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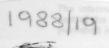
R.V.RIG SEISMIC RESEARCH CRUISE 3,

OFFSHORE, OTWAY BASIN:

EXPLANATORY NOTES TO ACCOMPANY RELEASE OF NON-SEISMIC DATA

by

C. Lawson & M. Hazell



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Bureau of Mineral Resources, Geology & Geophysics
DIVISION OF MARINE GEOSCIENCES & PETROLEUM GEOLOGY

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#### CONTENTS

INTRODUCTION	Page	1
GEOPHYSICAL SYSTEMS & PERFORMANCE	Page	1
DATA ACQUISITION SYSTEM (DAS)	Page	2
DATA PROCESSING	Page	5
DATA AVAILABILITY	Page	17
FIGURES		
FIGURE 1: Bathymetry traces before and after processing by program SALVG.	Page	13
FIGURE 2: Satellite fix assessment plot - prior to processing	Page	14
FIGURE 3: Satellite fix assessment plot - post processing	Page	15
FIGURE 4: Tracks of Rig Seismic Survey 48 in the Bass Strait	Page	16
TABLES		
TABLE 1: Field tape channel allocations.	Page	3
TABLE 2: Processing channel allocations.	Page	6
TABLE 3: Filter coefficients and approximate response of filter to sine wave for magnetics filter.	Page	8
TABLE 4: Sample satellite fix listing.	Page	10
TABLE 5: Final channel allocations.	Page	12

#### INTRODUCTION

The purpose of this report is to summarise the processing techniques applied to the non-seismic geophysical data on R.V.Rig Seismic Research Cruise 3 (BMR Marine Survey 48, Otway Basin of Bass Strait). The cruise was conducted between 15 June and 12 July 1985 and formed part of project 1D06 (1985/1986) and project 1CO3 (1986/1987) .

#### GEOPHYSICAL SYSTEMS & PERFORMANCE

The following non-seismic geophysical systems were employed during Survey 48:

#### Navigation

Three totally independent navigation techniques were run simultaneously;

- 1. Magnavox Global Positioning System (GPS) T-Set, giving continous 2-D positioning to within 35 m RMS, during periods of satellite availability and good geometry.
- 2. Motorolla Miniranger Radio Navigation System, utilizing four shore based transponders. This system has a potential accuracy to within 5 metres.
- 3. A dead reckoning (DR) system, incorporating satellite navigators, gyro compasses, and sonar dopplers. The primary system, consisted of a Magnavox MX1107RS dual-channel satellite navigator, with speed input from Magnavox MX610D sonar doppler and headings from an Arma-Brown gyro-compass. The secondary system, consisted of a Magnavox MX1142 single channel satellite navigator, with speed input from Raytheon DSN 450 sonar doppler and headings from a Robertson gyro-compass. This system has a potential accuracy of 0.2km at fixes rising to around 1km between fixes in deep water.

Performance Comments: Both satellite navigators generally performed reliably. The MX1107RS was interfaced to the Data Acquisition System (DAS) and latitude, longitude, course, speed (every 10 seconds) and all satellite fix details were transferred and recorded. The percentage of the total time that each system was the primary navigation system during the cruise is;

T-Set :27%

Radio Nav :12%

Dead Reckoning :61%

Both gyro-compasses performed satisfactorily for the entire survey. Both sonar dopplers performed fairly satisfactorily in low sea states but were generally erratic in high sea states.

#### Bathymetric Systems

Raytheon Deep-sea Bathymetric System, with a maximum power output of 2 kW at 12 kHz. This system, purchased in the early 1970's, was of very sophisticated design for its day, providing in addition to digital depths and various alarm flags, an automatic tracking facility that should theoretically provide usable bathymetric data even in marginal recording conditions.

A new 3.5 kHz system was installed in Melbourne prior to Survey 48. This new system included an additional 8 transducers bringing the total to 16.

Performance Comments: Data quality was generally poor due to the high sea states encountered on the survey. The extensive processing required to retrieve acceptable bathymetric data is described fully later in this report.

#### <u>Magnetics</u>

Two Geometrics G801/803 proton precession magnetometers were installed in the instrument room; signals were acquired from both single and dual channel (horizontal gradient) sensors towed astern of the vessel.

Performance Comments: Performance was not as good as expected due to excessive noise. Noise level for the magnetometer was in excess of plus/minus 3 nT.

#### **Gravity**

A Bodenseewerk KSS-31 marine gravity meter has been installed on the Rig Seismic. Gravity data were recorded for the entire survey.

Performance Comments: The KSS-31 is a highly sophisticated single-axis marine gravity meter with extensive microprocessor control. The KSS-31 is designed to be interfaced to an external navigation system that can provide speed and heading input at a rate of as fast as 1 second; the speed and heading are then used by the processor to provide gyro corrections to the gravity meter to improve performance in heavy seas or during turns. For Survey 48, satisfactory gravity data have been achieved with appropriate post-survey filtering, except at sample sites where poor speed control and continuous vessel manoeuvring have produced erratic Eotvos corrections.

Due to system malfunction no data were acquired between 48,181,213200 and 48,183,055000.

## DATA ACQUISITION SYSTEM (DAS)

The shipboard DAS is based on a Hewlett-Packard (HP) 1000 E-Series 16-bit minicomputer. The DAS programs run under the HP Real Time Executive (RTE-6/VM) disc-based operating system, which allows a multiprogramming environment and a large number of interactive users. Data are acquired either directly from the appropriate device through an RS-232C interface (gravity, Magnavox MX1107RS), or through a BMR-designed 16-bit digital multiplexer (magnetics, bathymetry) and attached gyro-log interface (for both sonar dopplers and gyro-compasses). After preliminary processing, plotting on strip-chart recorders, and listing on a variety of printers, the data were recorded on 9-track, 1600 bpi, phase-encoded magnetic tape in HP's 32-bit floating-point format.

Data were acquired and saved at a 10-second rate, regardless of ship speed and independently of the seismic acquisition system. The data were written to tape in 2.0 minute (12 record) blocks with 80 channels of data being recorded. The channels that were recorded are listed in Table 1.

#### TABLE 1: Field tape channel allocations

- 1 Clock (survey & day number)
- 2 GMT acquisition time from computer clock (hours ,minutes and seconds)
- 3 Master clock time at acquisition (hours, minutes and seconds)
- 4 Latitude (radians)
- 5 Longitude (radians)
- 6 Speed (knots) best estimate
- 7 Heading (degrees) best estimate
- 8 Magnetometer No 1 (nT)
- 9 Magnetometer No 2 (nT)
- 10 Bathymetry No 1 (metres)
- 11 Bathymetry No 2 (metres)
- 12 Magnavox sonar doppler fore/aft
- 13 Magnavox sonar doppler port/starboard
- 14 Raytheon sonar doppler fore/aft
- 15 Raytheon sonar doppler port/starboard
- 16 Not used
- 17 Not used
- 18 Arma-Brown gyro-compass (degrees)
- 19 Robertson gyro-compass (degrees)
- 20 Not used
- 21 Miniranger 1
- 22 Miniranger 2
- 23 Miniranger 3
- 24 Miniranger 4
- 25 Not used
- 26 Not used
- 27 Not used
- 28 Not used
- 29 Not used
- 30 Not used
- 31 Not used
- 32 T-Set Time (GMT seconds)\*2
- 33 T-Set (DOP)
- 34 T-Set Latitude (Radians)
- 35 T-Set Longitude (Radians)
- 36 T-Set (Height above Geoid)
- 37 T-Set Speed (knots) \* 10
- 38 T-Set Course (degrees) \* 10
- 39 T-Set frequency bias No 1
  40 T-Set GMT (.hhmmss)
- 41 Not used
- 42 Not used
- 43 Not used
- 44 Not used
- 45 Not used
- 46 Not used
- 47 Not used
- 48 Not used
- 49 Not used
- 50 GMT time from MX1107RS satnav
- 51 Dead-reckoning time from MX1107RS
- 52 Latitude (radians) from MX1107RS
- 53 Longitude (radians) from MX1107RS
- 54 Speed (knots) from MX1107RS
- 55 Heading (degrees) from MX1107RS
- 56 Set (degrees) from MX1107RS
- 57 Drift (knots) from MX1107RS
- 58 Set/drift flag, 0 = No 1, 1 = auto
- 59 GMT from MX1142RS satnav

- 60 Dead-reckoning time from MX1142RS
- 61 Latitude (radians) from MX1142RS
- 62 Longitude (radians) from MX1142RS
- 63 Speed (knots) from MX1142RS
- 64 Heading (degrees) from MX1142RS
- 65 Set (degrees) from MX1142RS
- 66 Drift (knots) from MX1142RS
- 67 Set/drift flag from MX1142, 0 = manual,
  - 1 = automatic
- 68 Vector speed Magnavox sonar doppler
- 69 Vector speed Raytheon sonar doppler
- 70 Not used
- 71 Not used
- 72 Not used
- 73 Not used
- 74 Gravity (ums\*\*-2 \* 1000)
- 75 ACX (ms\*\*2 \* 1000)
- 76 ACY (ms\*\*2 \* 1000)
- 77 Sea State
- 78 Not used
- 79 Not used
- 80 Not used

#### DATA PROCESSING

The data were processed on an in-house Hewlett-Packard 1000 F-Series minicomputer utilising similar hardware and the same operating system as the DAS. The processing was applied in two phases, as follows:

<u>Phase 1:</u> transcription of field tapes; correction of time errors; production of raw data plots; bulk editing (principally deletion of bad data segments); retrieval of water depth data; assessment and retrieval of velocities; medium filter of magnetics and gravity; manual editing of problem areas; computation of incremental latitudes and longitudes; anti-alias filtering (smoothing) of magnetics, gravity, incremental latitudes and longitudes; production of final check plots; final editing.

<u>Phase 2:</u> tying of the dead-reckoned (DR) track to the satellite fixes using a cubic spline fitting technique to model ocean currents; assessment and deletion of poor quality satellite fixes; computation of final positions for each DR system; computation of final ship position from an appropriate mix of the available DR systems, GPS system and radio nav system; computation of final Eotvos-corrected gravity, including a correction for gravity meter drift; final data editing (particularly gravity data during turns).

A brief summary of the processing steps follows, with some detail of the techniques applied.

#### PHASE 1

FCOPY: All field tapes were transcribed to processing tapes with several field tapes being combined into a single processing tape. Processing tapes were separated at obvious breaks (such as recording system crashes), or after about seven days recording. Time jumps (positive or negative) were reported for processing in the next phase.

FIXTM: Time jumps reported in FCOPY were corrected, either automatically, or with a file of manual time corrections. Data channels were re-ordered (Table 2) to simplify further processing.

SALVG (Water depth recovery): Briefly stated, the problem of bathymetry recovery is to fill in all the gaps left after the Raytheon hardware/software flags were removed and to discriminate against the bad bathymetric values that still remain. To accomplish this, a file was first created of manually digitised water depths at selected points; this file was then read in conjunction with the processing data file. SALVG then performs a straight line interpolation between adjacent tie points and compares the interpolated depth with the 10-second digital depth. If the difference is less than a user-specified threshold, then the digital depth is accepted and is used to replace the previous first tie point. If the difference is greater than the threshhold, then the 10-second digital depth is replaced by the interpolated depth. In this way, the program tracks along the acceptable water depths, providing the threshold is small enough to reject bad data and large to accept good data. In the case of good digital data being totally unacceptable, as during poor sea conditions, the threshold was set to a very small number (0.01m) and the process became one of very simple linear interpolation between adjacent tie points.

### TABLE 2: Processing channel allocations

```
Clock (survey & day number)
 2
       GMT acquisition time from computer clock (hours
       ,minutes and seconds)
 3
       Master clock time at acquisition (hours,
       minutes and seconds)
 4
    - Latitude (radians)
 5
      Longitude (radians)
 6
   - Heading (degrees) - best estimate
 7
       Speed (knots) - best estimate
 8
       Bathymetry No 1 (metres)
 9
       Bathymetry No 2 (metres)
10
   - Magnetometer No 1 (nT)
11
      Magnetometer No 2 (nT)
12
       Magnetic gradient
       Gravity (ums**-2 * 1000)
13
14
       Pitch acceleration (m/s**2)
15
   - Roll acceleration (m/s**2)
16
   - Sea state filter number
17
   - Magnavox sonar doppler - fore/aft
18
   - Magnavox sonar doppler - port/starboard
19
   - Raytheon sonar doppler - fore/aft
   - Raytheon sonar doppler - port/starboard
20
21
       T Set Latitude
22
      T Set Longitude
23
      Arma-Brown gyro-compass (degrees)
24
      Robertson gyro-compass (degrees)
25
      Not used
26
   - Miniranger 1
27
   - Miniranger 2
28
   - Miniranger 3
29
      Miniranger 4
30
      Not used
31
      Not used
32
      Not used
33
   - Not used
34
   - Not used
35
   - Not used
37
   - 10-sec delta longitude - Magnavox S/D + Arma-Brown
38
      10\text{-sec} delta latitude - Magnavox S/D + Robertson
39
      10-sec delta longitude - Magnavox S/D + Robertson
40
      10-sec delta latitude - Raytheon S/D + Arma-Brown
   - 10-sec delta longitude - Raytheon S/D + Arma-Brown
41
42
   - 60-sec delta latitude - Magnavox S/D + Arma-Brown
43
   - 60-sec delta longitude - Magnavox S/D + Arma-brown
44
       60-sec delta latitude - Magnavox S/D + Robertson
      60-sec delta longitude - Magnavox S/D + Robertson
45
46
       60-sec delta latitude - Raytheon S/D + Arma-Brown
47
       60-sec delta longitude - Raytheon S/D + Arma-Brown
48-64
       -Not used
```

In practice the interval between manually digitised tie points varied from several hours in the case of good digital 10-second data, to several minutes in the case of poor 10-second data or a very rugged sea bed. The success of this process, which is routinely applied to all Rig Seismic bathymetric data, can be seen in the 'before' and 'after' plots of Figures 1 and 2.

VARPL: All raw data channels requiring processing were plotted as strip records on a drum plotter. These plots were used to determine where editing was required and as a first guide for the setting of filter parameters.

FTAPE: This program was used for a variety of tasks as follows - (1) Removal of hardware/software flags in the bathymetric data. The Raytheon echo-sounder system provides, in addition to digital bathymetry, 'flags' indicating that the echo-sounder has lost track or that the digitiser gate is searching for an echo. These flags were removed, as appropriate, and such values were replaced by the number 1.0E10 (10 raised to the power 10), to indicate absent data.

(2) 'Bulk' deletions were done of any large blocks of irretrievable data in particular channels. (3) Automatic interpolations were done across data gaps of up to 120 seconds for selected data channels.

FDATA: The magnetic, gravity, and Magnavox and Raytheon speed log data were filtered using a sophisticated form of the medium filter, a highly successful spike deletion tool.

EDATA: This is a utility program used for the manual editing of problem areas that are not amenable to filtering or automatic editing.

MUFF: This program uses a SINC function filter to smooth selected data channels. All velocity channels were smoothed to provide acceptable speeds, while gravity and magnetic data were filtered as an anti-aliasing measure prior to resampling to 60 s. The filter coefficients and the approximate responses of the filters to a sine wave are given in Table 3.

DELTA: Incremental (delta) latitude/longitudes were produced every 10 seconds by combining the ship speed with the headings from the Arma-Brown and Robertson gyro-compasses. This effectively gave two distinct dead-reckoning (DR) systems.

INTEG: The filtered incremental latitude/longitudes were re-integrated over running 60-second intervals. These 60-second incremental distances were then used in the Phase 2 processing to compute the DR vector over each satellite fix interval.

VARPL/EDATA: As the final stage of the Phase 1 processing, all processed channels were plotted again as 'strip' plots with program VARPL. Program EDATA was then used to correct any minor residual data problems.

```
SMOOTH FILTER 1 PUTS CHANNEL 11 INTO 11
FILTER CUT-OFF AT 3.RD ZERO
SAMPLING INTERVAL IN SECONDS 10.0
PERIOD OF FILTER IN SECONDS 180.0
```

## APPROXIMATE RESPONSE OF FILTER TO SINE WAVE

## NUMBER OF POINTS IN FILTER 53 FILTER COEFFICIENTS AS FOLLOWS

	FILTER COEFFICIE						
.000	.001 .002 .003	.004	.004	.004	.003	000	004
008	012015018	018	015	009	.000	.012	.027
.043	.060 .076 .091	.102	.109	.111	.109	.102	.091
.076	.060 .043 .027	.012	.000	009	015	018	018
015	012008004		.003	.004	.004	.004	.003
.002	.001 .000					••••	
	100.						
	FRACTION	PERIOD		RESP	ONSE	db	
	TRACTION	ILKIOD		KLUI	OHOL	GD.	
	.500	90.0		.00	108	-59.3	
	.518	93.2		.00		-47.1	
	.536	96.5		.00		-43.5	
	.555	99.9		.00		-43.5	
	.574	103.4		.00		-48.4	
	.595	107.0		00		-55.0	
	.616	110.8		00		-41.1	
	.637	114.7		01		-36.2	
	.660	118.8		01		-34.3	
	.683	122.9		01		-34.3	
				00			
	.707	127.3				-10.5	
	.732	131.8			793	-42.0	
	-758	136.4			500	-29.1	
	.785	141.2		.07		-22.9	
	-812	146.2			784	-18.6	
	-841	151.4			184	-15.3	
	.871	156.7		. 23		-12.7	
	.901	162.2			728	-10.5	
	.933	167.9			499 755	-8.8	
	.966	173.9			355	-7.3	
	1.000	180.0			127	-6.0	
	1.035	186.3		.56		-4.9	
	1.072	192.9			872	-4.0	
	1.110	199.7		.68		-3.3	
	1.149	206.8			918	-2.6	
	1.189	214.1			669	-2.1	
	1.231	221.6			882	-1.6	
	1.275	229.4			564	-1.3	
	1.320	237.5		.89		9	
	1.366	245.9		.92		7	
	1.414	254.6			676	5	
	1.464	263.5			527	3	
	1.516	272.8			024	2	
	1.569	282.5			210	1	
	1.625	292.4		1.00		.0	
	1.682	302.7		1.00		.1	
	1 741	313 A		1 01	スクク	1	

313.4

324.5 335.9 347.7

360.0

1.741

1.803

1.866 1.932

2.000

TABLE 3: Filter coefficients and approximate response of filter to sine wave for magnetics smoothing filter.

1.01322

1.01665 1.01881

1.01994

1.02028

#### PHASE 2

Phase 2 processing encompasses the following steps -

- 1. Re-formatting and production of assessment listings of satellite fixes;
- 2. Resampling Phase 1 data;
- 3. Assessment of satellite fixes and deletion of those considered dubious or unacceptable;
- 4. Constrainment of DR track to remaining satellite fixes and computation of 1-minute positions for each DR system;
- 5. Selection of a suitable mix of navigation systems to produce final positions;
- 6. Application of Eotvos and drift corrections to gravity data and conversion to absolute values;
- 7. Final plots and editing as necessary.

In rather more detail, the programs applied were as follows -

RESAF: Re-format the ASCII parameter file of satellite fixes and adjust each fix to the nearest whole minute of survey time using the ship speed and heading applying at that time in the Phase 1 data file.

FIXES: Produce a listing of the satellite fixes for assessment purposes (Table 4).

RESAM: Concatenate the Phase 1 data files, as appropriate, and resample to produce 1-minute data.

SAT12: Two passes of this program are required for each round of satellite fix assessment. During each pass, a number of options are called, as follows:

#### Pass 1

- a. SATEL reads in the file of satellite fixes and stores them in memory. Any fix intervals with dubious speeds (too low or too high) or any intervals that are very short (<15 minutes) or very long (>120 minutes) are flagged in the output listing.
- b. DRNAV uses the incremental latitude/longitudes stored on the Phase 1 file and the satellite fix information to compute the DR path (or DR vector) for each satellite fix interval. This is saved as an ASCII parameter file.
- c. CALNV reads the DR file created by DRNAV and computes the ratio of the average DR velocity to the velocity computed from successive satellite fixes. This is done for each DR system used, and the results are listed.
- d. CALPL produces a line printer plot of the velocity ratios for each satellite fix interval.

NAME OF INPUT PARAMETER FILE - SATO1
SECURITY CODE, CARTRIDGE (DEFAULT=888,36) - ,20

2 48.166.020000 38 31.087 144 24.684 1107 500 Y 10 25 4 NE .13 106 0 0 20.1 3.7 3.8 38.166.042300 38 36.465 144 18.578 1107 110 Y 14 24 4 NE .71 178 0 0 269.2 2.7 4 42.166.053700 38 37.134 144 14.094 1107 200 Y 34 28 2 NE .03 140 0 0 237.3 4.6 48.166.053200 38 37.134 144 14.793 1142 110 N 84 34 3 7.08 0 0 0 1 232.5 4.6 48.166.073700 38 38.154 144 14.793 1142 110 N 84 34 3 7.08 0 0 0 1 232.5 4.6 48.166.073700 38 38.42 144 15.003 1107 200 Y 29 26 3 NU .11 186 0 0 59.5 5.6 8 48.166.073700 38 38.442 144 15.003 1107 480 Y 10 2 26 2 .80 134 0 0 6 60.3 5.7 11 48.166.111800 38 31.288 144 37.880 1107 480 Y 27 32 3 SU .25 109 0 0 84.3 4.6 12 48.166.111800 38 38.36 144 27.447 1107 800 Y 15 27 5 5 8 48.25 144 27.447 1107 800 Y 15 27 5 8 48.25 144 27.447 1107 800 Y 15 27 5 8 8 1.8 113 10 0 0 84.3 4.6 12 48.166.111800 38 38.36 144 24.6510 1107 800 Y 27 32 3 SU .25 109 0 0 8 84.3 4.6 12 48.166.13300 38 43.867 144 15.160 1142 110 Y 14 27 2 1.50 289 0 0 1 239.3 5.7 14 48.166.13300 38 43.867 144 15.160 1142 110 Y 14 27 2 1.50 289 0 0 1 239.3 5.7 14 48.166.194000 38 43.867 144 15.160 1142 110 Y 14 27 2 1.50 289 0 0 1 239.3 5.7 14 48.166.194000 38 47.521 144 15.787 1107 200 Y 39 0 0 5 8 .8 12 29 0 0 240.0 4.5 15 48.166.194000 38 47.521 144 15.787 1107 200 Y 33 31 3 SE .08 97 0 0 1 162.4 2.6 12 2.	FIX	FIX TIME	LAT	FONG	SYSTEM	SAT	ĐΚ	ETEA	THUOJ	ITER	GEDH	ERROR	DIE	SLT	814	CODE	COURSE	SPEED
3	1	48.165.232000	38 24.710	144 28.072	1107	480	Y	35	32	3	иü	.03	317	0	0		22.4	2,1
4 48.166.053700 38 37.106 144 15.184 1107 500 Y 18 26 2 NW .09 225 0 0 0 261.3 3.2 5 48.166.053200 38 37.134 144 14.094 1107 200 Y 34 28 2 NE .03 140 0 0 237.3 4.6 6 48.166.061000 38 38.154 144 14.793 1142 110 N 84 34 3 .70 80 0 0 1 232.5 4.6 7 48.166.073700 38 39.442 144 15.023 1107 200 Y 29 26 3 NW .11 186 0 0 559.5 5.5 8 8 48.166.073700 38 38.949 144 17.791 1142 110 Y 12 26 2 .30 137 0 0 60.3 5.1 10 48.166.09400 38 34.55 144 27.447 1107 480 Y 50 36 3 5E .25 114 0 0 66.3 4.6 10 48.166.111800 38 31.268 144 37.850 1107 480 Y 50 36 3 5E .25 114 0 0 66.3 4.6 11 48.166.113200 38 30.461 144 37.850 1107 480 Y 27 32 3 5W .25 109 0 0 84.3 4.6 11 48.166.113200 38 38.36 144 26.510 1107 500 Y 15 27 5 5E .48 213 0 0 239.2 4.6 13 48.166.160100 38 43.867 144 16.477 1142 500 N 88 34 2 1.50 289 0 0 1 239.3 5.4 14 48.166.162300 38 48.4892 144 15.160 1142 110 Y 14 27 2 1.20 288 0 0 240.0 4.5 15 48.166.19400 38 44.892 144 15.160 1142 110 Y 14 27 2 1.20 288 0 0 240.0 4.5 15 48.166.19400 38 41.407 144 15.787 1107 200 Y 39 0 0 5E -9.1 0 0 0 5 22.5 5.5 11 48.166.19400 38 41.407 144 15.787 1107 30 Y 14 27 2 1.20 288 0 0 240.0 4.5 16 48.166.19400 38 41.407 144 15.787 1107 130 Y 14 27 2 1.20 288 0 0 0 20.0 4.5 16 48.166.19500 38 39.781 144 15.585 1107 107 10 Y 14 27 2 1.20 28 0 0 0 5 20.5 5.1 14 2.20 28 10 48.166.19400 38 41.407 144 15.787 1107 130 Y 14 25 3 5 5 0.9 146 0 0 5 24.5 5 2.5 5 2.5 4 2.0 48.166.213000 38 35.643 144 22.8555 1142 130 N 85 27 3 5 5 0.9 146 0 0 5 24.5 5 2.5 14 2.20 28 12 2.20 28 12 2.20 28 12 2.20 28 12 2.20 28 2.20 2	2	48.166.020000	38 31.087	144 24.684	1107	500	Υ	10	25	4	NE	.13	106	0	0		210.1	3.7
5 48.166.055200 38 37.134 144 14.094 1107 200 Y 34 28 2 NE .03 140 0 0 1 237.3 4.6 48.166.061000 38 38.154 144 14.793 1142 110 N 84 34 3 7.0 80 0 0 1 237.5 4.6 48.166.075000 38 38.442 144 15.023 1107 200 Y 29 26 3 NU .11 186 0 0 59.5 5.5 5.6 8 48.166.075000 38 38.442 144 15.023 1107 480 Y 10 26 2 .30 137 0 0 60.3 5.7 9 48.166.075000 38 31.268 144 37.273 1142 110 Y 10 26 2 .80 134 0 0 66.3 4.8 11 48.166.113200 38 31.268 144 37.273 1142 130 Y 11 26 2 .80 134 0 0 66.3 4.8 11 48.166.113200 38 31.268 144 37.273 1142 130 Y 11 26 2 .80 134 0 0 66.3 4.8 11 48.166.113200 38 38.316 144 26.510 1107 500 Y 15 27 5 5E .48 213 0 0 238.2 4.5 11 48.166.162300 38 44.882 144 15.160 1107 500 Y 15 27 5 5E .48 213 0 0 238.2 4.5 11 48.166.162300 38 44.882 144 15.160 1142 110 Y 14 27 2 1.20 298 0 0 1 239.3 5.7 11 48.166.192600 38 44.882 144 15.160 1142 110 Y 14 27 2 1.20 298 0 0 1 200.0 4.5 11 48.166.192600 38 44.892 144 15.160 1142 110 Y 14 27 2 1.20 298 0 0 1 200.0 4.5 11 48.166.192600 38 44.407 144 15.787 1107 480 Y 29 34 3 SE .58 217 0 0 20 208.0 1.5 11 48.166.192600 38 38.7521 144 13.949 1107 110 Y 12 18 3 SE .58 217 0 0 20 208.0 1.5 11 41 48.166.192600 38 38.7521 144 13.749 1107 107 107 107 107 107 107 107 107 10	3	48.166.042300	38 36.475	144 18.578	1107	110	Y	14	24	Ą	NF	.17	178	0	Ģ		269.2	2.2
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7	5	48.166.055200	38 37.134	144 14.054	1107	200	Y	34	28	2	NE	.03	140	0	0		237.3	4.0
8 48.166.075600 38 38.949 144 17.791 1142 110 Y 12 26 2 3.0 137 0 0 60.3 5.7 9 48.166.094400 38 34.455 144 27.447 1107 480 Y 50 36 3 EE .25 114 0 0 66.5 4.1 14 48.166.113200 38 30.461 144 37.850 1107 480 Y 27 32 3 SW .25 109 0 0 88.3 4.6 12 48.166.113200 38 38.316 144 26.510 1107 500 Y 15 27 5 SE .48 213 0 0 239.2 4.6 13 48.166.161000 38 43.867 144 16.477 1142 500 N 88 34 2 1.50 289 0 0 1 239.3 5.4 14 48.166.174000 38 44.892 144 15.160 1142 110 Y 14 27 2 11.20 298 0 0 1 239.3 5.4 14 48.166.174000 38 44.892 144 15.60 1142 110 Y 14 27 2 11.20 298 0 0 1 240.0 4.5 15 48.166.174000 38 46.183 144 11.609 1107 200 Y 33 31 3 SE .58 217 0 0 240.0 4.5 16 48.166.19400 38 47.521 144 13.949 1142 110 N 86 32 3 .80 97 0 0 1 162.4 2.6 17 48.166.19400 38 47.521 144 13.949 1142 110 N 86 32 3 .80 97 0 0 1 162.4 2.6 17 48.166.19400 38 40.408 144 17.357 1107 130 Y 14 25 3 SE .09 146 0 0 5 28.5 5.7 14 48.166.195600 38 39.781 144 18.584 1107 1107 Y 12 18 3 SW 13.5 0 0 0 43.1 6.7 14 14 15.804 1107 130 Y 14 25 3 SE .09 146 0 0 5 28.5 5.7 14 14 14 15.804 1107 130 Y 14 25 3 SE .09 146 0 0 5 249.1 3.1 6.7 14 14 15.804 1107 130 Y 14 25 3 SE .09 146 0 0 5 249.1 3.1 6.7 14 14 15.804 1107 1107 110 Y 12 18 3 SW 13.5 0 0 0 43.1 6.7 14 14 15.804 1107 1107 110 Y 12 18 3 SW 13.5 0 0 0 43.1 6.7 14 14 15.804 1107 110 Y 12 18 3 SW 13.5 0 0 0 5 249.1 3.1 6.7 14 14 15.804 1107 110 Y 12 18 3 SW 13.5 0 0 0 0 243.4 2.5 14 14 15.804 1107 110 Y 12 18 3 SW 13.5 0 0 0 0 243.4 2.5 14 14 14 15.804 1107 110 Y 12 18 3 SW 13.5 0 0 0 0 243.4 2.5 14 14 14 15.804 1107 110 Y 12 18 3 SW 13.5 0 0 0 0 243.4 2.5 14 14 14 15.804 1107 110 Y 12 18 3 SW 13.5 0 0 0 0 243.4 2.5 14 14 14 15.804 1107 110 Y 12 18 3 SW 13.5 0 0 0 0 243.4 2.5 14 14 14 15.804 1107 110 Y 12 18 3 SW 13.5 0 0 0 0 243.4 2.5 14 14 14 15.804 1107 110 Y 12 18 3 SW 13.5 0 0 0 0 243.4 2.5 14 14 14 14 14 14 14 14 14 14 14 14 14	6	48.166.061000	38 38.154	144 14.793	1142	110	14	84	34	3		.70	80	Û	0	1	232.5	<b>4</b> . O
9	7	48.166.073700	38 39.442	144 15.023	1107	200	Y	29	26	3	ИÚ	.11	186	6	Ð		59.5	5.9
10 48.166.111800 38 31.268 144 37.273 1142 130 Y 11 26 2 880 134 0 0 66.5 4.5 11 48.166.113200 38 38.36 144 37.850 1107 480 Y 27 32 3 5W .25 109 0 0 84.3 4.6 12 48.166.143300 38 38.316 144 26.510 1107 500 Y 15 27 5 5E .4E 213 0 0 239.2 4.6 13 48.166.16100 38 43.867 144 16.477 1142 500 N 88 34 2 1.50 289 0 0 1 239.3 5.6 14 48.166.162300 38 44.892 144 15.160 1142 110 Y 14 27 2 1.20 298 0 0 240.0 4.5 15 48.166.174000 38 45.857 144 13.949 1142 110 N 86 32 3 .80 97 0 0 1 162.4 2.6 16 48.166.192400 38 41.407 144 15.787 1107 0 Y 39 0 0 5E -9.1 0 0 5 28.5 5.7 18 48.166.192400 38 41.407 144 15.787 1107 0 Y 39 0 0 5E -9.1 0 0 5 28.5 5.7 18 48.166.195400 38 39.781 144 18.584 1107 110 Y 12 18 3 SW 13.5 0 0 0 43.1 6.2 20 48.166.213000 38 36.63 144 22.744 1107 480 Y 29 34 3 NE .19 31 0 0 41.4 21 48.166.213000 38 35.530 144 25.855 1142 130 N 85 27 3 .50 06 0 0 1 40.2 4.6 22 48.166.225800 38 30.041 144 28.313 1107 480 Y 29 34 3 NE .19 31 0 0 41.4 23 48.166.233000 38 35.530 144 27.799 1107 130 Y 12 18 3 SW 13.5 0 0 0 243.4 2.7 24 48.166.233000 38 37.781 144 18.584 1107 110 Y 12 18 3 SW 13.5 0 0 0 243.4 2.7 25 48.166.213000 38 35.530 144 27.799 1107 130 Y 12 18 3 SW 13.5 0 0 0 243.4 2.7 26 48.166.225800 38 30.041 144 28.313 1107 480 Y 29 34 3 NE .19 31 0 0 41.4 27 48.166.233000 38 35.530 144 27.894 1142 500 N 6 20 2 .70 310 0 0 1 239.0 243.4 2.6 26 48.167.032600 38 39.035 144 9.441 1107 500 Y 53 37 3 SE .35 246 0 0 235.0 4.5 26 48.167.032600 38 39.035 144 9.441 1107 500 Y 53 37 3 SE .35 246 0 0 235.3 4.5 27 48.167.052800 38 43.505 144 3.520 1142 200 Y 8 22 2 .60 29 0 0 1 233.3 5.5 28 48.167.052800 38 43.505 144 3.520 1142 200 Y 8 22 2 .60 29 0 0 1 233.3 5.5 29 48.167.052800 38 43.505 144 3.520 1142 200 Y 8 22 2 .60 29 0 0 235.3 4.5 29 48.167.062800 38 43.505 144 3.520 1142 200 Y 8 22 2 .60 29 0 0 1 233.3 5.5 31 48.167.062800 38 57.347 143 37.531 1107 110 Y 30 30 30 3 NW .29 229 0 0 235.3 4.5 31 48.167.062900 38 57.347 143 37.531 1107 0 Y 35 0 0 NW 14.8 0 0 0 2 233.3 5.5 31 48.167.062900 38 57.347 143 37.531 1107 100 Y 35 0 0 NW	8	48.166.075600	38 38.949	144 17.791	1142	110	Y	12	26	2		.30	137	Ģ.	Û		60.3	5.7
11 48.166.113200 38 30.461 144 37.850 1107 480 Y 27 32 3 5W .25 109 0 6 84.3 4.1 12 48.166.141300 38 38.316 144 26.510 1107 500 Y 15 27 5 5E .48 213 0 0 239.2 4.5 13 48.166.160100 38 43.867 144 16.477 1142 500 N 88 34 2 1.50 289 0 0 1 279.3 5.4 14 48.166.164000 38 44.892 144 15.160 1142 110 Y 14 27 2 1.20 298 0 0 240.0 4.5 15 48.166.180900 38 44.892 144 15.160 1142 110 N 86 32 3 .80 97 0 0 1 162.4 2.6 17 48.166.180900 38 47.521 144 13.949 1142 110 N 86 32 3 .80 97 0 0 1 162.4 2.6 17 48.166.195600 38 40.408 144 17.357 1107 130 Y 14 25 3 SE .09 146 0 0 54.3 6.7 19 48.166.195600 38 39.781 144 18.584 1107 110 Y 12 18 3 SH 13.5 0 0 0 43.1 6.6 20 48.166.218000 38 35.530 144 22.744 1107 480 Y 12 18 3 SH 13.5 0 0 0 43.1 6.6 22 48.166.231800 38 35.530 144 25.855 1142 130 N 85 27 3 .50 106 0 0 1 40.2 4.8 22 48.166.231800 38 35.530 144 25.855 1142 130 N 85 27 3 .50 106 0 0 1 40.2 4.8 22 48.166.231800 38 35.530 144 25.855 1142 130 N 85 27 3 .50 106 0 0 1 40.2 4.8 22 48.166.231800 38 35.530 144 25.855 1142 130 N 85 27 3 .50 106 0 0 1 40.2 4.8 22 48.166.231800 38 35.530 144 25.855 1142 130 N 85 27 3 .50 106 0 0 1 40.2 4.8 22 48.167.013600 38 35.530 144 25.855 1142 130 N 85 27 3 .50 106 0 0 1 40.2 4.8 22 48.167.02600 38 35.530 144 25.855 1142 130 N 85 27 3 .50 106 0 0 1 40.2 4.8 22 48.167.013600 38 35.530 144 25.855 1142 130 N 85 27 3 .50 106 0 0 1 40.2 4.8 22 48.167.013600 38 35.530 144 25.855 1142 130 N 85 27 3 .50 106 0 0 1 40.2 4.8 22 48.167.013600 38 35.530 144 25.855 1142 130 N 85 27 3 .50 106 0 0 1 40.2 4.8 22 48.167.002600 38 35.530 144 35.50 1142 200 N 64 20 2 .70 310 0 0 1 239.0 2.5 249.1 3.3 24 48.167.002600 38 35.353 144 35.6533 1142 200 N 64 20 2 .70 310 0 0 1 239.0 2.5 249.1 3.3 24 48.167.002600 38 49.04 143 53.633 1142 200 N 76 26 31 3 NU .18 959 0 0 235.3 4.5 24 48.167.002600 38 49.04 143 53.633 1142 200 N 76 26 31 3 NU .18 959 0 0 235.3 4.5 24 48.167.002600 38 55.77 143 40.816 1107 130 Y 42 32 3 NE .11 120 0 0 233.3 5.3 3 48.167.002000 38 55.77 143 40.816 1107 130 Y 42 32 3 NE .11 120 0 0 2 233.3 4.6 233.3 5.	9	48.166.094400	38 34.455	144 27.447	1107	480	Y	50	36	3	£E.	.25	114	Ģ	Ũ		66.3	4.8
12	10	48.166.111800	38 31.248	144 37.273	1142	130	Y	11	26	2		.80	134	G	ŋ		69.5	4.5
13 48.166.160100 38 43.867 144 16.477 1142 500 N 88 34 2 1.50 289 0 0 1 239.3 5.2 14 48.166.162300 38 44.892 144 15.160 1142 110 Y 14 27 2 1.20 298 0 0 240.0 4.5 15 48.166.174000 38 46.183 144 11.609 1107 200 Y 33 31 3 SE .58 217 0 0 208.0 1.5 16 48.166.180900 38 47.521 144 13.949 1142 110 N 86 32 3 .80 97 0 0 1 162.4 2.6 17 48.166.192600 38 47.521 144 15.787 1107 0 Y 39 0 0 SE -9.1 0 0 0 5 28.5 5.7 18 48.166.192600 38 40.408 144 17.357 1107 130 Y 14 25 3 SE .09 146 0 0 5 43.1 6.0 19 48.166.195600 38 39.781 144 18.584 1107 1107 Y 12 18 3 SN 13.5 0 0 0 43.1 6.0 20 48.166.213000 38 36.643 144 22.744 1107 480 Y 29 34 3 NE .19 31 0 0 41.4 4.2 4.3 148.166.213000 38 35.530 144 25.855 1142 130 N 85 27 3 SE .50 106 0 0 1 40.2 4.6 24 48.166.231800 38 30.747 144 27.109 1107 130 Y 12 24 3 SN .10 56 0 0 S 249.1 3.3 23 48.166.231800 38 35.143 144 19.294 1142 500 N 6 20 2 .70 310 0 0 1 239.0 2.5 25 48.167.032600 38 35.530 144 27.109 1107 130 Y 12 24 3 SN .14 158 0 0 243.4 2.6 2.6 48.167.032600 38 35.143 144 19.294 1142 500 N 6 20 2 .70 310 0 0 1 239.0 2.5 25 48.167.032600 38 35.530 144 27.109 1107 130 Y 12 24 3 SN .14 158 0 0 235.0 4.5 25 48.167.032600 38 35.143 144 19.294 1142 500 N 6 20 2 .70 310 0 0 1 239.0 2.5 25 48.167.032600 38 35.143 144 19.294 1142 500 N 6 20 2 .70 310 0 0 1 239.0 2.5 25 48.167.032600 38 35.143 144 19.294 1142 500 N 6 20 2 .70 310 0 0 1 239.0 2.5 25 48.167.032600 38 43.505 144 3.520 1142 200 Y 8 22 2 .60 293 0 0 229.3 5.5 27 48.167.032600 38 43.505 144 3.520 1142 200 Y 8 22 2 .60 293 0 0 229.3 5.5 27 48.167.032600 38 53.747 143 59.506 1107 500 Y 53 37 3 SE .35 246 0 0 235.3 4.5 24 48.167.032600 38 53.747 143 59.506 1107 500 Y 26 31 3 NN .18 959 0 0 235.3 4.5 24 48.167.032600 38 53.747 143 59.506 1107 500 Y 26 31 3 NN .18 959 0 0 235.3 4.5 24 48.167.032600 38 53.747 143 59.506 1107 500 Y 26 31 3 NN .18 959 0 0 235.3 4.5 24 48.167.032600 38 53.747 143 59.506 1107 500 Y 30 30 3 NN .18 959 0 0 235.3 4.5 24 24 48.167.032600 38 53.747 143 59.506 1107 500 Y 30 30 3 NN .18 959 0 0 2235.3 4.5 24 24 24 25 24 2	11	48.166.113200	38 30.461	144 37.850	1107	480	Y	27	32	3	51	.25	109	G	G		84.3	4.8
14	12	48.166.141300	38 38.316	144 26.510	1107	500	Y	15	27	5	SĘ	.48	213	0	ŷ		239.2	4.8
14	13	48.166.160100	38 43.867	144 16.477	1142	500	Ŋ	88	34	2		1,50	289	0	Ŋ	1	239.3	5.4
16	14	48.166.162300	38 44.892	144 15.160	1142	110	Y	14	27	2		1.20	298	Û	0		240.0	4.5
16	15	48.166.174000	38 46.183	144 11.609	1107	200	Y	33	31	3	SE	.58	217	ŋ	0		208.0	1.9
18	16	48.166.180900	38 47.521	144 13.949	1142	110	N	86	32	3		.80	97	Û	G	1	162.4	2.6
19	17	48.166.192600	38 41.407	144 15.787	1107	0	Y	39	G	0	SE	-9.1	0	0	Ŋ	5	28.5	5.7
20	18	A8.166.194400	38 40.408	144 17.357	1107	130	Y	14	25	3	SE	.09	146	O	6		54.3	6.7
21 48.166.213000 38 35.530 144 25.855 1142 130 N 85 27 3	19	48.166.195600	38 39.781	144 18.584	1107	110	Y	12	31	3	54	13.5	0	0	G		43.1	6.0
22 48.166.225800 38 30.041 144 28.313 1107 480 Y 48 37 3 NE .10 56 0 0 S 249.1 3.3 23 48.166.231800 38 30.747 144 27.109 1107 130 Y 12 24 3 SN .14 158 0 0 243.4 2.6 24 48.167.013600 38 35.143 144 19.294 1142 500 N 6 20 2 .70 310 0 0 1 239.0 2.5 48.167.032600 38 39.035 144 9.441 1107 500 Y 53 37 3 SE .35 246 0 0 235.0 4.5 26 48.167.044200 38 43.505 144 3.520 1142 200 Y 8 22 2 .60 293 0 0 229.3 5.7 27 48.167.051500 38 44.881 143 59.506 1107 500 Y 26 31 3 NN .18 959 0 0 235.3 4.5 28 48.167.062800 38 49.049 143 53.633 1142 200 N 76 26 3 .90 281 0 0 1 233.4 5.4 29 48.167.070800 38 50.741 143 49.154 1107 110 Y 30 30 3 NN .29 229 0 0 235.3 4.5 30 48.167.081200 38 53.922 143 43.404 1107 200 Y 13 22 4 NN .05 220 0 0 1 233.3 5.7 31 48.167.084200 38 57.347 143 40.816 1107 130 Y 42 32 3 NE .11 120 0 0 233.3 4.5 32 48.167.092100 38 57.347 143 37.531 1107 0 Y 35 0 0 NN .14.8 0 0 0 0 2 233.3 4.5 33 48.167.092100 38 57.347 143 37.531 1107 0 Y 35 0 0 NN .14.8 0 0 0 0 2 233.3 4.5 33 48.167.092100 38 57.347 143 37.531 1107 0 Y 35 0 0 NN .14.8 0 0 0 0 2 233.3 4.5 33 48.167.092100 38 57.347 143 37.531 1107 0 Y 35 0 0 NN .14.8 0 0 0 0 2 233.3 4.5 33 48.167.102900 39 .421 143 31.488 1107 130 Y 30 31 3 NN .12 218 0 0 226.5 6.6				144 22.744	1107	480	Y	29	-	3	NE	.19	31	Ç.	Ù		41.4	4.3
23 48.166.231800 38 30.747 144 27.109 1107 130 Y 12 24 3 SW .14 158 0 0 243.4 2.6 24 48.167.013600 38 35.143 144 19.294 1142 500 N 6 20 2 .76 310 0 0 1 239.6 2.5 25 48.167.032600 38 39.035 144 9.441 1107 500 Y 53 37 3 5E .35 246 0 0 235.0 4.6 26 48.167.044200 38 43.505 144 3.520 1142 200 Y 8 22 2 .60 293 0 0 229.3 5.7 27 48.167.051500 38 44.881 143 59.506 1107 500 Y 26 31 3 NW .18 959 0 0 235.3 4.6 28 48.167.062800 38 49.049 143 53.633 1142 200 N 76 26 3 .90 281 0 0 1 233.4 5.4 29 48.167.070800 38 50.741 143 49.154 1107 110 Y 30 30 3 NW .29 229 0 0 235.3 4.5 30 48.167.081200 38 53.922 143 43.404 1107 200 Y 13 22 4 NW .05 220 0 0 1 233.3 5.7 31 48.167.084200 38 55.477 143 40.816 1107 130 Y 42 32 3 NE .11 120 0 0 234.2 3.6 32 48.167.092100 38 57.347 143 37.531 1107 0 Y 35 0 0 NW .14.8 0 0 0 2 233.3 4.5 33 48.167.102900 39 .421 143 31.488 1107 130 Y 30 31 3 NW .12 218 0 0 236.5 6.6	_				1142		И			3		.50	106	0	G	1	40.2	4.8
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25 48.167.032600 38 39.035 144 9.441 1107 500 Y 53 37 3 SE .35 246 0 0 235.0 4.5 26 48.167.044260 38 43.505 144 3.520 1142 200 Y 8 22 2 .60 293 0 0 229.3 5.7 27 48.167.051500 38 44.881 143 59.506 1107 500 Y 26 31 3 NW .18 959 0 0 235.3 4.5 28 48.167.062800 38 49.049 143 53.633 1142 200 N 76 26 3 .90 281 0 0 1 233.4 5.4 29 48.167.070800 38 50.741 143 49.154 1107 110 Y 30 30 3 NW .29 229 0 0 255.3 4.5 30 48.167.081200 38 53.922 143 43.404 1107 200 Y 13 22 4 NW .05 220 0 0 1 223.3 5.3 48.167.084200 38 55.477 143 40.816 1107 130 Y 42 32 3 NE .11 120 0 0 234.2 3.5 32 48.167.092100 38 57.347 143 37.531 1107 0 Y 35 0 0 NW .14.8 0 0 0 2 233.3 4.5 33 48.167.092100 39 .421 143 31.488 1107 130 Y 30 31 3 NW .12 218 0 0 236.5 6.6							•			-	SW	-		Ũ			243.4	2.9
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Table 4: Sample satellite fix listing from Survey 48. Headings are
follows: -
FIX - fix number within file; FIXTIME - time of fix to nearest
minute:
LAT, LONG - fix position adjusted to nearest minute;
SYSTEM - indicates MX1107 or MX1142 fix; SAT - satellite ID code;
OK - Y or N indicates fix accepted or rejected by satellite
navigator;
ELEV - maximum of elevation during fix, in degrees;
COUNT - number of doppler counts received during pass;
ITER - number of iterations required for fix to compute;
GEOM - geometry of pass;
ERROR, DIR - distance (nautical miles) and bearing (degrees) of
fix update (based on shipboard DR data);
SLT, SLN - standard deviation of latitude and longitude (metres);
CODE - error code, blank if fix accepted by MX1107 or MX1142;
COURSE, SPEED - course (degrees) and speed (knots) of ship at
time of fix.
```

#### Pass 2

- a.  $\mathit{CFACT}$  uses the DR file and a user-created file of calibration factor intervals to compute velocity calibration factors for each DR system.
- b. APROX uses the calibration factors computed in CFACT and the DR file to produce an approximately calibrated DR file.
- c. ASSES uses the approximately calibrated DR file created by APROX to produce a line printer plot of the current and summed error vectors at and between satellite fixes. The plot is produced at a 10-minute sample interval.

The basis of the processing is that option 'ASSES' takes the summed latitude and longitude error vectors at each fix (ie a running sum of the DR position to satellite fix position vectors at the time of each fix) and uses a piece-wise cubic polynomial curve-fitting function (the Akima spline) to compute error vectors at all times between satellite fixes. It is assumed that the ensuing smooth variation of the error vector is due to ocean currents, winds, etc. Poor quality fixes will produce unrealistic or large and variable ocean currents. At each round of assessment (and usually at least three rounds are required for each file), the satellite fixes are checked wherever the summed error and current vectors suggest a problem, and those fixes of poor quality are deleted for the next program run. The effect of this process can be seen in the example in Figures 2 and 3.

SAT3: uses the final file of satellite fixes and the DR data to produce final positions for each DR system. This program again uses the Akima spline to compute the assumed currents acting at all times between satellite fixes and applies those currents to the DR data to compute positions.

FINAV: performs the following functions -

- a. Computes final 1-minute positions based on a 'mix' of DR systems, Global Positioning System and Miniranger according to a file specified by the user. The final navigation is shown at small scale in Figure 4.
- b. The gravity data (which was in mgals relative to an arbitrary datum) was converted to absolute values corrected for meter drift and with Eotvos corrections applied. Gravity ties were performed in Melbourne, Victoria prior to the cruise, and in Brisbane, Queensland at the end of the cruise. Summary of results are as follows:

Ship's value (ums\*\*-2) Corrected Value (ums\*\*-2)

Pre-Otway = -4349.75 9799884.6

Time & Date 4/6/85 1515 hrs (local)

Post Otway =-12618.75 9791675.63

Time & Date 19/7/85 1430 hrs (local)

Difference = 8269.0 8209.0

Drift = 60 ums\*\*-2.

VARPL/EDATA: As a final check, the Phase 2 positions, water depths, magnetic, and gravity data were plotted and editing applied as necessary. Program FIXTM was then used to re-block the data to 8 channels x 60 records per block. The final channel allocations are shown in Table 5. As a final editing stage, the residual gravity spikes at turns are removed (EDATA) and the gravity channel is smoothed by a filter of 15 minute period to remove any remaining sea noise (MUFF).

Table 5: Final channel allocations.

Channel No	Contents
1	Time(SS.DDD)
2	Time(.HHMMSS)
3	Latitude(radians)
4	Longitude(radians)
	relative to 100E.
5	Water depth(metres)
6	Gravity(mgals)
7	Total magnetic field 1(nT)
8	Total magnetic field 2(nT)

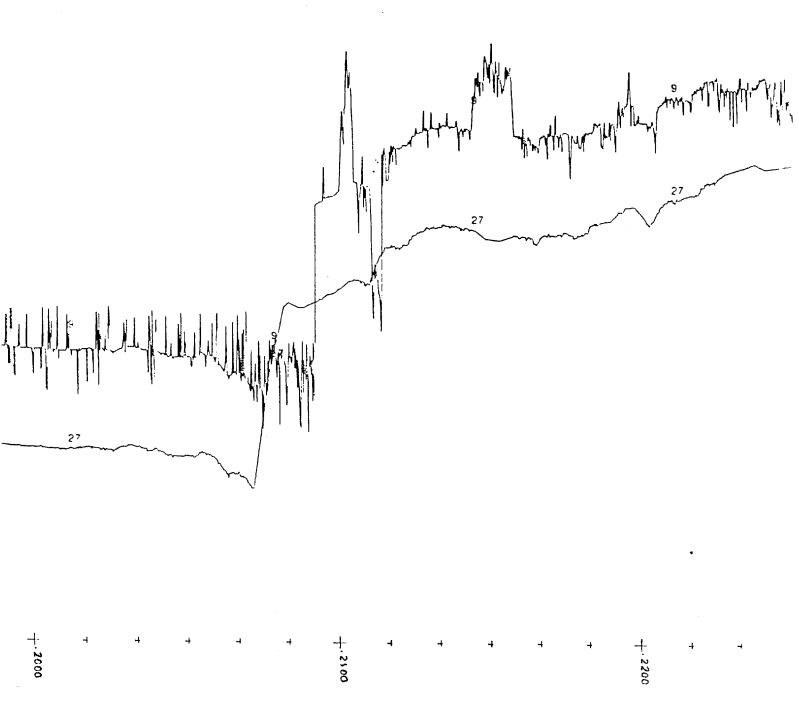


Figure 1: Bathymetry traces before (upper) and after processing by program SALVG. Vertical scale is 100 m/inch; horizontal scale is 3 inches/hour.



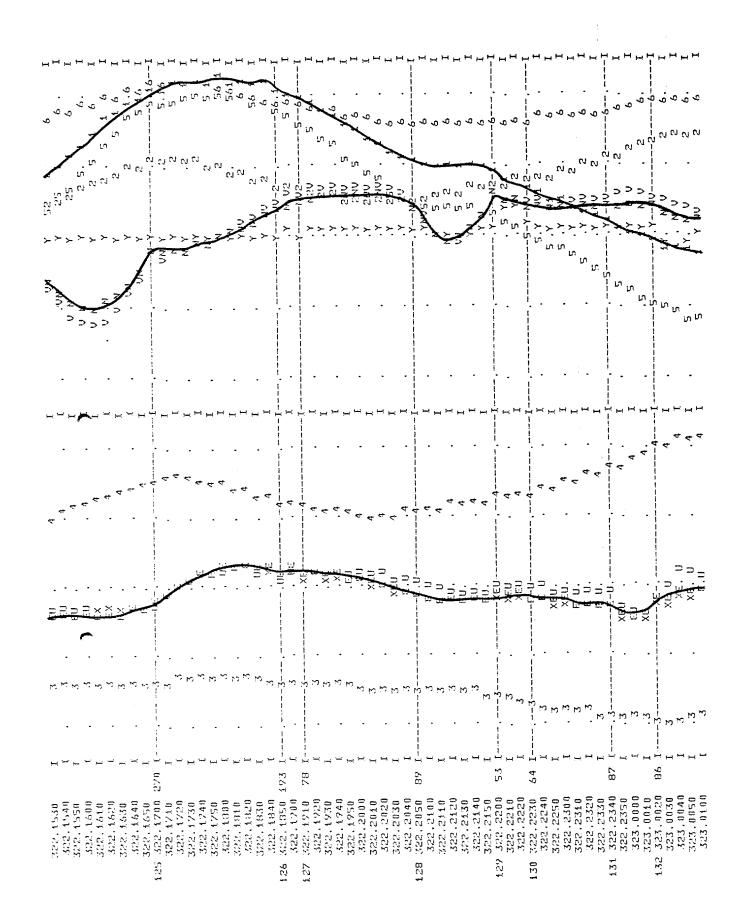
1.7cm = 1 nautical mile

Figure 2: Satellite fix assessment plot. 10-minute time (DD.HHMM) along bottom of plot; satellite fixes indicated by row of dashes (eg. at 322.1700); traces on the plot are as follows:-

N & E - north & east currents for DR system 1;

1 & 2 - north & east summed error vectors for DR system 1; Y & X - north & east currents for DR system 2; 3 & 4 - north & east summed error vectors for DR system 2.

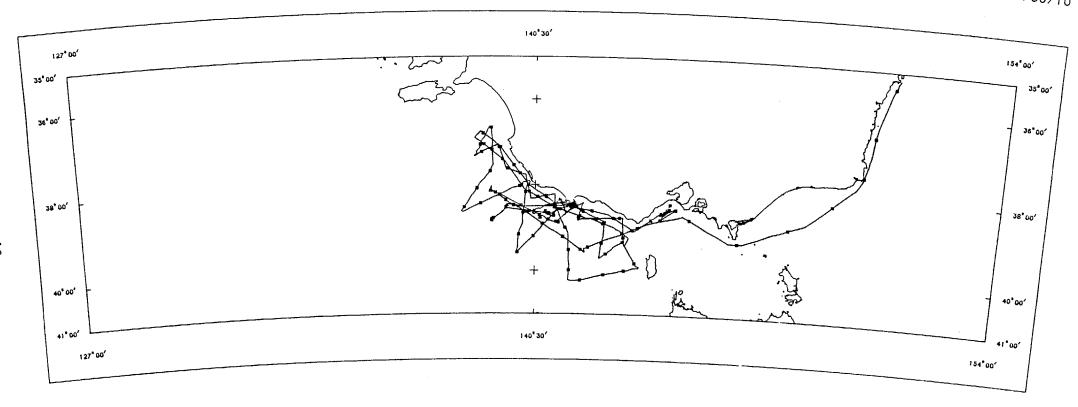
Note in particular the large fluctuations in the east current and the east summed error vector on the left-hand half of the plot.



#### 1.7cm = 1 nautical mile

Figure 3: Same plot as for Figure 2, but after removal of satellite fixes at 332.1830 and 332.2020. Note that the large fluctuations in the east currents and summed vectors have been smoothed out.

SCALE 1:10000000



AUSTRALIAN NATIONAL SPHEROID SIMPLE CONICAL PROJECTION WITH TWO STANDARD PARALLELS AT 18°00' AND 36°00' SOUTH Otway Basin - Bass Strait B.M.R.Survey 48

Track Map

Figure 4: Tracks of Rig Seismic , Survey 48 in the Offshore Otway Basin.

#### DATA AVAILABILITY

The Otway Basin non-seismic data are available in two forms:

- Magnetic Tape 9-track, 1600 bpi, phase-encoded, as either
   ASCII records, 80 characters per record, 10x1-minute records per block; or
  - Hewlett-Packard 32-bit floating point, 8 channels, 60x1-minute records per block.

Enquiries concerning the digital data should be addressed to

Chief Scientist,
Division of Marine Geosciences &
Petroleum Geology,
Bureau of Mineral Resources,
GPO Box 378
Canberra, ACT 2601, Australia

2. b. Anologue Displays - in film or paper form.

Product Code

- Otway survey Track Map, 1:1000000 Map sheet M-480001P
- Otway survey: 1:1000000 Map sheets(2 sheets in each set)
  Residual Magnetic Anomalies profile maps

  Free-air Anomalies profile maps

  M-480004P
  Observed Magnetics posted map values
  Observed Magnetic Anomalies posted map values
  Observed Gravity posted value maps

  M-480006P
  M-480007P

Enquiries concerning the anologue data should be addressed to :

Copy Service, Bureau of Mineral Resources G.P.O. Box 378 Canberra A.C.T 2601 , Australia.