



**Centre for Advanced Data Inference
Research School of Earth Sciences**



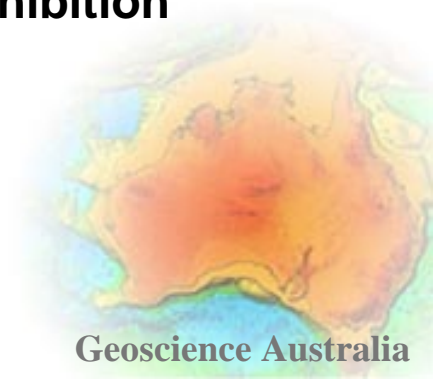
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Holistic inversion of time-domain AEM data

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**ASEG 20th International Geophysical Conference & Exhibition
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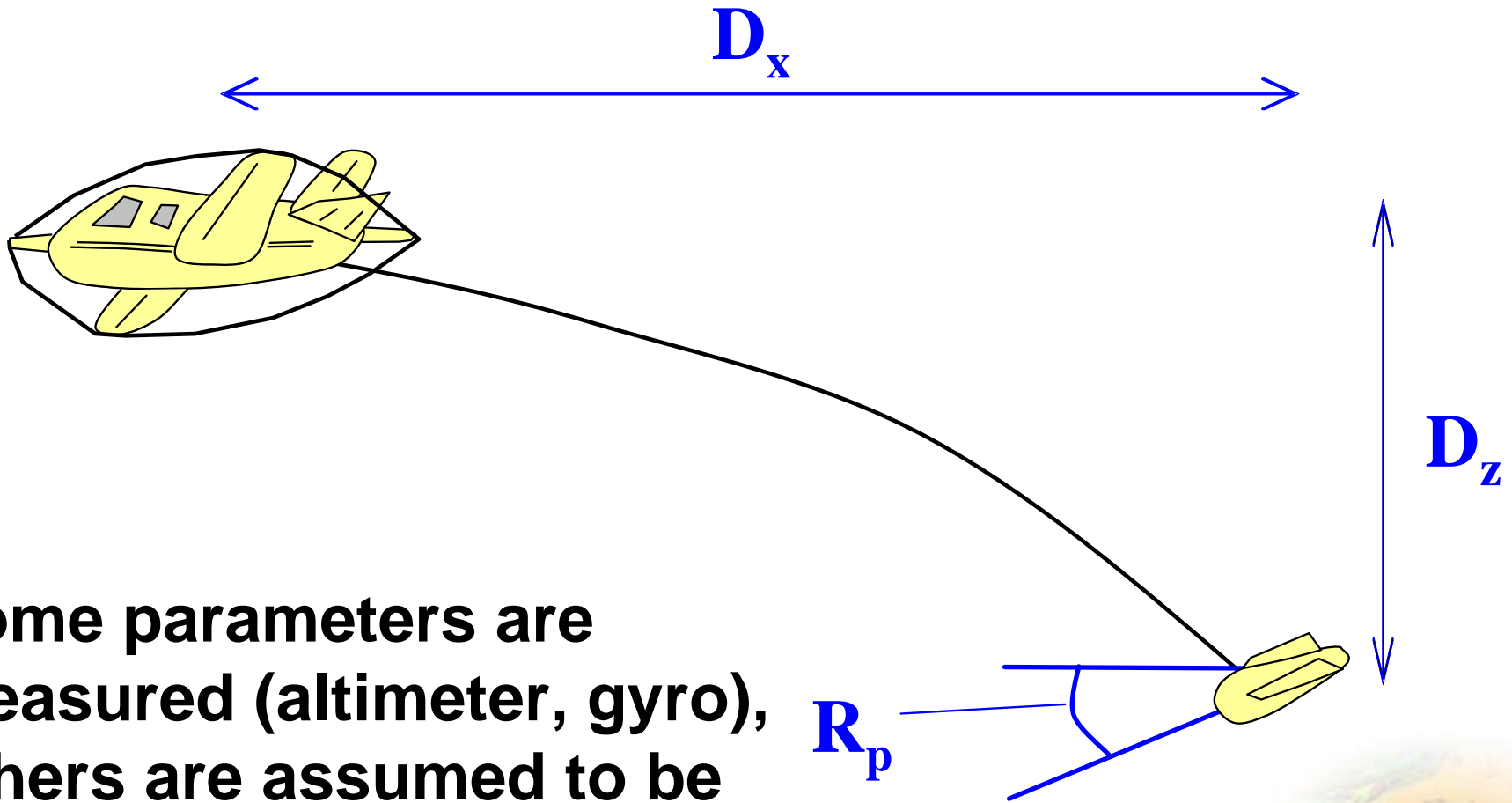
Outline

- **Motivation**
- **Methodology**
- **Example**
- **Future Possibilities**
- **Conclusions**

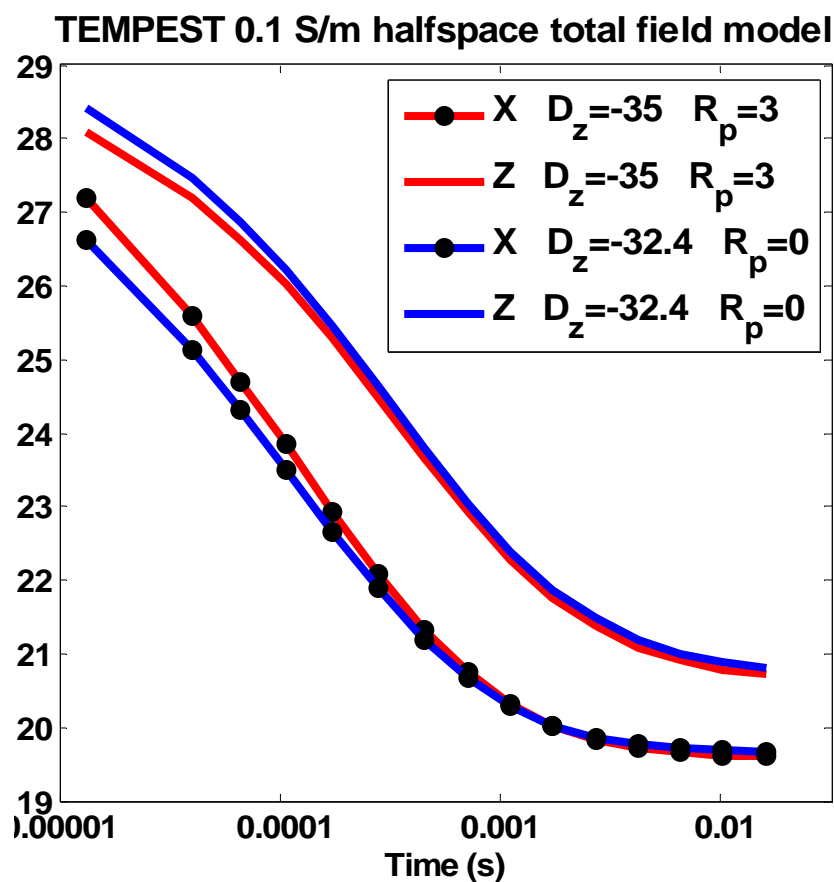
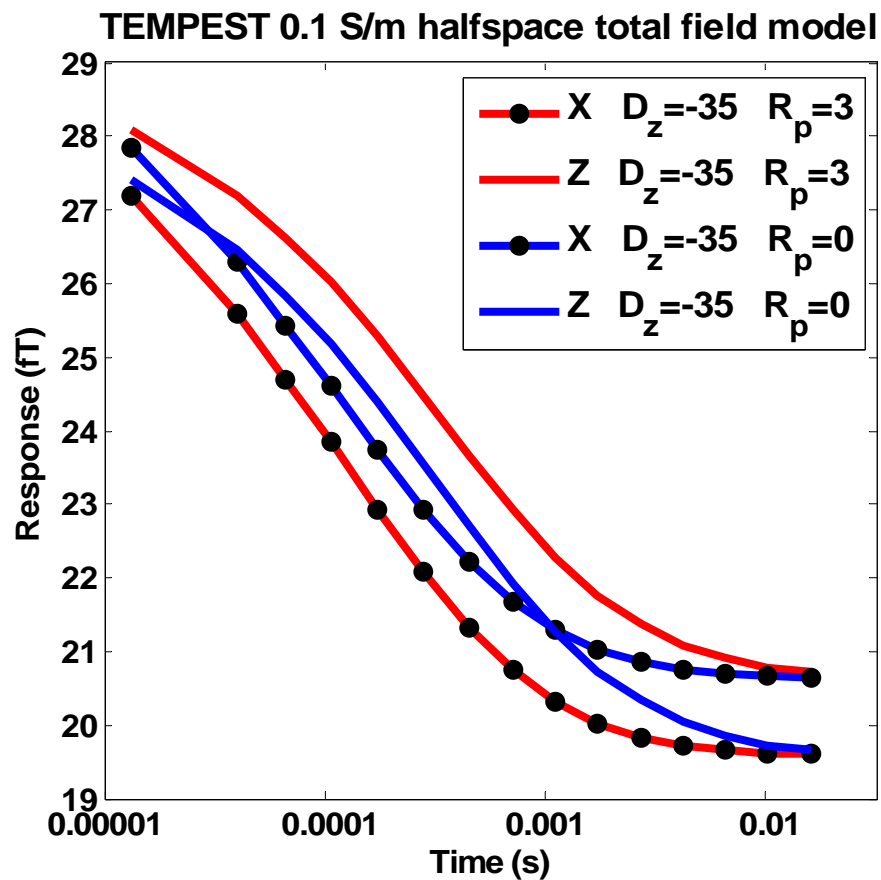
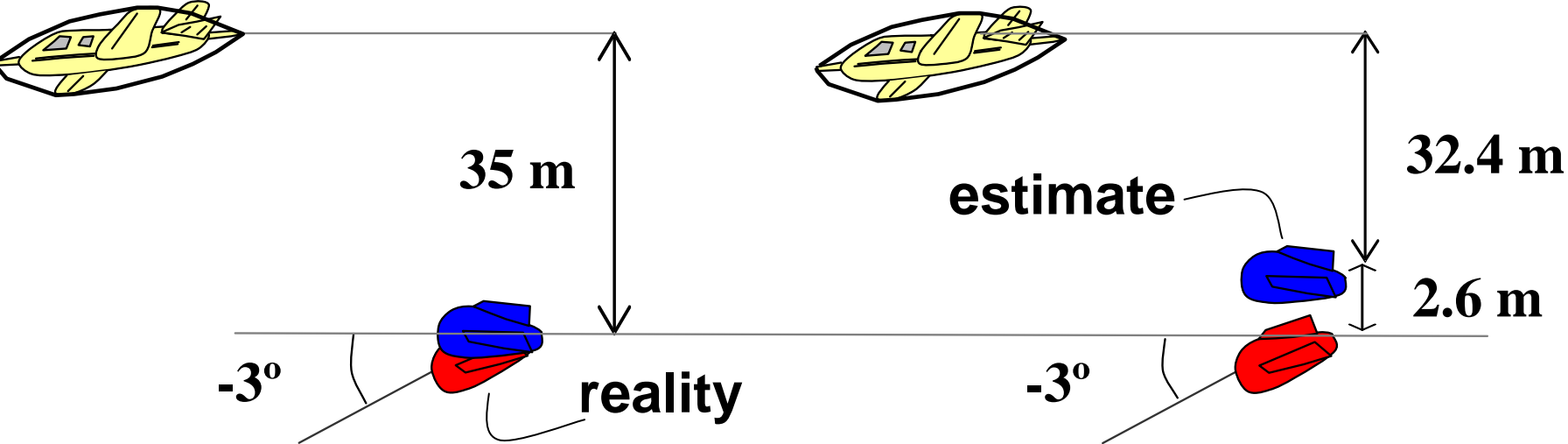
Motivation

- **Bringing together 3 established ideas**
 1. **Solving for geometry – improves results by simulating the real system & allowing data to be fitted**
[Lane et al \(2004\)](#), [Sattel et al \(2004\)](#).
 2. **Laterally/spatially constrained - exploits spatial coherency via inversion of whole lines or datasets, instead of inverting single samples and then stitching them together.** [Auken & Christiansen \(2004\)](#), [Brodie & Sambridge \(2006\)](#), [Vieozzli et al \(2008\)](#), [Vallee & Smith \(2008\)](#).
 3. **Simultaneous inversion for conductivity and calibration parameters ensures consistency.**
[Brodie & Sambridge \(2006\)](#).

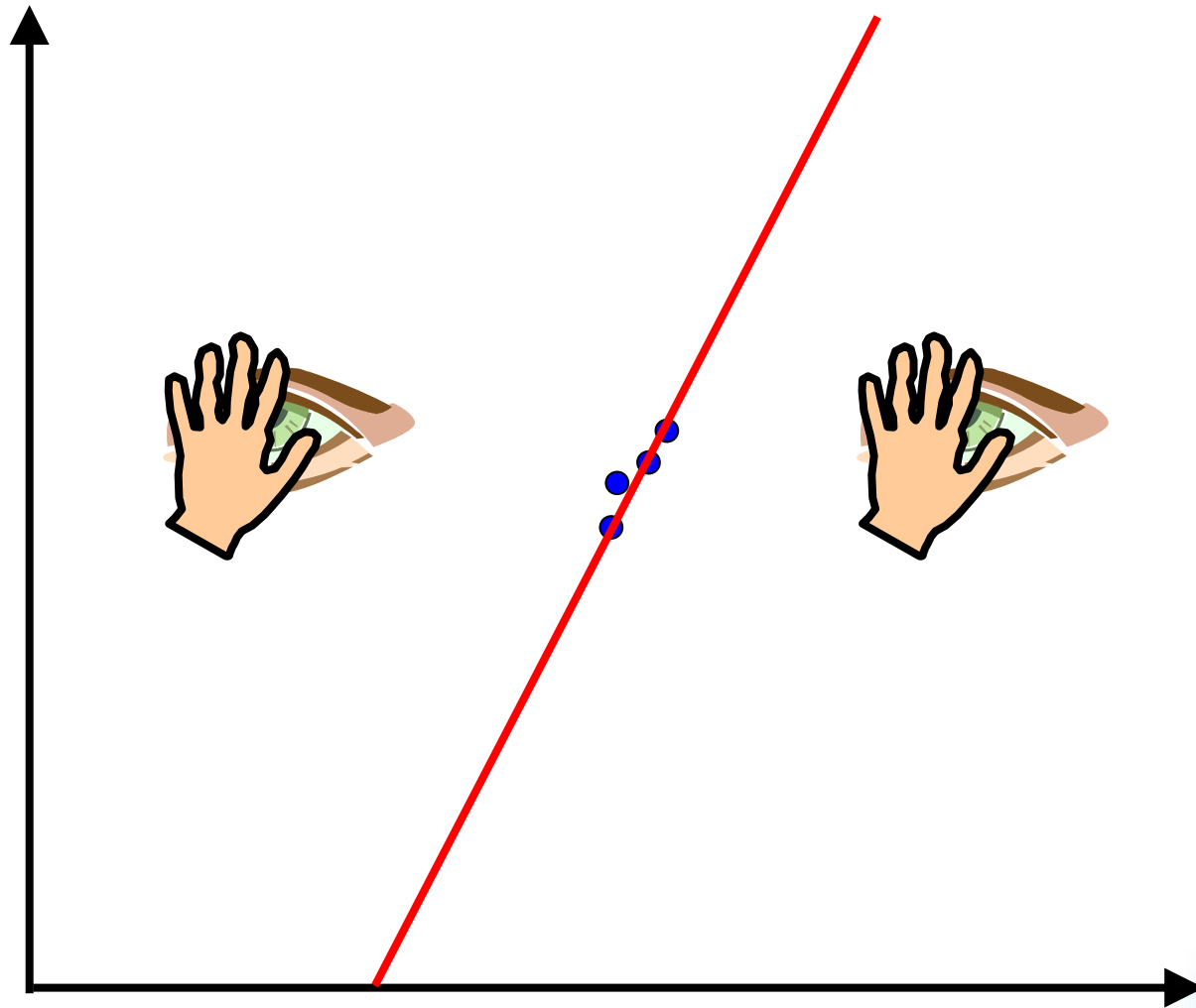
Fixed wing AEM geometry



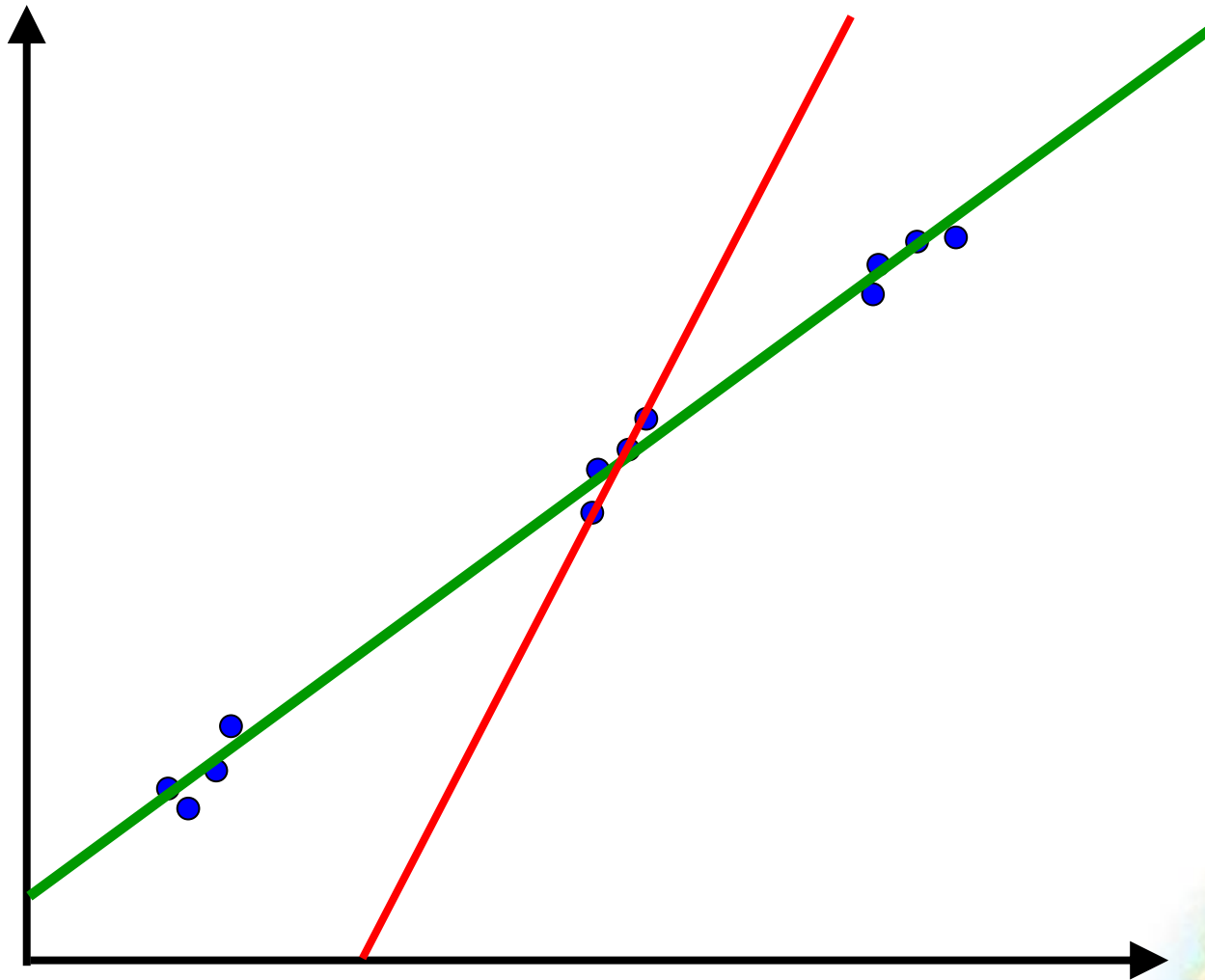
Some parameters are measured (altimeter, gyro), others are assumed to be zero, D_x & D_z are estimated



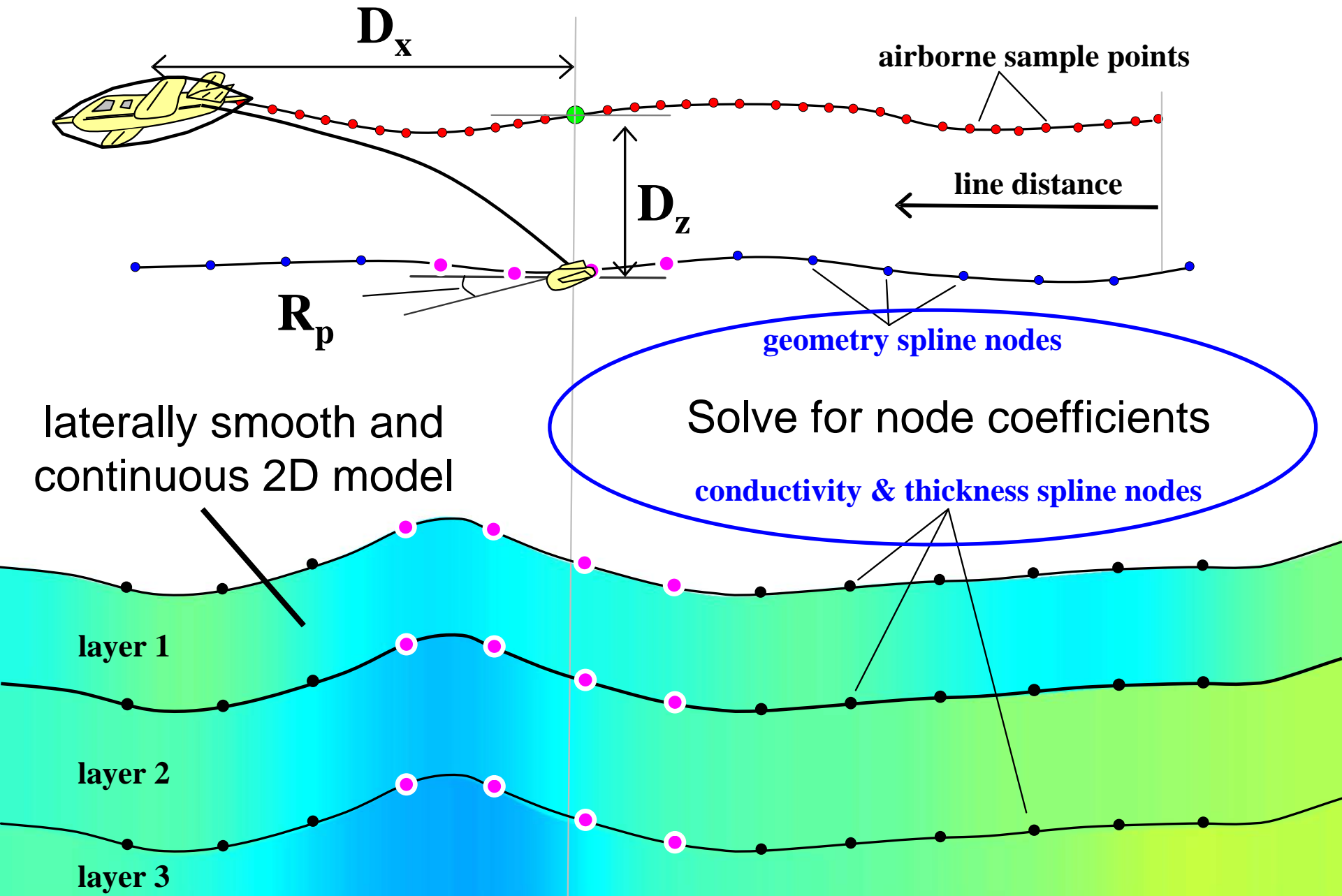
Sample by sample (stitched) inversion



Laterally/spatially constrained inversion

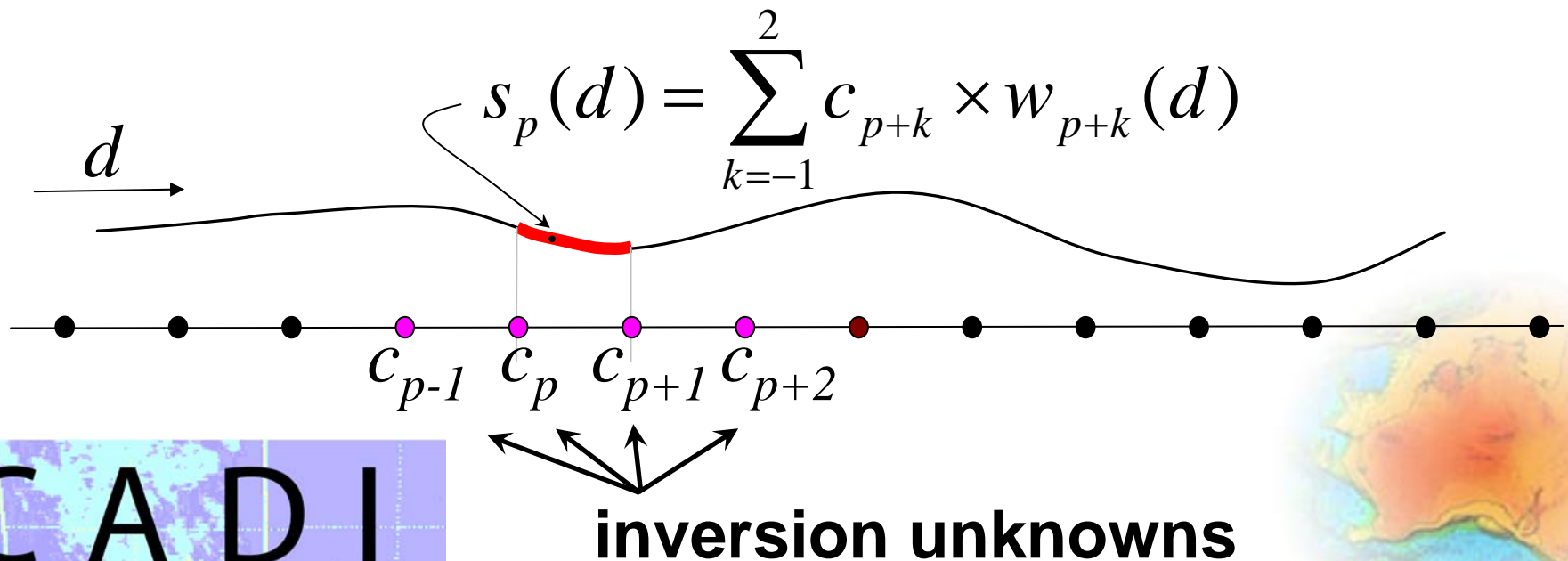


Fixed-wing AEM formulation



Cubic B-Splines

- Continuous valued functions
- Smooth functions (C^2 continuous)
- At the point d , the spline value $s(d)$ is a weighted sum of 4 node coefficients
- A spline for each layer conductivity and/or thickness and geometry value

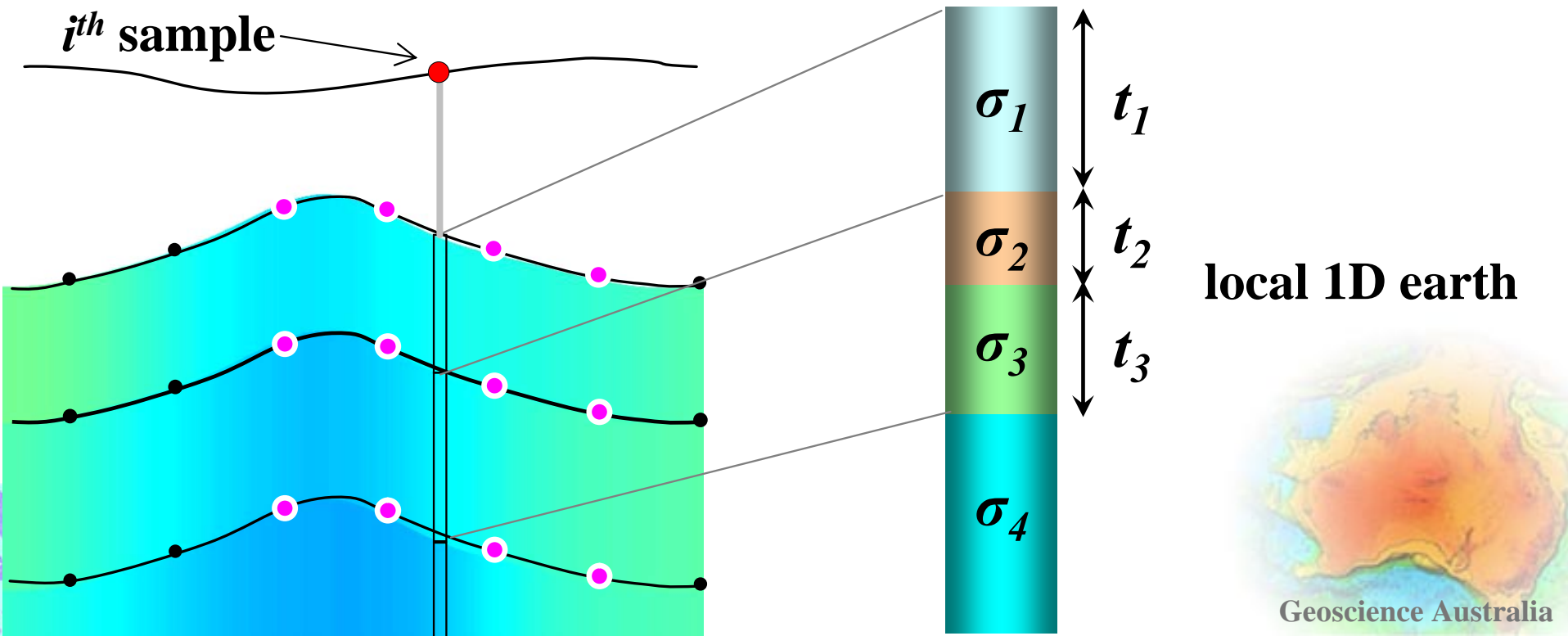


1D Forward problem for i^{th} sample

Compute **local geometry values** from splines

Compute **local 1D earth** from splines

$$d_i^{\text{mod}} = f_{1D}(\sigma^l, t^l, T_h, T_r, T_p, T_y, D_x^l, D_y, D_z^l, R_r, R_p^l, R_y)$$



Objective function

$$\phi = \phi_d + \lambda \phi_m$$

data misfit

model regularisation

Data misfit

- **Noise normalised squared error**
- **Sum over N_c channels = windows \times components**
- **Sum over N_s samples = samples in line**

$$\phi_d = \frac{1}{N_s N_c} \sum_s \sum_c \left(\frac{d_{s,c}^{\text{mod}} - d_{s,c}^{\text{obs}}}{d_{s,c}^{\text{err}}} \right)^2$$

Model regularisation

- **Reference model misfit**
 - difference between inversion model and reference model
- **Horizontal roughness**
 - second derivative of logarithm of conductivity between horizontally adjacent conductivity spline nodes
 - second derivative of logarithm of thickness between horizontally adjacent thickness spline nodes
- **Vertical roughness**
 - second derivative of logarithm of conductivity between adjacent layers
- **Alpha values control relative importance of terms**

$$\phi_m = \alpha_r \phi_r + \alpha_h \phi_h + \alpha_v \phi_v$$

Objective function minimisation

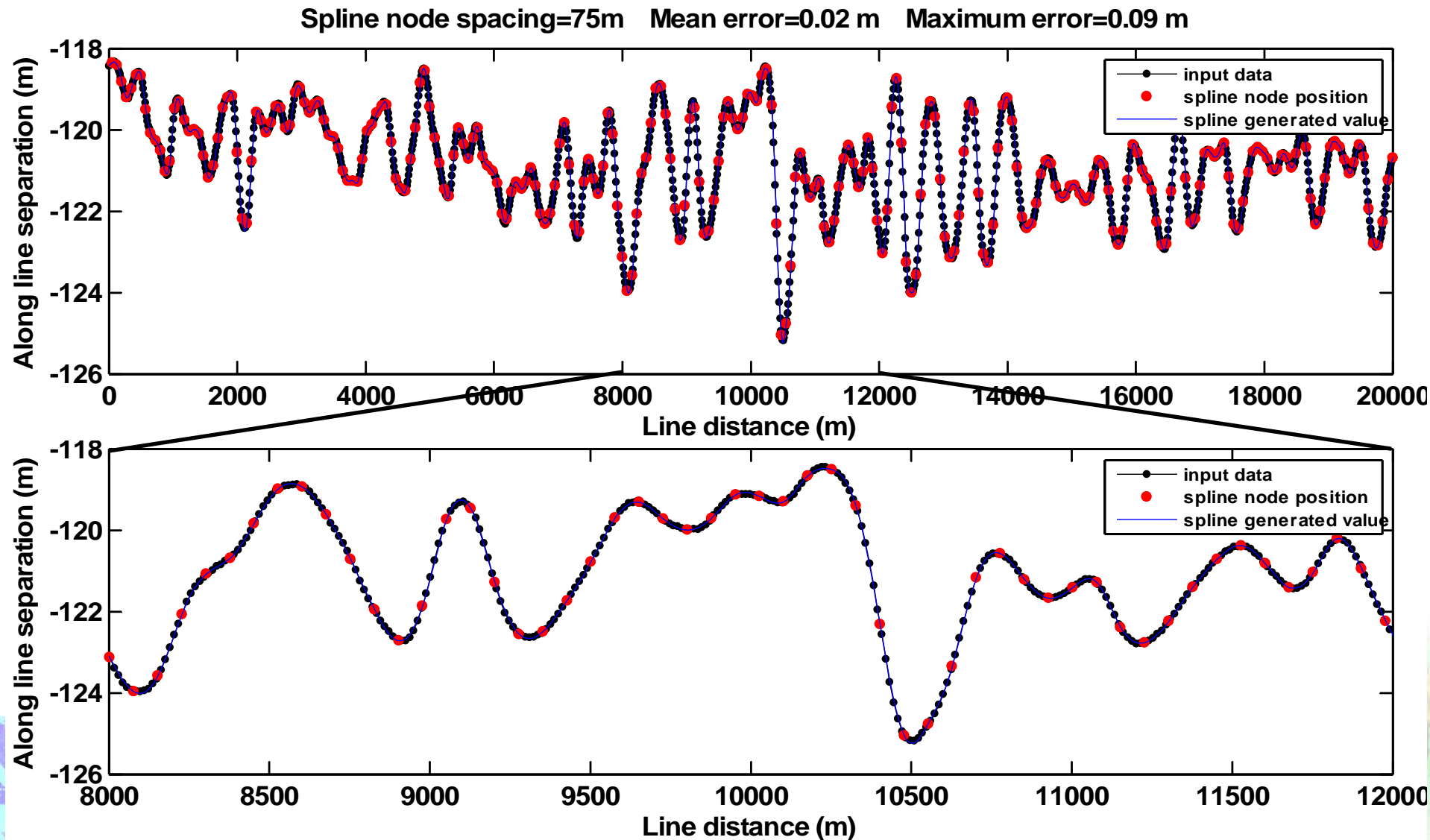
- Iterative non-linear gradient based scheme
- Conjugate gradient method used to solve linearised problem within each iteration
- The α values are chosen and remain fixed
- In each iteration a line search is done on λ to find its value that reduces data misfit by ~30%

$$\mathbf{A}\mathbf{m}_{n+1} = \mathbf{b}$$

$$\mathbf{A} = \left[\mathbf{J}^t \mathbf{W}_d \mathbf{J} + \lambda \left(\alpha_r \mathbf{S}^t \mathbf{W}_r \mathbf{S} + \alpha_h \mathbf{S}^t \mathbf{L}_h^t \mathbf{L}_h \mathbf{S} + \alpha_v \mathbf{S}^t \mathbf{L}_v^t \mathbf{L}_v \mathbf{S} \right) \right]$$

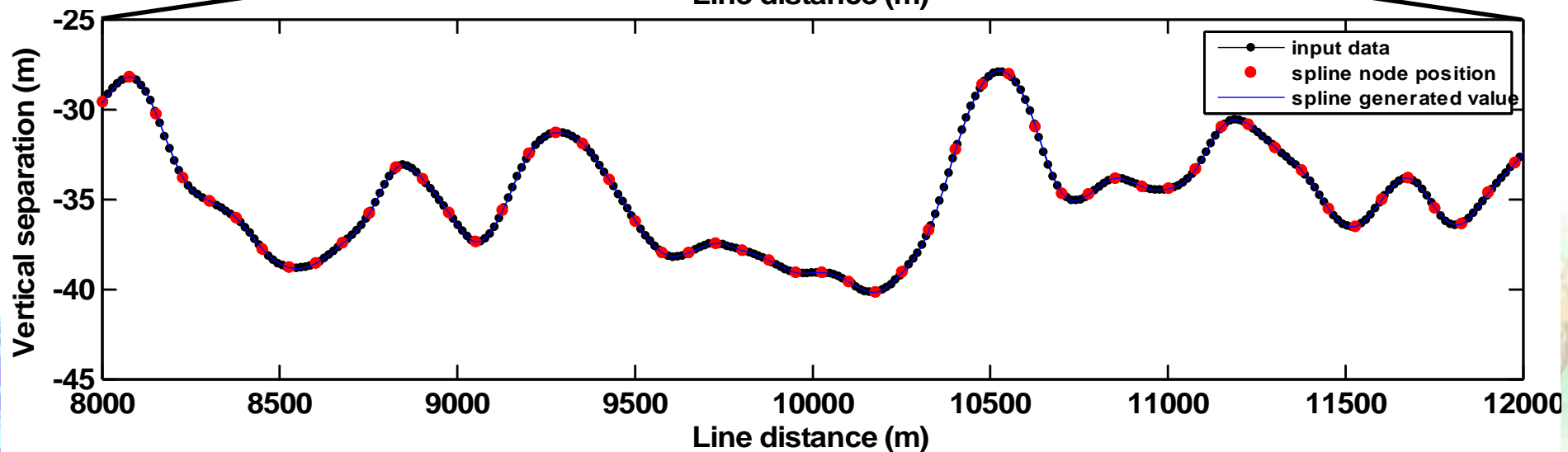
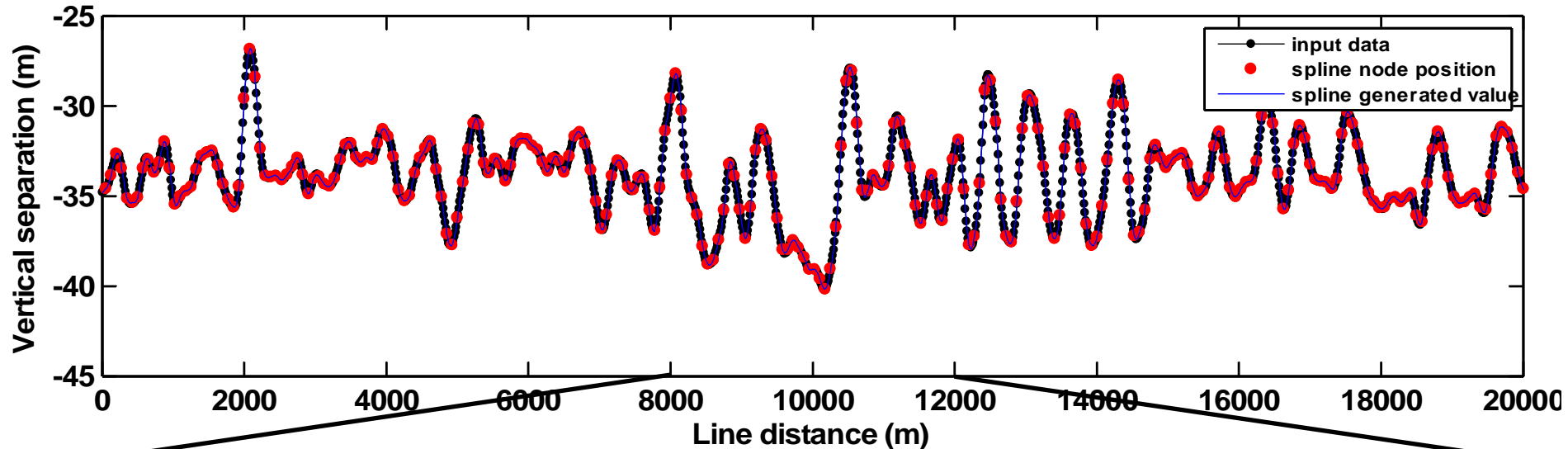
$$\mathbf{b} = \mathbf{J}^t \mathbf{W}_d \left[\mathbf{d}^{obs} - \mathbf{d}_n^{mod} + \mathbf{J}\mathbf{m}_n \right] + \lambda \mathbf{S}_t^t \mathbf{W}_r \mathbf{r}$$

Choosing a spline node spacing (D_x)



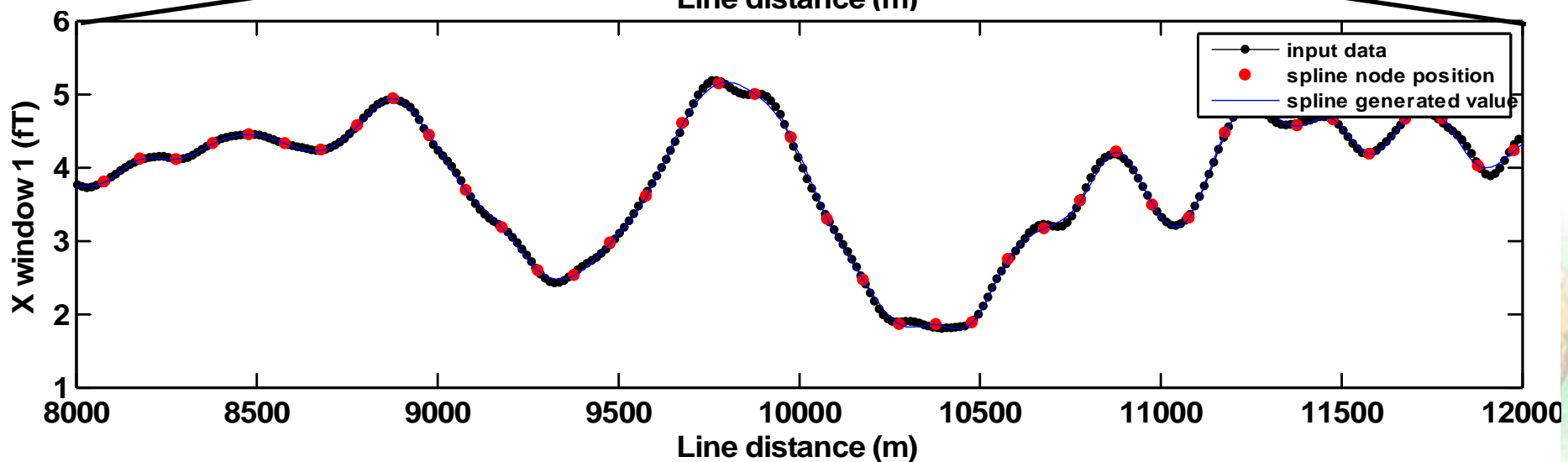
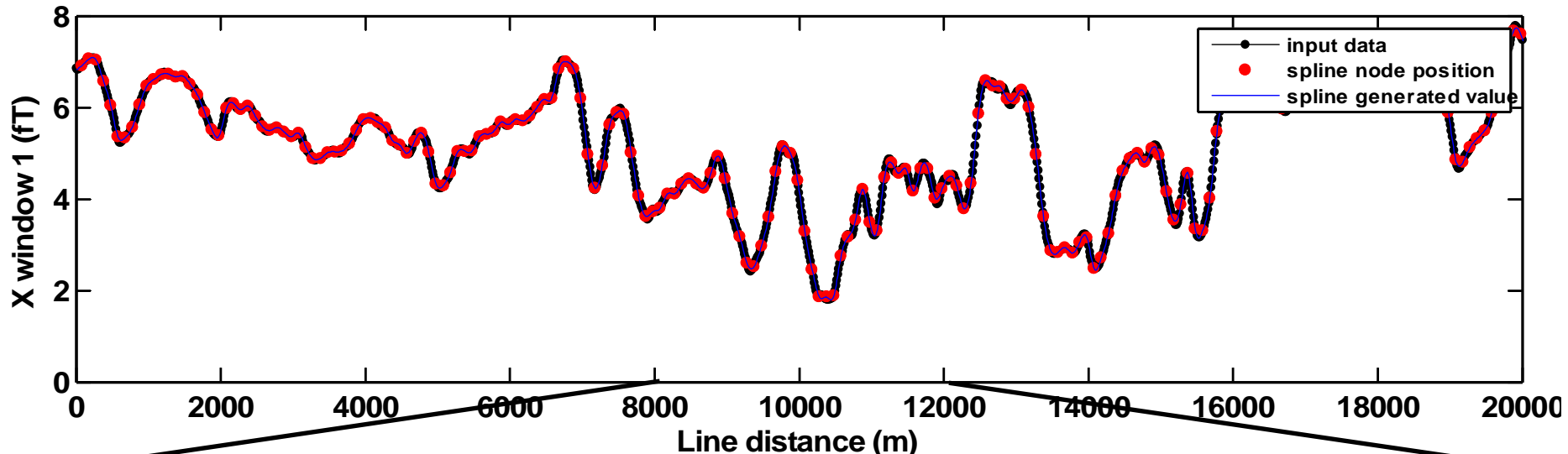
Choosing a spline node spacing (D_z)

Spline node spacing=75m Mean error=0.02 m Maximum error=0.16 m



Choosing a spline node spacing (σ)

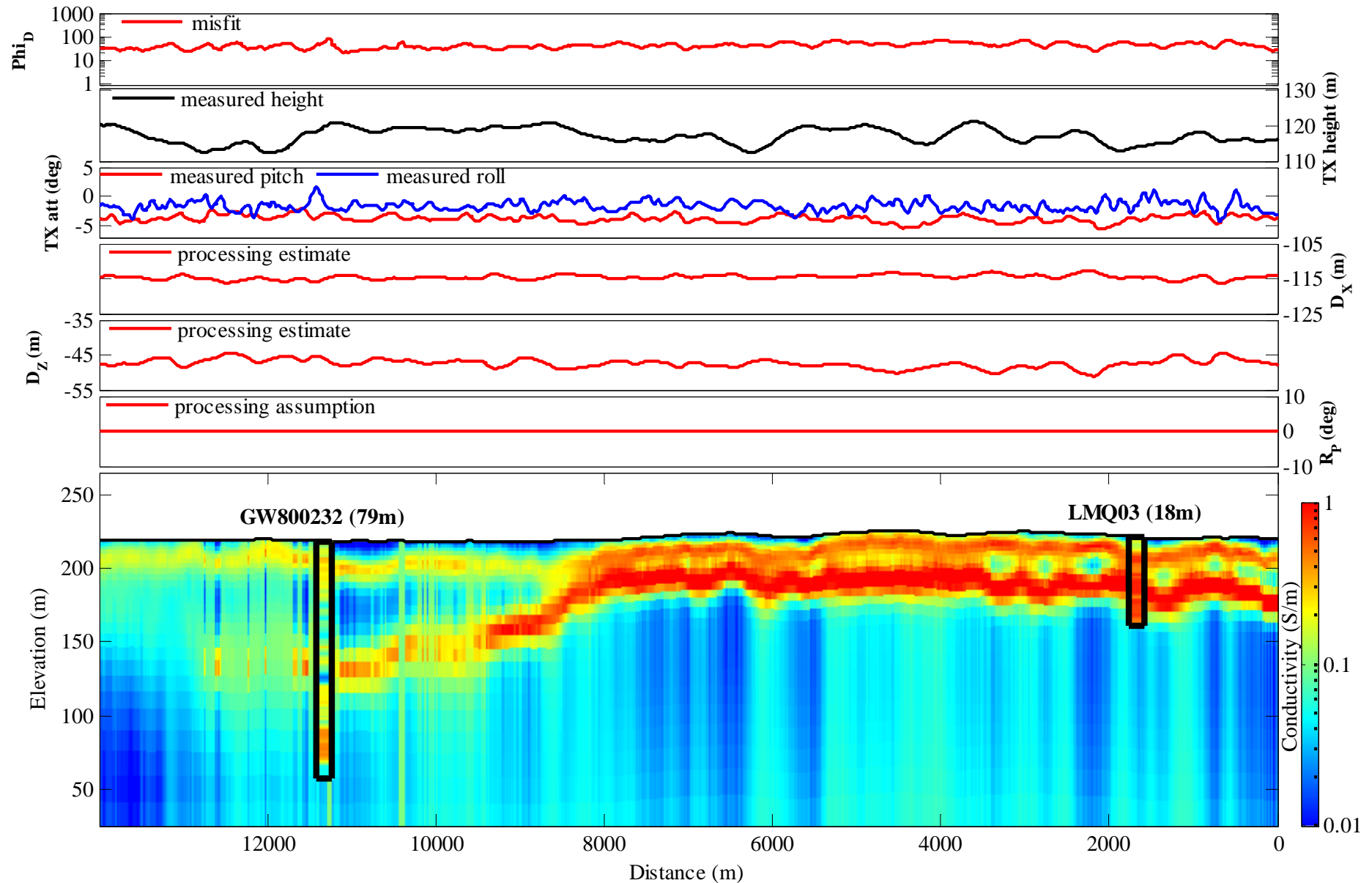
Spline node spacing=100m Mean error=0.44% Maximum error=2.31%



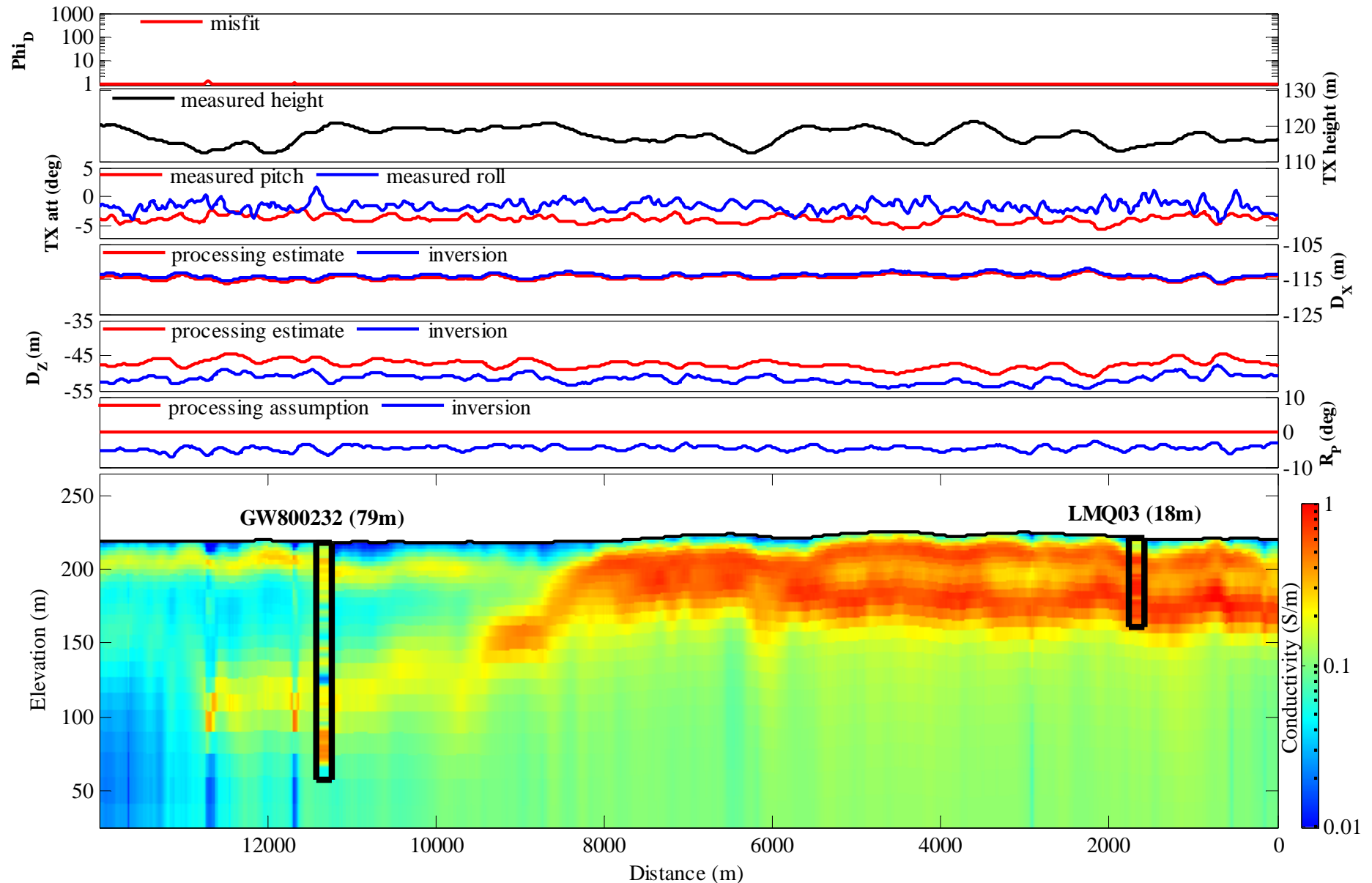
Lower Macquarie Example

- **2007 TEMPEST survey near Dubbo, NSW**
- **Total field X and Z component data inverted**
- **Occam's style vertically smooth model with 25 fixed thickness (2, 2.1, ..., 17.9m) layers**
- **0.1 S/m halfspace conductivity reference**
- **Processing estimates as geometry reference**
- **Nodes – conductivity 100m & geometry 75m**
- **Three comparative inversions run**
 - **Sample by sample – not solving for geometry**
 - **Sample by sample – solving for geometry**
 - **Line by line holistic – solving for geometry**

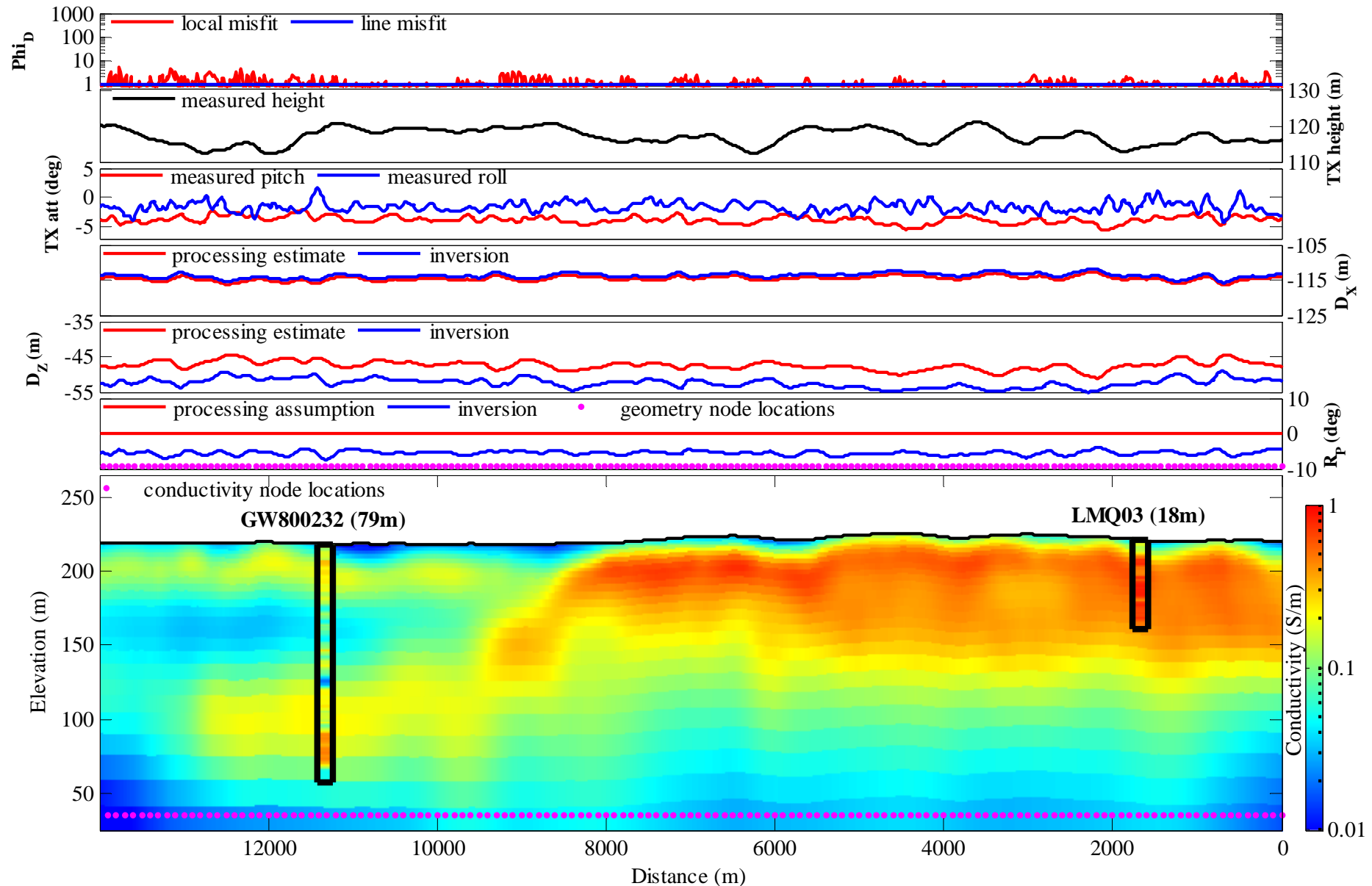
Sample by sample - not solving for geometry

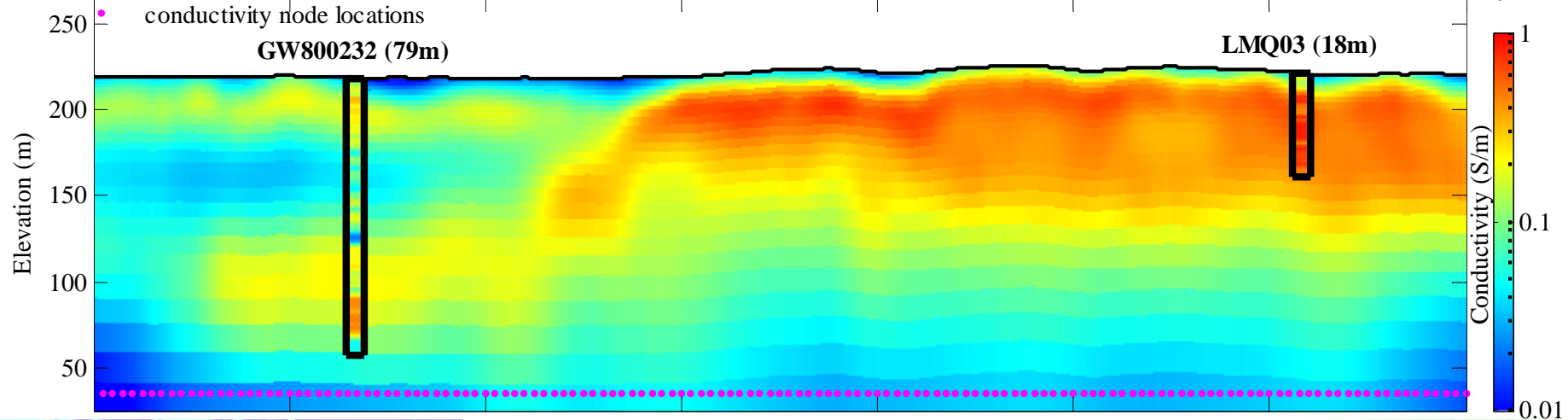
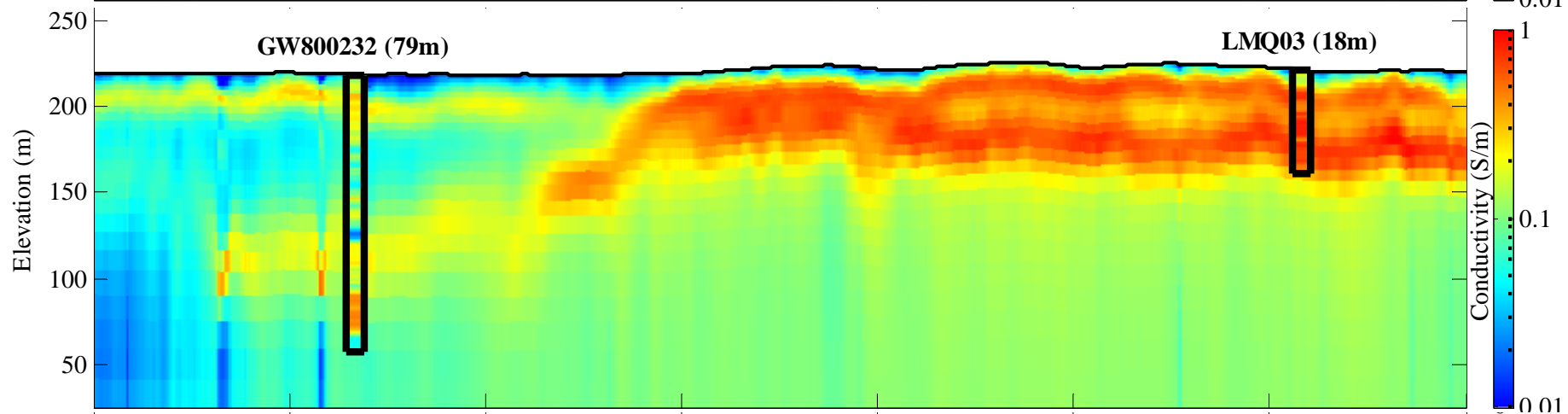
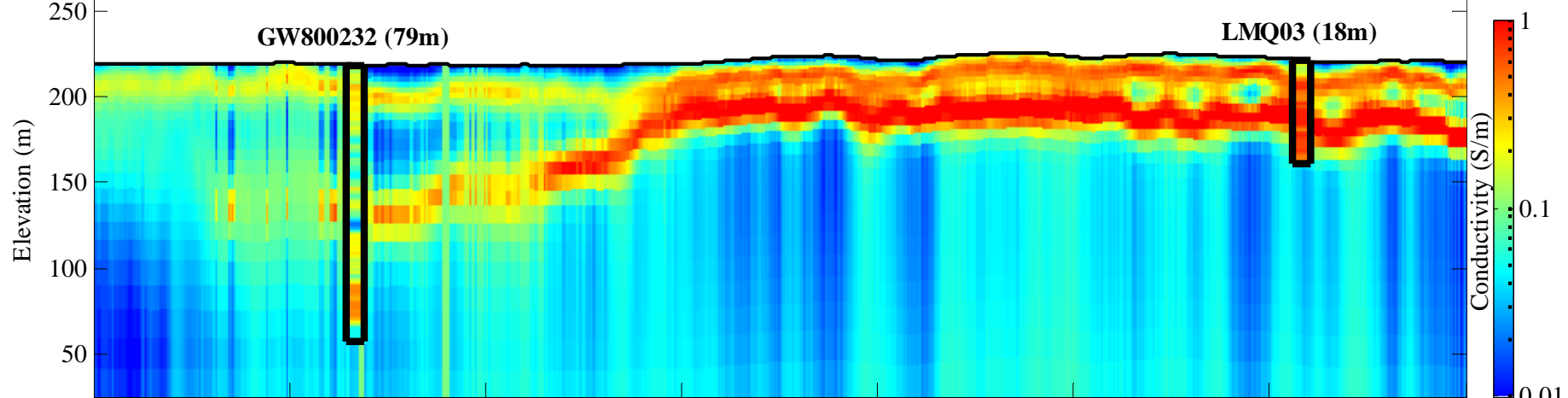


Sample by sample - solving for geometry



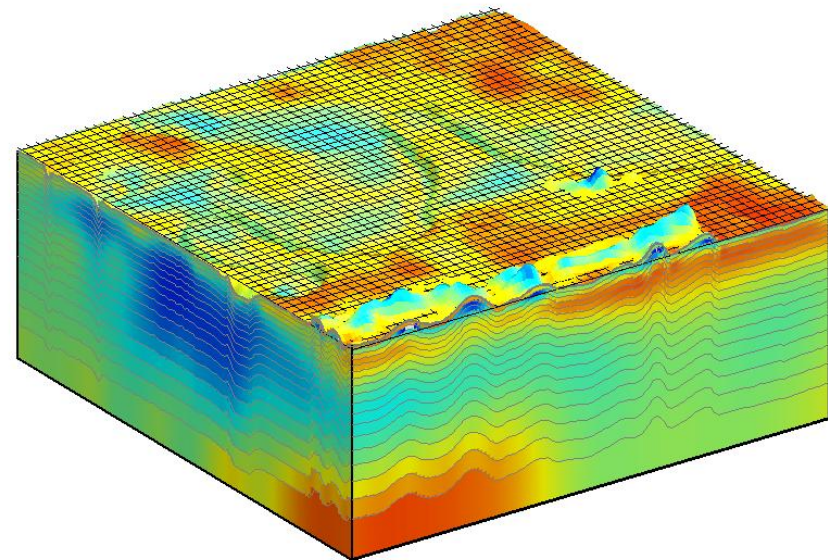
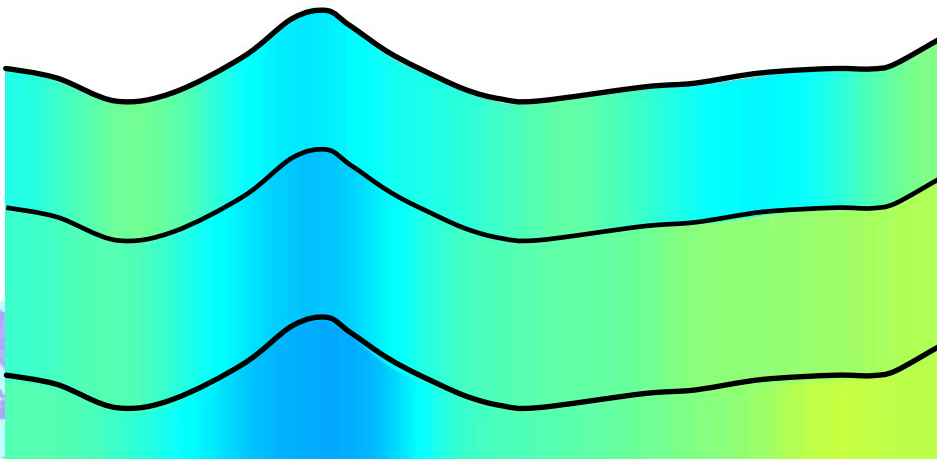
Holistic - solving for geometry





Future possibilities

- Include other types of “calibration” parameters – e.g. zero-level drift or gain
- Extend to spatial as in frequency-domain holistic inversion
- Hard constraints – e.g. downhole log & watertable



Conclusions

- **AEM data are not always what we think they are – we must do our best to simulate the real AEM system, not the theoretical one**
- **Solving for geometry allows data to be fitted**
- **Inverting whole lines takes advantage of expected spatial continuity of geology and system geometry**

Acknowledgements

- **Geoscience Australia for supporting the PhD research**
- **The Bureau of Rural Science for permission to use the Lower Macquarie downhole logs and AEM data**

