predictive mineral discovery*Cooperative Research Centre
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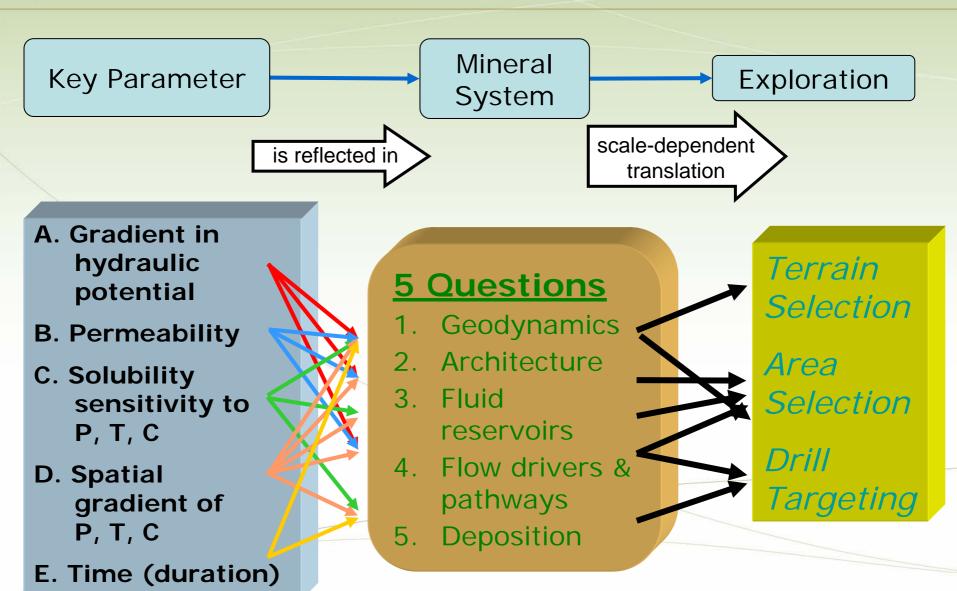
Enabling Technologies

Mechanical Modelling





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Deformation & Fluid Flow

Deformation exerts a crucial control on the permeability of a fluid-rock system.

Understanding deformation processes is essential to predict the permeability evolution of the system at conceptual and simulation level.

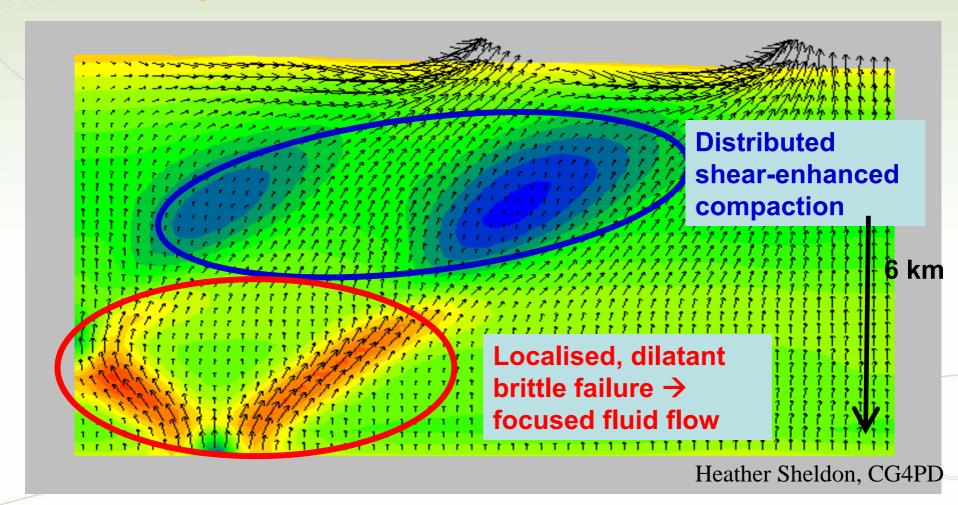
Existing and emerging structure define permeability structure through localisation and reactivation.

Compaction and dilation can be different responses to similar causes.

Fracturing and plastic dilation can occur in the same architecture because of different hydraulic regimes and different rock properties



Cam Clay Constitutive model



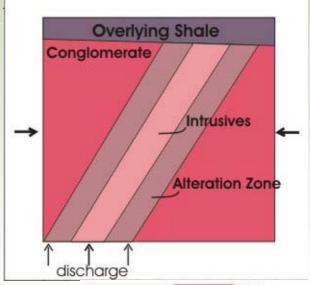
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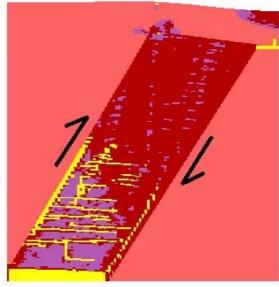
2 types of modelling

Conceptual models ('soft model')
little quantitative description
Initial understanding of the system
(behaviour and potential processes)

Numerical models
to test and improve this
understanding
Inputs may be tuned to satisfy the original
conceptual model
OR modify inputs to test new outcomes

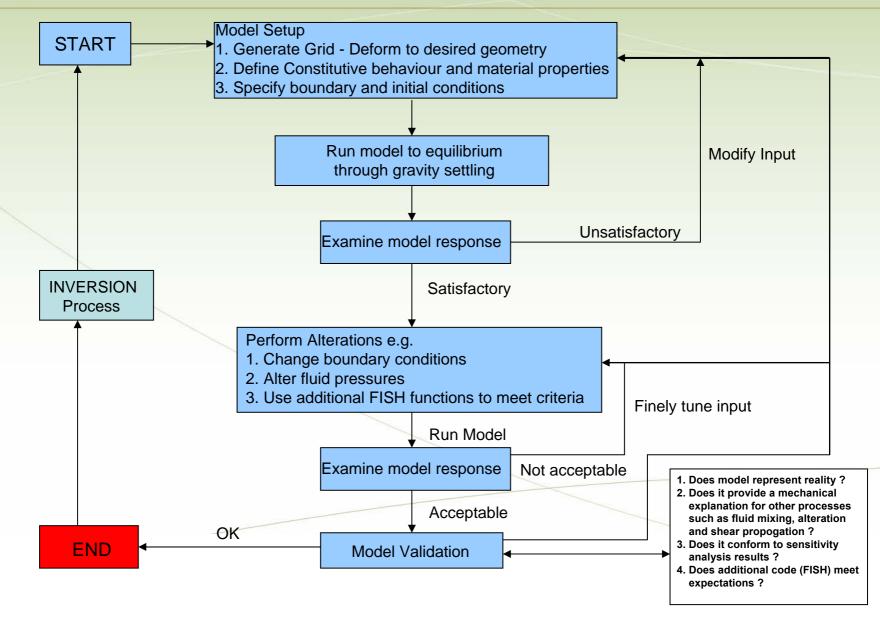
Iterative process: testing, validation and identifying key critical parameters







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2 Approaches

Continuum modeling (e.g. FLAC)

Smoothing of physical reality based on continuum mechanics Suitable for e.g. behaviour of geological material, porous media flow

Mohr-Coulomb for most rocks (other constitutive models Cam-Clay, Drucker-Prager)

- 1. Differential approach (finite difference)
- 2. Integral approach (finite element)

Discontinuum modeling (e.g. UDEC)

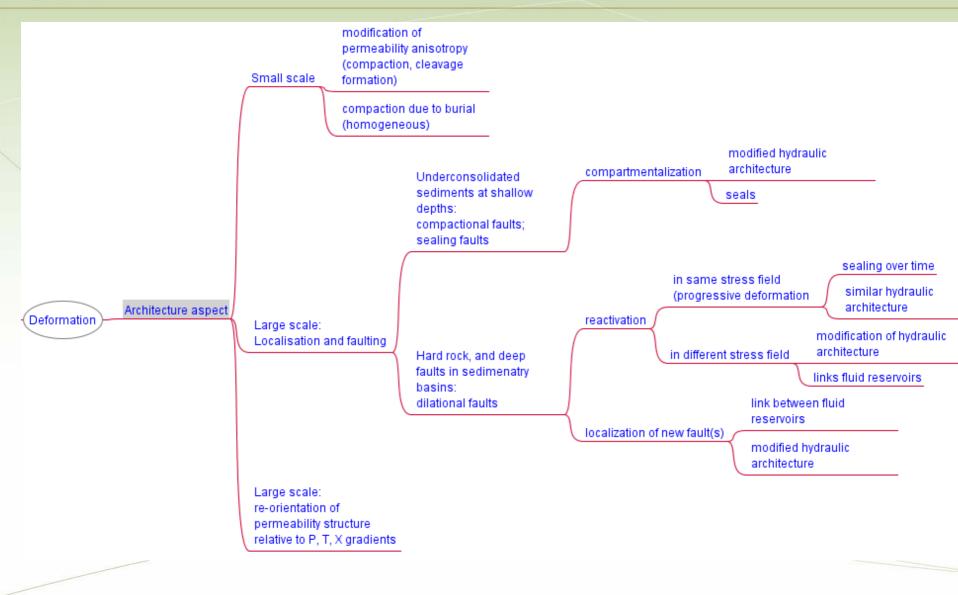
Modelling of interfaces or contacts between rigid bodies

- 1. Behaviour of discontinuities
- 2. Behaviour of the solid material
 - → rigid or deformable

Distinct element method



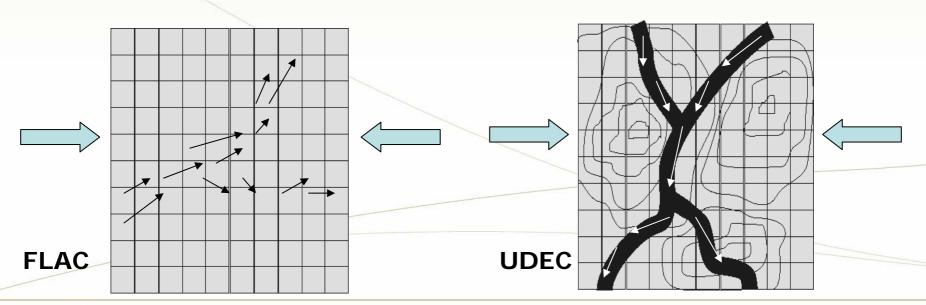
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Fluid flow in fractured rocks

- 1. Cracks are main permeability, rocks impermeable
- 2. Continuum approach, treats fractures by averages, determines bulk fractured rock permeability
- 3. Discontinuum approach, flow must be described relative to individual fractures or fracture sets





Some types of codes

Continuum codes:

Finite difference

Finite element

Distinct element codes

Particle codes

Computational Fluid Dynamics (CFD) codes

Particle in cell codes

Boundary element-finite element combinations

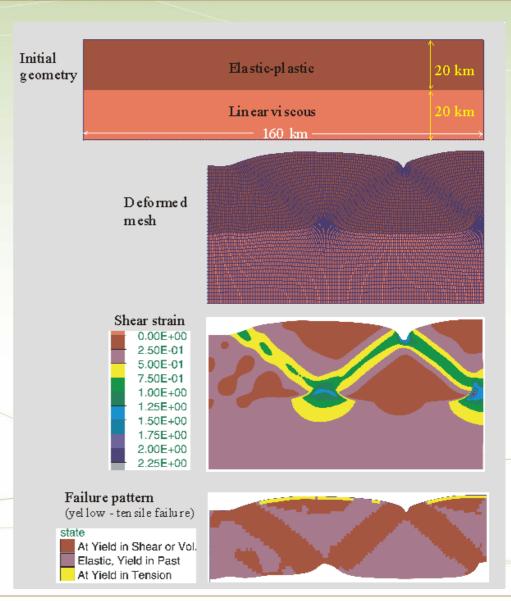
Reactor-style chemical codes

Reactive transport codes

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Continuum Models

A two-layer crust subject to horizontal shortening

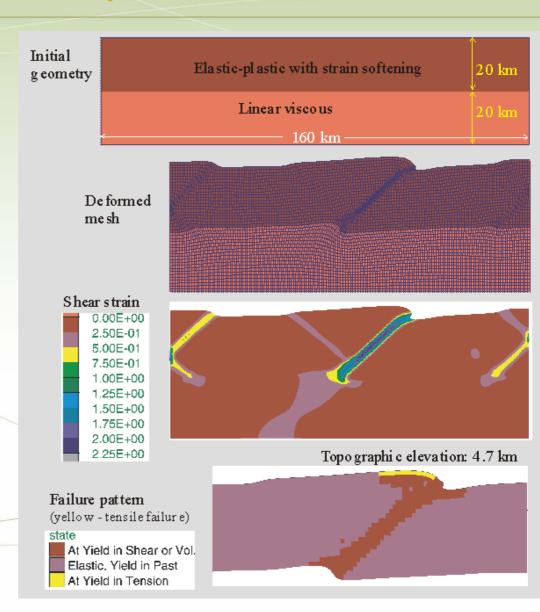


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Continuum Models

A two-layer crust subject to horizontal shortening

Strain softening is incorporated, which accelerated the development of one thrusting fault

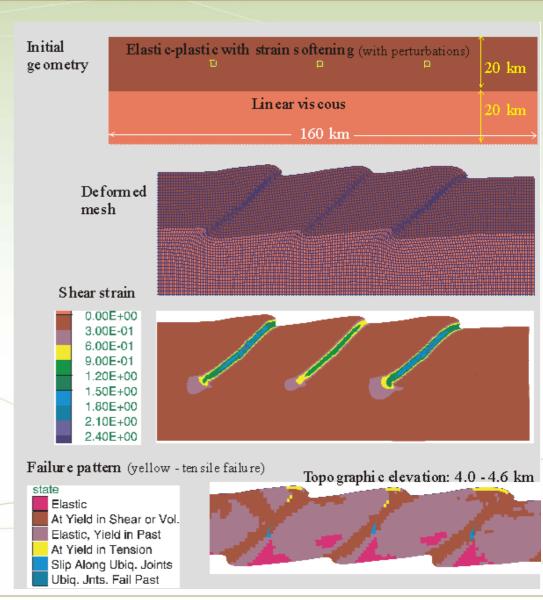


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Continuum Models

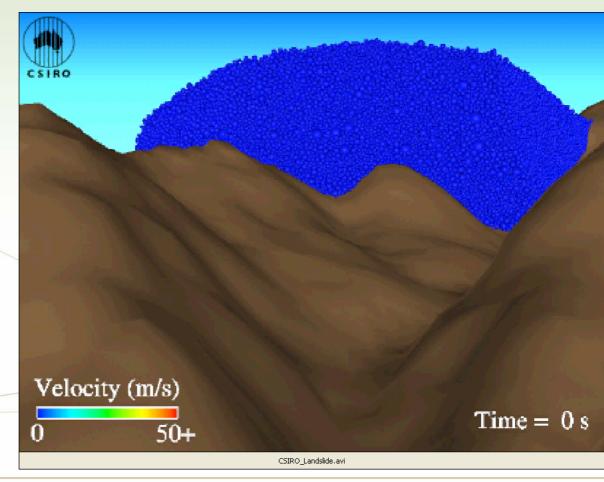
A two-layer crust subject to horizontal shortening

Strain softening is incorporated and initial mechanical perturbations are seeded in the model.



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FE, CFD & Particle Codes





Representative Elementary Volumes (REV's)

Darcy's law is a macroscopic relation

Volume must be large enough to represent a meaningful statistical average of the continuum (scale dependent)

→ large relative to the scale of microscopic heterogenity, but small relative to the entire domain of interest

How much volume of the material (e.g. fractures rock) is representative of the whole rock in a continuum sense?

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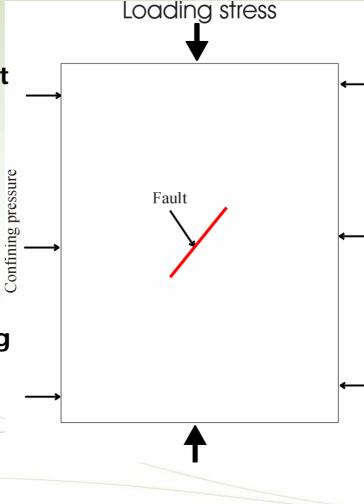
Stress Transfer Models

used to identify areas around a fault that have been brought closer to failure as a consequence of slip on that fault

"transferred" from the fault to the wall rocks (Fault slip produces a change in elastic strain, and hence a change in effective stress, in the rocks surrounding The fault.)

STM can tell us where deposits are located

(Suggests relationship between mineralisation and aftershocks)



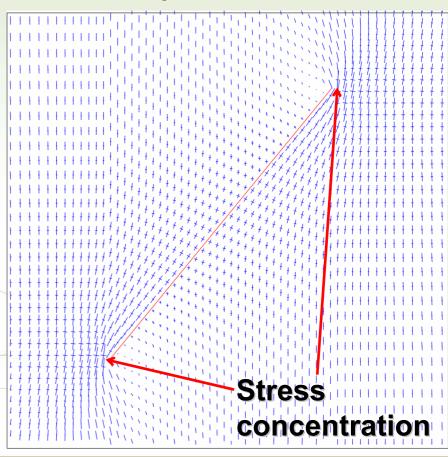


Stress Transfer Models

Distribution of displacement vectors near the fault

max. displacemen

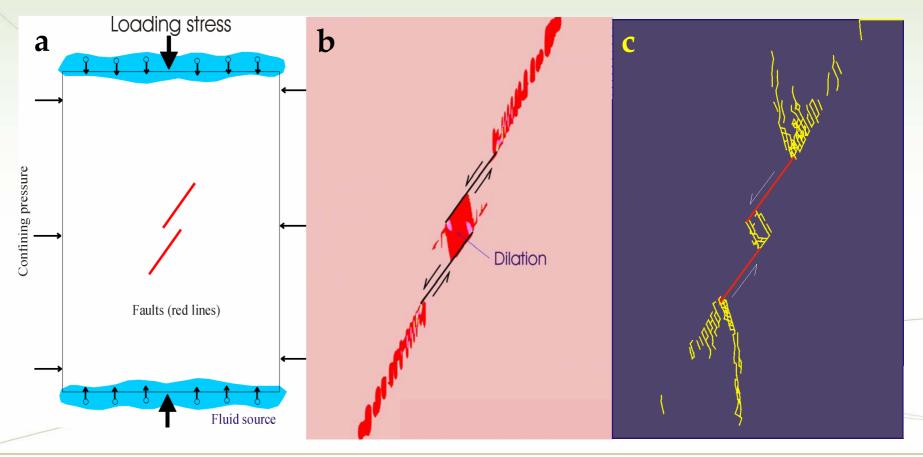
Principal stress vectors





Stress Transfer Models

Fault propagation and, dilatancy and vein formation

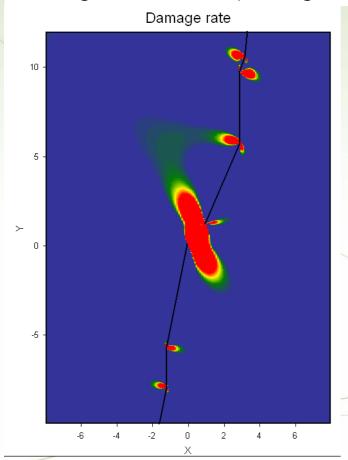




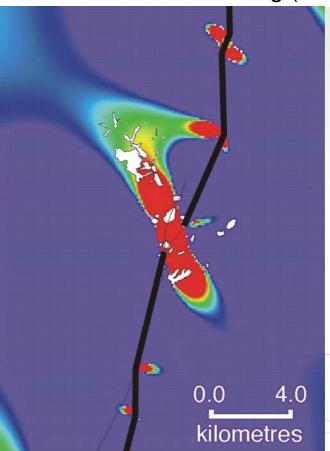
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Example

Damage mechanics (damage rate > 0)

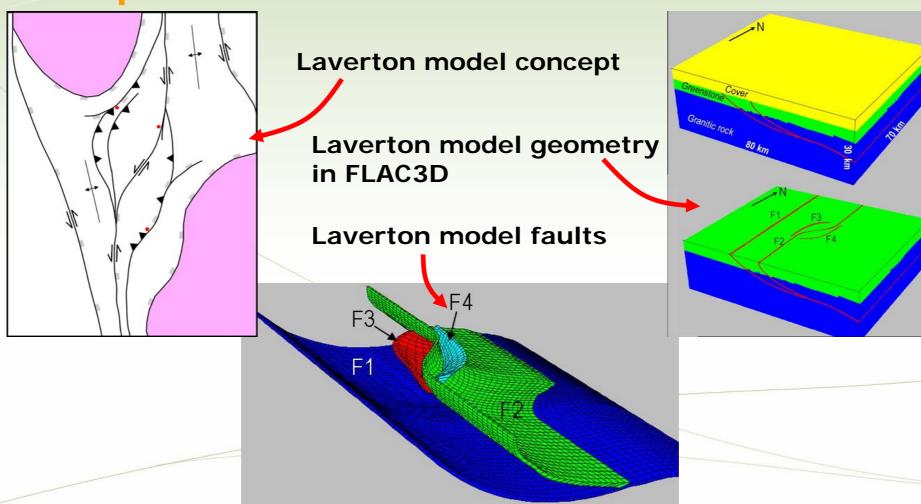


Stress Transfer Modelling ($\triangle CFS > 0$)



Micklethwaite & Cox 2006

Example Laverton



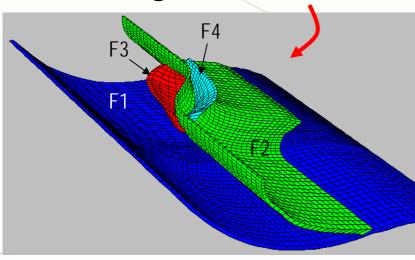


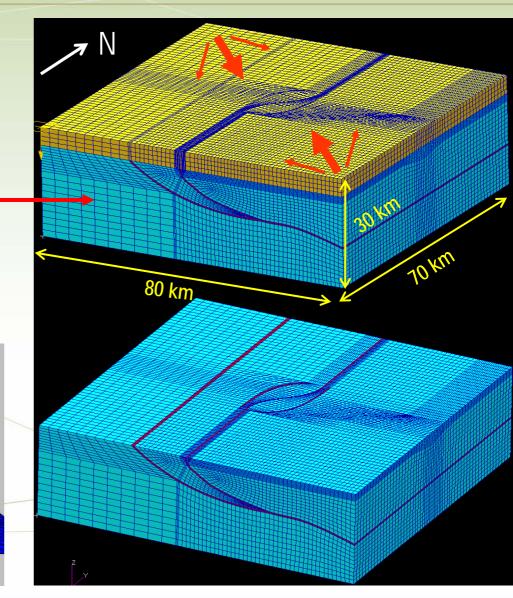
Example Laverton

A generic numerical model

The numerical mesh

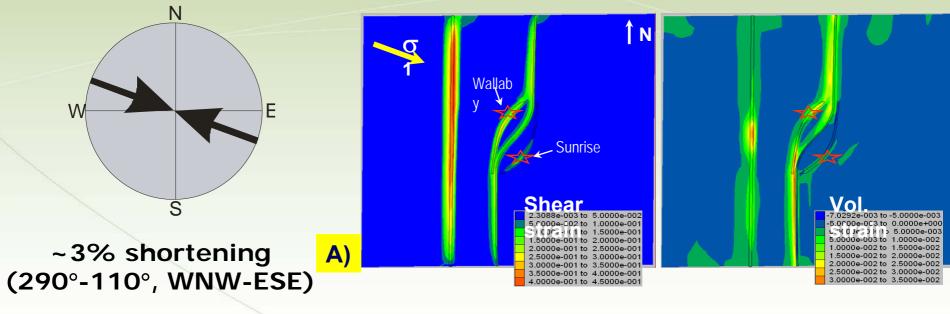
The model is explored for a range of far-field stress (shortening) orientations





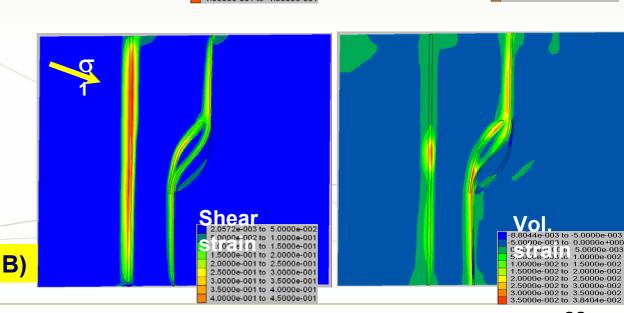


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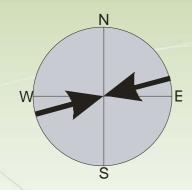
A), B) plan-views at 0.5 and 1.0 km below the top surface of greenstone

Greater shear and dilation localization at Wallaby than at Sunrise





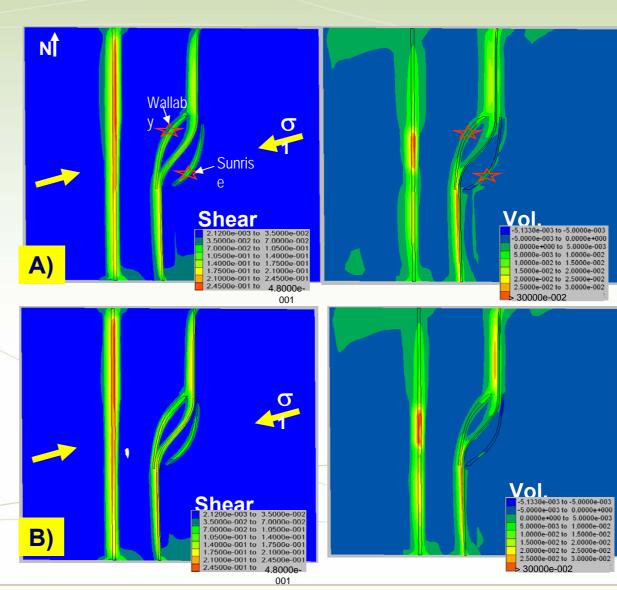
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~3% shortening (75°-255°, ENE-WSW)

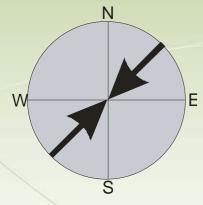
A), B) plan-views at 0.5 and 1.0 km below the top surface of greenstone

Faults through Wallaby and Sunrise sites show clear shear localization and also dilation – note less shear and dilation at Wallaby than in the NW-SE shortening case.





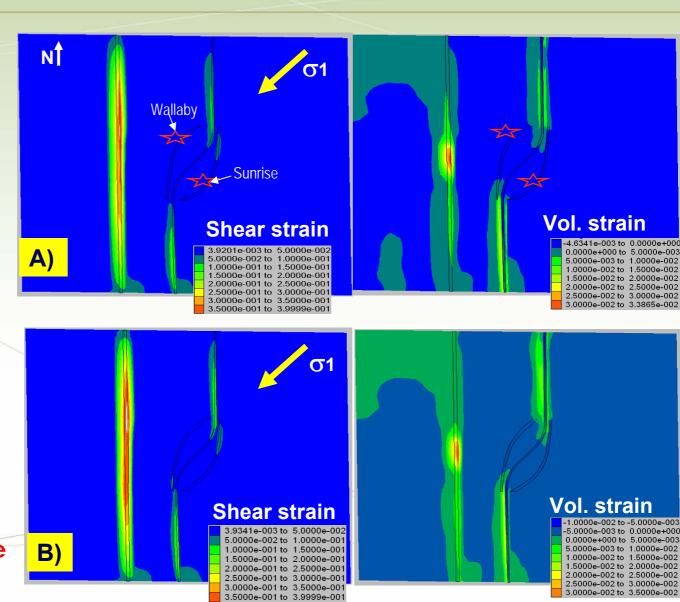
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~3% shortening (45°-225°, NE-SW)

A), B) plan-views at 0.5 and 1.0 km below the top surface of greenstone

No clear shear localization or dilations at both Wallaby and Sunrise sites





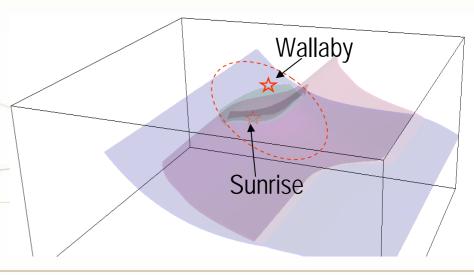
Example Laverton

Summary of key points

A wide range of possible shortening orientations from NW-SE to NNW-SSE seems to be clearly favourable for structural reactivation (Shear & dilation) of the Wallaby system and mineralization. Sunrise site also shows some shear localization and dilation under such conditions but to a much less degree.

A ENE-WSW shortening orientation (75 to 255 degree) led to enhanced shear and dilation at Sunrise. Wallaby now shows weakened activities.

Shortening orientations around NE-SW are unfavourable.



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MECHANICAL SIMULATIONS ARE USED TO SIMULATE THE DEFORMATION OF ROCKS UNDER STRESS. METHODS VARY ACCORDING TO PRESSURE, TEMPERATURE, AND SPATIAL AND TEMPORAL SCALE. FLOW DRIVEN BY DEFOEMATION DRIVEN CHANGE IN HYDRAULIC HEAD.

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