# From geological models to reservoir simulation

# Lincoln Paterson (CO2CRC/CSIRO) CAGS Technical Workshop 21 January 2010







# Modelling

- Modelling is used to:
  - design injection (location and number of wells, monitoring);
  - forecast the migration of injected carbon dioxide.
- Modelling can include:
  - coupled geochemistry;
  - coupled geomechanics;
  - tracer migration.
- Most modelling uses computer models;
  - Although analytical models are being developed.



#### **Computer models**

- Computer models usually:
  - solve the multiphase equations for fluid flow in porous media;
  - use finite-difference techniques for solving the flow equations;
  - require the simulated region to be broken up into grid blocks;
  - are based on techniques and code developed in the petroleum industry over several decades.



Darcy's law for fluid flow

$$\mathbf{q} = -\frac{k}{\mu} (\nabla p - \rho \mathbf{g})$$

$$\nabla p = \frac{\partial p}{\partial x} + \frac{\partial p}{\partial y} + \frac{\partial p}{\partial z}$$

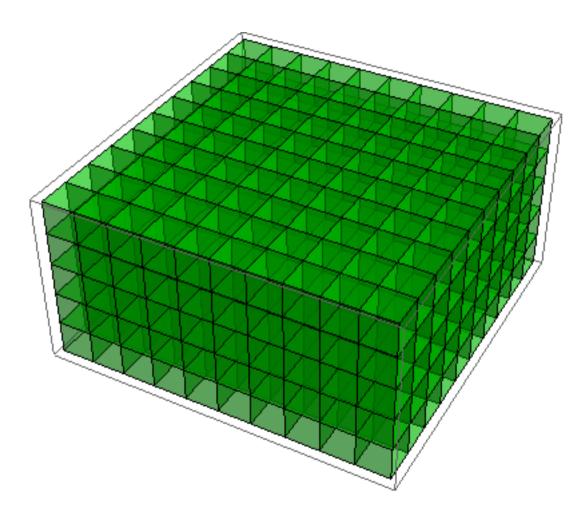


#### **Finite-difference** approximation

$$\frac{\partial p}{\partial x} \longrightarrow \frac{\Delta p}{\Delta x} = \frac{p_{i+1} - p_i}{x_{i+1} - x_i}$$

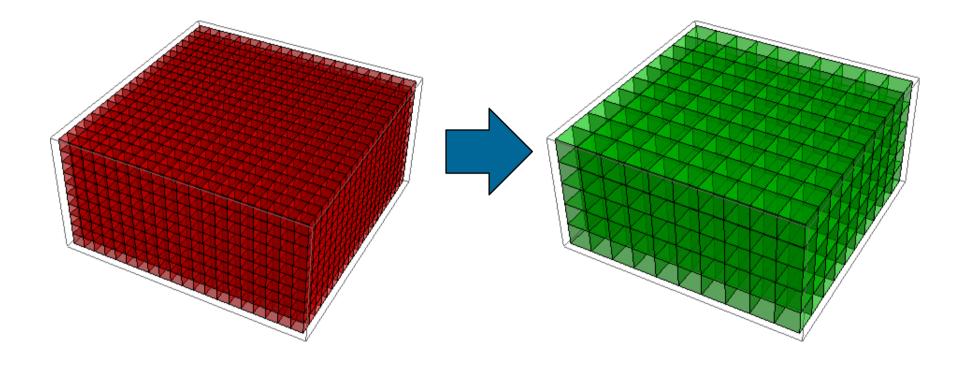


# **Simulation grid**





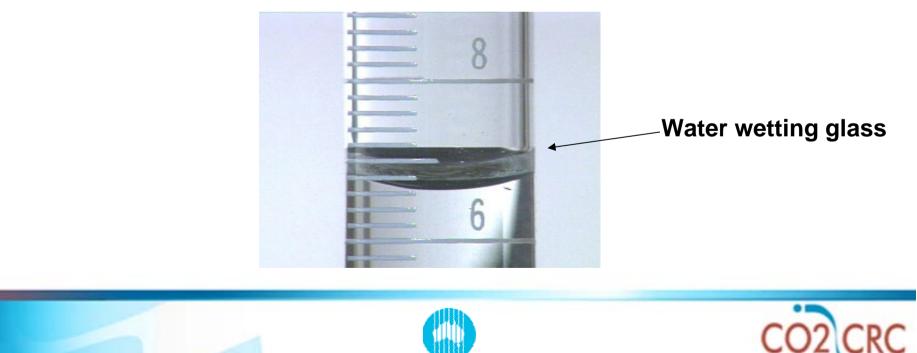
# Upscaling





#### **Two-phase immiscible flow terminology**

- Drainage two-phase flow with CO<sub>2</sub> displacing brine where the brine preferentially contacts (wets) the rock surfaces.
- Imbibition two-phase flow with brine displacing CO<sub>2</sub> where the brine preferentially contacts the rock surfaces.
- Relative permeability in two-phase flow, the reduction in effective permeability due to the presence of the other fluid.



# **Multiphase flow equations**

$$\mathbf{q}_{\mathbf{w}} = -\frac{kk_{rw}}{\mu_w} (\nabla p_w - \rho_w \mathbf{g})$$

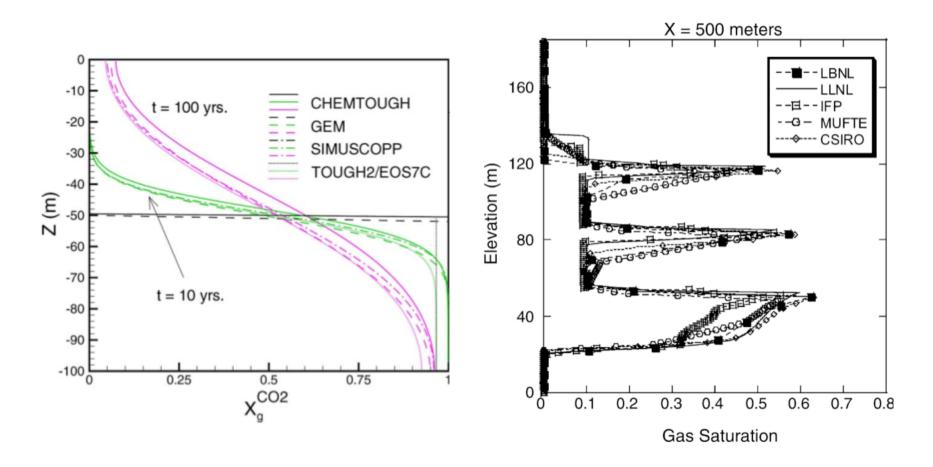
$$\mathbf{q_{nw}} = -\frac{kk_{rnw}}{\mu_{nw}}(\nabla p_{nw} - \rho_{nw}\mathbf{g})$$

$$\phi \frac{\partial S_w}{\partial t} + \nabla \mathbf{q_w} = 0 \qquad \qquad S_w + S_{nw} = 1$$

$$\phi \frac{\partial S_{nw}}{\partial t} + \nabla \mathbf{q_{nw}} = 0 \qquad p_c = p_{nw} - p_w$$



#### **Code comparison**



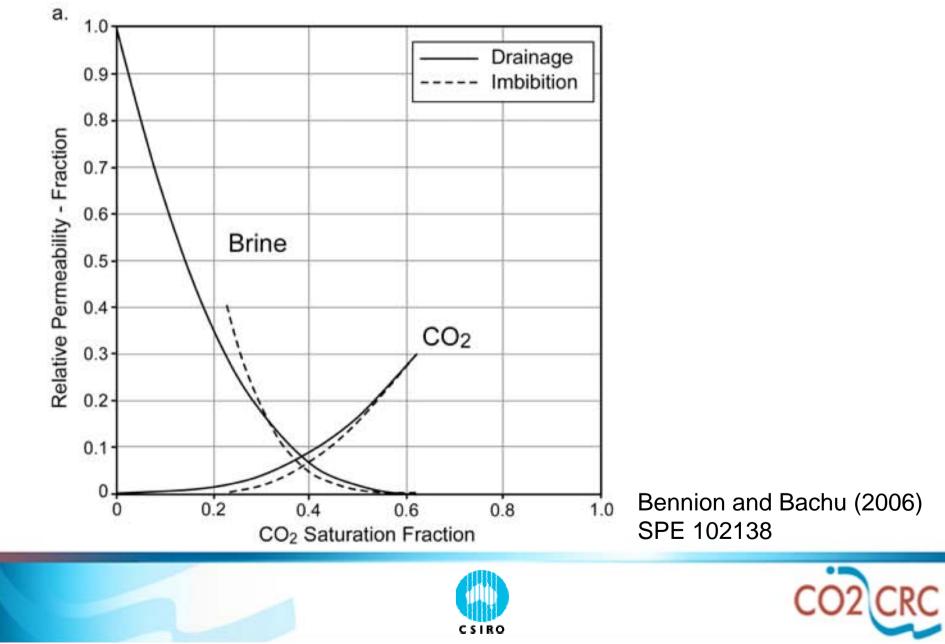


# Models used in Class et al. 2009 comparison

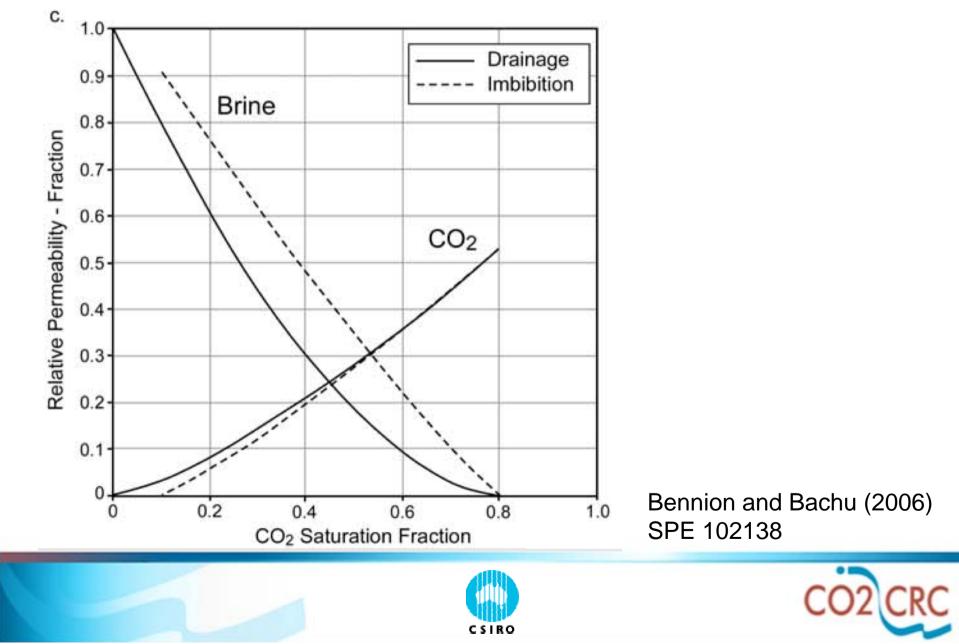
Name of code/model	Applying institution	Participation in problem(s)	Discretisation	
			In space	In time
COORES	IFP	1.1, 1.2, 2.1, 2.2, 3.1	FV	Implicit
DuMux	Uni. Stuttgart	1.1	BOX	Implicit
ECLIPSE	Schlumberger, Heriot-Watt Uni.	1.1, 1.2, 2.1, 2.2, 3.1, 3.2	IFDM	Implicit
FEHM	LANL	1.1, 1.2	CVFE	Implicit
GEM	Heriot-Watt Uni.	3.1, 3.2	IFDM	Implicit
GPRS	Stanford Uni.	3.1, 3.2	FV	Implicit
IPARS-CO2	CSM Uni. Texas	1.1, 2.1, 2.2 3.1	Mix. FEM	Impl. pressure expl. conc.
MoReS	Shell	3.1, 3.2	IFDM	Implicit
MUFTE	Uni. Stuttgart	1.1, 1.2, 2.1 2.2, 3.1	BOX	Implicit
ROCKFLOW	BGR	1.1, 1.2	FE	Implicit
RTAFF2	BRGM	1.2	FEM	Implicit
ELSA	Uni. Bergen/Princeton	1.1		-
TOUGH2	CSIRO, BRGM, RWTH Aachen	1.1, 2.1, 2.2 3.1	IFDM	Implicit
VESA	Princeton Uni.	1.1, 3.1, 3.2	FD, vertic. averaged	Impl. pressure expl. interface



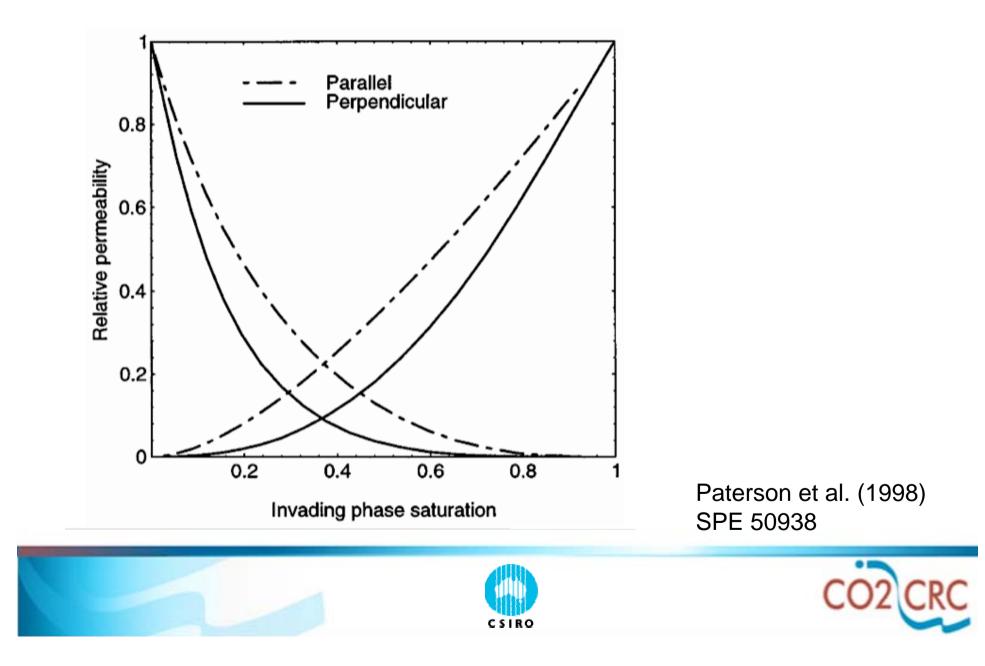
#### **Relative permeability**



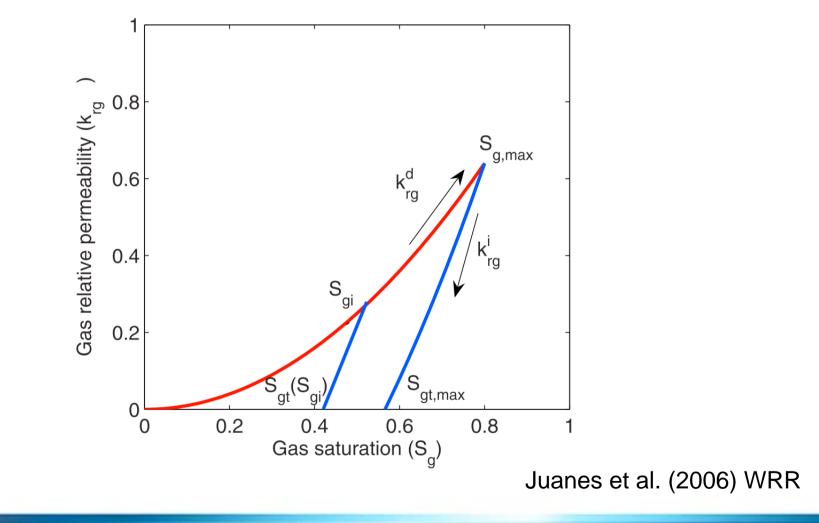
#### **Relative permeability**



#### **Relative permeability can depend on direction**



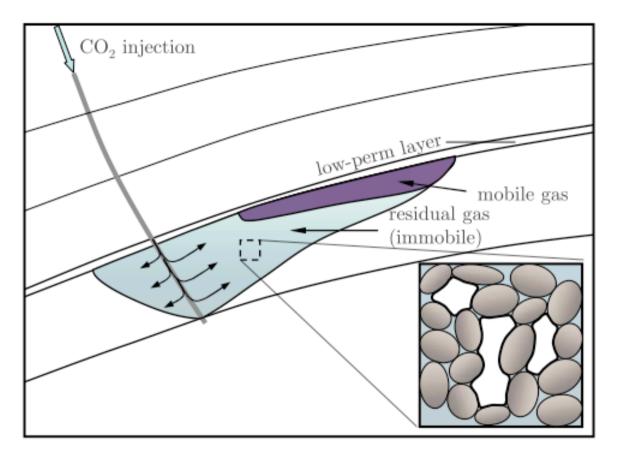
#### **Relative permeability hysteresis**







# **Residual capillary trapping**

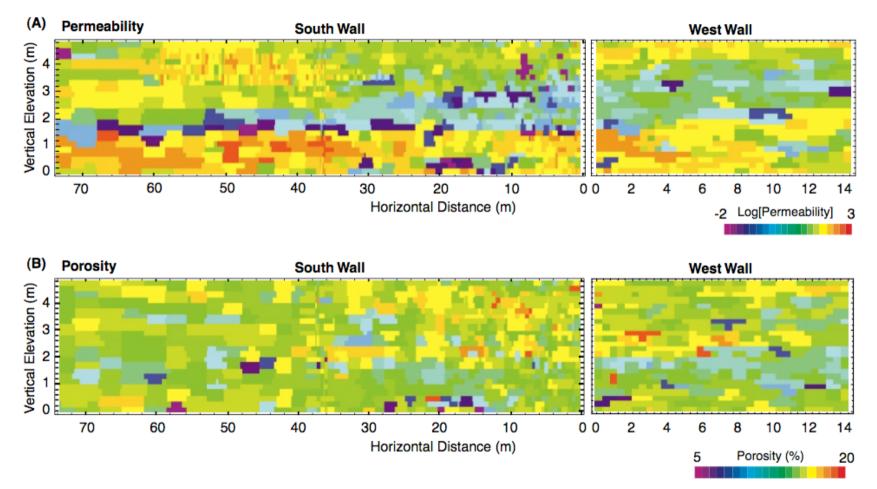


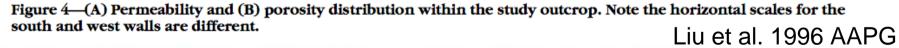
**Figure 1.** Schematic of the trail of residual  $CO_2$  that is left behind because of snap-off as the plume migrates upward during the postinjection period.

Juanes et al. (2006) WRR



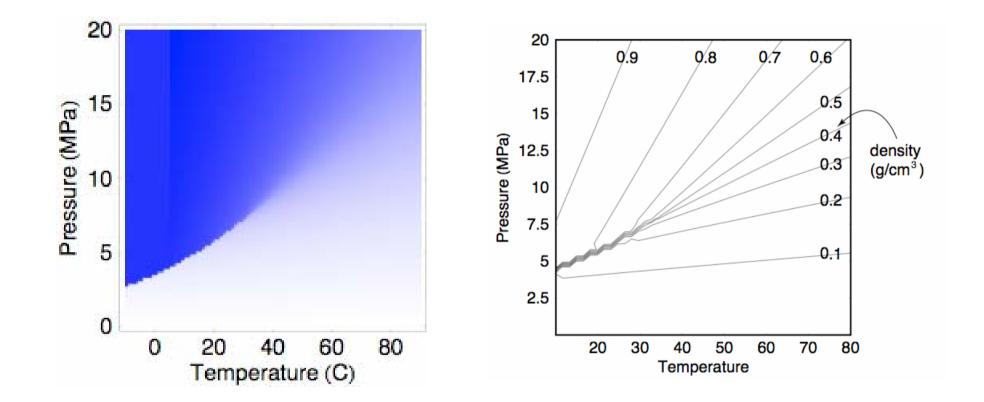
#### **Permeability and porosity**







#### **Carbon dioxide density**





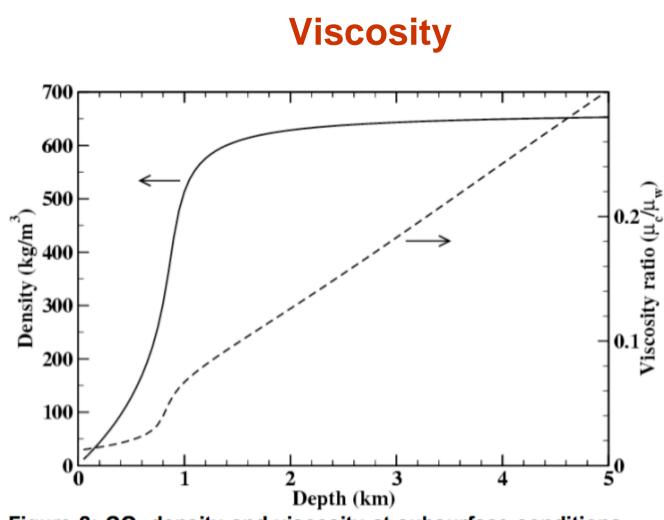
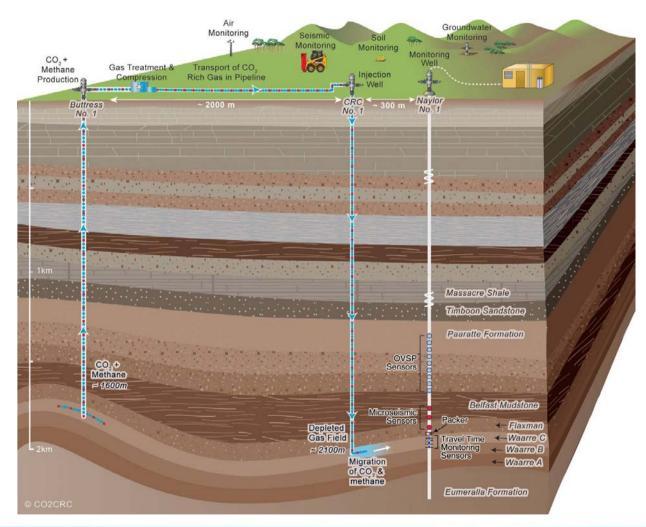


Figure 2: CO<sub>2</sub> density and viscosity at subsurface conditions, surface temp. 15 C, 30 C/km and 10 MPa/km.

Ennis-King & Paterson 2002 SPE 77809

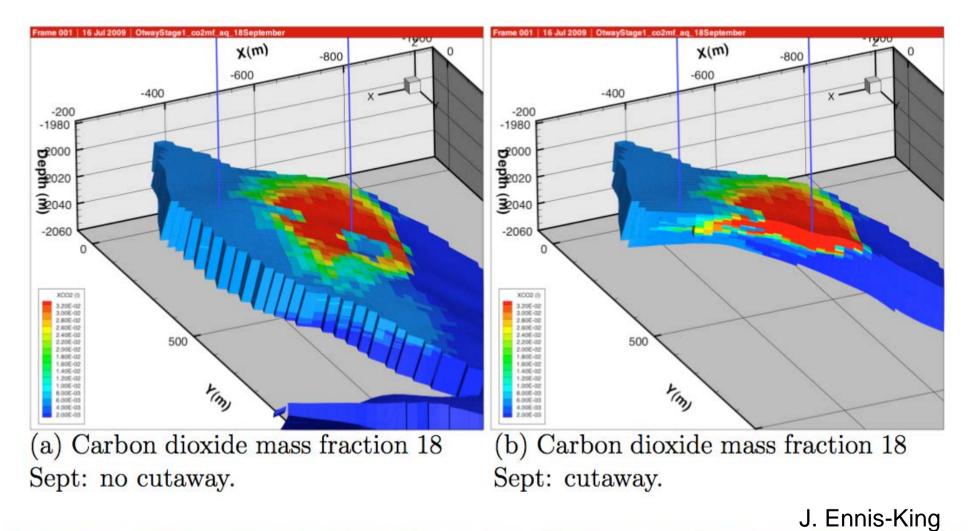


#### **CO2CRC Otway Project**



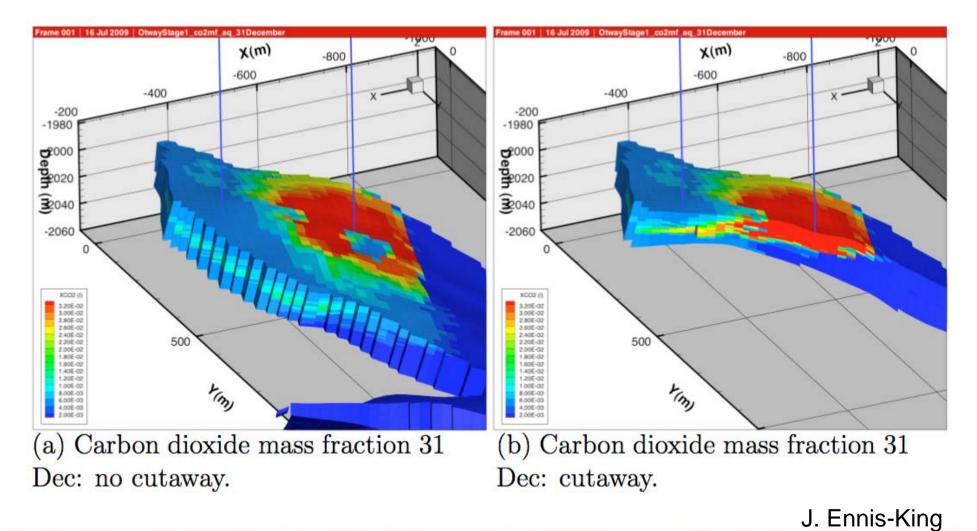


#### **CO2CRC** Otway project: CO<sub>2</sub> mass fraction



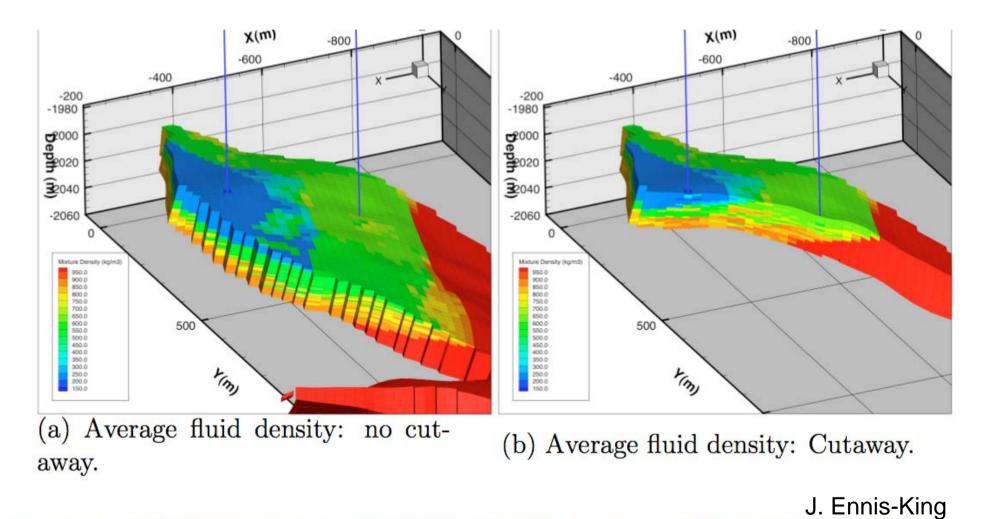


#### **CO2CRC Otway project: CO<sub>2</sub> mass fraction**



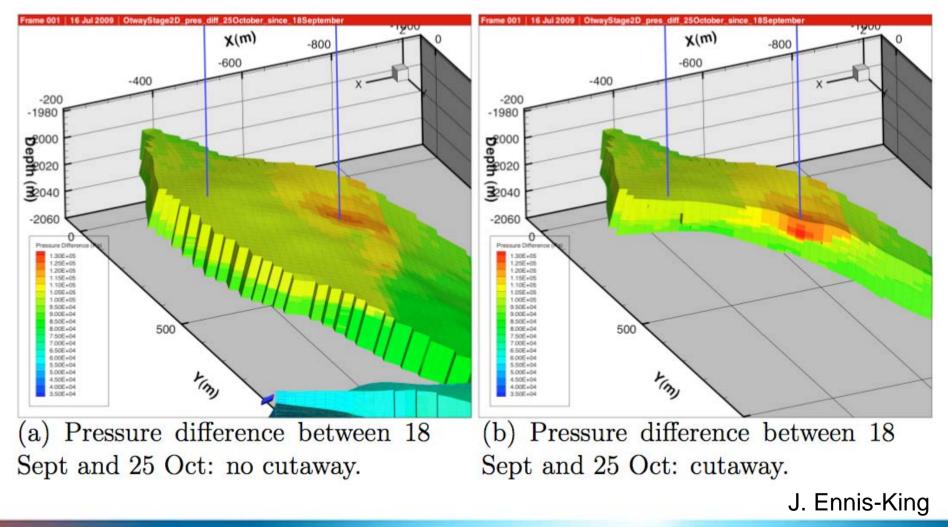
CO2 CRC

#### **CO2CRC** Otway project: total fluid density





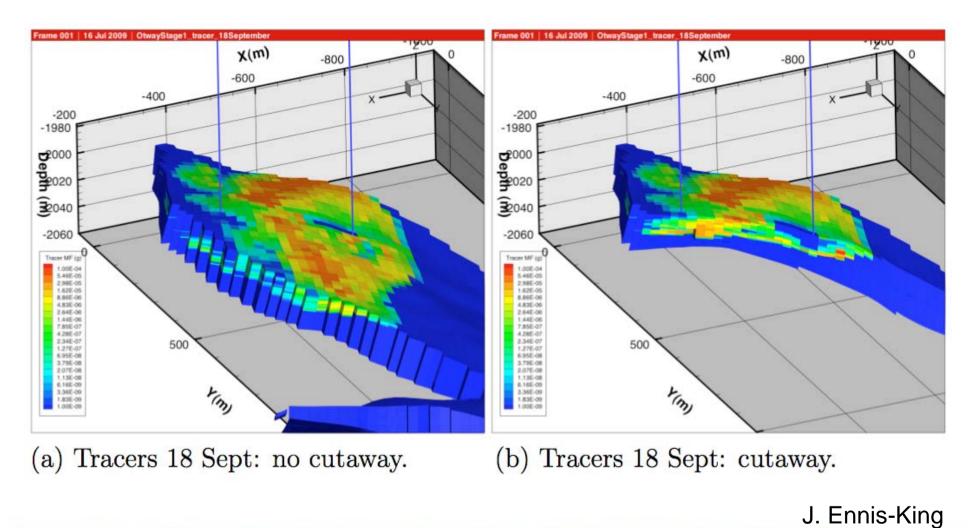
#### **CO2CRC Otway project: pressure difference**



CSIRO

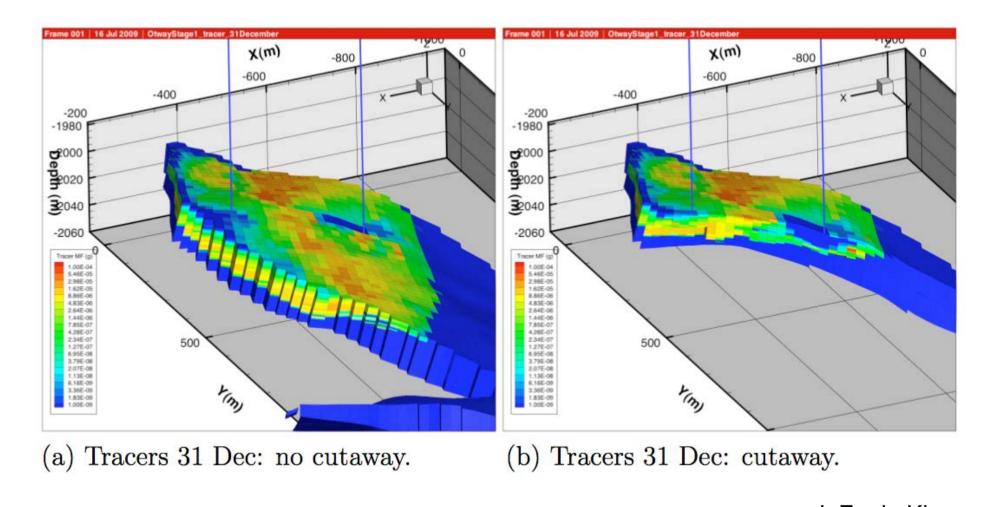


#### **CO2CRC Otway project: tracers**





#### **CO2CRC Otway project: tracers**





# Simulation input and output

- Input:
  - Static model (permeability, porosity, fault boundaries...)
  - Dynamic properties (relative permeability, capillary pressure)
  - Initial conditions (pressure, temperature,...)
  - Boundary conditions (aquifer drive, ...)
  - Flow rates at wells
- Output:
  - Maps of pressure, fluid saturation, ....
  - Tracer concentration (if implemented)
  - Dissolved components (if implemented)
  - Chemical reaction products (if implemented)
  - Stress and strain (if implemented in a geomechanical model)



#### **Dissolution and convection**

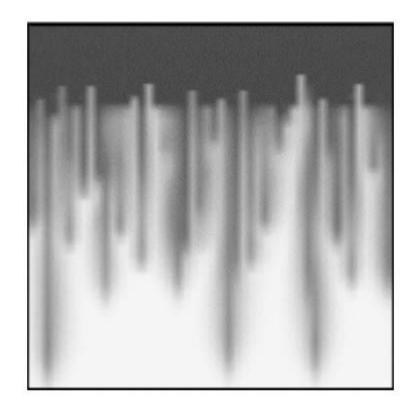
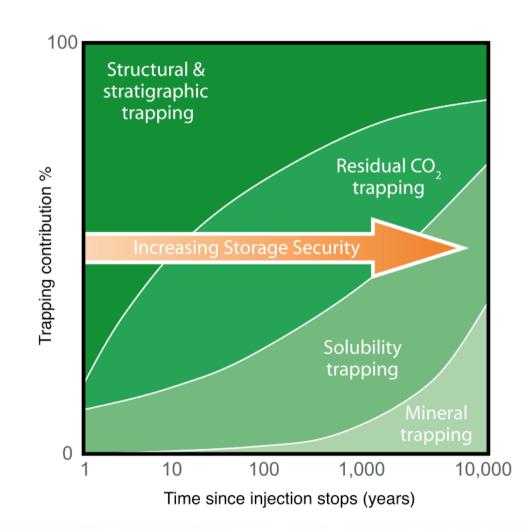


Fig. 5—Distribution of dissolved  $CO_2$  for  $k_v/k_h=0.1$  after 2,100 years. The width of simulation cell is 500 m. The full width is shown in this figure, but only the top 80 m vertically.

Ennis-King & Paterson 2005 SPE J

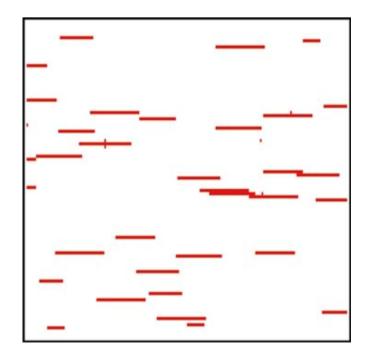


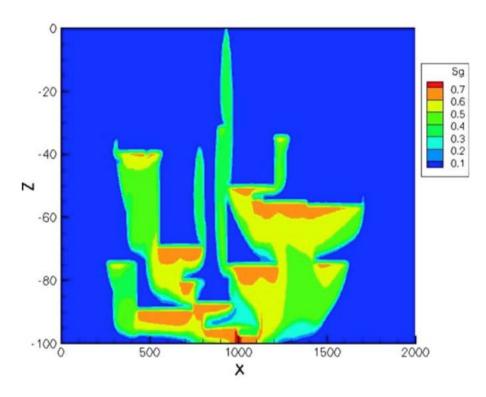
### **Trapping mechanisms over time**





#### **Upscaling vertical permeability**





Green & Ennis-King, TiPM, 2009





# Conclusions

- Modelling is a useful tool in the design of carbon dioxide storage projects.
- Modelling depends on the quality of the data and the skill of the user (old saying: garbage in, garbage out).
- In the right hands with correct questions it can provide powerful answers.



#### **CO2CRC** Participants



Supporting participants: Supporting participants: Department of Resources, Energy and Tourism CANSYD | Meiji University Process Group | University of Queensland | Newcastle University | U.S. Department of Energy | URS

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