cm)	Defect description thickness, type, inclination, planarity, roughness, coating, strength.		Rock condition No.	
										0.03 0.1 0.3 0.5 1.0 2.0	10 30 50 100 300	Particular	General		
Rock Rolled				NOT TESTED											
				NOT CORED											
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GEOLOGICAL LOG OF DRILL HOLE

ANGLE FROM HORIZONTAL (θ) 90° DIRECTION —
COORDINATES E 197749 N 608790 R.L. OF COLLAR 540 m

SHEET 2 OF 2

Drilling Information				Rock Substance		Rock Mass Defects								
Method	Casing	Water	Pressure test * (lugeons)	Lift & % core recovery	Depth (metres)	Graphic log & core loss	Substance description rock type: grain characteristics colour, structure, minor components.	RQD	Weathering	Strength Is (50) (MPa)	Defect spacing (cm)	Defect description thickness, type, inclination, planarity, roughness, coating, strength.	Rock condition No.	
												Particular	General	
Diamond coring			NOT TESTED	100	21	X	RHYOLITE As above	60	FR	0.03	3	Some crushed seams up to 1cm, but most fractures are drill induced. Core close jointed generally < 20 cm. Many incipient fractures partly healed. Joint surfaces strongly slickensided with chlorite. Some calcite cement.		3-4
	100	22		X	60	0.1		5						
						23	X	END OF HOLE 23.0m			0.3			
										1.0	100			
										3.0	300			

Drill type - Meyhew - - -
Feed - Hydraulic - - -
Core barrel type TRELFUS 23
triple tube - split inner
Driller - E. Lodwick (BMR)
Commenced - 5/9/75 - - -
Completed - 12/9/75 - - -
Logged by - P.A. Lang - - -
Vertical scale - 1 cm = 1 m

Weathering
Fr — Fresh
SW — Slightly weathered
MW — Moderately weathered
HW — Highly weathered
EW — Extremely weathered

Notes:
Bedding & Joint Planes — Angles are measured relative to a plane normal to the core axis.
* Water Pressure Tests — Values in lugeons should be read in conjunction with computation sheets. Test sections are indicated by blacked in strips.

Water

10 Oct. '73 water level date shown

Water inflow

Partial drilling water loss

Complete drilling water loss

Core Photograph Negative No.

Depth (m)	Black & White	Colour
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GEOLOGICAL LOG OF DRILL HOLE

ANGLE FROM HORIZONTAL (°) 90°
COORDINATES 198071E 609545NDIRECTION
R.L. OF COLLAR 574 m.

SHEET 1 OF 2

Drilling Information				Rock Substance				Rock Mass Defects				
Method	Casing	Water	Pressure test * (lugeons)	Lift & % core recovery	Depth (metres)	Graphic log	Substance description rock type: grain characteristics colour, structure, minor components	Weathering	Strength Is (50) (MPa)	Defect spacing (cm)	Defect description thickness, type, inclination, planarity, roughness, coating, strength Particular General	Rock condition No
Rock Rolling	NIL			Not Cored	1		NOT CORED				NOT CORED	
DRILL TECH TUNGSTEN BIT 2 1/2" core with triple tube core barrel & split inner tube					2							
					3							
				85%	4		QUARTZ FELDSPATHIC SANDSTONE Medium grained Brownish yellow & laminated. Rock is soft and weak. Some zones weathered to a sandy clay.				Clay on joints clay infillings up to 1cm. Joints spaced 3-12 cm.	Rock mass is weak. Core fragmented by drill into lengths 3-20 cm. 90% of breaks are horizontal (parallel to bedding) bedding planes mostly tight and moderately strong.
				100%	5			HW				
					6		Bedding horizontal					
				95%	7						Joints cemented with limonite. Weak.	Rock mass is weak. Defects weak joints mostly 30° to 45°, spaced 10-30 cm. Thin veneer of clay on some joints. Joints smooth, planar and moderately tight.
					8		Pale yellow laminated siltstone 80% & sandstone same as above 20%.					
					9		Small faults < 1m displacement. Cross bedding < 1m. Scour & fill structures < 1m.					
				85%	10		Intrusive contact, but no evidence of chilled margin or of baked sediments.					
					11		GRANITE PORPHYRY Light brown (HW) medium grained.					
				95%	12							
				95%	13							
				85%	14			HW				
				85%	15							
				85%	16							
				95%	17							
				100%	18							
				95%	19							
				90%	20							

Drill type Meyhew
Feed Hydraulic
Core barrel type Trifus 2 1/2"
triple tube - split inner
Driller T. Shanahan (BMR)
Commenced 11-4-75
Completed 17-4-75
Logged by P. Lang
Vertical scale 1cm = 1m.

Weathering
Fr - Fresh
SW - Slightly weathered
MW - Moderately weathered
HW - Highly weathered
EW - Extremely weathered

Notes:

Bedding & Joint Planes - Angles are measured relative to a plane normal to the core axis.
* Water Pressure Tests - Values in lugeons should be read in conjunction with computation sheets. Test sections are indicated by blocked in strips.

Water

10 Oct. '73 water level date shown
Water inflow
Partial drilling water loss
Complete drilling water loss

Core Photograph Negative No
Depth (m) Black & White Colour

155/A16/1484 1 of 2

HOLE NO. G.S.T.
22

ANGLE FROM HORIZONTAL (θ) 90° DIRECTION —
COORDINATES 198071E 609545N R.L. OF COLLAR 574m

SHEET 2 OF 2

Drill type <u>Meyhew</u>	<u>Weathering</u>	<u>Water</u>	Core Photograph Negative No
Feed <u>Hydraulic</u>	Fr — Fresh	10 Oct. '73 water level date shown	Depth (m) Black & White Colour
Core barrel type <u>Treifu 2 1/2</u>	SW — Slightly weathered	Water inflow	
triple tube — split inner	MW — Moderately weathered	Partial drilling water loss	
Driller <u>T. Shanahan (BHR)</u>	HW — Highly weathered	Complete drilling water loss	
Commenced <u>11-4-75</u>	EW — Extremely weathered		
Completed <u>17-4-75</u>	Notes:		
Logged by <u>P. Lang</u>	Bedding & Joint Planes — Angles are measured relative to a plane normal to the core axis.		
Vertical scale <u>1cm = 1m</u>	* Water Pressure Tests — Values in lugeons should be read in conjunction with computation sheets. Test sections are indicated by blacked in strips.		
			<u>155/116/1484-2082</u>

GEOLOGICAL LOG OF DRILL HOLE

Drilling Information				Rock Substance		Rock Mass Defects																	
Method	Casing	Water	Pressure test * (lugeons)	Lift & % core recovery	Depth (metres)	Graphic log	Substance description rock type: grain characteristics colour, structure, minor components.	Weathering	Strength Is (50) (MPa)	Defect spacing (cm)	Defect description thickness, type, inclination, planarity, roughness, coating, strength Particular General	Rock condition No.											
TREIFUS 2 1/2" Tripple tube core barrel with split inner tube & bottom discharge diamond bit	Rock Rolled		NOT TESTED	Not Cored	1	NOT CORED	GRANITE PORPHYRY (with xenoliths) yellow brown when weathered Weak soft. Weak to mod. weak. Mod. hard.	EW	0.03 0.05 0.07 0.10 0.20 0.30 0.50 1.00 2.00 3.00	NOT CORED	NOT CORED	5											
					2																		
					3								+	+	+	+	+	+	+	+	+	+	+
					4								95	+	+	+	+	+	+	+	+	+	+
					5								98	+	+	+	+	+	+	+	+	+	+
					6								90	+	+	+	+	+	+	+	+	+	+
					7								+	+	+	+	+	+	+	+	+	+	+
					8								100	+	+	+	+	+	+	+	+	+	+
					9								+	+	+	+	+	+	+	+	+	+	+
					10								+	+	+	+	+	+	+	+	+	+	+
					11								100	+	+	+	+	+	+	+	+	+	+
					12								+	+	+	+	+	+	+	+	+	+	+
					13								+	+	+	+	+	+	+	+	+	+	+
					14								100	+	+	+	+	+	+	+	+	+	+
					15								+	+	+	+	+	+	+	+	+	+	+
					16								+	+	+	+	+	+	+	+	+	+	+
					17								100	+	+	+	+	+	+	+	+	+	+
					18								+	+	+	+	+	+	+	+	+	+	+
					19								95	+	+	+	+	+	+	+	+	+	+
					20								+	+	+	+	+	+	+	+	+	+	+

13/8

Rock mass is weak. 3 joint sets: J₁ 90°, J₂ 0-30° spaced 10-60 cms. J₃ 45° spaced 2m on core. Joint surfaces generally coated with clay & limonite. Some joints below 15m are cemented with powdery calcite (weak, soft). Most joint surfaces wavy & irregular to rough

Drill type MEYHEW
Feed Hydraulic
Core barrel type Treifus 2 1/2"
triple tube & split inner tube
Driller Shannahan (B.M.R.)
Commenced 9/5/75
Completed 9/6/75
Logged by P. Lang
Vertical scale 1cm = 1m

Weathering

Fr — Fresh
SW — Slightly weathered
MW — Moderately weathered
HW — Highly weathered
EW — Extremely weathered

Notes:

Bedding & Joint Planes — Angles are measured relative to a plane normal to the core axis.
* Water Pressure Tests — Values in lugeons should be read in conjunction with computation sheets. Test sections are indicated by blocked in strips.

Water

10 Oct. '73 water level data shown
Water inflow
Partial drilling water loss
Complete drilling water loss

Core Photograph Negative No.

Depth (m) Black & White Colour

155/116/1485 70F4

GEOLOGICAL LOG OF DRILL HOLE

ANGLE FROM HORIZONTAL (°) 90°

DIRECTION ---

COORDINATES 198,296 E 610,074 N

R.L. OF COLLAR 585m

Drilling Information			Rock Substance		Rock Mass Defects							
Method	Casing	Water	Pressure test * (lugeons)	Lift & % core recovery	Depth (metres)	Graphic log & core loss	Substance description rock type: grain characteristics colour, structure, minor components.	Weathering	Strength Is (50) (MPa)	Defect spacing (cm)	Defect description thickness, type, inclination, planarity, roughness, coating, strength. Particular General	Rock condition No.
TREIFUS 2 1/2" Tripple tube core barrel with split inner tube, & bottom discharge diamond bit.			NOT TESTED	60	21	+	GRANITE PORPHYRY (many xenoliths up to 10cms) Pale greenish grey. Very hard, very strong	mostly HW	03	00	<p>Rockmass is weak. Core is fragmented due to a vertical joint which runs full length of this zone. Many EW seams and EW joint fillings. Clay on joints.</p> <p>Rockmass is tight & strong. Joints with little calcite. Rock MW near joints, FR-MW between joints. Joints all at 0-30°, irregular.</p> <p>core fractured</p> <p>1cm calcite & clay seam. 10 cm. of joints at 30° spaced 1-3cm.</p> <p>10 cm healed shear horizontal</p> <p>10 cm healed shear horizontal</p> <p>10 cm shear 2 Ca + chl. slickensided</p> <p>10 cm crushed seam 2 chl. & Ca on its + limonite staining.</p> <p>20cms of close jointed rock 2 chl. & Ca slickensides. Jts. at 30°</p> <p>Rockmass is very strong and very tight. R.Q.D. generally 95-100. Joints very tight. Joints cemented with calcite (strong). Some limonite staining. Surfaces rough & irregular.</p> <p>Joints generally cemented with calcite & chlorite and strongly slickensided. Surfaces rough. Some sheared zones healed with chlorite, spaced 30 cm. to 2m.</p>	5
				100	22	+		some EW seams	00	00		
				100	23	+			00	00		
				85	24	+			00	00		
				93	25	+		SW	00	00		
				100	26	+			00	00		
				100	27	+			00	00		
				100	28	+			00	00		
				100	29	+			00	00		
				100	30	+			00	00		
				100	31	+		FS	00	00		
				100	32	+			00	00		
				100	33	+			00	00		
				100	34	+			00	00		
				100	35	+			00	00		
				100	36	+			00	00		
				100	37	+			00	00		
				100	38	+		FR	00	00		
				100	39	+			00	00		
				100	40	+			00	00		

Drill type MEYHEW

Feed Hydraulic

Core barrel type Treifus 2 1/2"

tripple tube & split inner tube

Driller Shannahan (B.M.R.)

Commenced 9/5/75

Completed 9/6/75

Logged by P. Lang

Vertical scale 1cm = 1m

Weathering

Fr - Fresh

SW - Slightly weathered

MW - Moderately weathered

HW - Highly weathered

EW - Extremely weathered

Notes:

Bedding & Joint Planes - Angles are measured relative to a plane normal to the core axis.

* Water Pressure Tests - Values in lugeons should be read in conjunction with computation sheets. Test sections are indicated by blacked in strips.

Water

10 Oct. '73 water level date shown

Water inflow

Partial drilling water loss

Complete drilling water loss

Core Photograph Negative No.

Depth (m) Black & White Colour

155/A16/1485 2074

GEOLOGICAL LOG OF DRILL HOLE

Drilling Information				Rock Substance		Rock Mass Defects							
Method	Casing	Water	Pressure test * (lugeons)	Lift & % core recovery	Depth (metres)	Graphic log & core loss	Substance description rock type: grain characteristics colour, structure, minor components.	Weathering	Strength Is (50) (MPa)	Defect spacing (cm)	Defect description thickness, type, Inclination, planarity, roughness, coating, strength. Particular General	Rock condition No.	
TREIFUS 2½" Triple tube core barrel with split inner tube + bottom discharge diamond bit.				100	41	+	GRANITE PORPHYRY (many xenoliths) Pale grey Very hard. Very strong	FR	0.3	0.3	<p>Several jts at 60° + incipient fractures healed with calcite</p> <p>Rock sheared at 60°-80° but healed ± chlorite Mod. strong</p> <p>2 Vertical jts at rt. angles Very wavy + irregular + rough but tight. Weakly cemented with calcite + powdery calcite clay. Also some joints slickensided with chlorite</p> <p>Rockmass strong. Joints very tight. Cemented with calcite. Some chlorite. All fractures are at 0-30° (Probably drill induced)</p>	1-2	
				100	42	+			0.1-1.3	0.1-1.3			
					43	+				0.003-1.00			0.003-1.00
					44	+				0.000-1.00			0.000-1.00
				100	45	+							
					46	+							
				100	47	+							
					48	+							
					49	+							
					50	+							
				100	51	+							
					52	+							
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				100	54	+							
					55	+							
					56	+							
					57	+							
					58	+							
				100	59	+							
					60	+							

Drill type MEYHEW
Feed Hydraulic
Core barrel type Treifus 2½"
tripple tube & split inner tube
Driller Shanahan (B.M.R.)
Commenced 9/5/75
Completed 9/6/75
Logged by P. Lang
Vertical scale 1cm = 1m

Weathering

Fr - Fresh
SW - Slightly weathered
MW - Moderately weathered
HW - Highly weathered
EW - Extremely weathered

Notes:

Bedding & Joint Planes - Angles are measured relative to a plane normal to the core axis.
* Water Pressure Tests - Values in lugeons should be read in conjunction with computation sheets. Test sections are indicated by blacked in strips.

Water

10 Oct. '73 water level date shown
Water inflow
Partial drilling water loss
Complete drilling water loss

Core Photograph Negative No.

Depth (m) Black & White Colour

155/116/1485 3 of 4

UBS BURE
HOLE NO. . .
GST 23
Canberra 137
SHEET 4 OF 4

ANGLE FROM HORIZONTAL (θ) 90° DIRECTION $-$
COORDINATES $198,296E$ $610,074N$ R.L. OF COLLAR $585m$

NOT TESTED

GRANITE PORPHYRY

Pale grey.
Very hard. Very strong.

FR

Rockmass very strong.
Joints very tight. Mostly
cemented with calcite
(strong). All fractures
are at 0-30° (probably
drill induced)

Rockmass is strong + tight. 2 vertical joint sets at approx. 60° to each other. One is smooth and planar and spaced 3 cms. One is wavy and irregular spaced > 3 cms. Also one 45-60° joint set spaced > 1 m. Surfaces are weakly cemented with powdery calcite and calcite clay

Rockmass is very strong. Joints very tight. Slickensided with chlorite. All fractures are at $0-30^\circ$ (probably drill induced).

2

(2) - 3

2

TUNNEL

Weathering
Fr — Fresh
SW — Slightly weathered
MW — Moderately weathered
HW — Highly weathered
EW — Extremely weathered

Notes:

Bedding & Joint Planes — Angles are measured relative to a plane normal to the core axis.

* Water Pressure Tests — Values in lugeons should be read in conjunction with computation sheets. Test sections are indicated by blacked in strips.

Water

10 Oct. '73 water level date shown

Water inflow

Partial drilling water loss

Complete drilling water loss

Core Photograph Negative No.

Depth (m)	Black & White	Colour
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1551A1671485-40f4

GEOLOGICAL LOG OF DRILL HOLE

ANGLE FROM HORIZONTAL (°) 90°
COORDINATES 198021E 609440N

DIRECTION

R.L. OF COLLAR 575.7 m

Drilling Information				Rock Substance		Rock Mass Defects						
Method	Casing	Water	Pressure test * (lugesons)	Lift & % core recovery	Depth (metres)	Graphic log & core loss	Substance description rock type: grain characteristics colour, structure, minor components.	Weathering	Strength Is (50) (MPa)	Defect spacing (cm)	Defect description thickness, type, inclination, planarity, roughness, coating, strength. Particular General	Rock condition No.
TREFIUS 2 1/2" TRIPLE TUBE core barrel with split inner tube and Drill tek TUNGSTEN BIT.	Rock Rotted		NOT TESTED	Not Cored	1	Not Cored	NOT CORED				NOT CORED	5
					2	Cored						
					3	loss						
					4	70% +						
					5	50% loss +						
					6	65% loss +						
					7	50% core loss +						
					8	90% loss +						
					9	98% +						
					10	+						
					11	+						
					12	100% +						
					13	+						
					14	100% +						
					15	90% +						
					16	loss +						
					17	100% +						
					18	+						
					19	100% +						
						+						
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Drill type MAYHEW
Feed Hydraulic
Core barrel type TREFUS 2 1/2" with triple tube & split inner
Driller J. Shanahan (BMR)
Commenced 17-4-75
Completed 2-5-75
Logged by P. Lang
Vertical scale 1cm = 1m

Weathering
Fr - Fresh
SW - Slightly weathered
MW - Moderately weathered
HW - Highly weathered
EW - Extremely weathered

Notes:

Bedding & Joint Planes - Angles are measured relative to a plane normal to the core axis.
* Water Pressure Tests - Values in lugesons should be read in conjunction with computation sheets. Test sections are indicated by blacked in strips.

Water

10 Oct. 73 water level date shown
Water inflow
Partial drilling water loss
Complete drilling water loss

Core Photograph Negative No.

Depth (m) Black & White Colour

155/A6/1492 10/3

GEOLOGICAL LOG OF DRILL HOLE

ANGLE FROM HORIZONTAL (°) 90°

DIRECTION

COORDINATES 198021E 609440N

R.L. OF COLLAR 525.7m

Drilling Information				Rock Substance		Rock Mass Defects				Rock condition No.	
Method	Casing	Water	Pressure test # (lugeons)	Lift & % core recovery	Depth (metres)	Substance description rock type: grain characteristics colour, structure, minor components.	Weathering	Strength is (50) (MPa)	Defect spacing (cm)		Defect description thickness, type, inclination, planarity, roughness, coating, strength. Particular General
DRILL TEK TUNGSTEN BIT		17/4/75		90%	21	GRANITE PORPHYRY Weak, moderately hard Yellow brown.	HW to MW	0.3-0.5 0.00-0.10 0.00-0.10	0.00-0.10 0.00-0.10 0.00-0.10	Joints at 30°, 45°, 60°, 80° and 90°. Clay on joint surfaces.	5
				90%	22					Joints at 80° and 30°	
DIAMOND BIT.				100%	23	GRANITE PORPHYRY Hard and strong. Green gray with some very thin calcite veins, and some xenoliths up to 20cm thick.	SW to FS			Planar joints with limonite coating 80° Joints with up to 5mm of clay at 30°	4
				100%	24					Joints at 30° and 90° with up to 5mm of clay. Crushed seam with clay. 80° joint planar and smooth with clay. Joints at 30° and 80° with limonite.	
				100%	25						
				100%	26						
				100%	27						
				100%	28						
				100%	29						
				100%	30						
				100%	31						
				100%	32						
				100%	33						
				90%	34						
				100%	35						
				100%	36						
				100%	37						
				100%	38						
				100%	39						
100%											
TREIFUS 2 1/2" TRIPLE TUBE core barrel with split inner-tube											

Drill type MAYHEW
Feed Hydraulic
Core barrel type TREIFUS 2 1/2
with triple tube & split inner
Driller I. Shanahan (BMB)
Commenced 17.4.75
Completed 8.5.75
Logged by P. Lang
Vertical scale 1:100

Weathering

Fr - Fresh
SW - Slightly weathered
MW - Moderately weathered
HW - Highly weathered
EW - Extremely weathered

Notes:

Bedding & Joint Planes - Angles are measured relative to a plane normal to the core axis.
* Water Pressure Tests - Values in lugeons should be read in conjunction with computation sheets. Test sections are indicated by blacked in strips.

Water

10 Oct. '73 water level date shown
Water inflow
Partial drilling water loss
Complete drilling water loss

Core Photograph Negative No.

Depth (m) Black & White Colour

155/A16/1492 20P3

GEOLOGICAL LOG OF DRILL HOLE

ANGLE FROM HORIZONTAL (B) 90°
COORDINATES 198021E 609440NDIRECTION —
R.L. OF COLLAR 525.7mCANLERRA 138
SHEET 2 OF 2

Drilling Information				Rock Substance		Rock Mass Defects						
Method	Casing	Water	Pressure test * (lugeons)	Lift & % core recovery	Depth (metres)	Graphic log & core loss	Substance description rock type: grain characteristics colour, structure, minor components.	Weathering	Strength Is (50) (MPa)	Defect spacing (cm)	Defect description thickness, type, inclination, planarity, roughness, coating, strength. Particular General	Rock condition No.
TREIFUS 1 1/2" TUBE CORE BARREL WITH 3/8" DIAMOND BIT.				98%	41	+	GRANITE PORPHYRY Green grey to pink. Very hard, very strong.	FR	0.03 0.1 0.3 0.5 1.0 2.0 5.0 10.0 20.0 30.0 50.0 100 300		Vertical joints spaced 1cm. Slickensided with chlorite.	Rock mass moderately strong and tight. Joints generally wavy and irregular (cement veins) - some joints at 0-35° (wavy and irregular), some joints at 60-80° (smooth).
				95%	42	+					Chlorite and clay seams. Core fragmented.	
					43	+					60°-40° Joints	
				100%	44	+						
					45	+						
				100%	46	+					Epidote & chlorite on 80° joints (fractured)	
					47	+						
				100%	48	+					Chlorite coated joints and rock fragments. Fragments 1-10mm thick but long & platy.	
					49	+						
				100%	50	+					Wavy, rough vertical joints, in places cemented with calcite and chlorite & intact runs full length of core.	
				100%	51	+					Core fragmented. Joints at 90° & 0°. Probably due to shaking rig.	
				100%	52	+					Core in lengths up to 60cm but many incipient fractures mostly at 90° cemented with chlorite and calcite.	
				100%	53	+						
				100%	54	+					Most joints at 45-60° and 90°. Core partly fractured by rig.	
					55	+						
				100%	56	+					Vertical joints wavy and rough	
				100%	57	+					Vertical joints wavy but smooth.	
				100%	58	+					Vertical joints rough and irregular.	
				100%	59	+						

END OF HOLE 60.0m.

Drill type MAYHEW
Feed Hydraulic
Core barrel type TREIFUS 2 1/2"
Triple tube & split inner.
Driller J. Shanahan (BMR)
Commenced 17.4.75
Completed 8.5.75
Logged by R. Lang
Vertical scale 1cm = 1m

Weathering
Fr — Fresh
SW — Slightly weathered
MW — Moderately weathered
HW — Highly weathered
EW — Extremely weathered

Notes:
Bedding & Joint Planes — Angles are measured relative to a plane normal to the core axis.
* Water Pressure Tests — Values in lugeons should be read in conjunction with computation sheets. Test sections are indicated by blacked in strips.

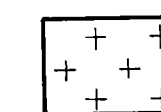
Water
10 Oct. '73 water level date shown
Water inflow
Partial drilling water loss
Complete drilling water loss

Core Photograph Negative No.
Depth (m) Black & White Colour
155/A16/1492 3 of 3

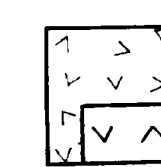
GINNINDERRA SEWER TUNNEL Interpretative Solid Geology

STRATIGRAPHIC SEQUENCE

ROCK NAME



Granite porphyry

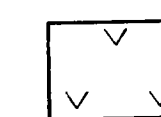


Light grey dacitic densely welded pyroclastic flows.

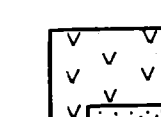


Dark grey member at base.

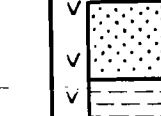
unconformity



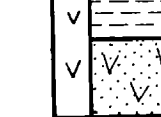
Dacitic densely welded tuffs & pyroclastic flows. Bedding in places.



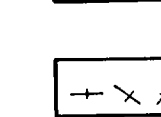
Dacitic welded tuffs, agglomerates, pyroclastic flows, sills & dykes.



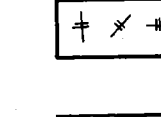
Quartz sandstone marker bed



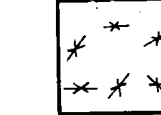
Shale. Thin beds interbedded with pyroclastics.



Sandstone. Thin beds interbedded with shales & pyroclastics.



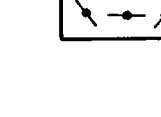
Green rhyolite



Purple rhyodacite



Purple rhyodacite



Pink rhyolite

UNIT NAME

Ginninderra Porphyry¹

Willow Bridge Tuff²

Walker Volcanics³

AGE

Ludlovian

Wenlockian

- 1 Registered
- 2 Named by Link 1971, replaces Laidlaw Volcanics
- 3 Refer 1:100000 Geological Sheet, BRINDABELLA, MDwen et al, 1975, Preliminary Edition.
- 4 Regarded as intrusive equivalent of Mount Painter Porphyry, with associated extrusive rocks.

REFERENCE

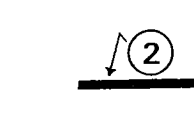


Tunnel line with tunnel station in metres



Shaft

FAULTS



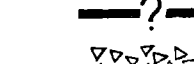
Fault number referred to in text



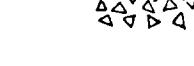
Position accurate (upthrown & downthrown sides indicated)



Position approximate



Fault inferred



Fault breccia

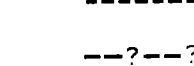
GEOLOGICAL BOUNDARIES



Position accurate



Position approximate



Boundary inferred

BEDDING

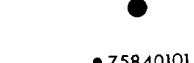


Dip and strike of bedding

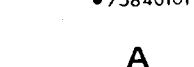
DRILL HOLES



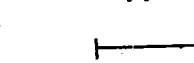
Diamond-drill hole



Specimen locality and registered number



Locality referred to in text



Seismic cross traverse

SCALE 500 0 500 1000m.

Grid coordinates in metres
Contours in feet above Mean Sea Level

Symbol	Description	Symbol	Description	Symbol	Description
—	Road, sealed	—	Coastal cable	—	Iron: tail
—	Road, not sealed	—	Telephone or telegraph line	—	Edge of dam
—	Vehicle track with grid	—	Power transmission line	—	Cutting: embankment
—	Railway line	—	Contours with contour value	—	Scour: rock outcrop
—	Bridge culvert	—	Triangulation station bench mark	—	Scour: rock outcrop
—	Property boundary, fenced	—	Spot elevation	—	Scour: rock outcrop
—	Property boundary, unfenced	—	Watercourse, intermittent	—	Scour: rock outcrop
—	Fence with gate	—	River or stream, perennial	—	Scour: rock outcrop

AMENDMENTS	Author	Checked	Date	Checked	Date
A1	Amended by P.A. LANG	DCP	12/7/75	DCP	12/7/75
A2	Amended by P.A. LANG	DCP	12/7/75	DCP	12/7/75
A3	Amended by P.A. LANG	DCP	12/7/75	DCP	12/7/75
A4	Amended by P.A. LANG	DCP	12/7/75	DCP	12/7/75
A5	Amended by P.A. LANG	DCP	12/7/75	DCP	12/7/75
A6	Amended by P.A. LANG	DCP	12/7/75	DCP	12/7/75
A7	Amended by P.A. LANG	DCP	12/7/75	DCP	12/7/75
A8	Amended by P.A. LANG	DCP	12/7/75	DCP	12/7/75
A9	Amended by P.A. LANG	DCP	12/7/75	DCP	12/7/75
A10	Amended by P.A. LANG	DCP	12/7/75	DCP	12/7/75

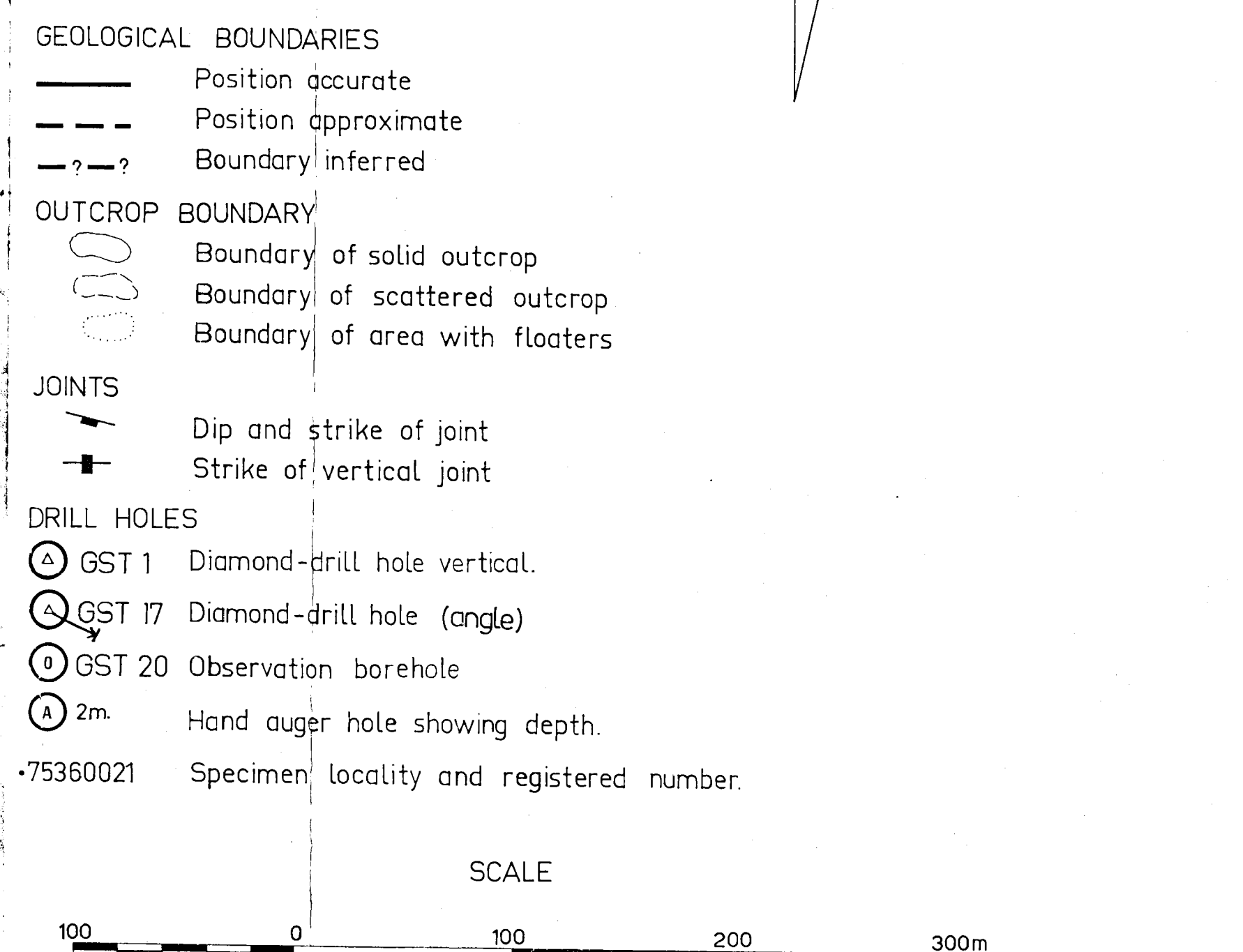


GINNINDERRA SEWER TUNNEL Surface Geology (STNS 00+79 to 8+00)

STRATIGRAPHIC SEQUENCE		ROCK NAME	UNIT NAME	AGE
	Granite porphyry		Ginninderra Porphyry ¹	Ludlovian
	Light grey dacitic densely welded pyroclastic flows		Willow Bridge Tuff ²	
	Dark grey member at base			
	Dacitic densely welded tuffs & pyroclastic flows. Bedding in places.		Walker Volcanics ³	Wentlockian
	Dacitic welded tuffs, agglomerates, pyroclastic flows sills & dykes.			
	Quartz sandstone marker bed.			
	Shale. Thin beds interbedded with pyroclastics.			
	Sandstone. Thin beds interbedded with shales & pyroclastics.			
	Green rhyolite			
	Purple rhyodacite			
	Purple tuffs, tuffaceous sandstones & shales.			
	Purple rhyodacite			
	Pink rhyolite			

- Registered
- Named by Link (1971) replaces Laidlaw Volcanics.
- Refer 1:100,000 Geological Sheet, BRINDABELLA, MÖwen et al, 1975, Preliminary Edition.
- Regarded as intrusive equivalents of Mount Painter Porphyry, with associated extrusive rocks.

- ## REFERENCE
- 54+00 Tunnel line with tunnel station in metres
- ## FAULTS
- Position accurate
 - Position approximate
 - Fault inferred
 - Sheared zone
 - Shear, vertical
 - Shear, showing dip
 - Fault breccia
 - Photo-lineament
- ## GEOLOGICAL BOUNDARIES
- Position accurate
 - Position approximate
 - Boundary inferred
- ## OUTCROP BOUNDARY
- Boundary of solid outcrop
 - Boundary of scattered outcrop
 - Boundary of area with floaters
- ## JOINTS
- Dip and strike of joint
 - Strike of vertical joint
- ## DRILL HOLES
- GST 1 Diamond-drill hole vertical.
 - GST 17 Diamond-drill hole (angle)
 - GST 20 Observation borehole
 - 2m Hand auger hole showing depth.
 - 75360021 Specimen locality and registered number.



REVISIONS		DATE	BY	REASON
1	Issue only	1980	PAL	ACT CONTOUR SERIES
2	Design by	1980	P A LANG	
3	Checked and checked	1980	PAL	
4	Project geologist	1980	EGW	
5	Supervising geologist	1980	TPK	

COMMONWEALTH OF AUSTRALIA BUREAU OF MINERAL RESOURCES CANBERRA, A.C.T.	TITLE DETAIL SURFACE GEOLOGY PROJECT GINNINDERRA SEWER TUNNEL STNS 00+79 to 8+00 Drawn by EGW Checked by PAL Scale 1:50,000 Drawing No. 155/AIS/1457
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GINNINDERRA SEWER TUNNEL Surface Geology (STNS 8+00 to 23+00)

STRATIGRAPHIC SEQUENCE

ROCK NAME	UNIT NAME	AGE
Granite porphyry	Ginninderra Porphyry ¹	
Light grey dacitic densely welded pyroclastic flows.	Willow Bridge Tuff ²	Ludlovian
Dark grey member at base		
unconformity		
Dacitic densely welded tuffs & pyroclastic flows. Bedding in places.		
Dacitic welded tuffs, agglomerates, & pyroclastic flows sills & dykes.		
Quartz sandstone marker bed.	Walker Volcanics ³	Wentlockian
Shale. Thin beds interbedded with pyroclastics.		
Sandstone. Thin beds interbedded with shales & pyroclastics.		
Green rhyolite		
Purple rhyodacite.		
Purple tuffs, tuffaceous sandstones & shales.		
Purple rhyodacite		
Pink rhyolite.		
1 Registered		
2 Named by Link (1971) replaces Laidlaw Volcanics.		
3 Regarded as intrusive equivalents of Mount Painter Porphyry with associated extrusive rocks.		
4 Refer 1:100000 Geological Sheet, BRINDABELLA, M.Owen et al, 1975, Preliminary Edition.		

REFERENCE

54+00 Tunnel line with tunnel station in metres

FAULTS

- Position accurate
- Position approximate
- Fault inferred
- Sheared zone
- Shear, vertical
- Shear, showing dip
- Fault breccia
- Photo-lineament

GEOLOGICAL BOUNDARIES

- Position accurate
- Position approximate
- Boundary inferred
- OUTCROP BOUNDARY
- Boundary of solid outcrop
- Boundary of scattered outcrop
- Boundary of area with floaters

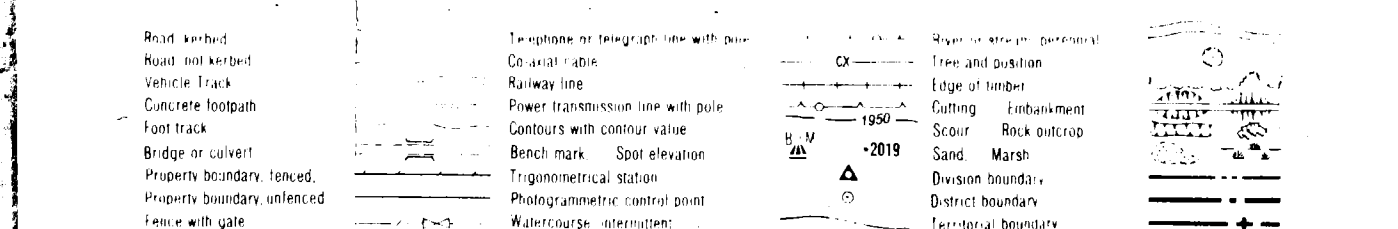
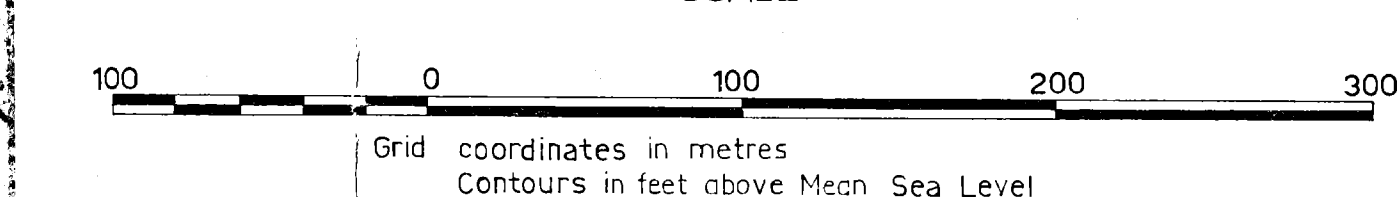
JOINTS

- Dip and strike of joint
- Strike of vertical joint

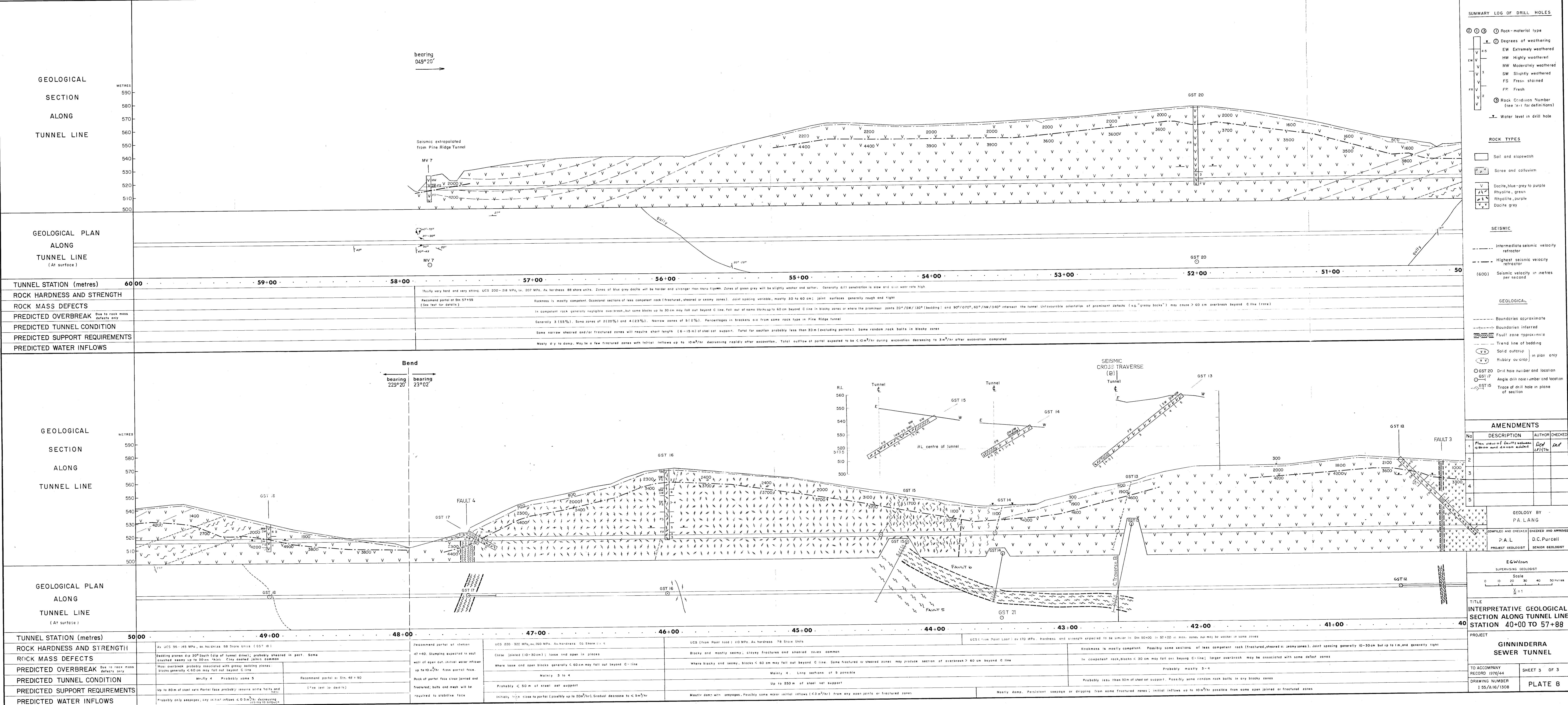
DRILL HOLES

- GST 1 Diamond-drill hole vertical.
- GST 17 Diamond-drill hole (angle)
- GST 20 Observation borehole
- 2m Hand auger hole showing depth.
- 75360021 Specimen locality and registered number.

SCALE



AMENDMENTS		SCALE		COMMONWEALTH OF AUSTRALIA BUREAU OF MINERAL RESOURCES CANBERRA, A.C.T.	
No.	Description	Author	Checked	Scale	Scale
1	GST 1 to 23+00	P.A. LANG	P.A. LANG	1:10000	1:10000
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REFERENCE

SUMMARY LOG OF DRILL HOLES

- ① ② ③ Rock - material type
- ④ Degrees of weathering
- EW Extremely weathered
- HW Highly weathered
- MW Moderately weathered
- SW Slightly weathered
- FS Fresh stained
- FR Fresh
- ⑤ Rock Condition Number (see text for definitions)
- Water level in drill hole

ROCK TYPES

- Soil and slopewash
- Scree and colluvium
- Dacite, blue-grey to purple
- Rhyolite, green
- Rhyolite, purple
- Dacite grey

SEISMIC

- Intermediate seismic velocity refractor
- Highest seismic velocity refractor
- (600) Seismic velocity in metres per second

GEOLOGICAL

- Boundaries approximate
- Boundaries inferred
- Fault zone approximate
- Trend line of bedding
- Solid outcrop
- Rubby outcrop
- in plan only
- GST 20 Drill hole number and location
- GST 17 Angle drill hole number and location
- Trace of drill hole in plane of section

AMENDMENTS

No	DESCRIPTION	AUTHOR	CHECKED
1	Plan view of fault between 4800 and 4900 added	D.P.	P.P.
2			
3			
4			
5			

GEOLOGY BY

P. A. LANG

COMPILED AND CHECKED

P. A. LANG

PROJECT GEOLOGIST

D. C. PURCELL

SENIOR GEOLOGIST

EG Wilson

SUPERVISING GEOLOGIST

Scale

0 10 20 30 40 50 metres

V = 1

TITLE

INTERPRETATIVE GEOLOGICAL

SECTION ALONG TUNNEL LINE

STATION 40+00 TO 57+88

PROJECT

GINNINDERRA

SEWER TUNNEL

TO ACCOMPANY

RECORD 1976/44

DRAWING NUMBER

155/A16/1308

SHEET 3 OF 3

PLATE 8