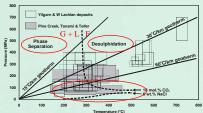
MULTI-PHASE FLOW: THE PROCESS THAT PRODUCES LARGE ORE BODIES? Bruce Hobbs, CSIRO, Perth.

SUMMARY.

Many mineralising systems imply that more than one fluid was involved in the mineralising process. However, it is commonly difficult to identify the various fluid supply plumbing systems that were responsible for bringing the various fluids together. A multi-phase fluid only needs one supply system. Moreover it supplies an intimate mixture of immiscible fluids in the pore spaces ready to do the job. This mixture varies in its composition with respect to whether the fluid system is proximal or distal within the flow

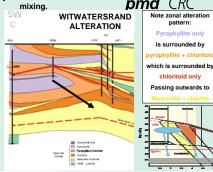
system.

1. MULTI-PHASE SITUATIONS MUST BE COMMON IN ORE ENVIRONMENTS



(T.P. Mernagh, E. Bastrakov, and Wyborn, 2005)

Many ore environments show evidence of fluid mixing with little field evidence of the plumbing system that enables the fluid



3. THE PHYSICS OF TWO-PHASE FLOW

Transport Laws

etting and non-wetting fluid transport is described by Darcy's law

$$q_i^w = -k_{ij}^w \kappa_r^w \frac{\partial}{\partial x_j} (P_w - \rho_w g_k x_k)$$
 (2)

$$e_{kj}$$
 is saturated mobility coefficient, which is a tensor, κ_r is relative permeability for the fluid, a is a function of saturation S_w , μ is dynamic viscosity, P is pore pressure, ρ is fluid density, is gravity. This means that for two phase flow, as is true for multi-phase flow,

 $q_i^g = -k_{ij}^w \frac{\mu_w}{\mu_g} \kappa_f^g \frac{\partial}{\partial x_i} (P_g - \rho_g g_k x_k)$

Capillary Pressure Law

The capillary pressure law relates the difference in fluid pore pressures to saturation

$$P_g - P_w = P_c(S_w)$$
 (2.6)

In FLAC, this empirical law is of the van Genuchten form (see Figure 2.2):

$$P_{\ell}(S_w) = P_0 \left[S_{\ell}^{-1/\alpha} - 1 \right]^{1-\alpha}$$

1.400
1.200
0.400

Figure 2.2 Capillary pressure, Pc, vs effective saturation, Se

Relative Permeability Laws

Relative permeabilities are related to saturation S_{tr} by empirical laws of the van Genuchten for (van Genuchten 1980).

$$\kappa_r^w = S_r^b \left[1 - \left(1 - S_r^{1/a}\right)^a\right]^c$$
(2.3)

$$\kappa_r^g = (1 - S_r)^c \left[1 - S_r^{1/\alpha}\right]^{sn}$$
(2)

n those laws, a, b and c are constant parameters and S_e is the effective saturation.

The effective saturation is defined as:

$$S_{e} = \frac{S_{e} - S_{e}^{*}}{1 - S_{e}^{*}}$$
(2.5)

apillary pressures, is referred to as "connate" in the case of water).

he parameter P₀ is larger for finer material, and its dependency on material properties may be sessed using the Leverett scaling law (see, e.g., Nikolaevskij 1990, p. 414). This law, derive ing dimensional analysis, has the form:

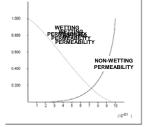
$$P_0 = \frac{\sigma}{\sqrt{\kappa/n}}$$
(2.8)

SATURATION DISTRIBUTION. THIS

EQUATES TO pH-Eh DISTRIBUTION

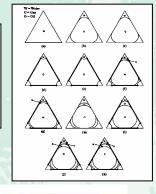
where σ is surface tension, a property of the matrix, κ is intrinsic permeability, and n is porosity.

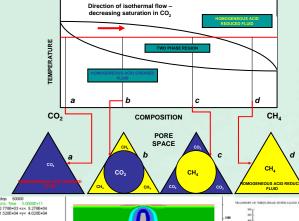
This means that the pore space has a structured distribution of fluids depending upon the wetting angle of each fluid. Depending upon how far down the flow path one is, the pore space may be filled with one end member of the multi-phase assemblage or another. In a system such as CO₂-CH₄-H₂O for instance, at early parts of the flow path the pores will be rich in CO₂. At more distal parts the pores will be rich in CH₄.



Relative permeabilities, κ_r^w , κ_r^g , vs effective saturation, S_ϵ

PORE FLUID DISTRIBUTIONS IN 3-PHASE SYSTEM





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Multi-phase flow provides a mechanism for supplying fluid to a site with a range of fluids with pH's and Eh's intimately structured within the pore space. Thus, different fluid conduits for different fluids are not required to supply contrasting fluid chemistries to a mineralising site. The complete range of chemistry is delivered in each pore ready for reaction with the country rock.



A WITWATERSRAND EXAMPLE

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