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EARTH SOUNDING

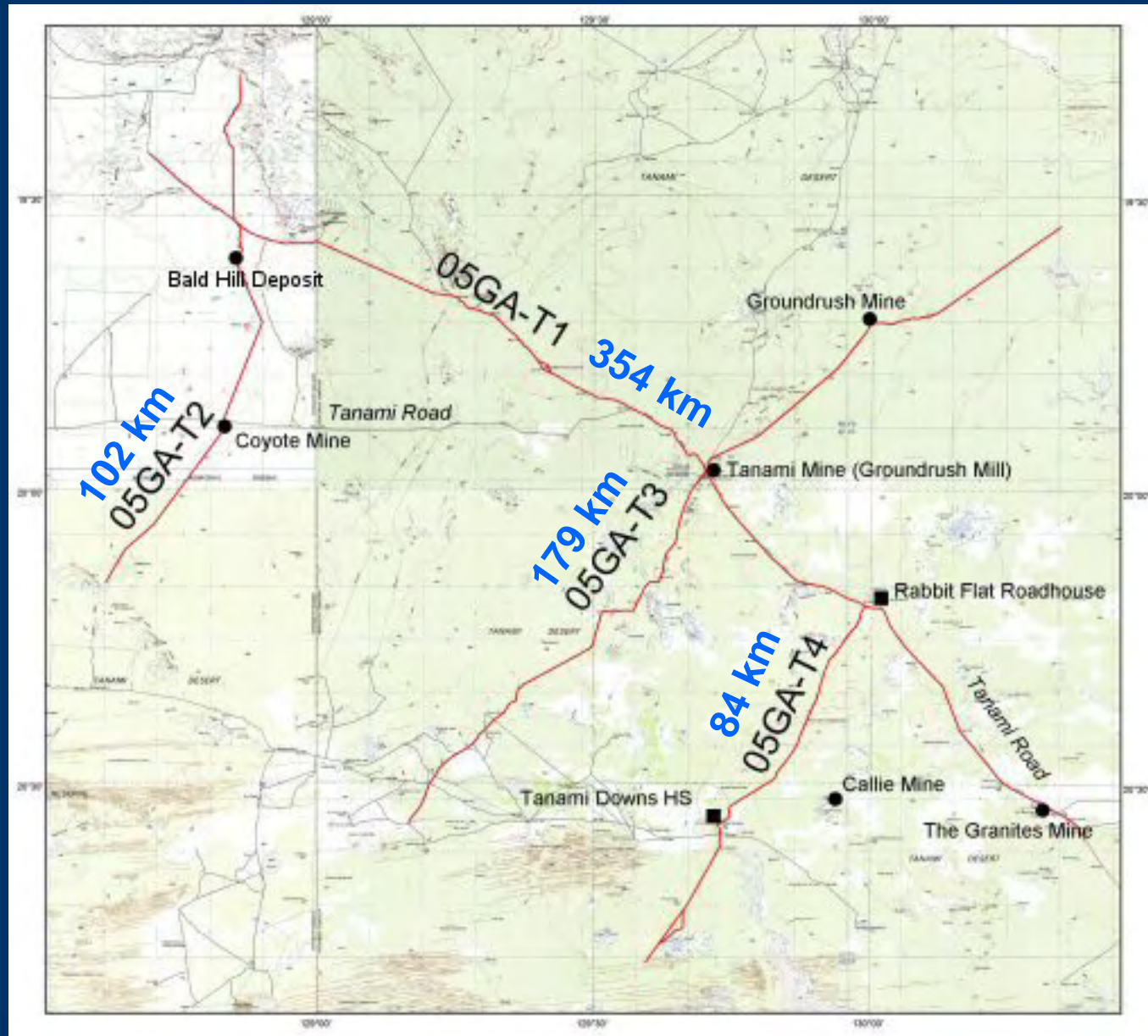
2005 TANAMI SEISMIC SURVEY: Acquisition, Processing & Pitfalls

Leonie Jones & Bruce Goleby

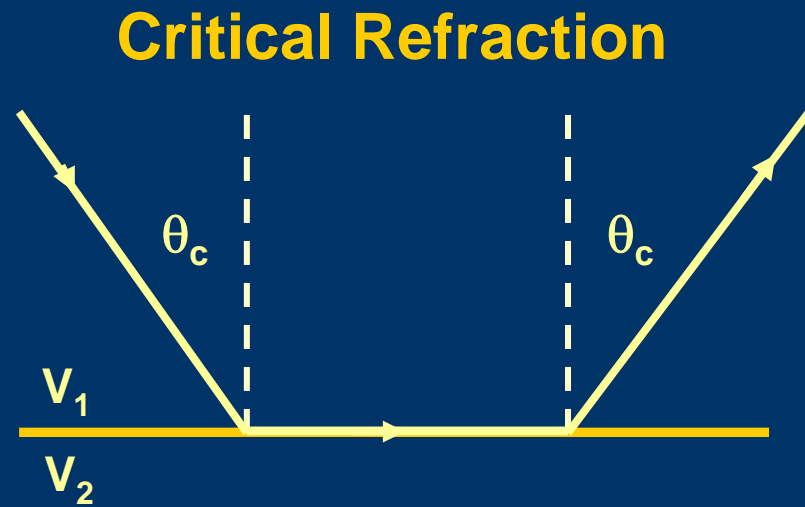
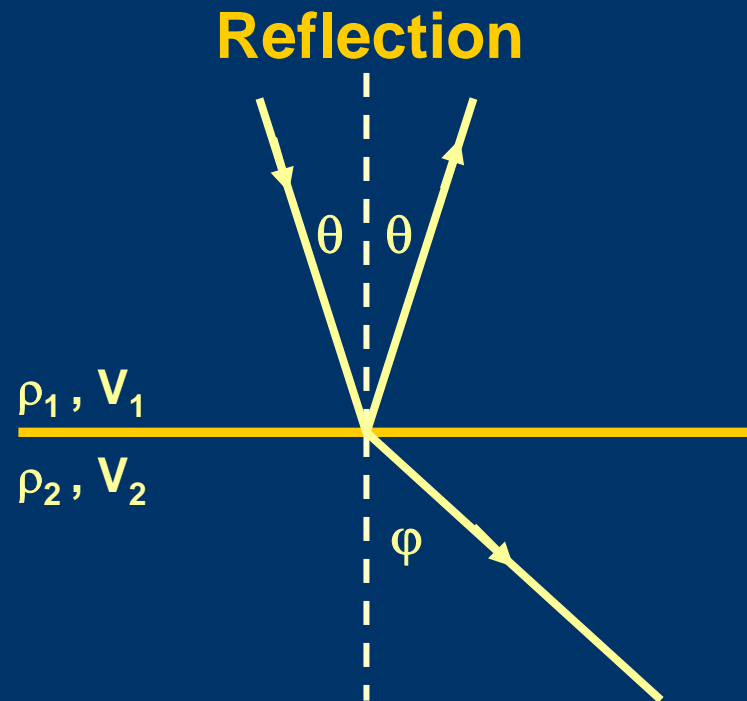
Acquisition: Leonie Jones, David Johnstone, Tim Barton & Tanya Fomin

Processing: Leonie Jones, Bruce Goleby & David Johnstone

Tanami Seismic Survey – Line Locations

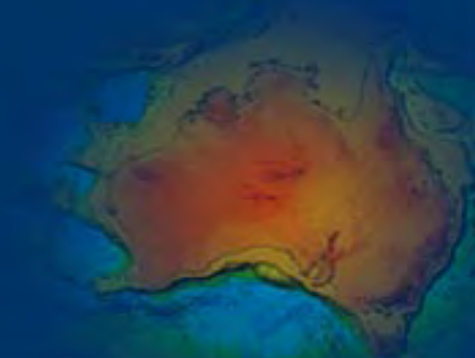


Behaviour of Seismic Waves at an Interface



$$\sin \theta_c = V_1/V_2 \text{ for } V_2 > V_1$$

Snell's Law $\sin \theta / \sin \phi = V_1 / V_2$



Amplitude of reflected waves governed by the reflection coefficient given by:

$$RC = \frac{\rho_2 V_2 - \rho_1 V_1}{\rho_2 V_2 + \rho_1 V_1}$$

- Reflections caused by **density contrasts**, since hard rock velocity approximately proportional to density.
- Typical reflection coefficients are small, e.g. mafic - felsic contacts up to +/- 0.075
- Negative reflection coefficients result in 180° phase change, i.e. the reflected wavelet is “flipped”



DEPTH

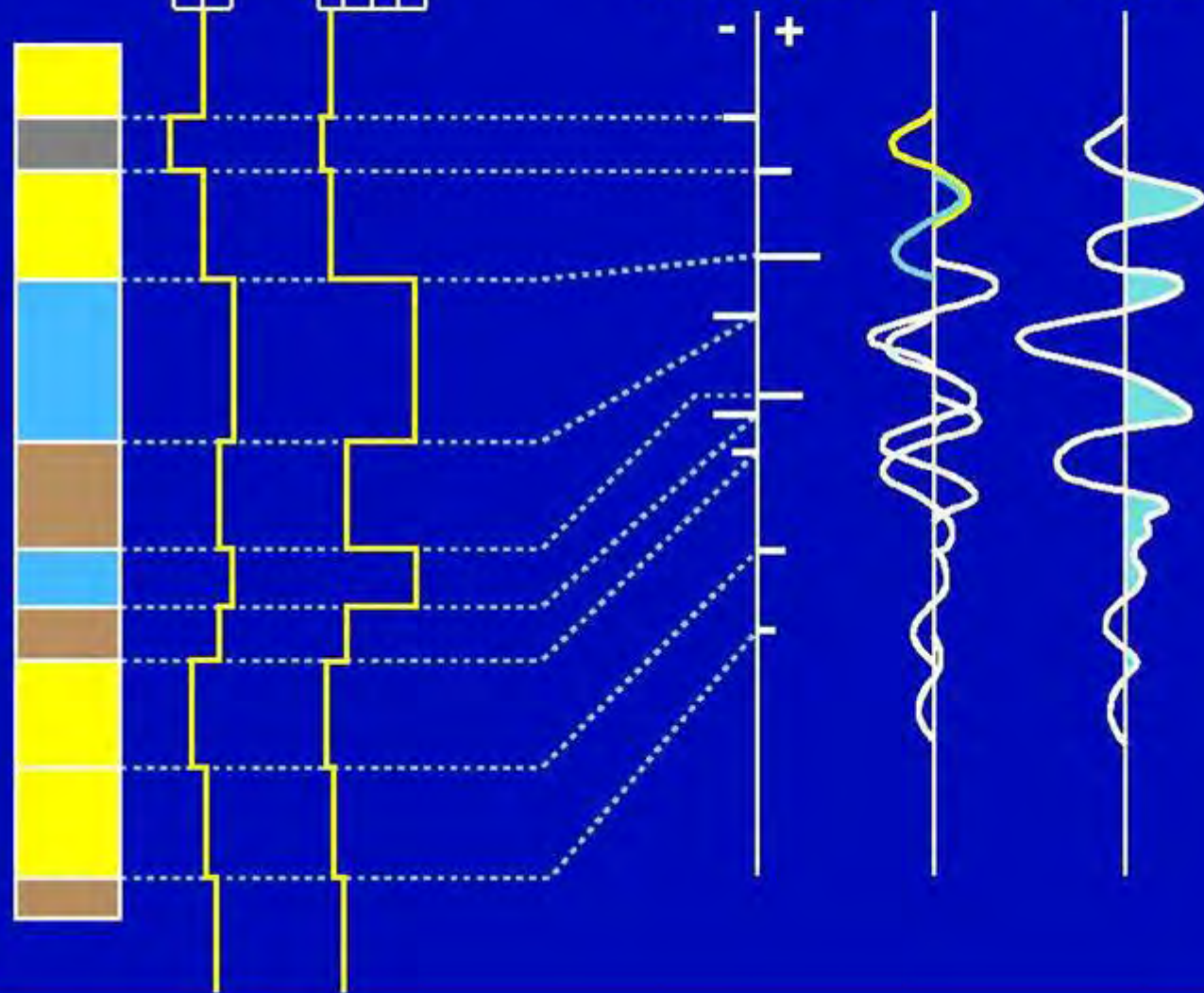
TIME

DENSITY VELOCITY

1.5 2.5 2 4 6

REFLECTION
COEFFICIENT

SEISMIC
TRACE



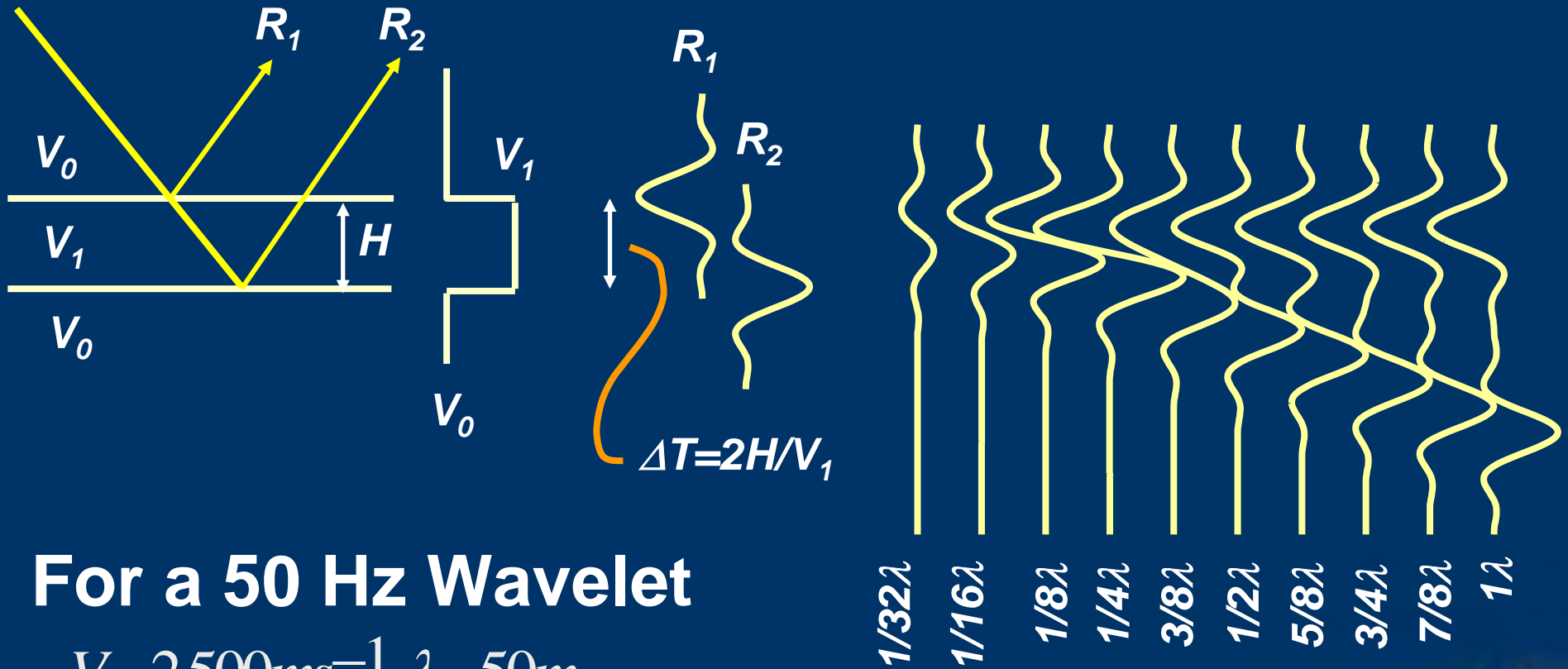
REFLECTION COEFFICIENT =

$$\frac{\rho_2 V_2 - \rho_1 V_1}{\rho_2 V_2 + \rho_1 V_1}$$

INPUT
WAVELET



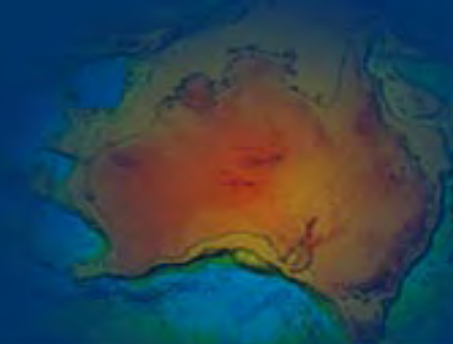
Vertical Resolution



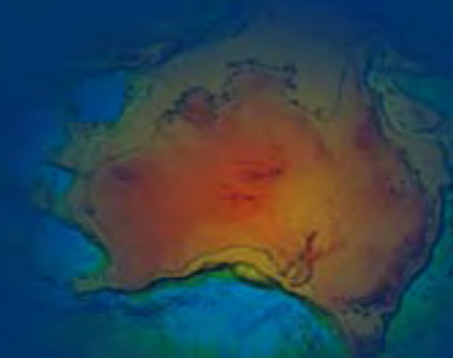
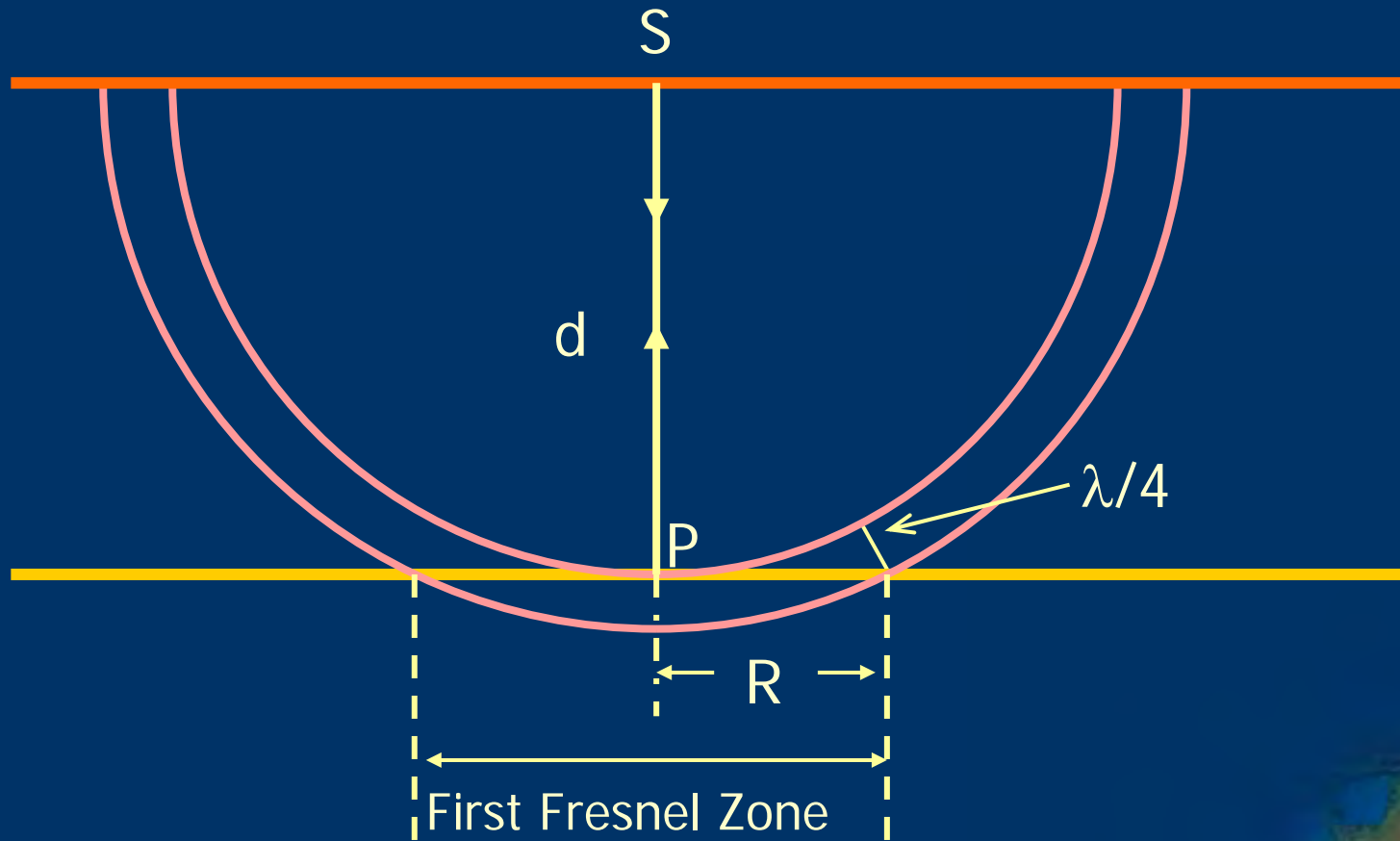
For a 50 Hz Wavelet

$$V = 2,500 \text{ms}^{-1}, \lambda = 50 \text{m}$$

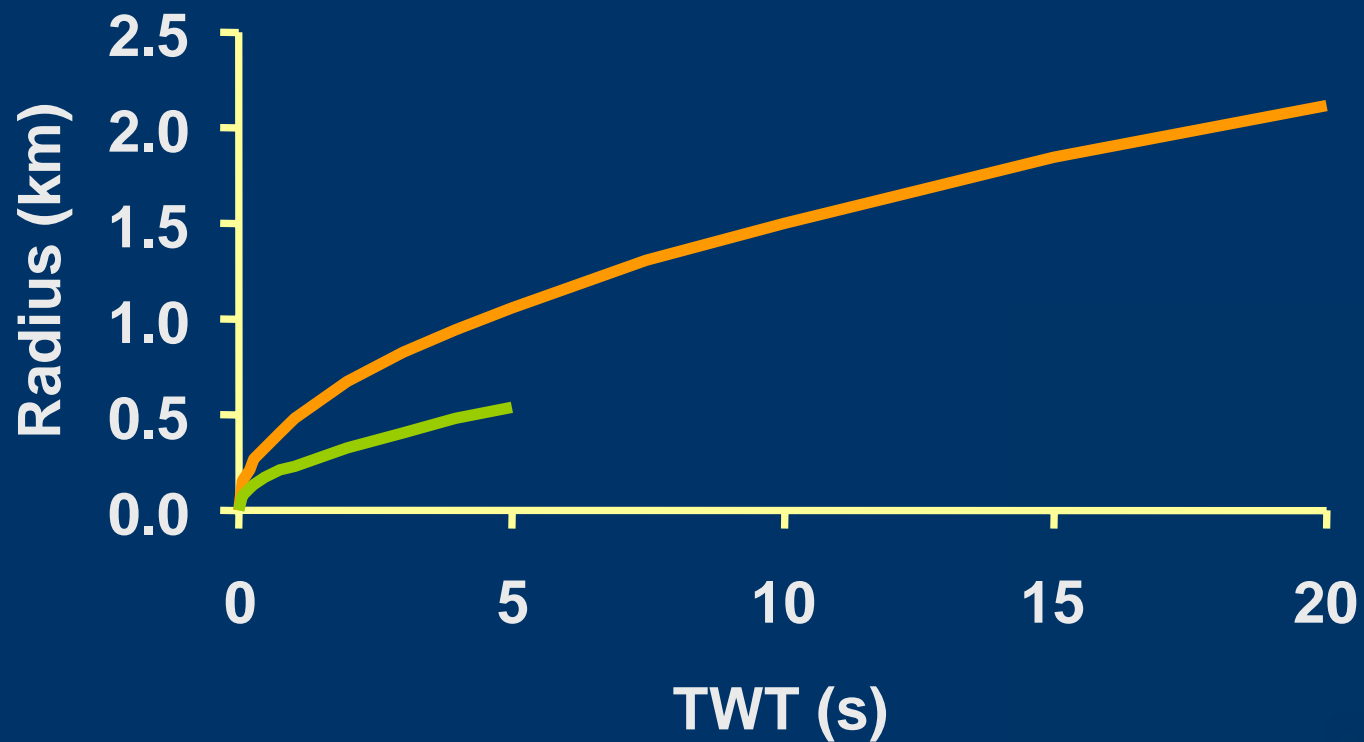
$$V = 5,000 \text{ms}^{-1}, \lambda = 100 \text{m}$$



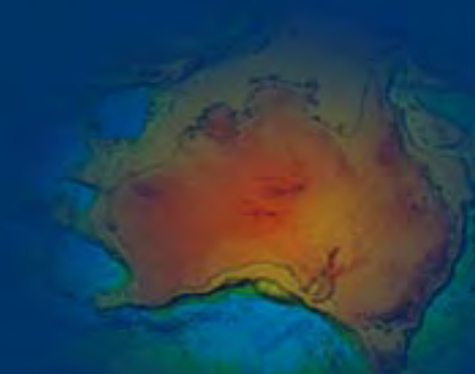
Horizontal Resolution



Fresnel Zone Radius



— Hard Rock — Sedimentary



Comparison of Hard Rock & Sedimentary Basins

Resolving power depends on **wavelength** $\lambda = V/f$

Hard rock

Sedimentary

f = 40 Hz

f = 40 Hz

V= 6000 m/s

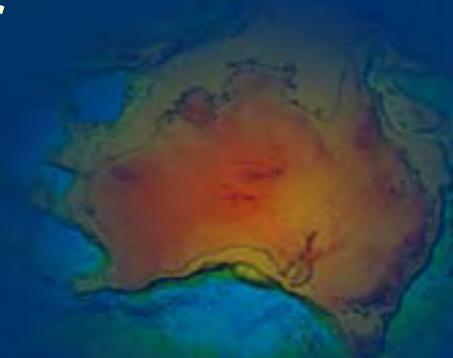
V= 3000m/s

$\lambda = 150$ m

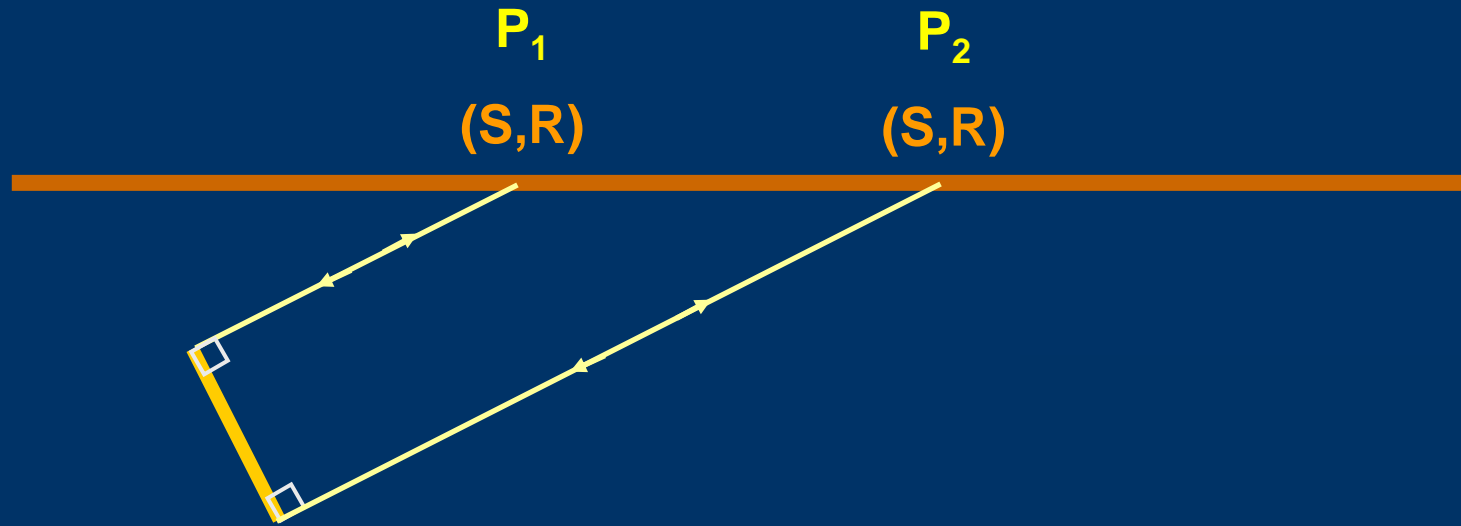
$\lambda = 75$ m

In hard rock, **vertical resolution** is only half as good.

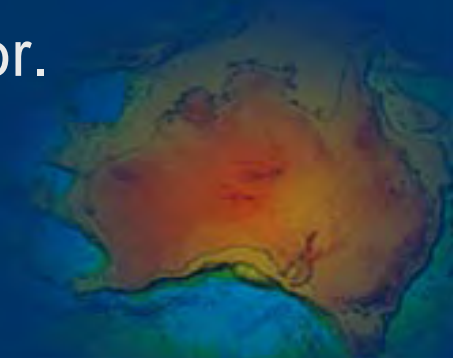
Horizontal resolution is about 70% as good as for sedimentary basins (for the same depth).



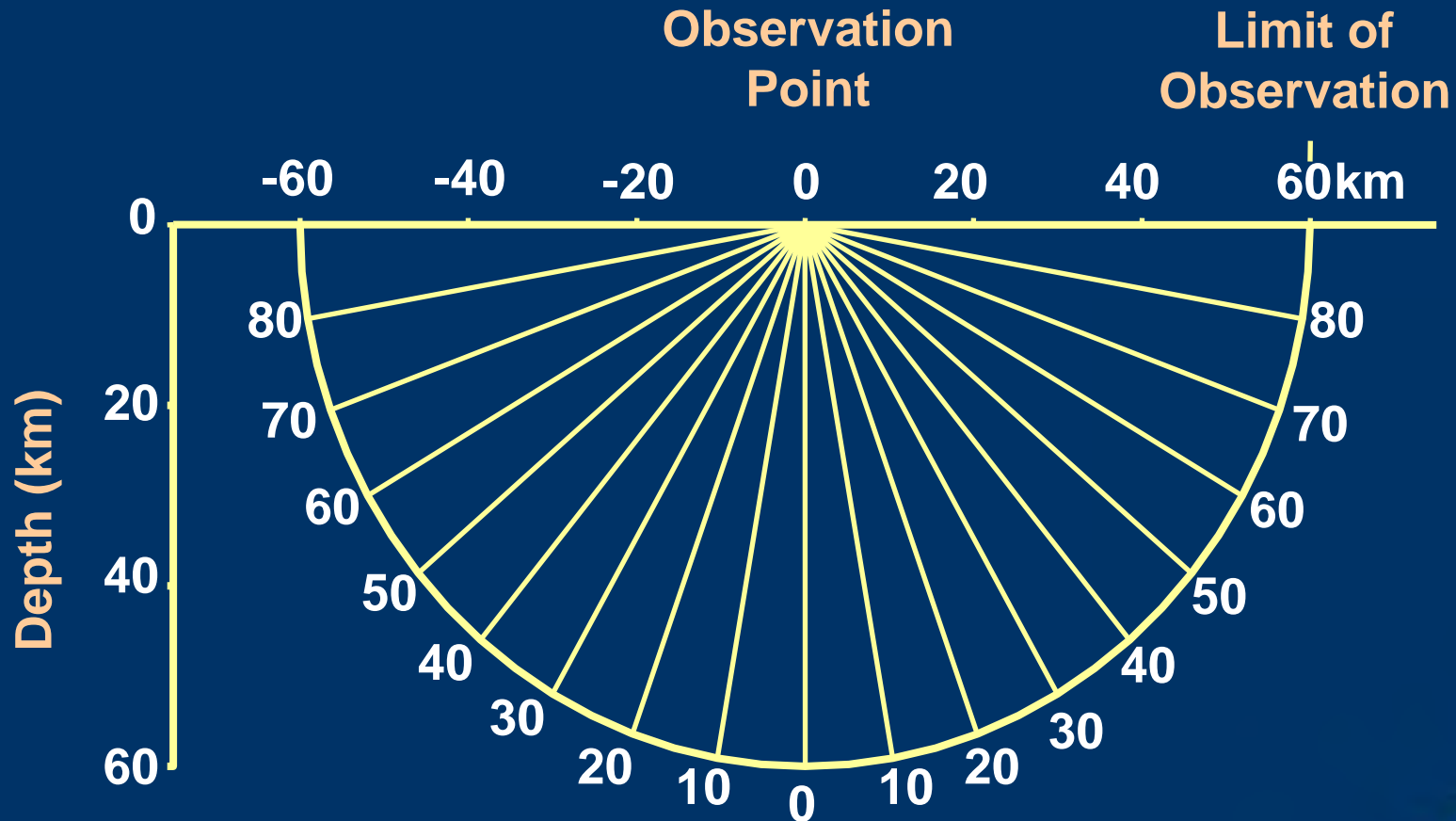
Dipping Reflector



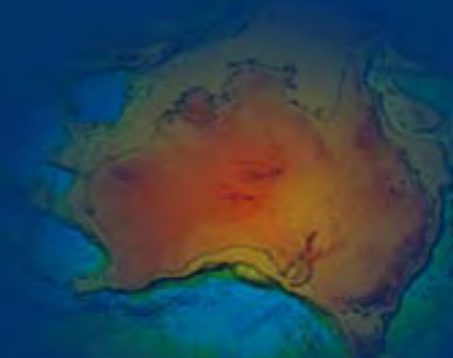
- The seismic line must be long enough to include the observation points and the reflector.
- The recording time must be long enough for seismic waves to travel to and from the reflector.



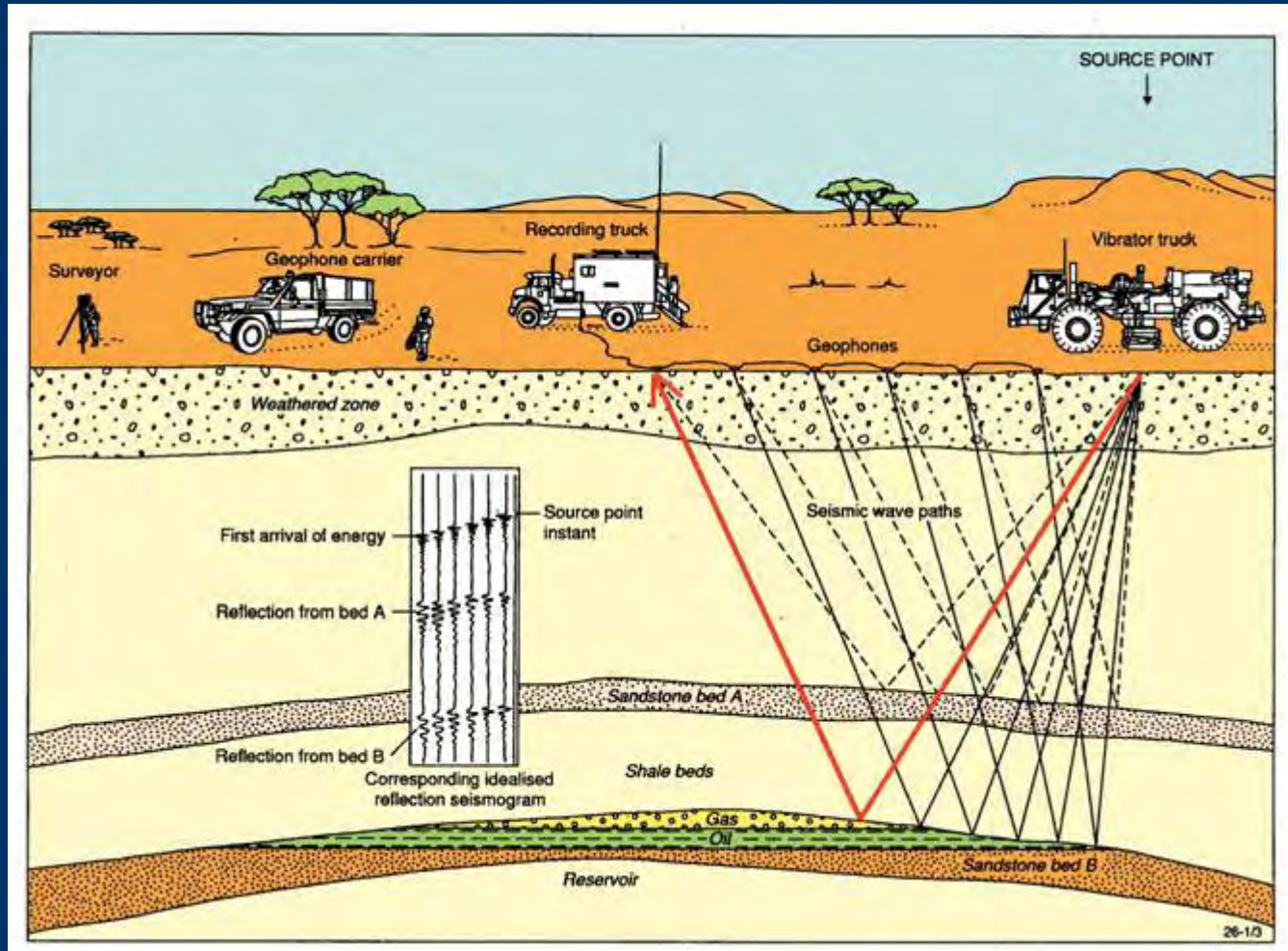
Dip Resolution



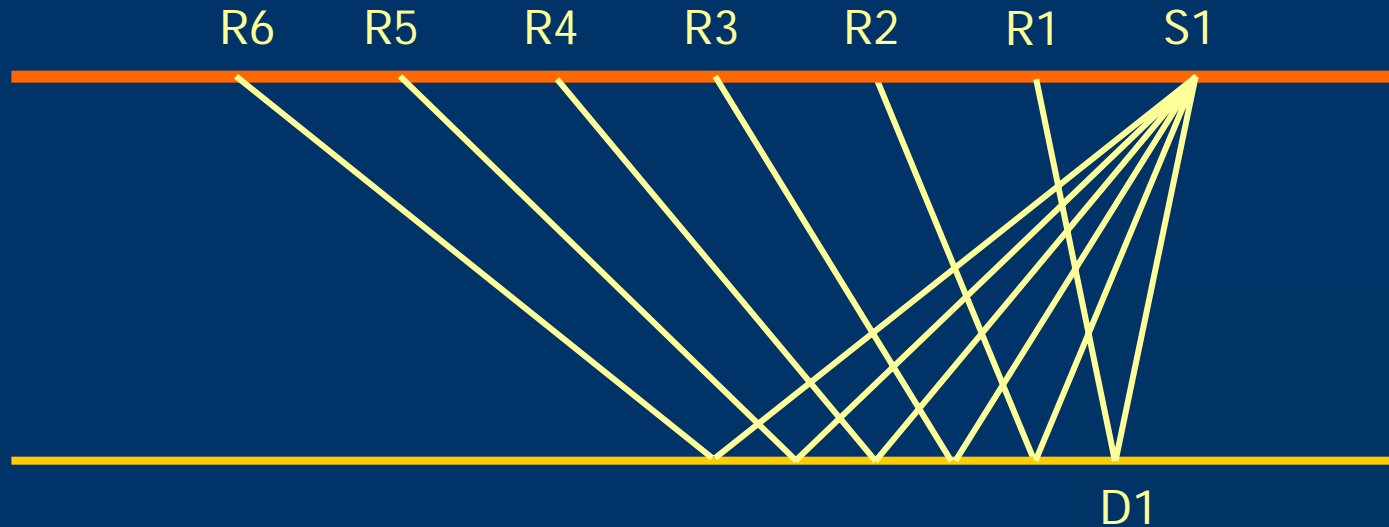
Velocity = 6.0 km/s
Max Record Time = 20s



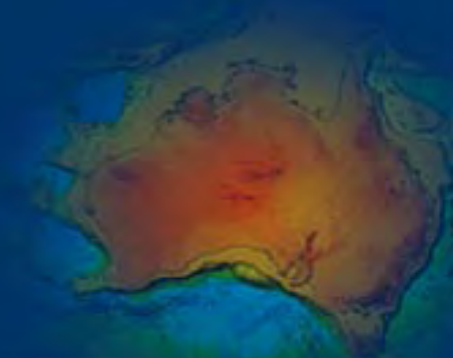
Seismic Reflection Method



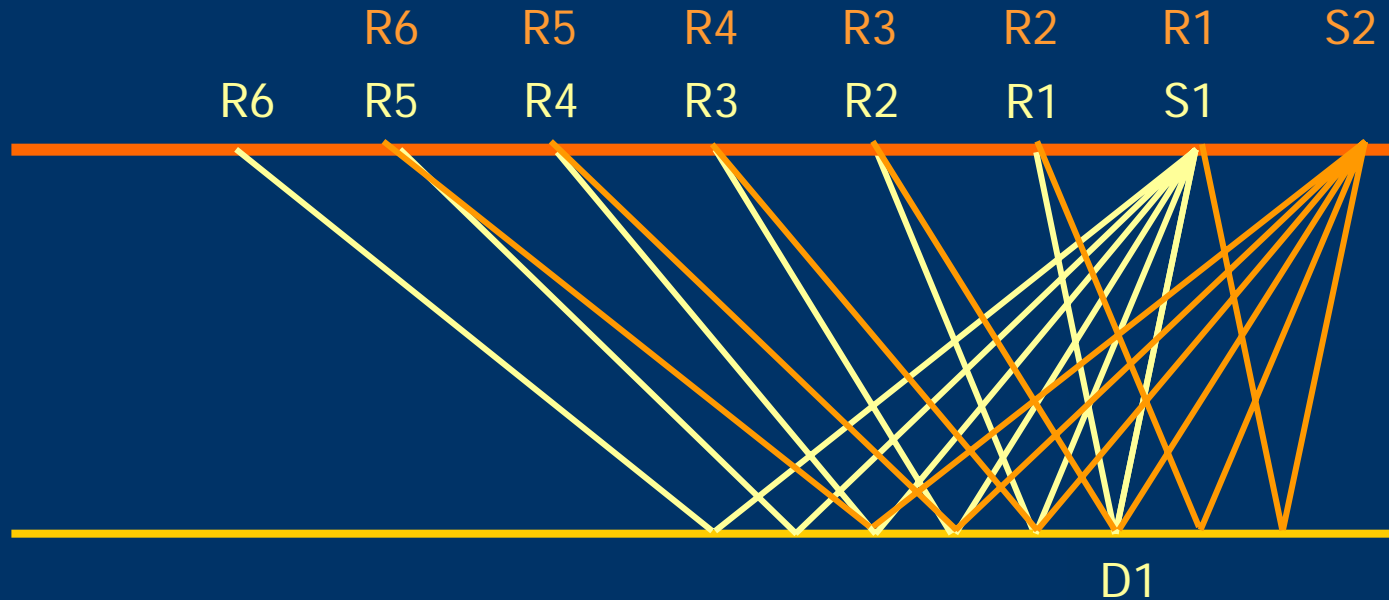
CDP (Common Depth Point) Method



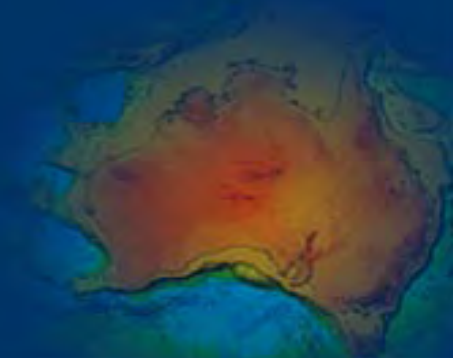
Reflecting points on the reflector are separated by half the receiver spacing.



CDP (Common Depth Point) Method



Depth point D1 is sampled by R1 for Shot 1 and R3 for Shot 2. Fold is the number of times a depth point is sampled.





Laying cable

Front Crew



Dropping geophone strings



Unclipping phones



Connecting takeout



Stomping geophone



Back Crew

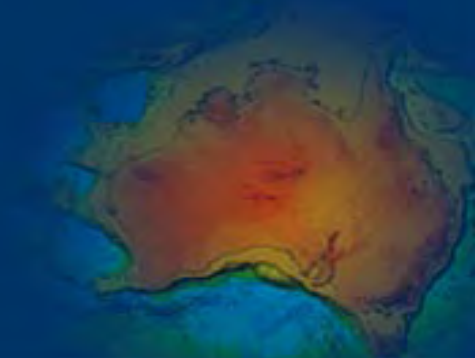
Pinning geophones



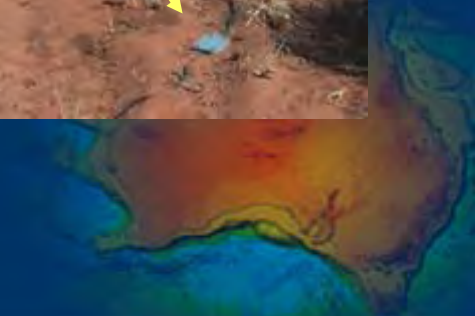
Dropping clip



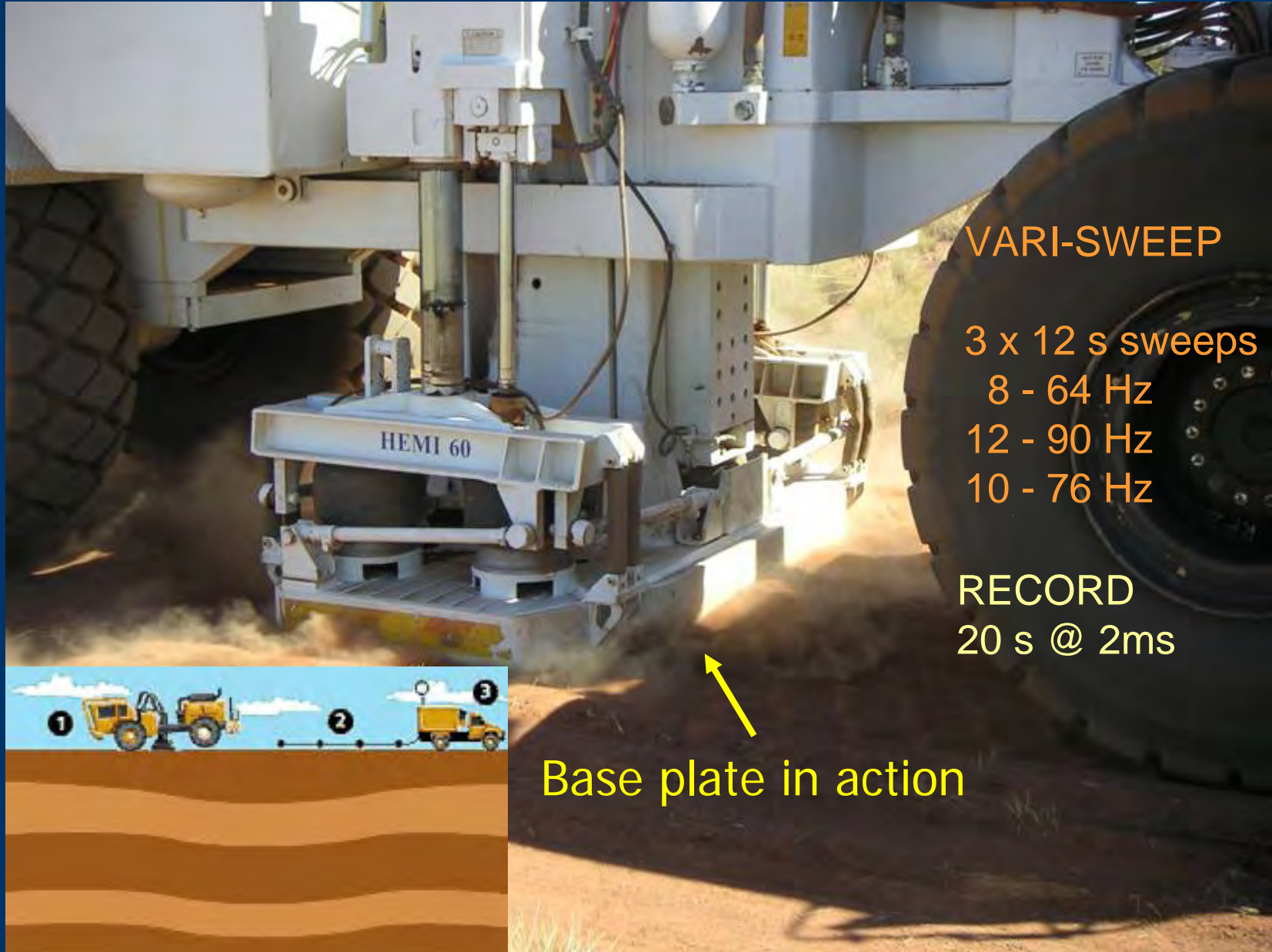
Pulling in cable



Acquisition Parameters I

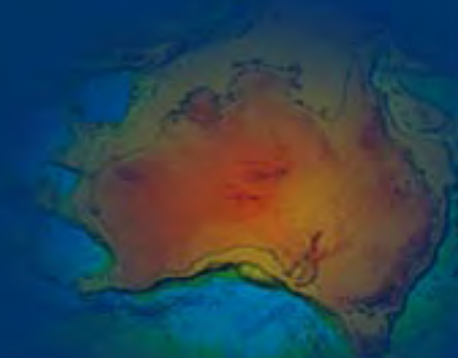


Acquisition Parameters II

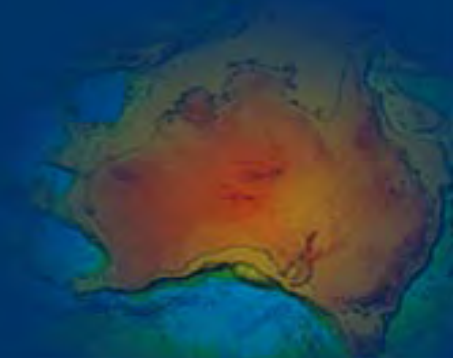
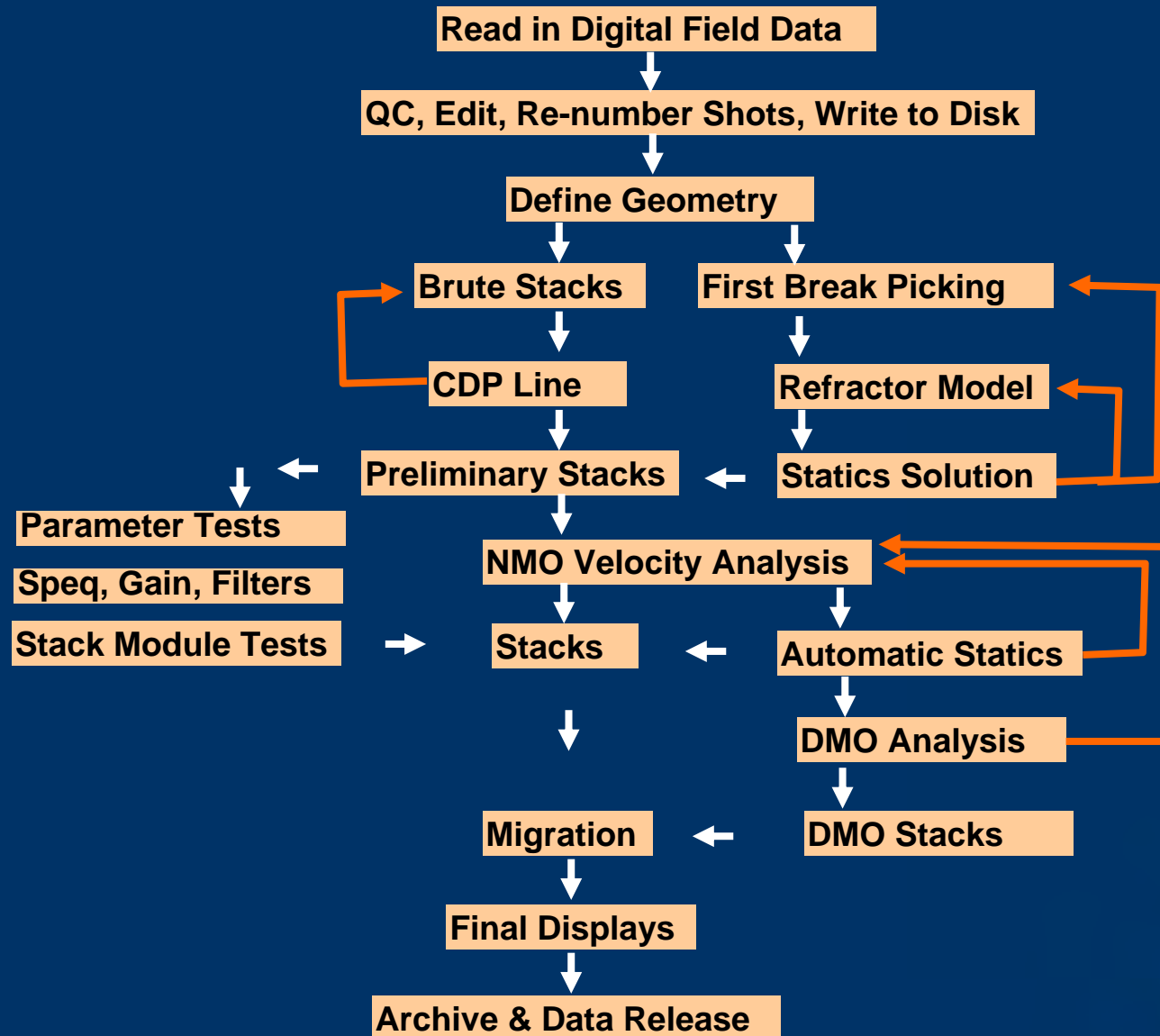


Seismic Processing

Overall goal is to produce an image of the sub-surface by enhancing and correctly positioning reflections and reducing undesired energy (noise)



Seismic Processing



Key Processing Steps

Crooked line geometry definition - including CDP line

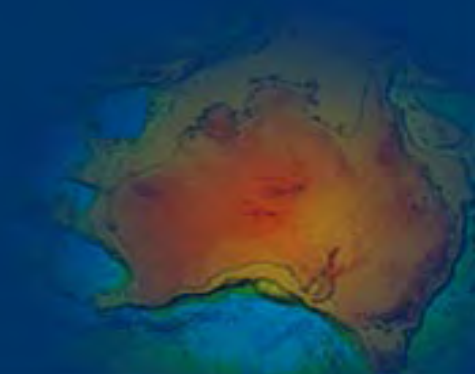
Statics correction - for variable time delays in regolith

Spectral equalisation - suppresses low f noise

CDP sort - collects traces with common mid point

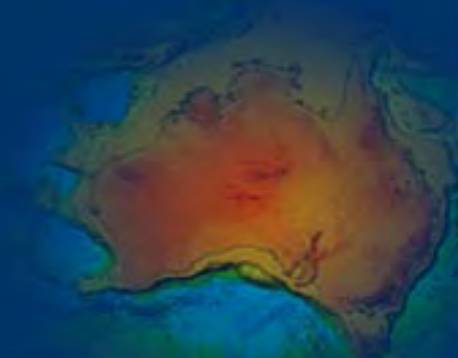
Velocity analysis - corrects for normal & dip moveout

Migration - moves reflectors to correct positions

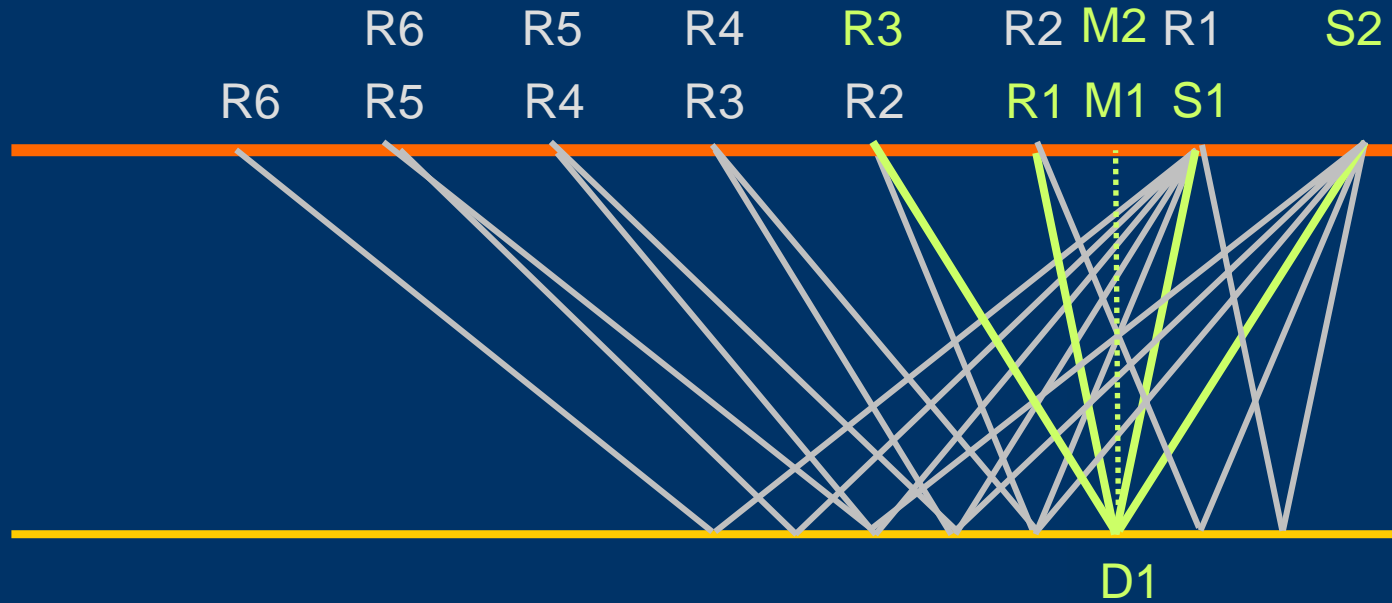


Geometry Definition

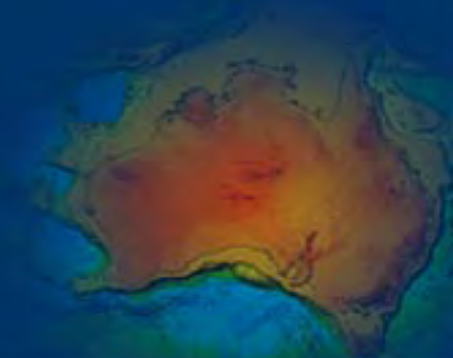
Locates sources and receivers and defines the CDP line



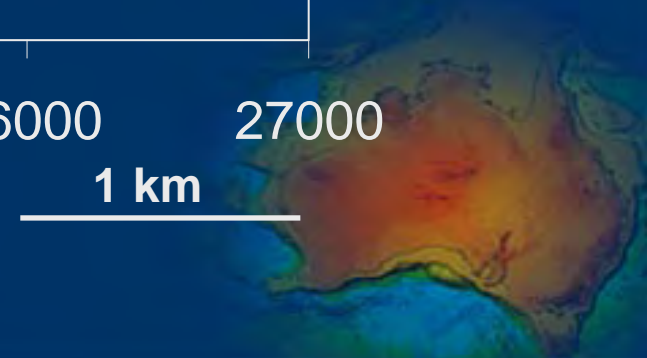
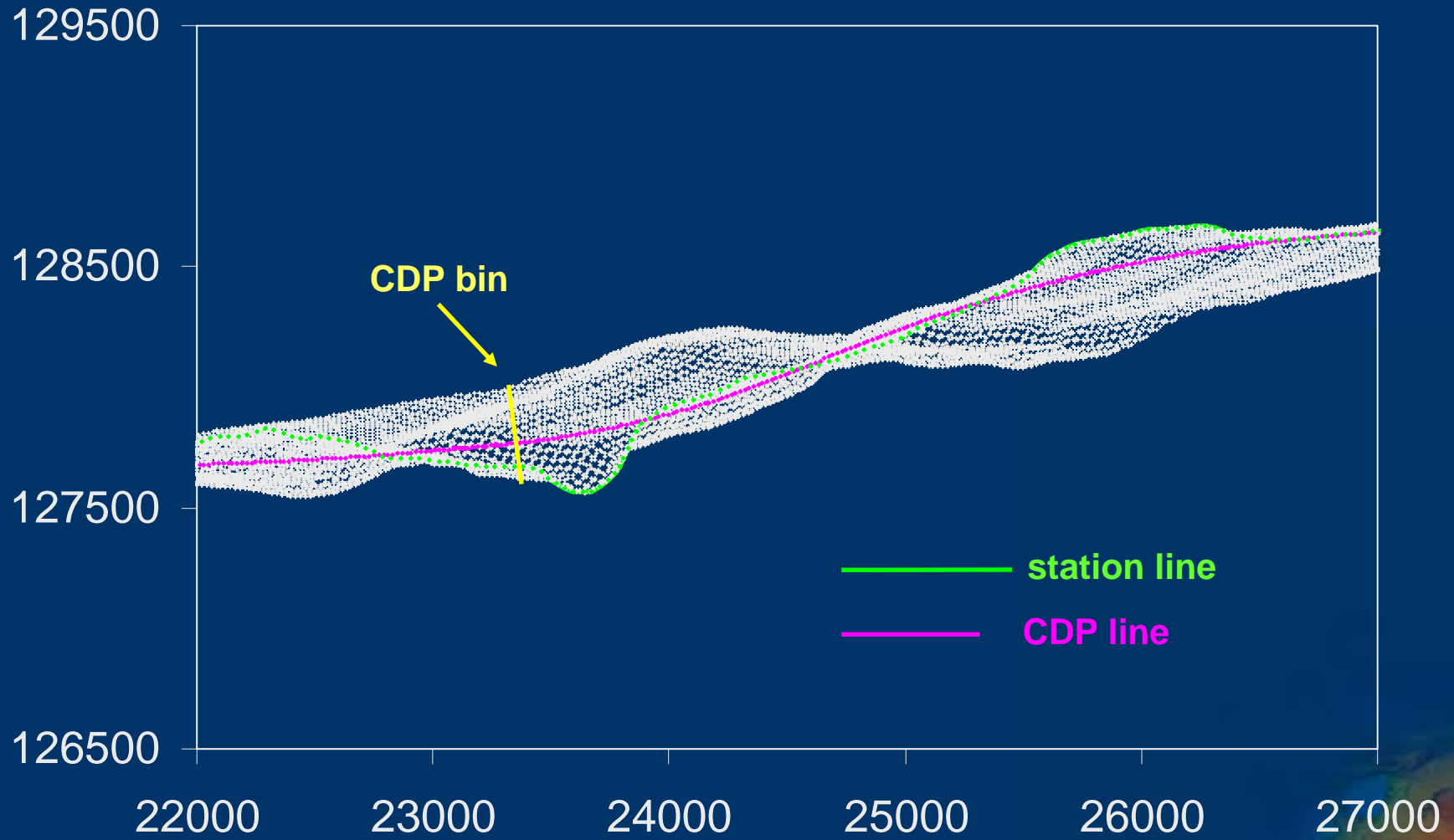
CDP (Common Depth Point) Binning



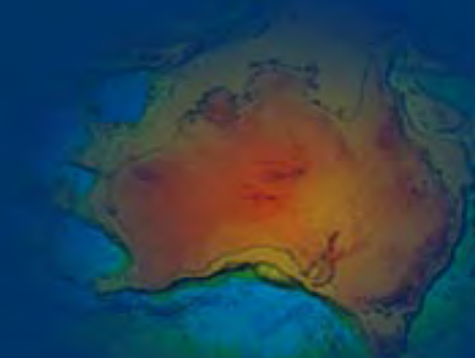
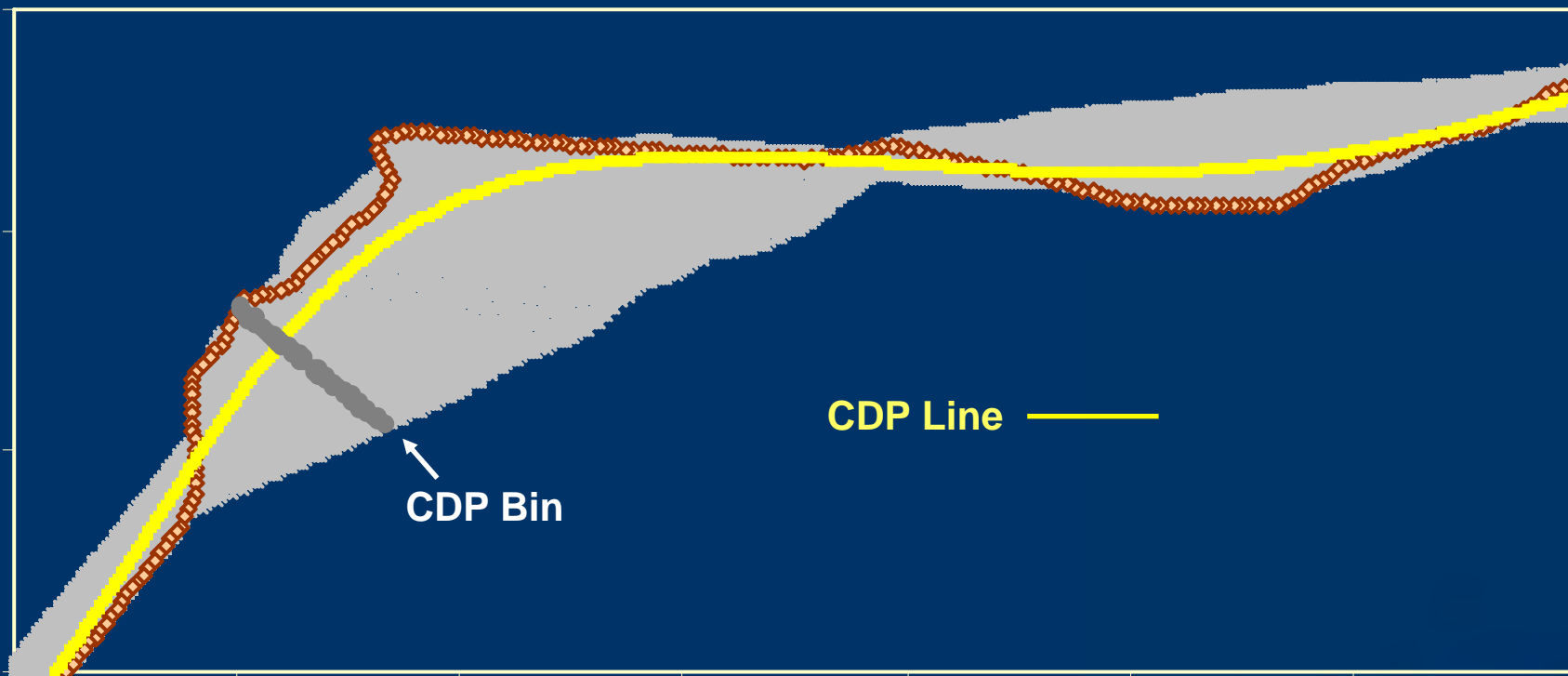
Assigns shot-receiver midpoints (M1 and M2) to common depth point D1



Crooked Line Geometry



Crooked Line Geometry

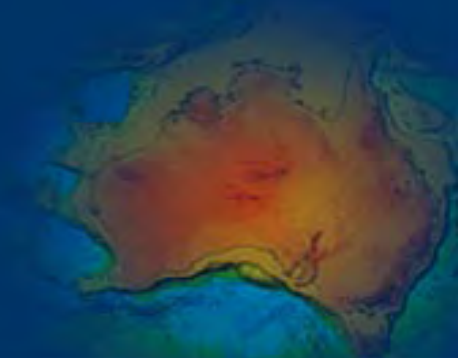


Refraction Statics Calculation

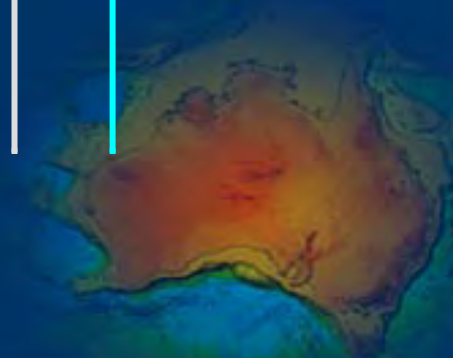
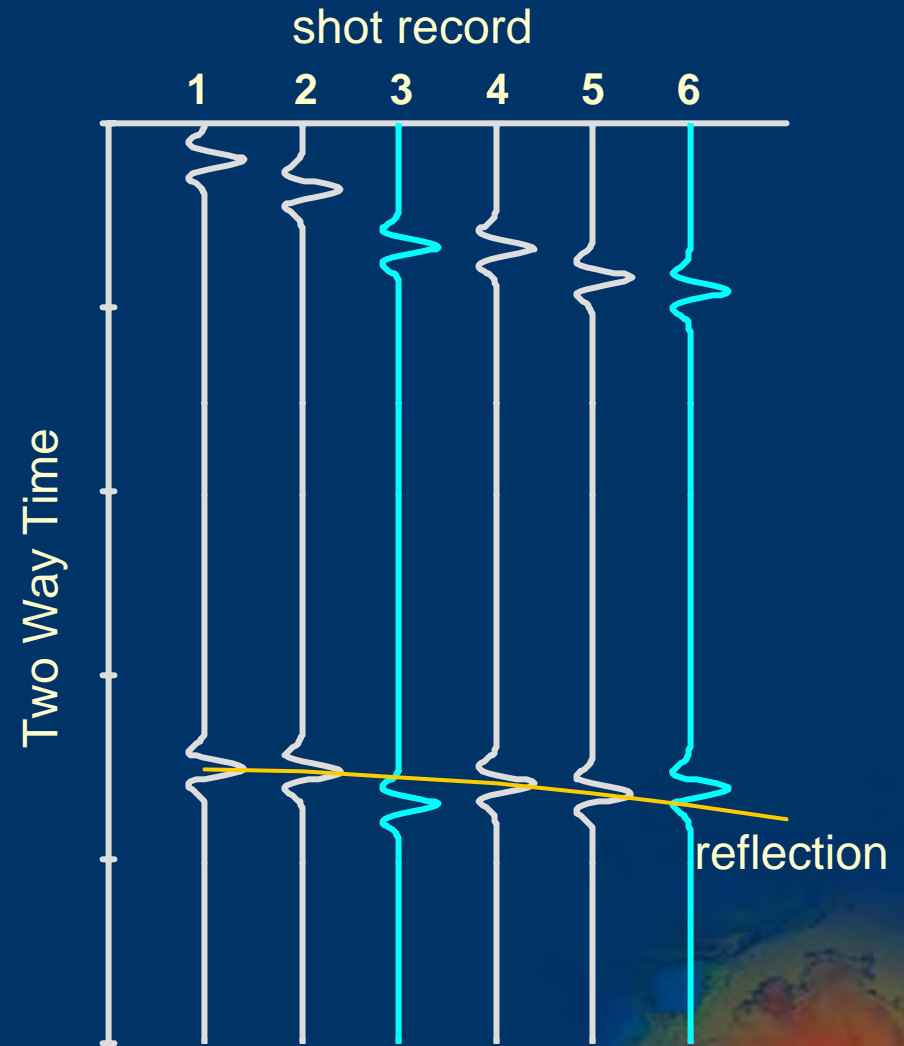
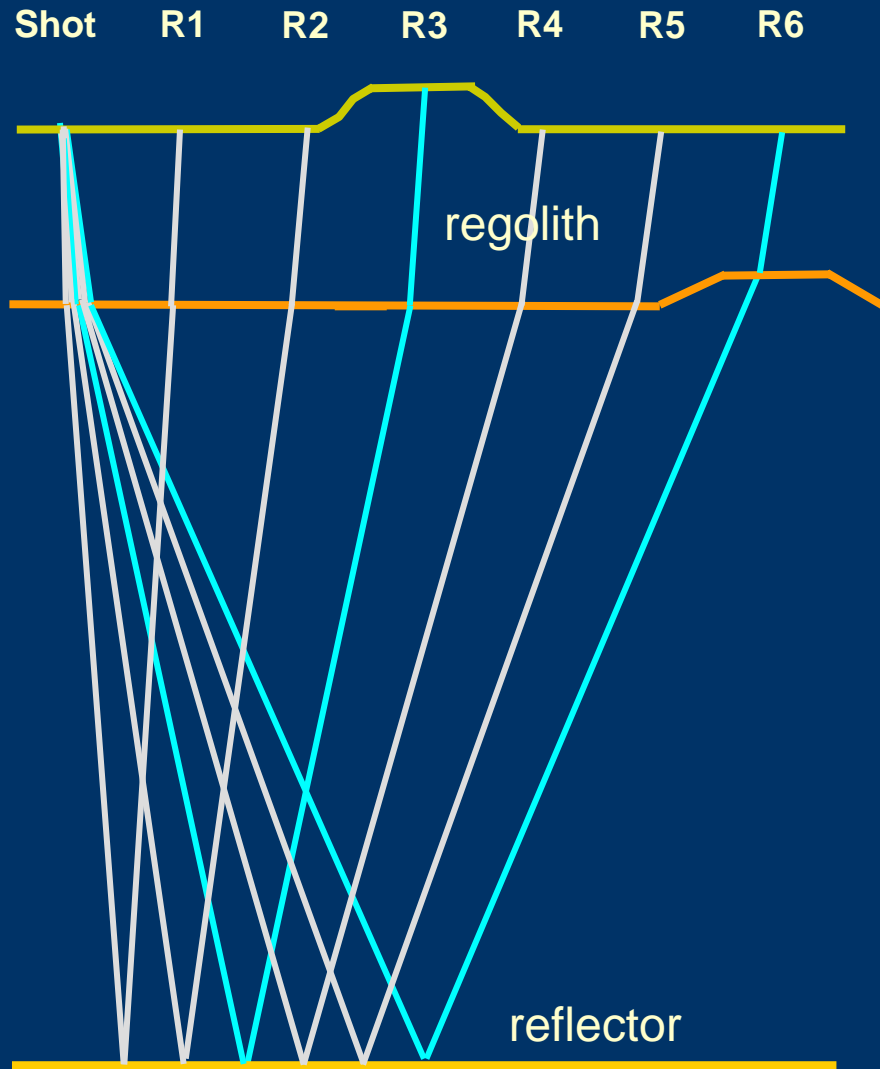
Corrects for varying travel times due to varying surface elevation and regolith thickness, else

False structures can occur

Data won't stack correctly

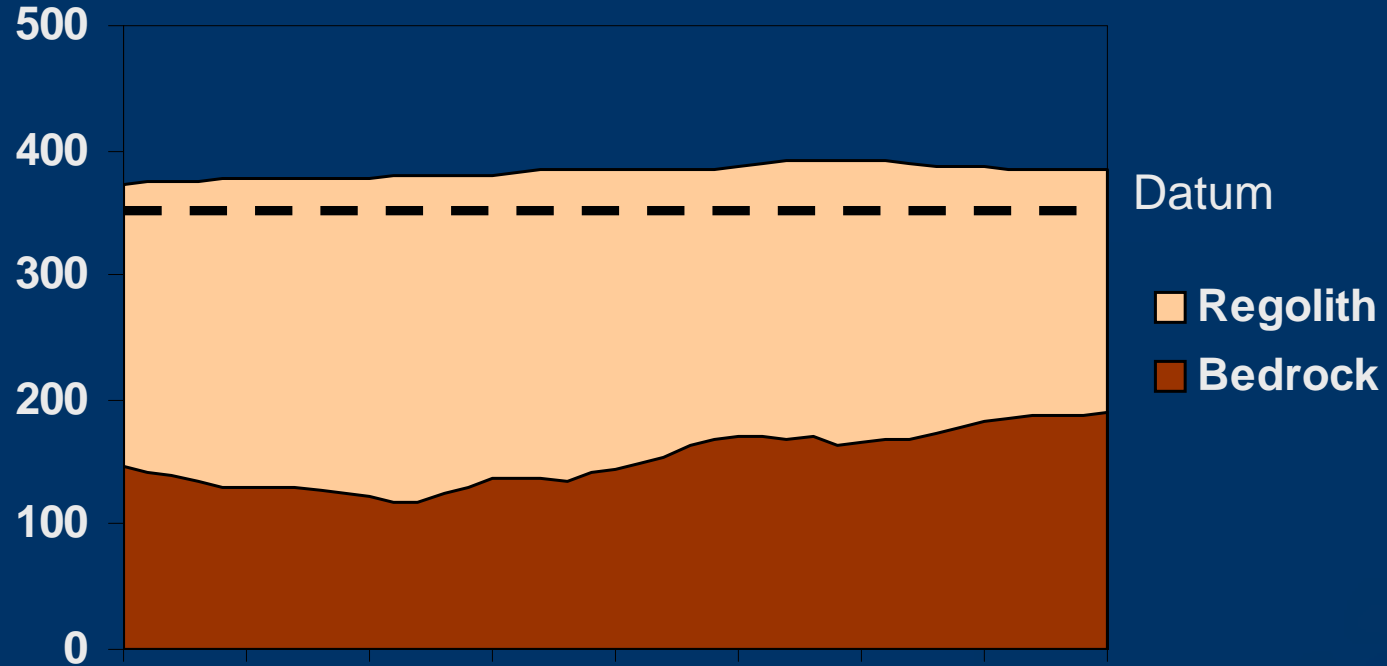


Statics Corrections needed for elevation and regolith

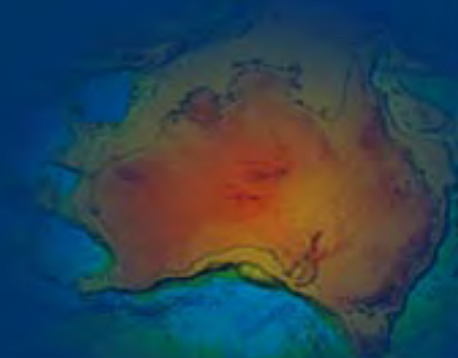


Statics Correction

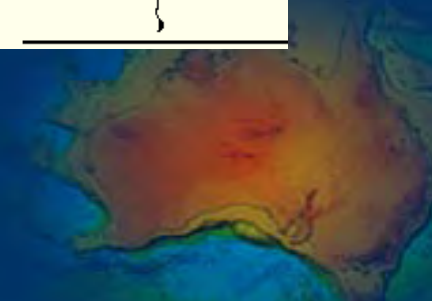
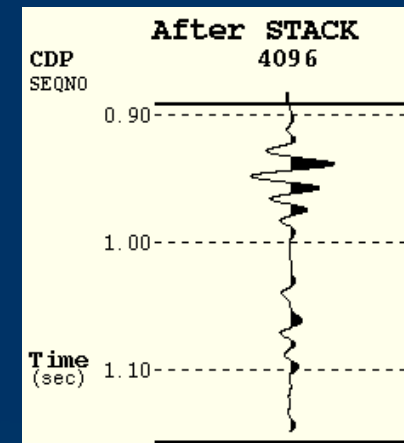
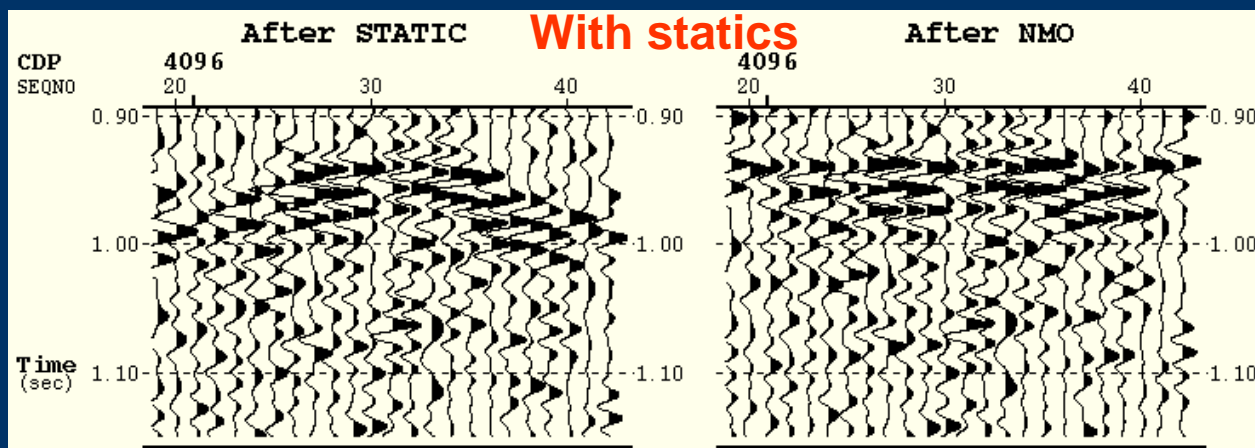
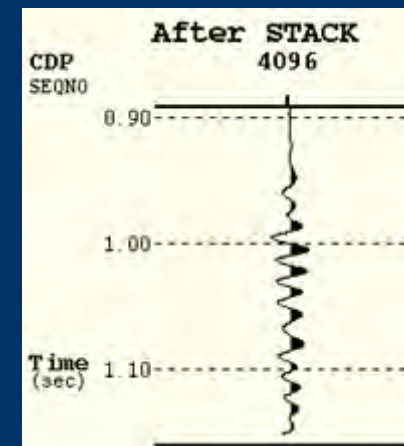
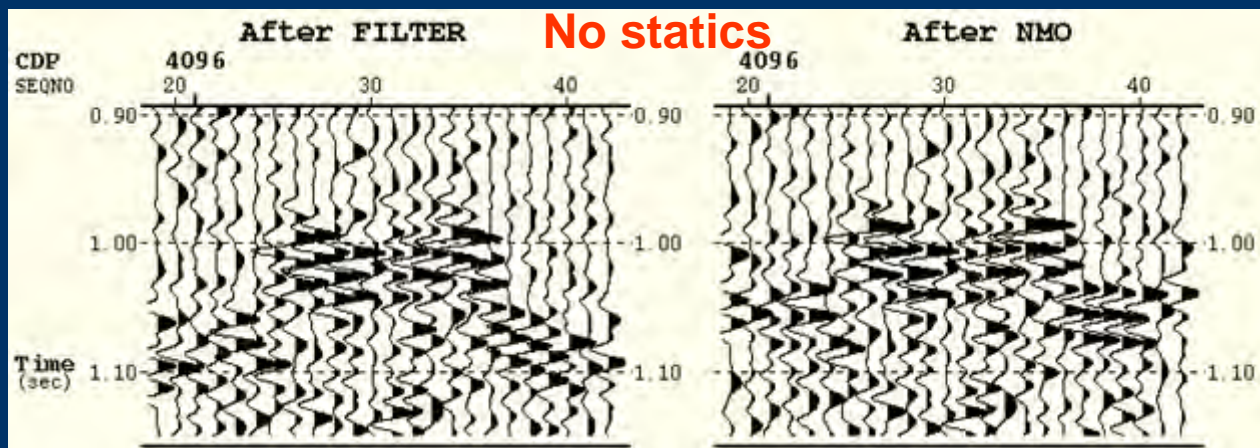
- subtracts travel time in lower velocity regolith
- adds travel time between bedrock & datum at bedrock velocity



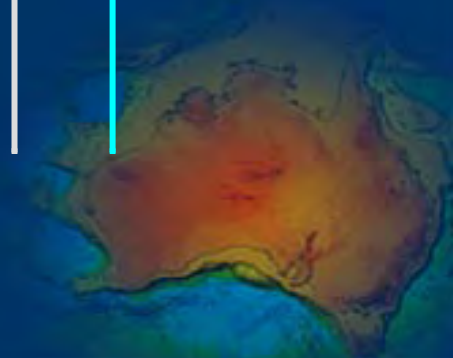
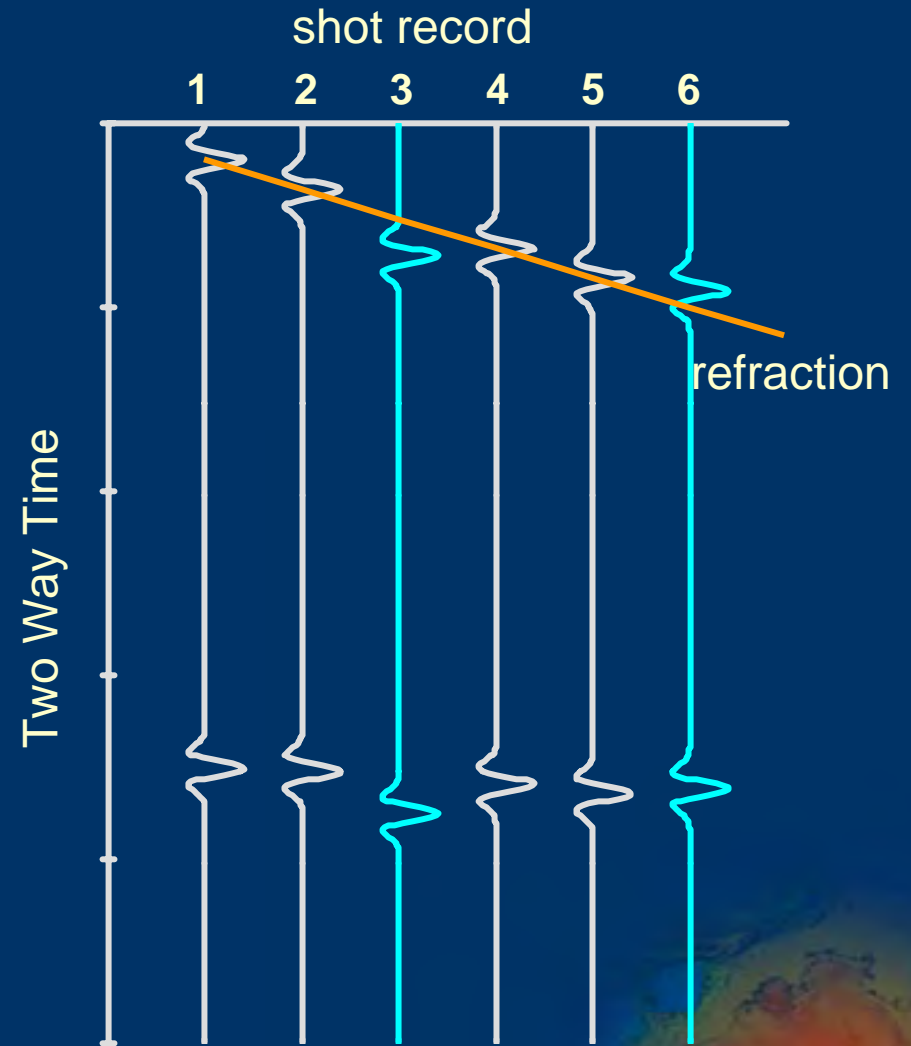
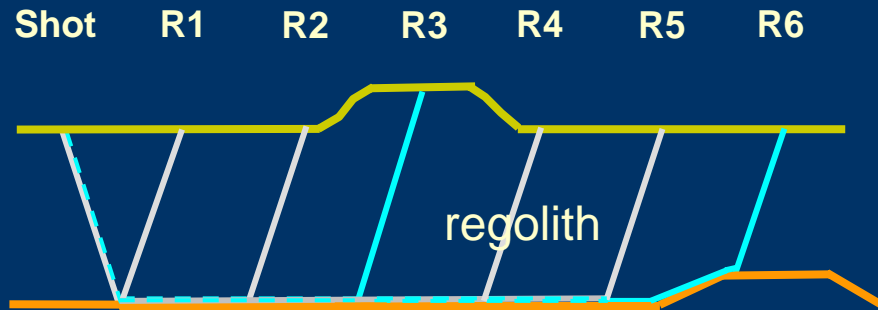
- Therefore, need a model for regolith/bedrock interface
- Note that static shift depends on chosen datum



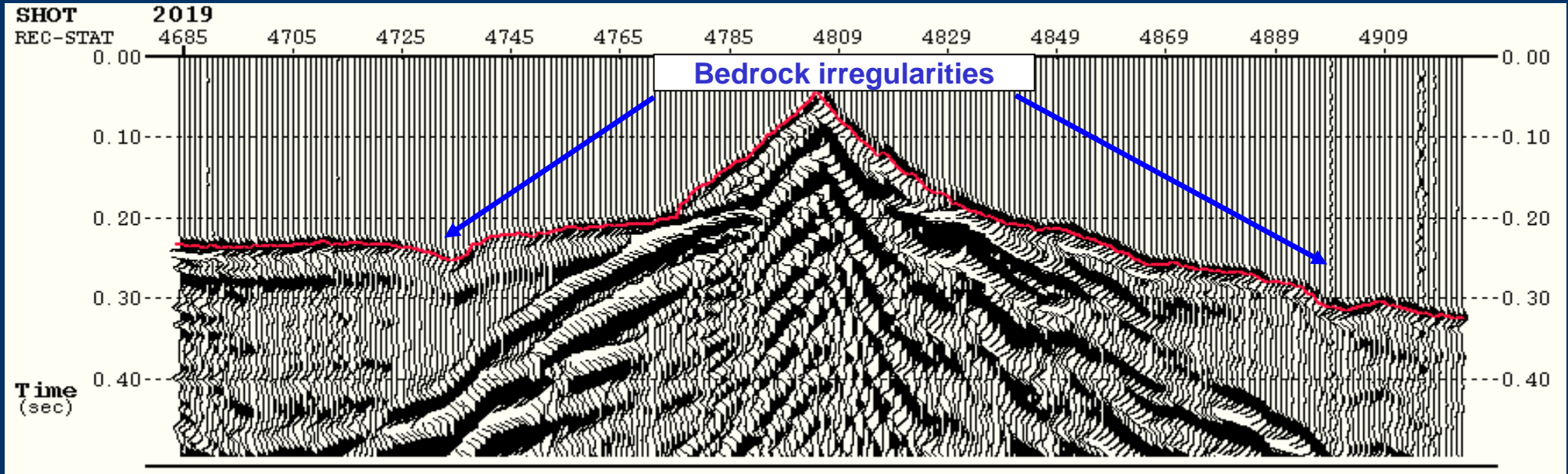
Effect of Statics Correction



First arrivals (refracted waves) are used for statics calculations



First break (first arrival) picking



TIME-CONSUMING TASK:

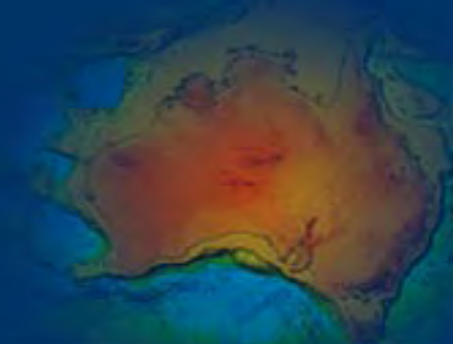
Pick first arrival for each shot record (240 traces) for

05GA-T1 - 4429 shots

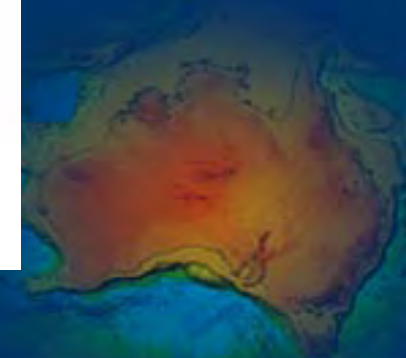
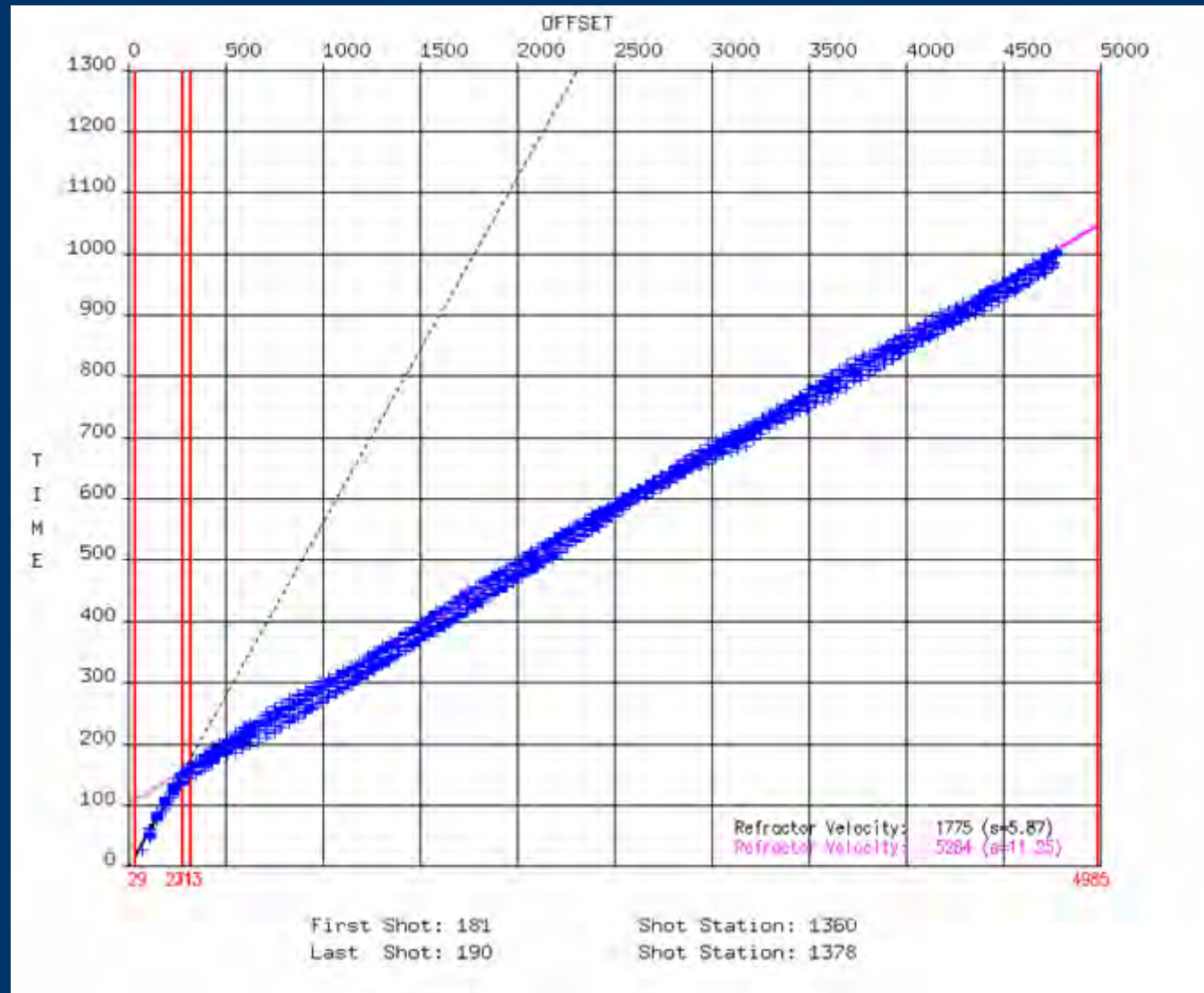
05GA-T2 - 1402 shots

05GA-T3 - 2361 shots

05GA-T4 - 1097 shots



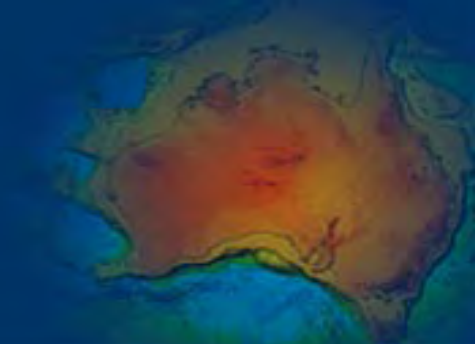
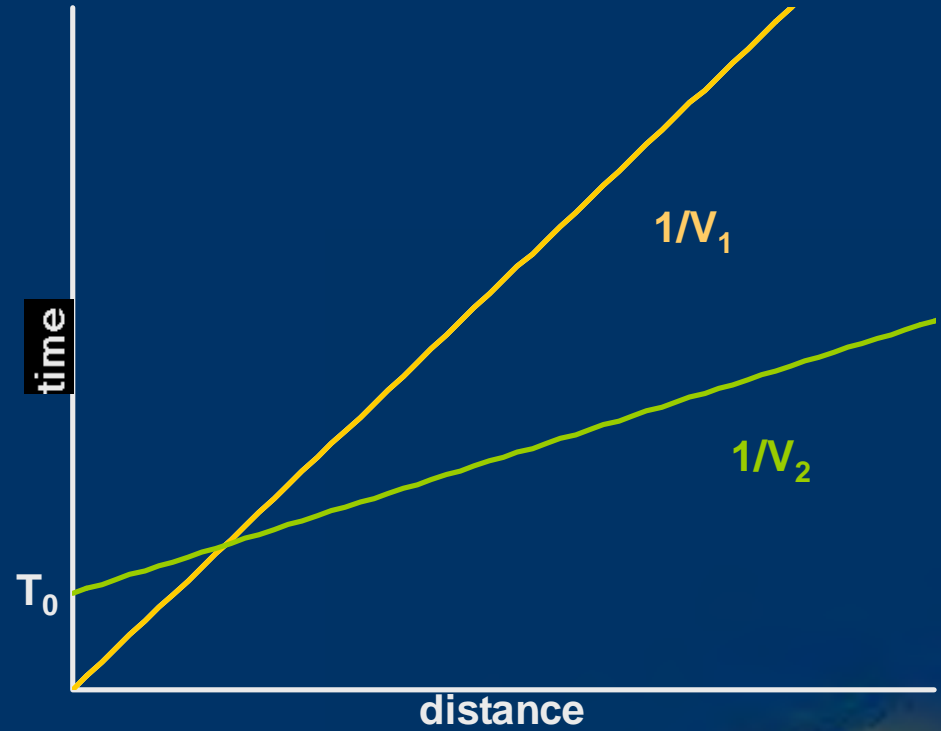
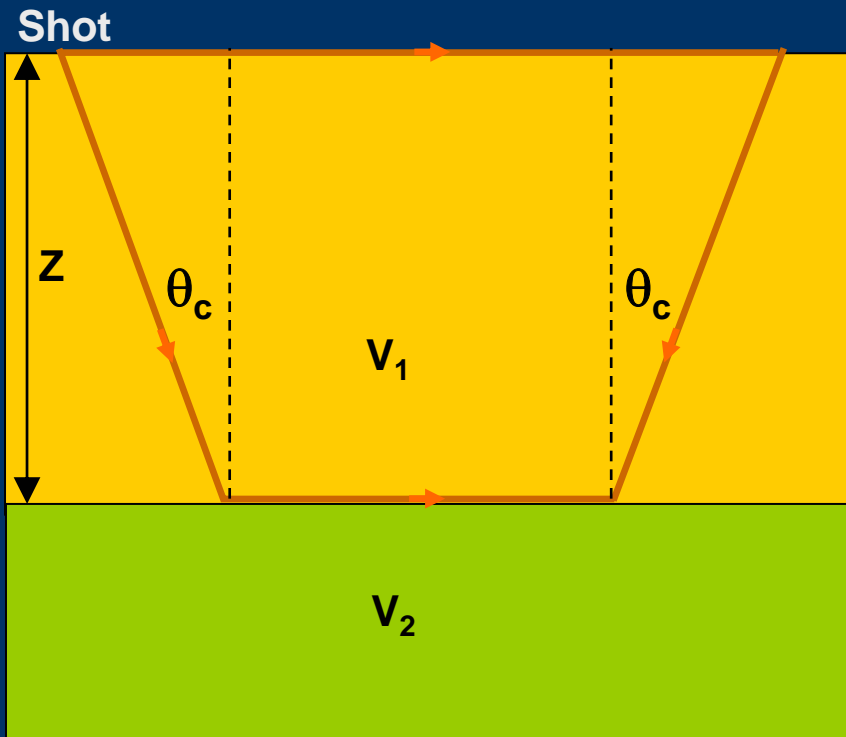
Use plot of first arrival time vs offset (distance) to identify refractor branch for refraction solution software



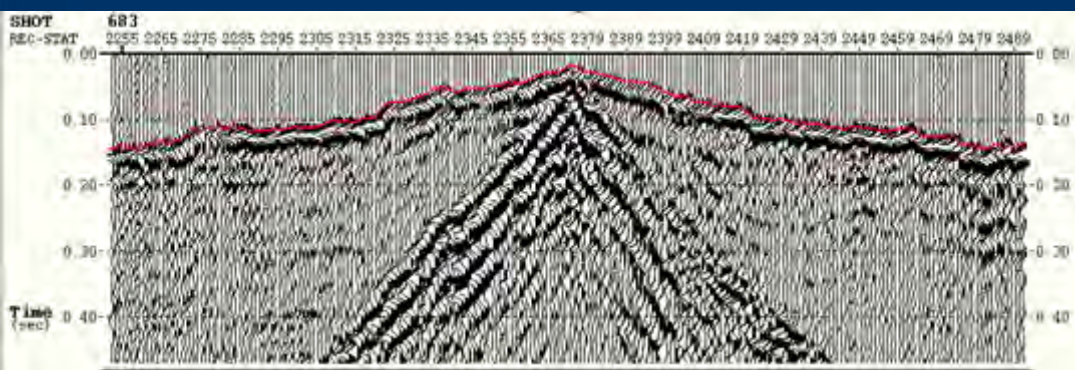
One-refractor model

$$\sin \theta_c = V_1/V_2$$

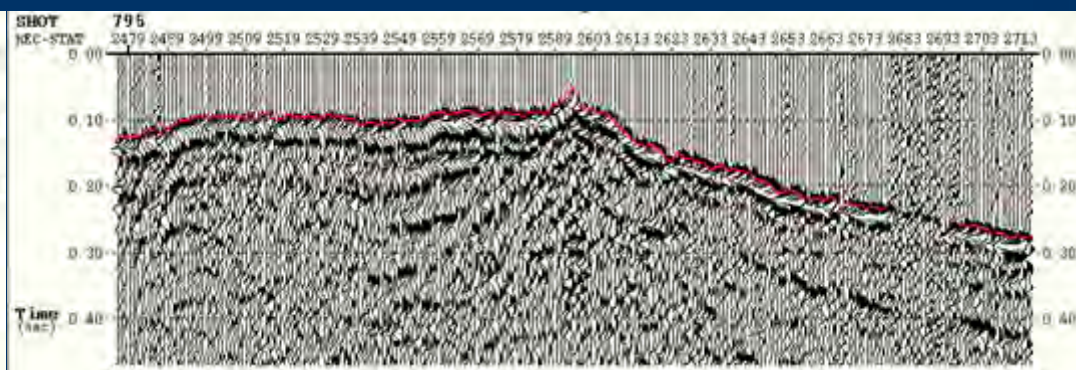
$$T_0 = 2 Z \cos \theta_c / V_1$$



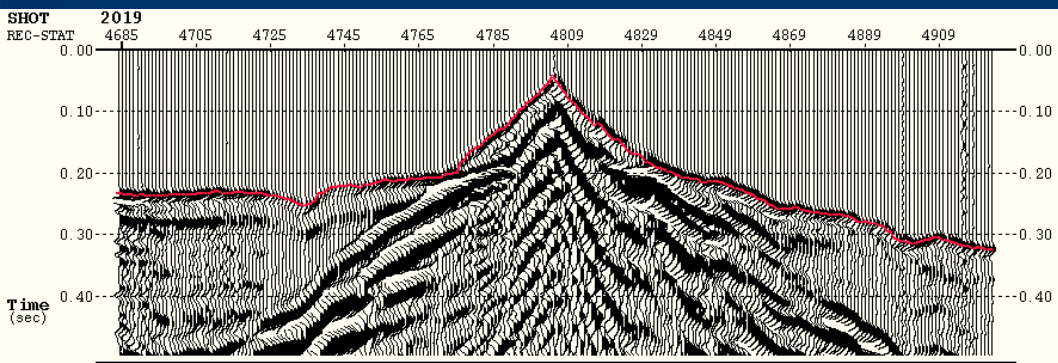
Characteristic shot records



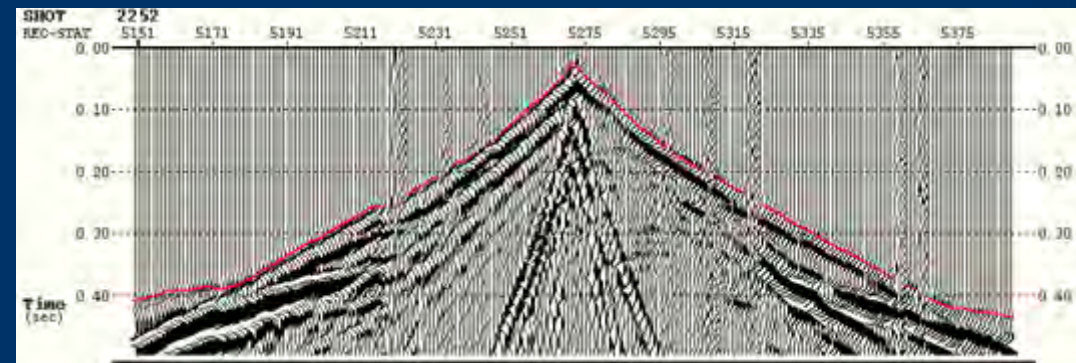
Near outcrop in hard rock



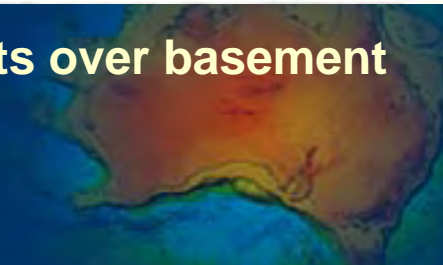
Approaching broad channel



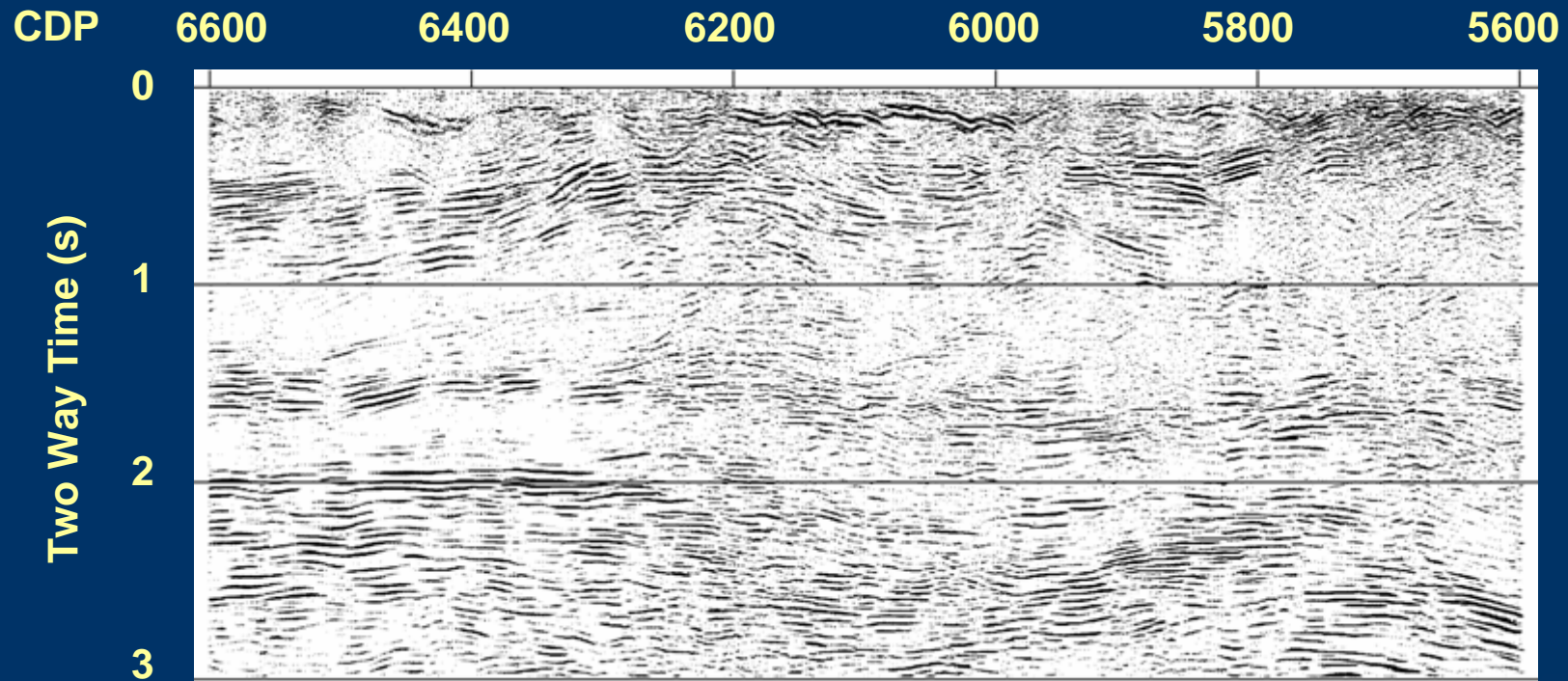
Thin Permian sediments over basement



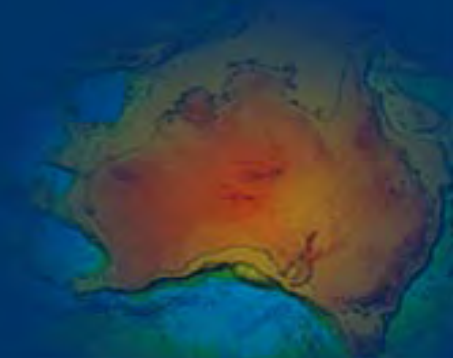
Thick Permian sediments over basement



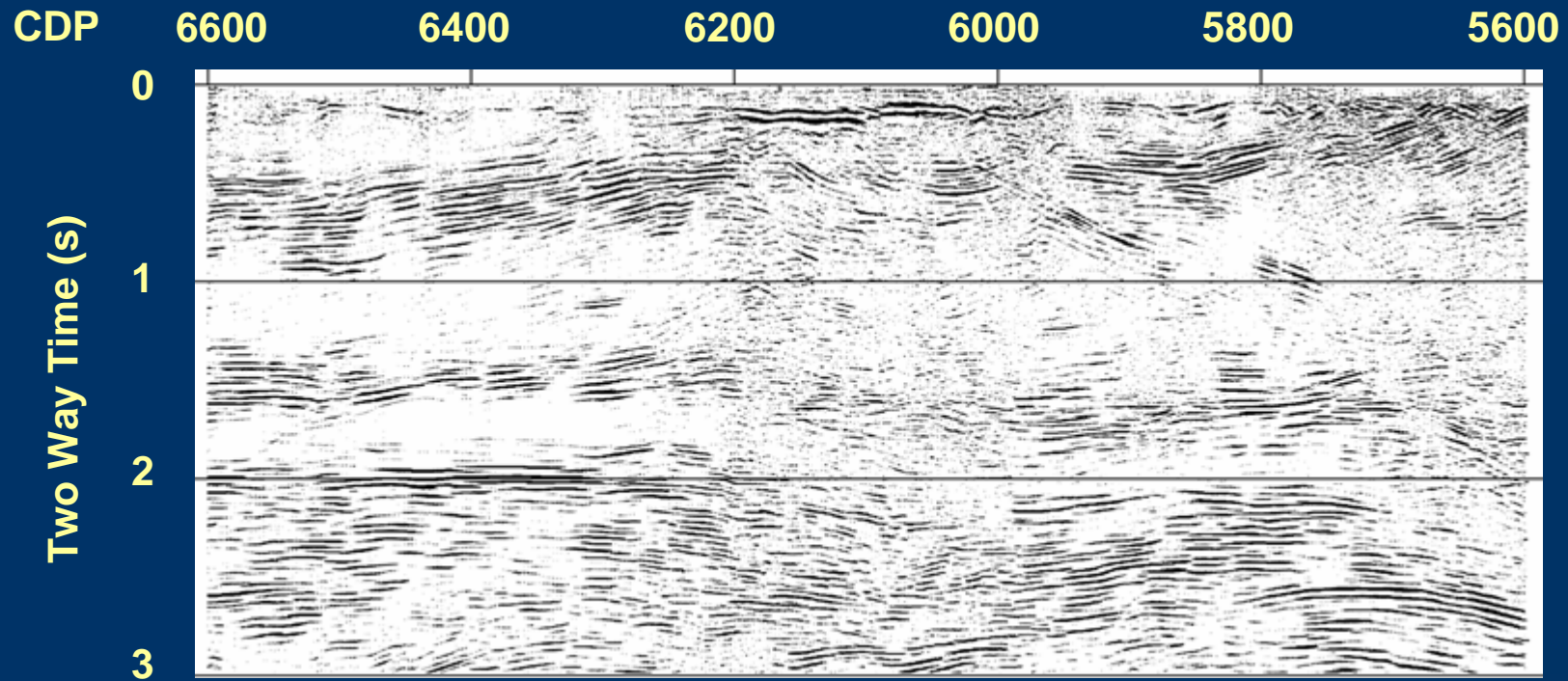
Line 05GA-T3 – No statics



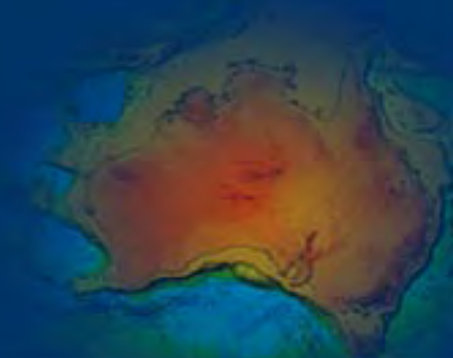
V/H = 1 4 km NE →



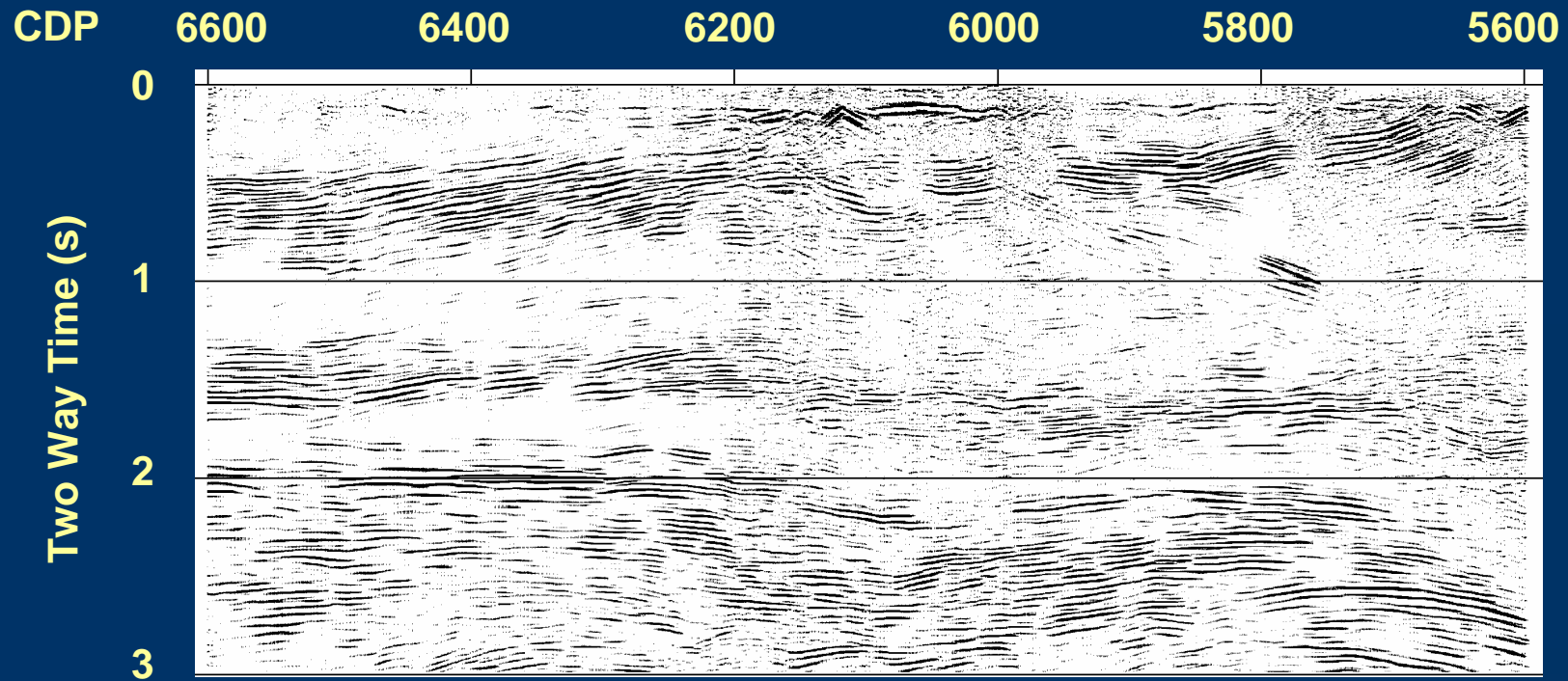
Line 05GA-T3 – Refraction statics



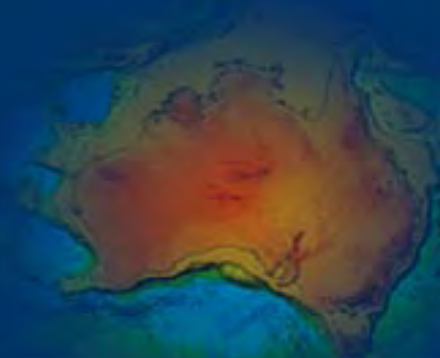
$V/H = 1$ $\overline{\hspace{1.5cm}}$ 4 km $\xrightarrow{\hspace{1.5cm}}$ NE



Line 05GA-T3 – Plus autostatics

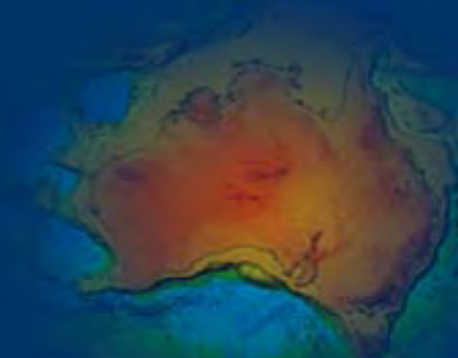


V/H = 1 4 km NE →

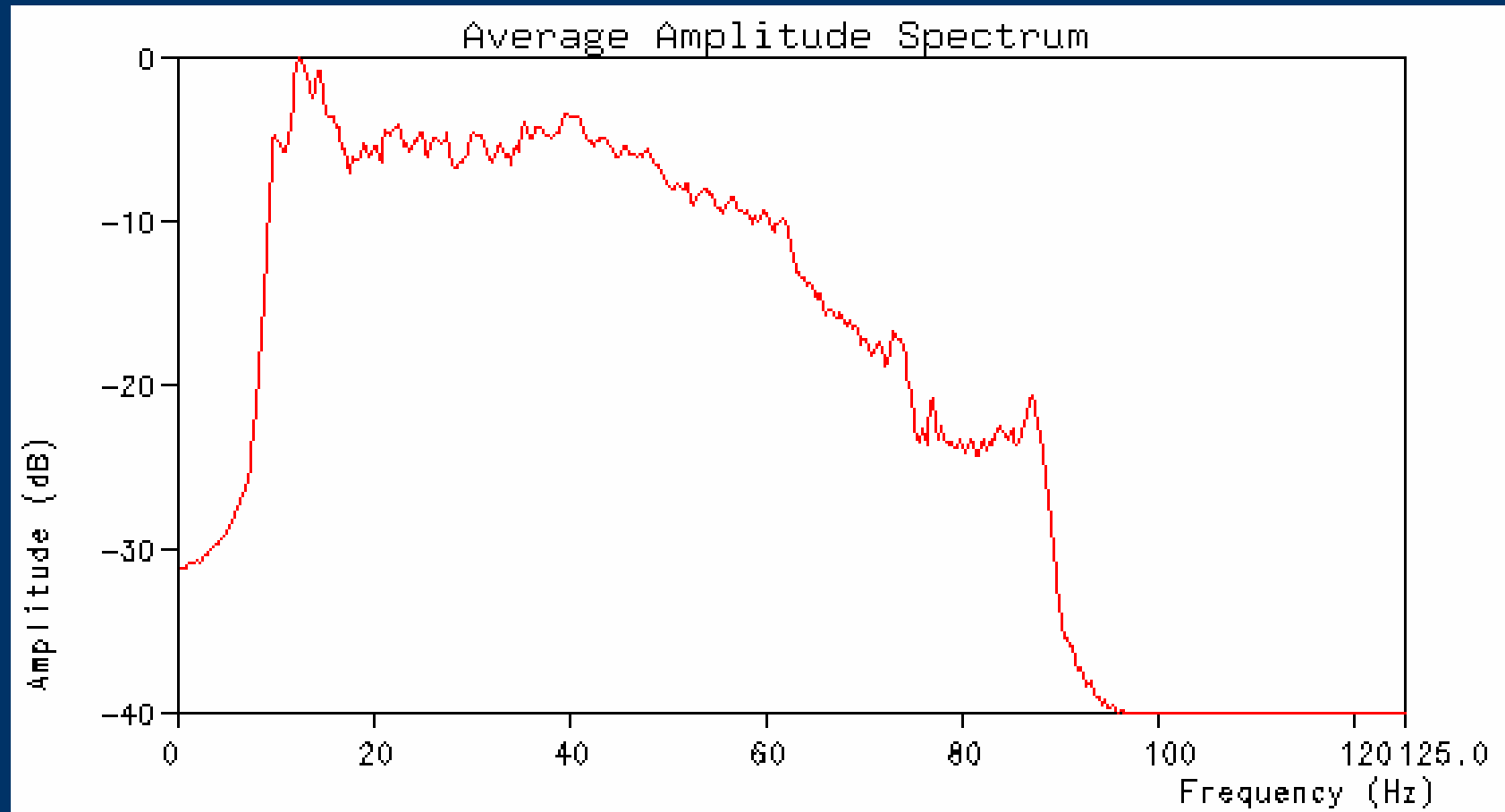


Spectral Equalisation

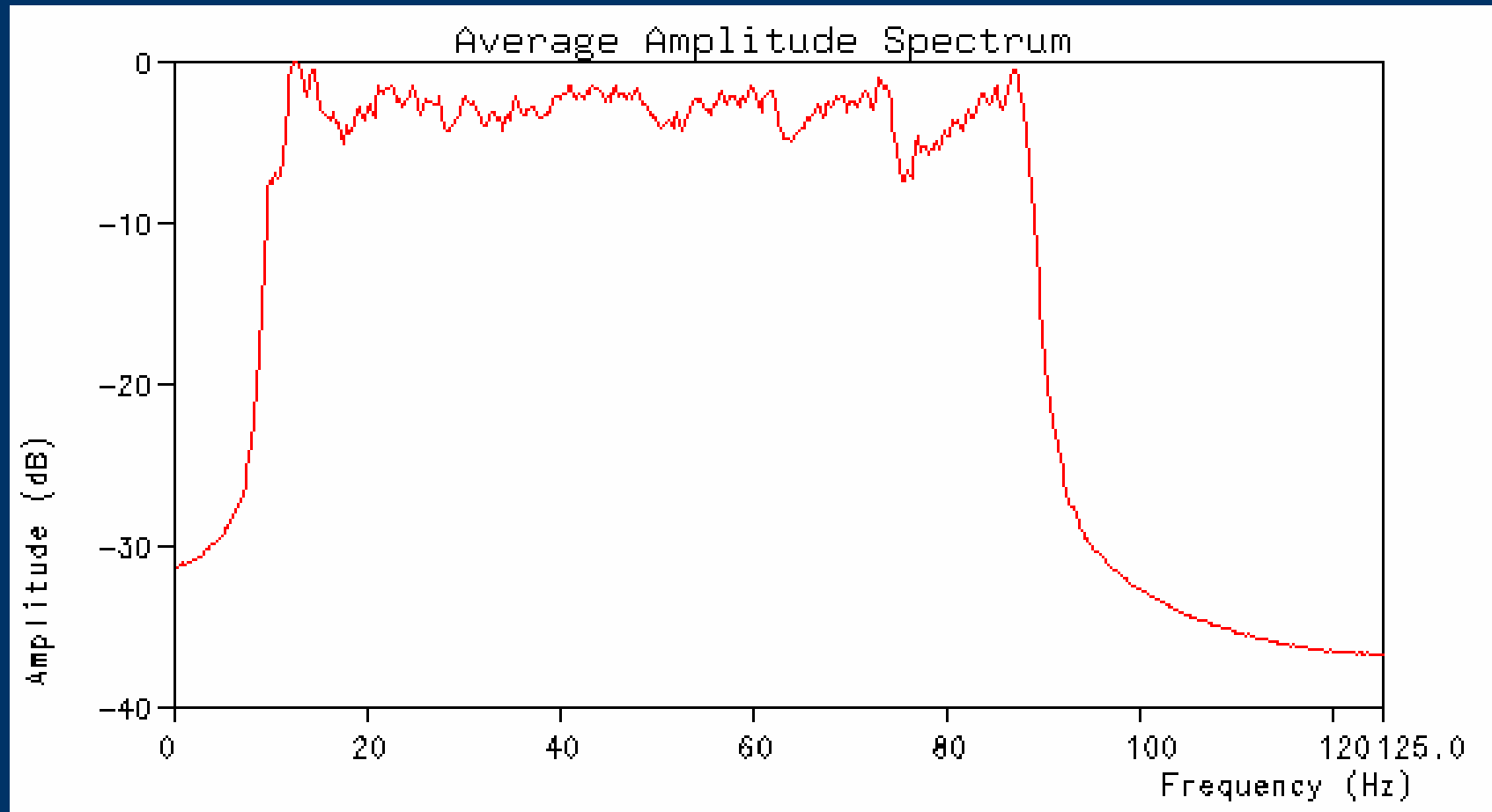
Boosts high frequencies relative to low frequencies, thus suppressing low frequency source generated noise



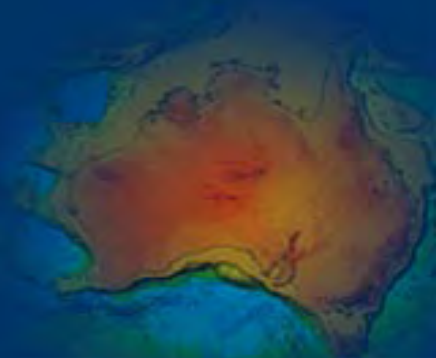
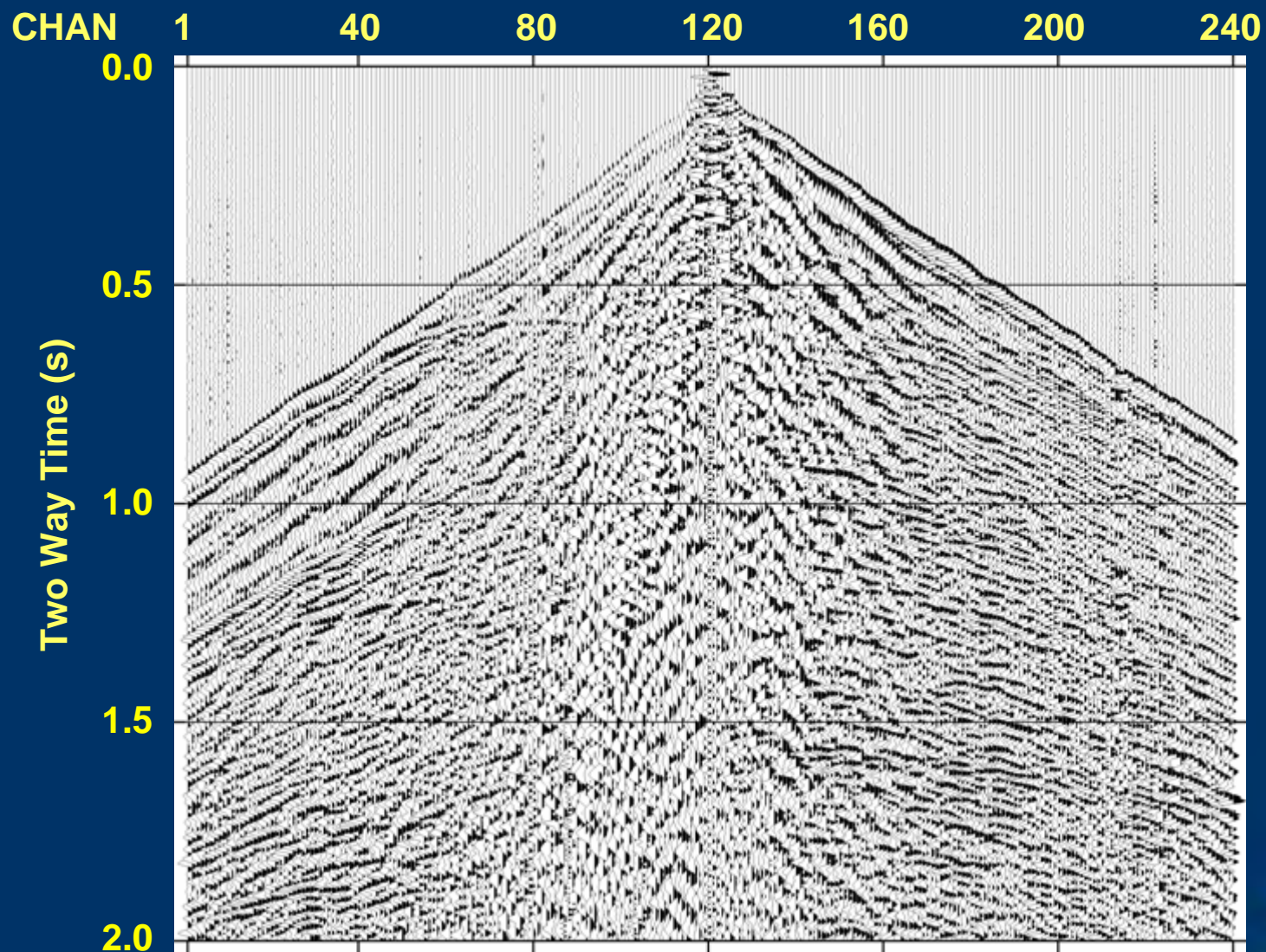
Frequency Spectrum - Pre spec



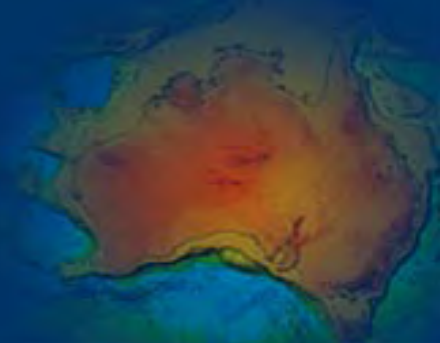
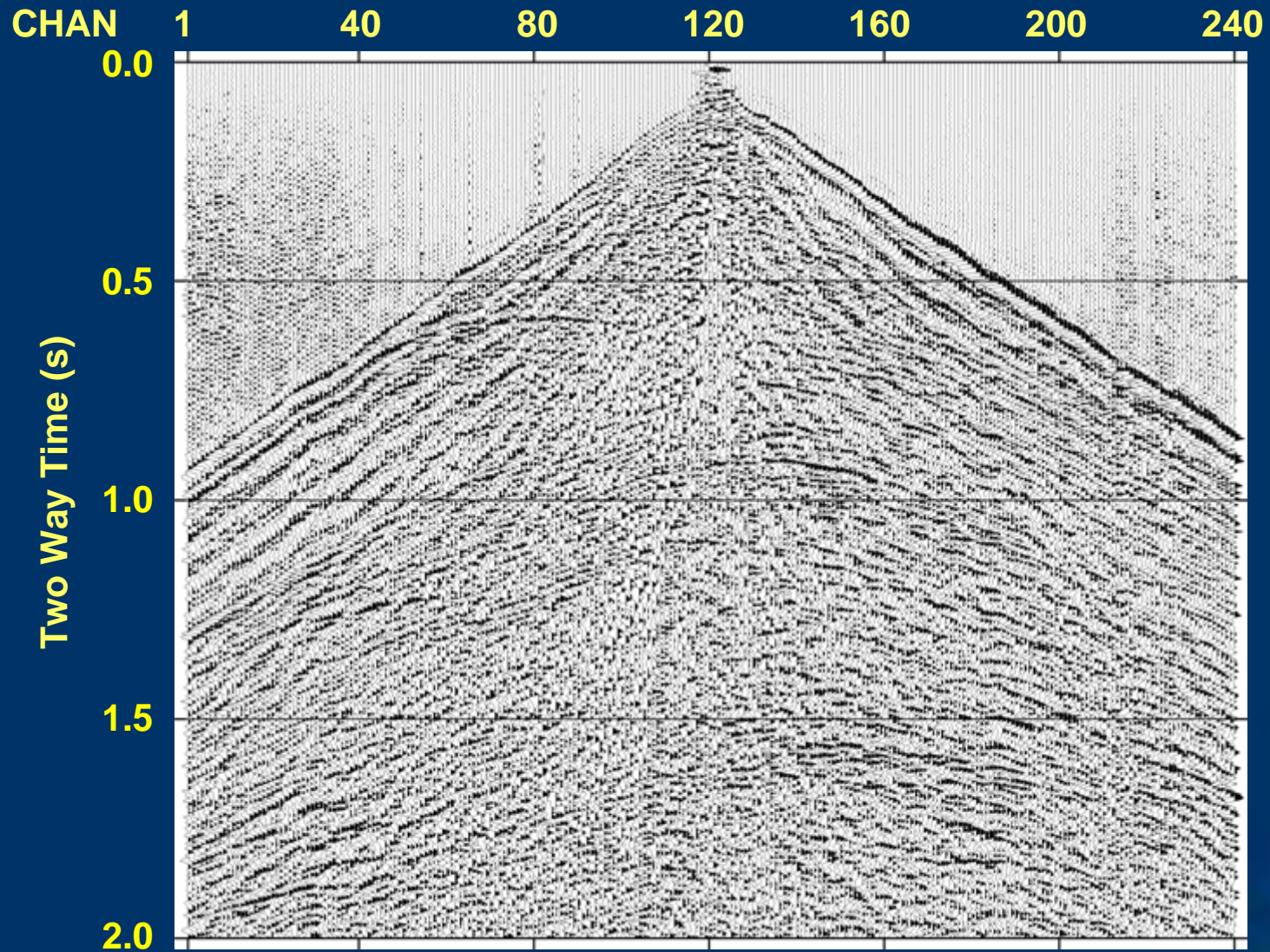
Frequency Spectrum - Post spec



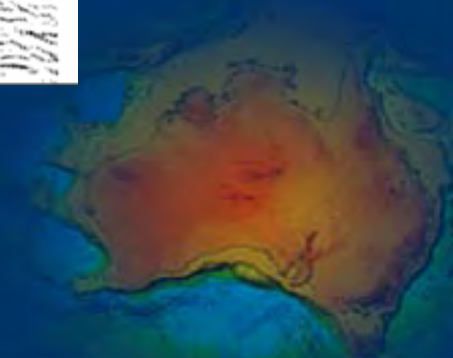
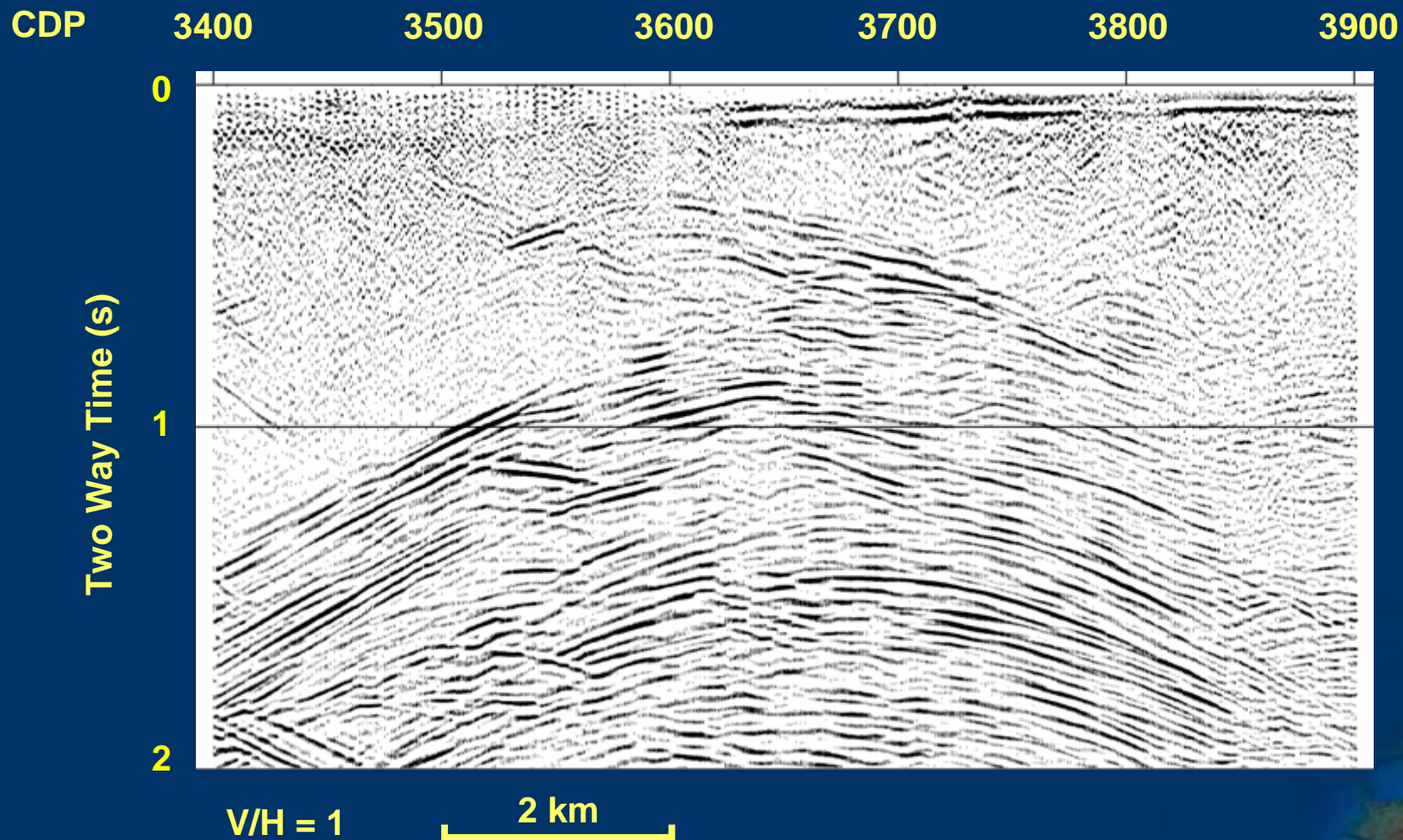
Shot Record - Pre spec



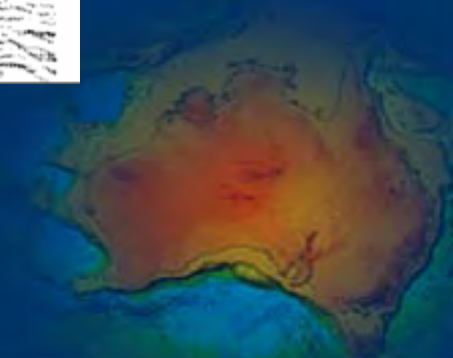
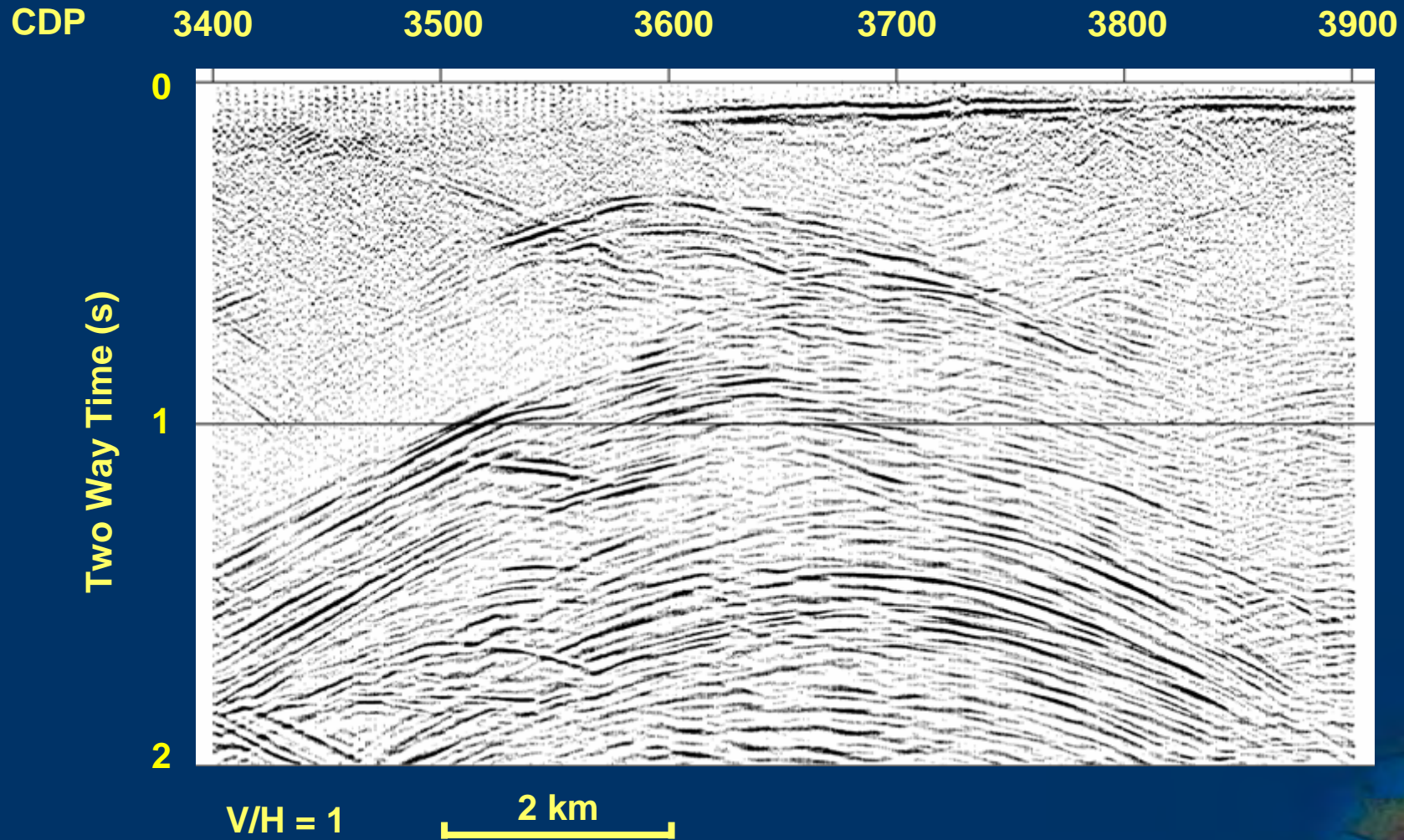
Shot Record - Post specq



Stack Section - Pre spec



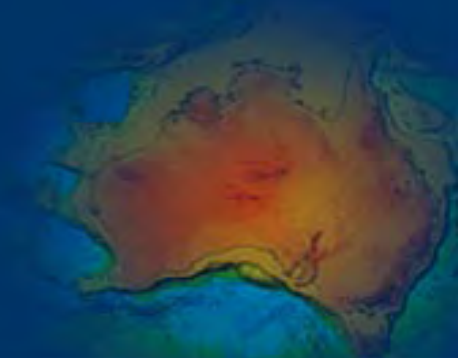
Stack Section - Post spec



Stacking (NMO) Velocity Analysis

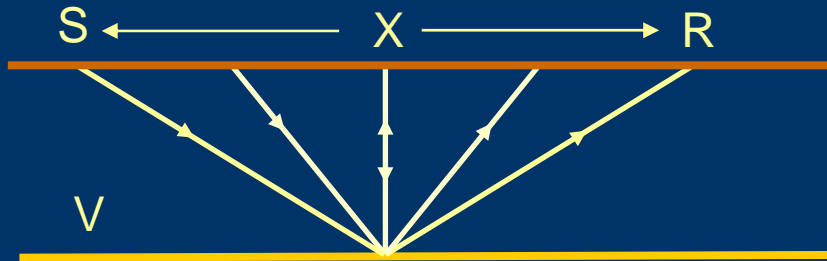
NMO correction corrects for non-coincidence of source and receivers

Stacking velocity is the velocity producing optimum stack across a CDP gather



Normal Moveout (NMO) Correction

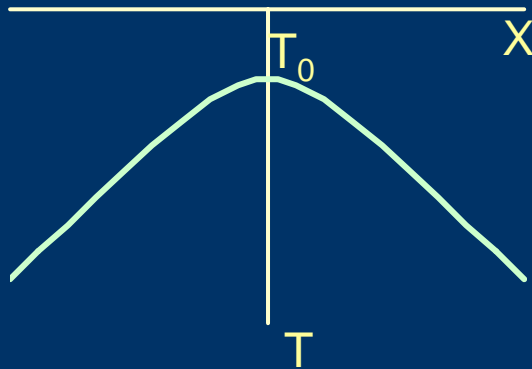
Horizontal reflector



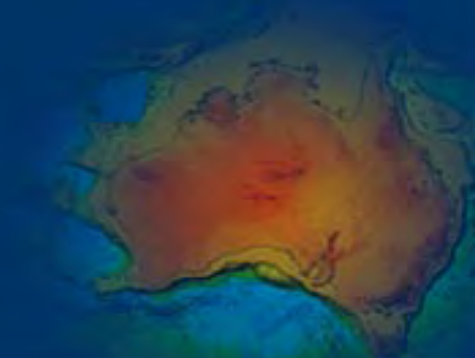
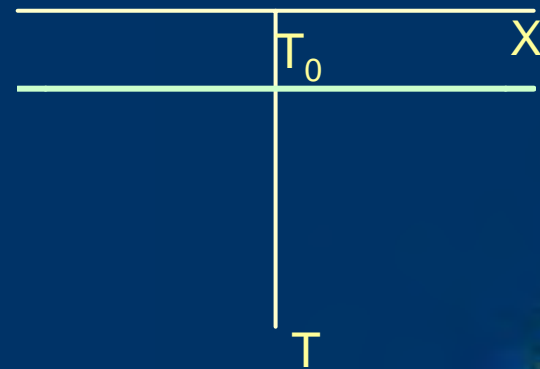
Moveout relationship

$$T^2 = T_0^2 + X^2/V^2$$

Uncorrected CDP gather



Corrected CDP gather

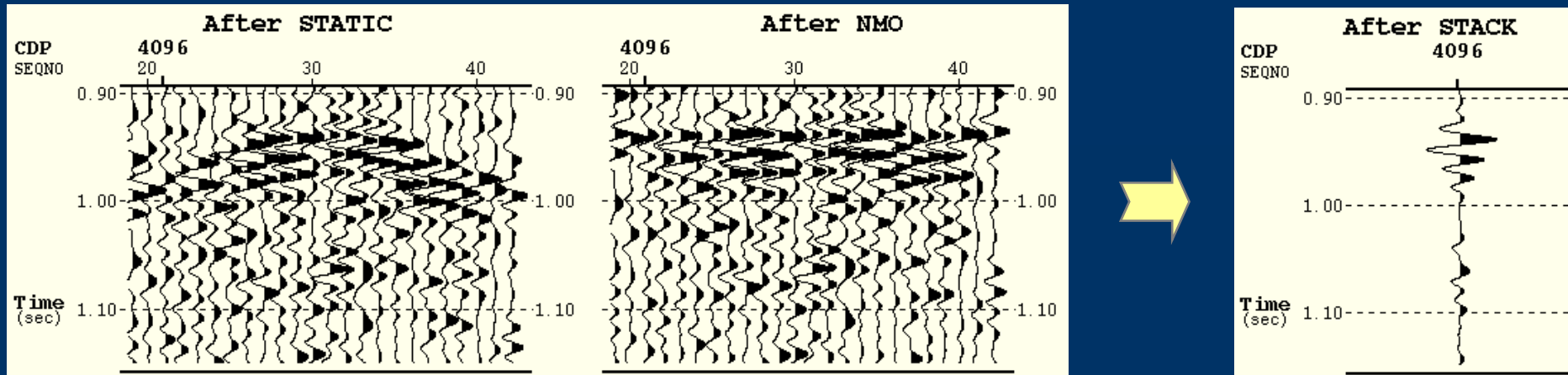


Normal Moveout (NMO) Correction and Stack

Uncorrected CDP gather

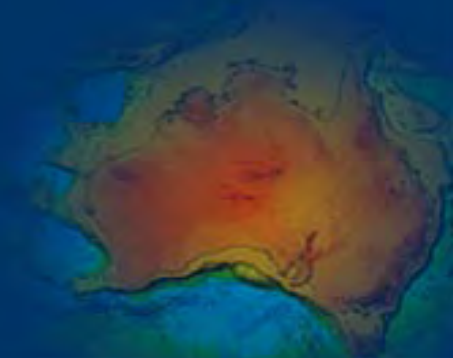
Corrected CDP gather

Stacked seismic trace



Stacking improves signal to noise by \sqrt{n} , where n is the fold

n	10	60	120
\sqrt{n}	3	8	11



Stacking velocities in hard rock

Higher velocity means less moveout, so easier to stack at TWT > 2 s, but can't convert to depth!

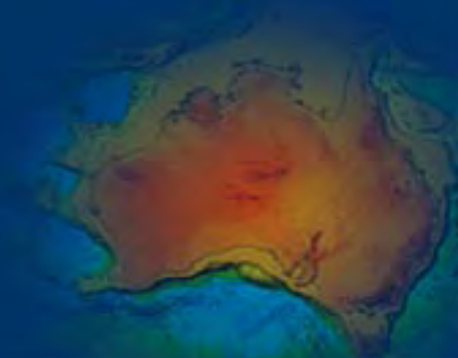
Velocity analysis is most critical (& difficult) in the top 1/2 second where moveout is greatest (& fold lowest).

Velocity is sensitive to

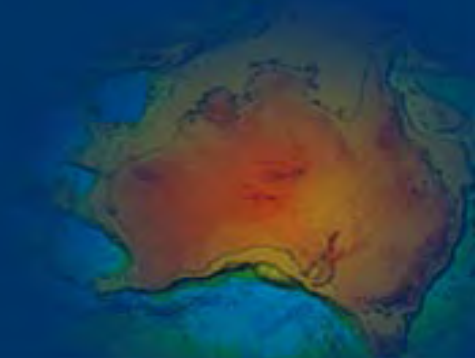
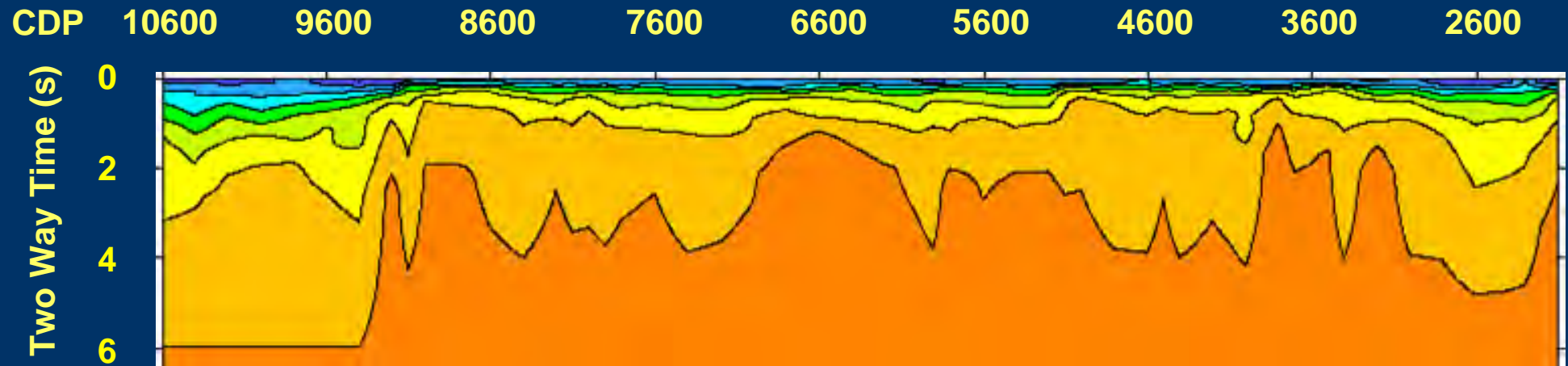
- Overlying low velocity layers

- Amount of static shift

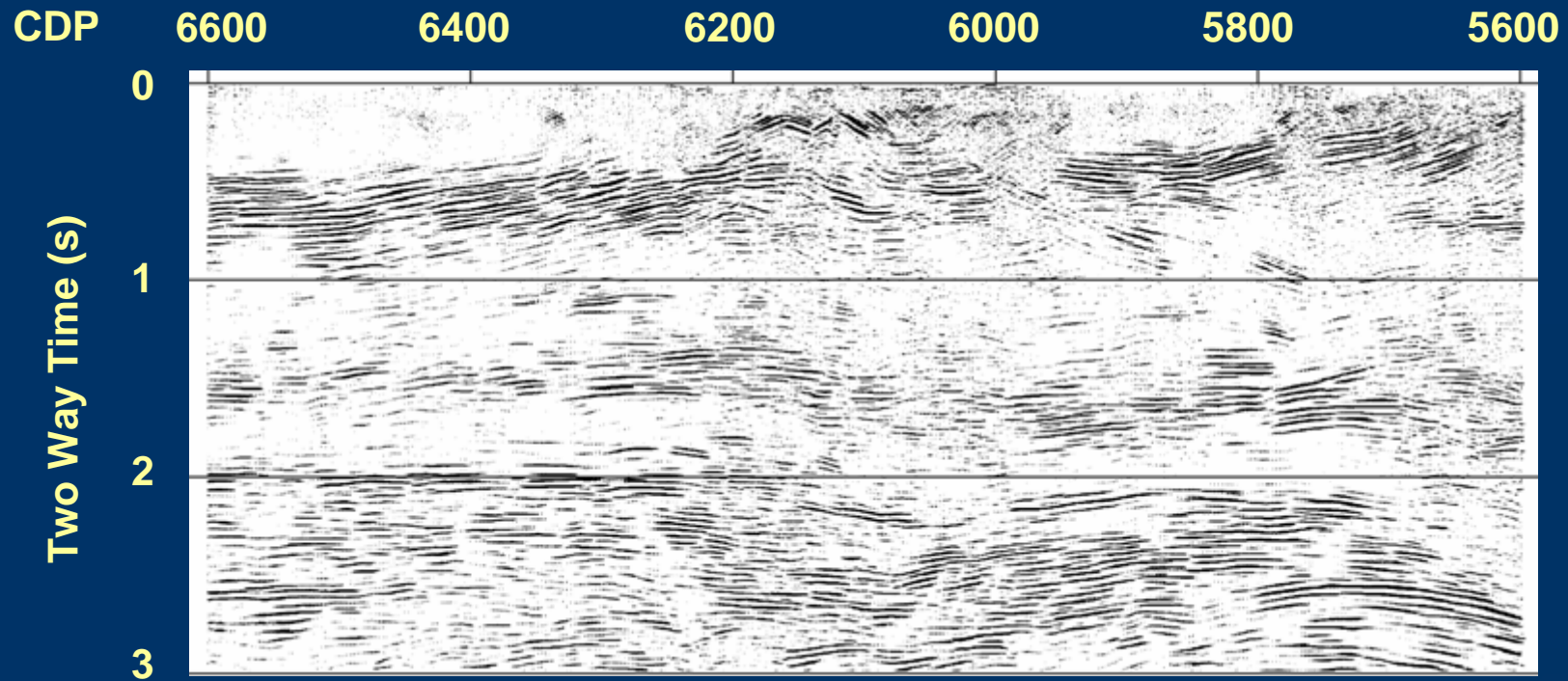
- Dip of reflectors



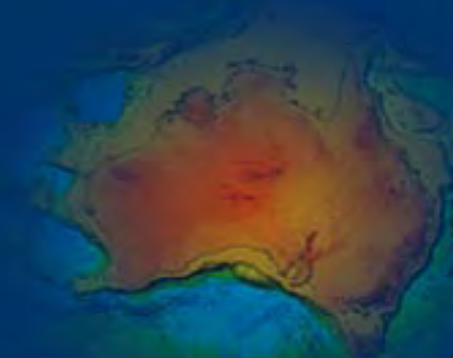
Normal Moveout (NMO) Velocity for 05GA-T3



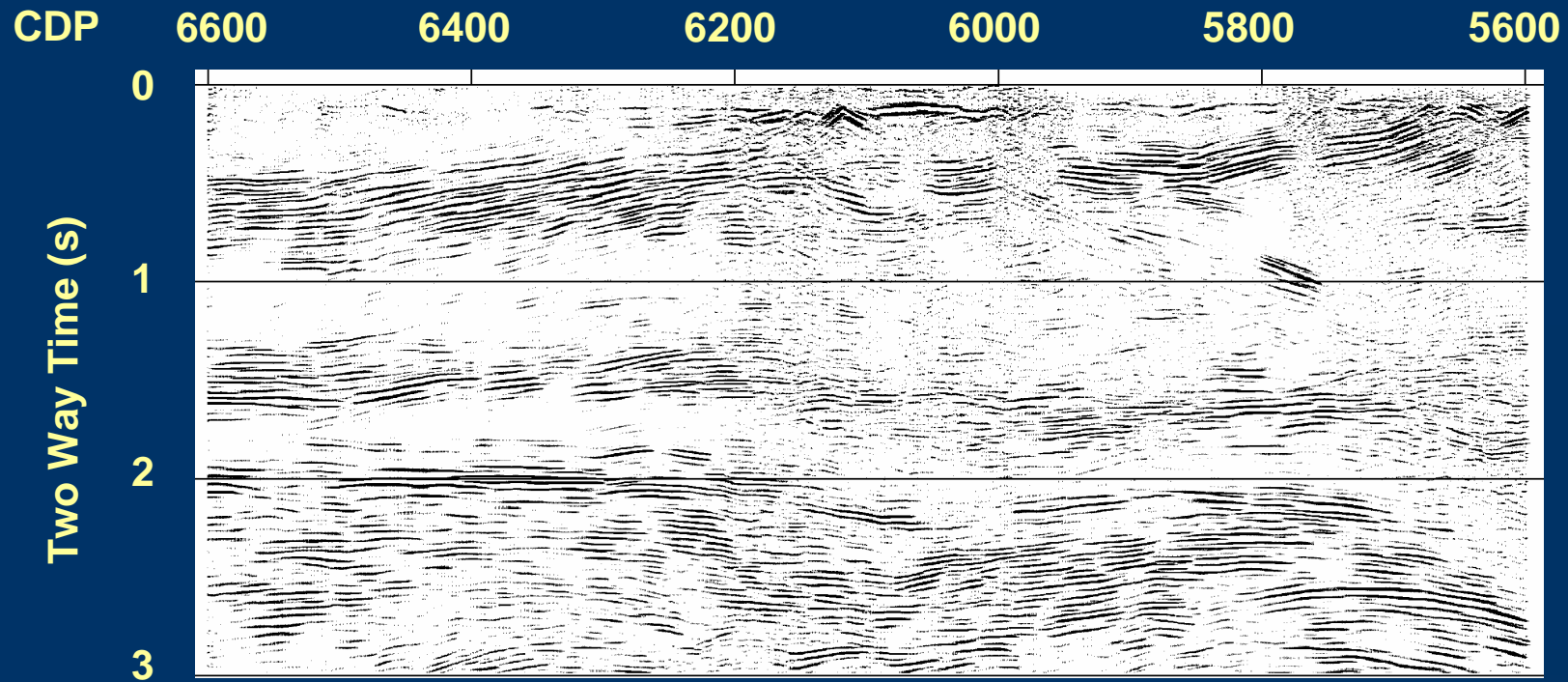
Line 05GA-T3 – Single velocity function



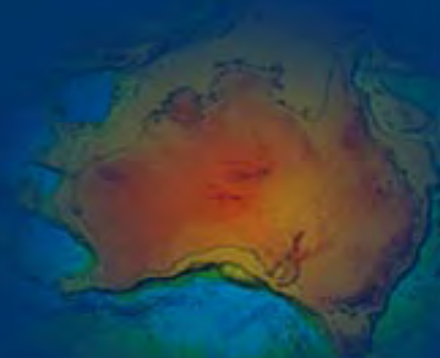
$V/H = 1$ | 4 km | NE →



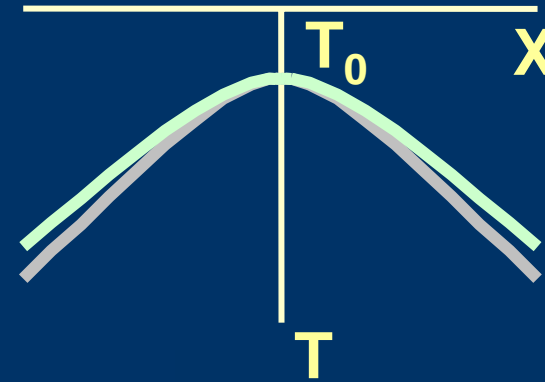
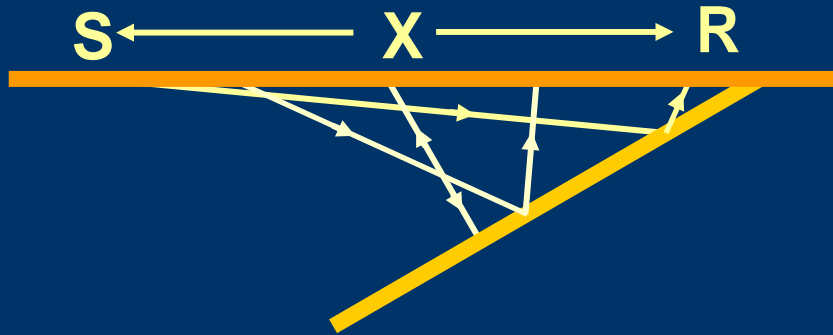
Line 05GA-T3 – Detailed velocity analysis



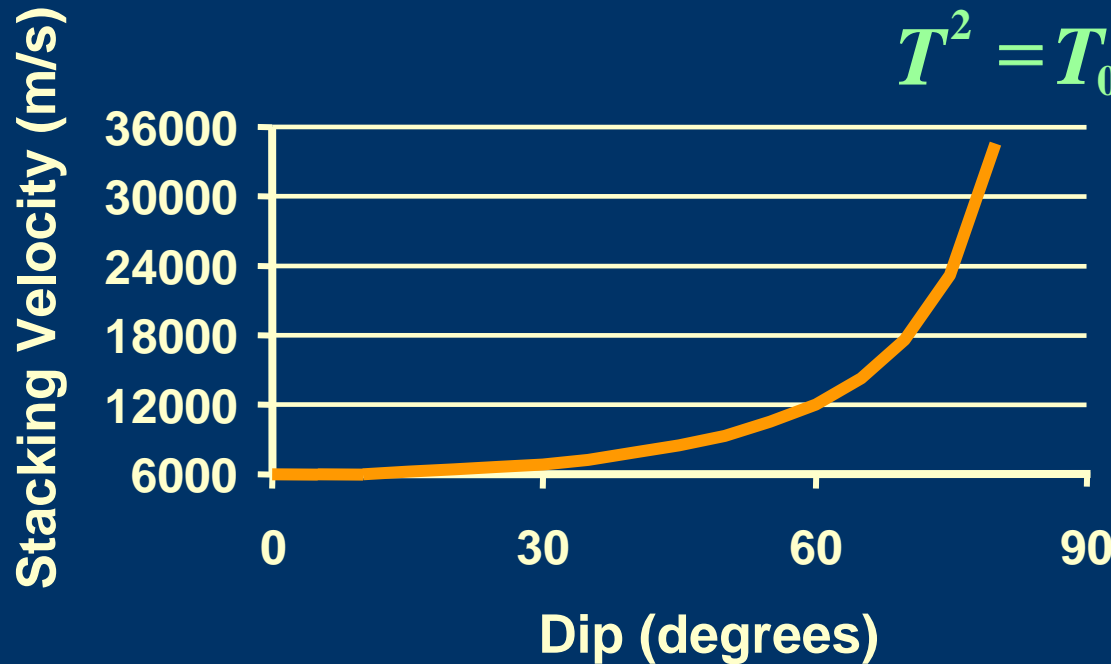
V/H = 1 | 4 km | NE →



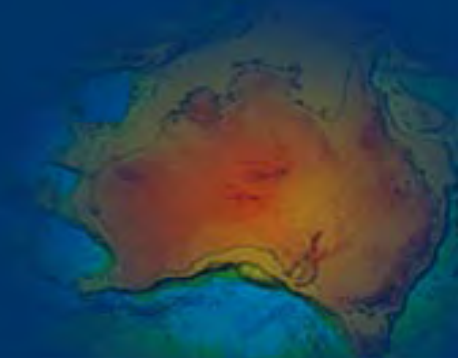
Effect of Dip on Stacking Velocity



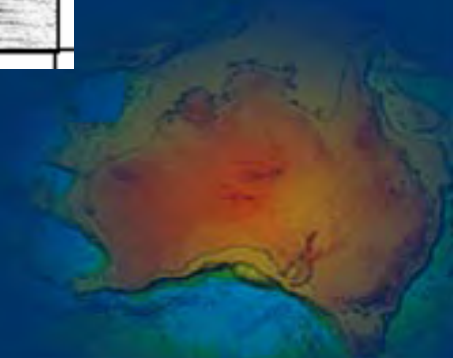
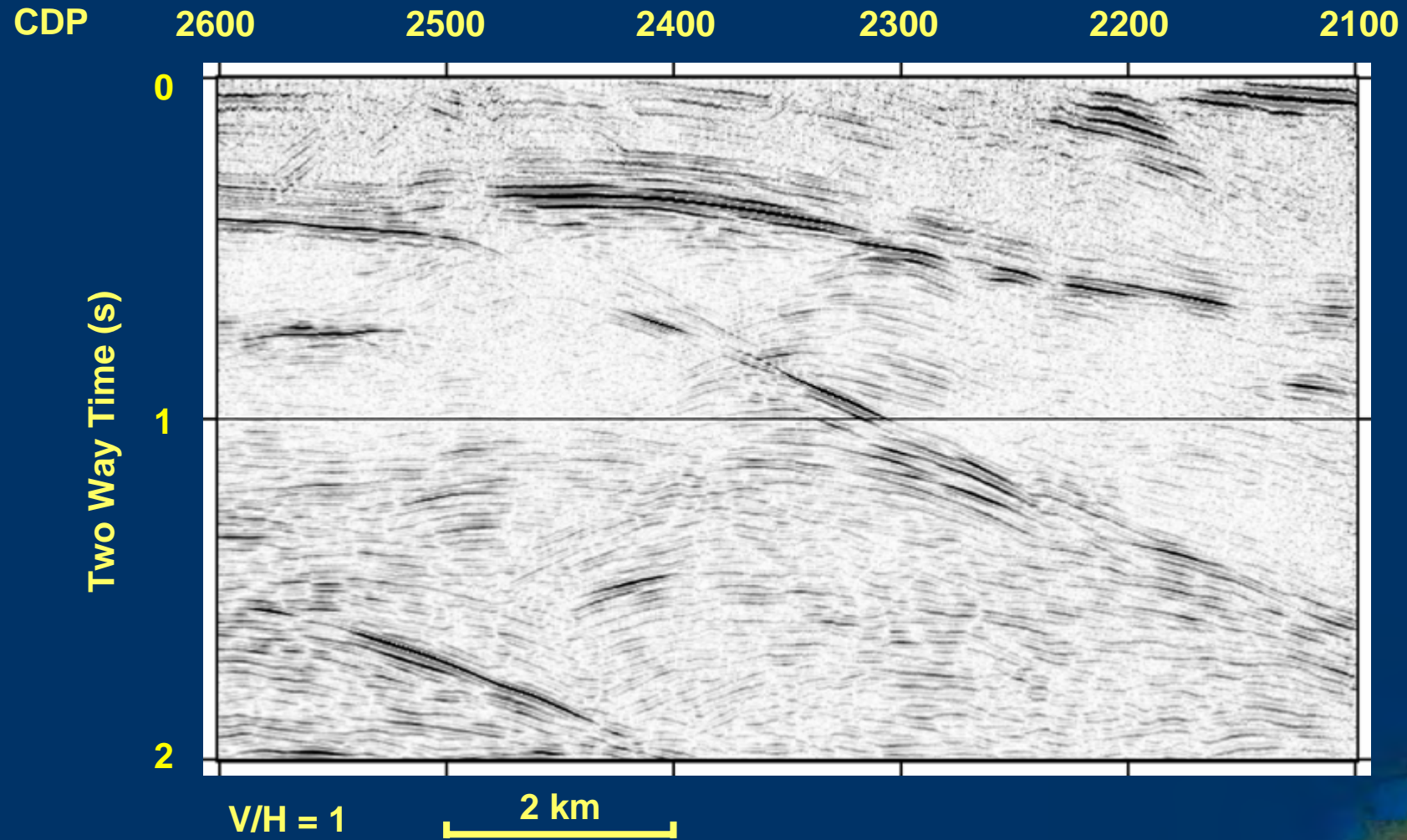
$$T^2 = T_0^2 + X^2 \cos^2 \alpha / V^2$$



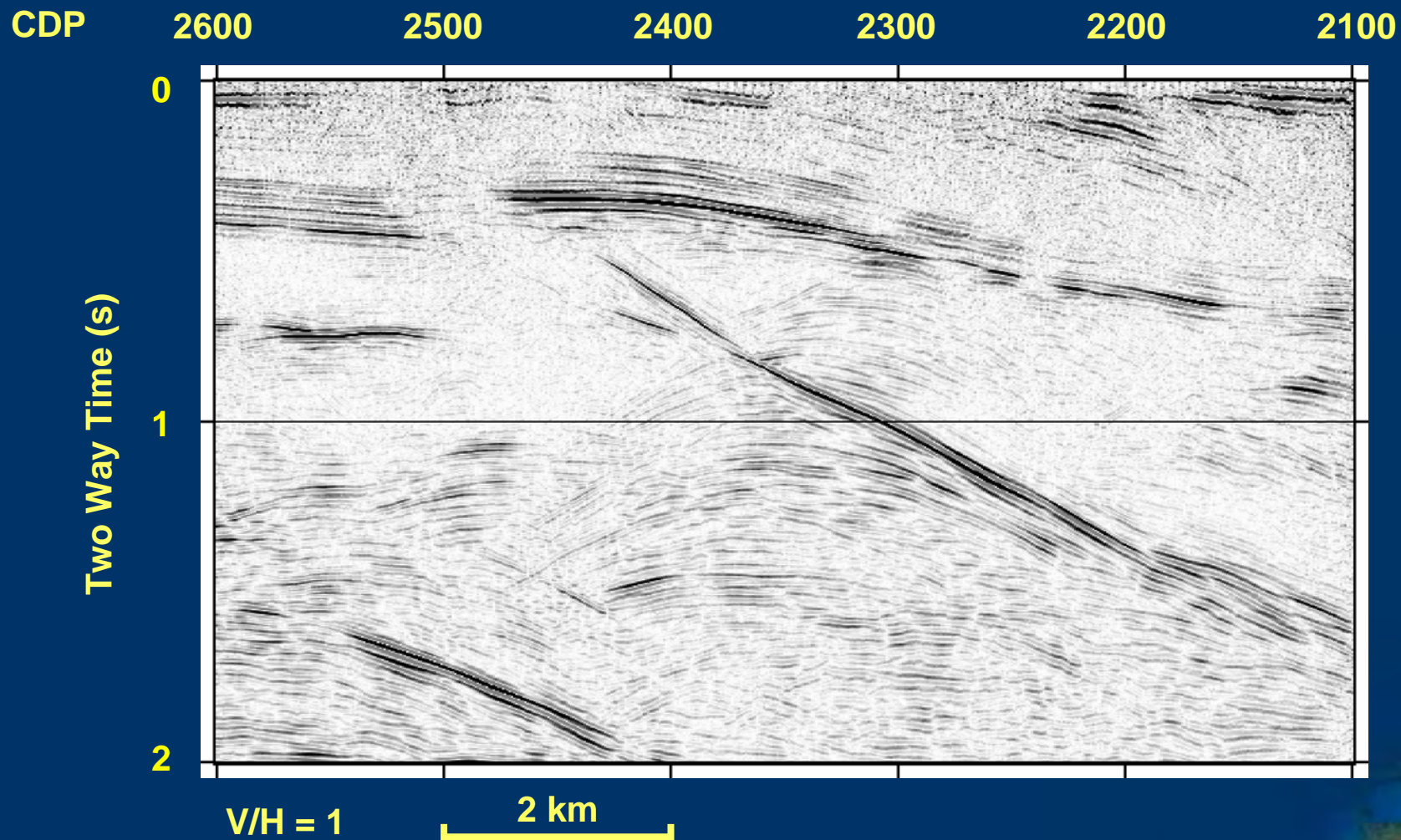
Need Dip Moveout Correction (DMO)



05GA-T3 - Stack

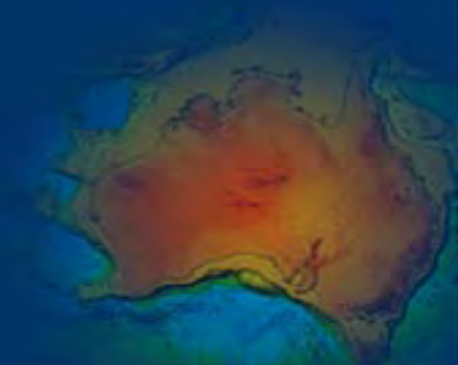


05GA-T3 - Stack with DMO

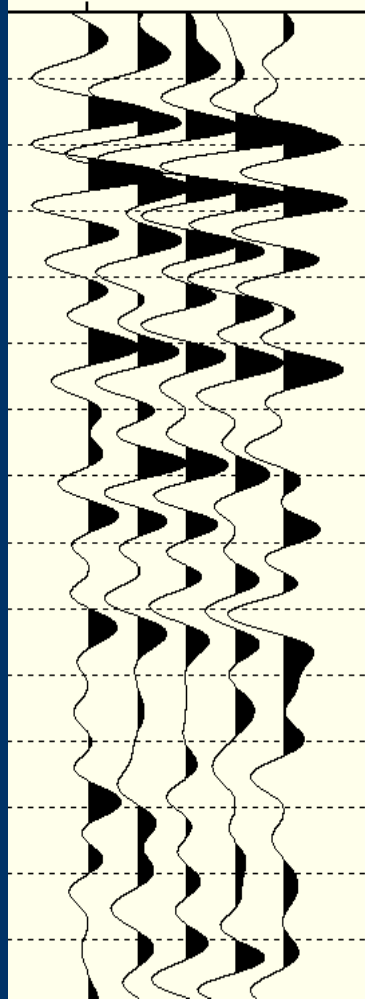


Migration

Moves reflectors to their correct positions

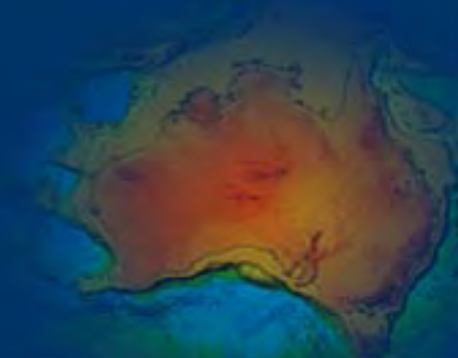


Seismic Section - Set of Stacked Traces

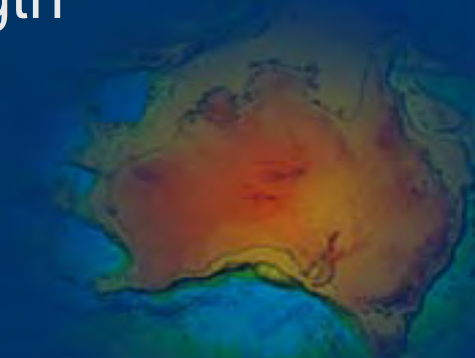
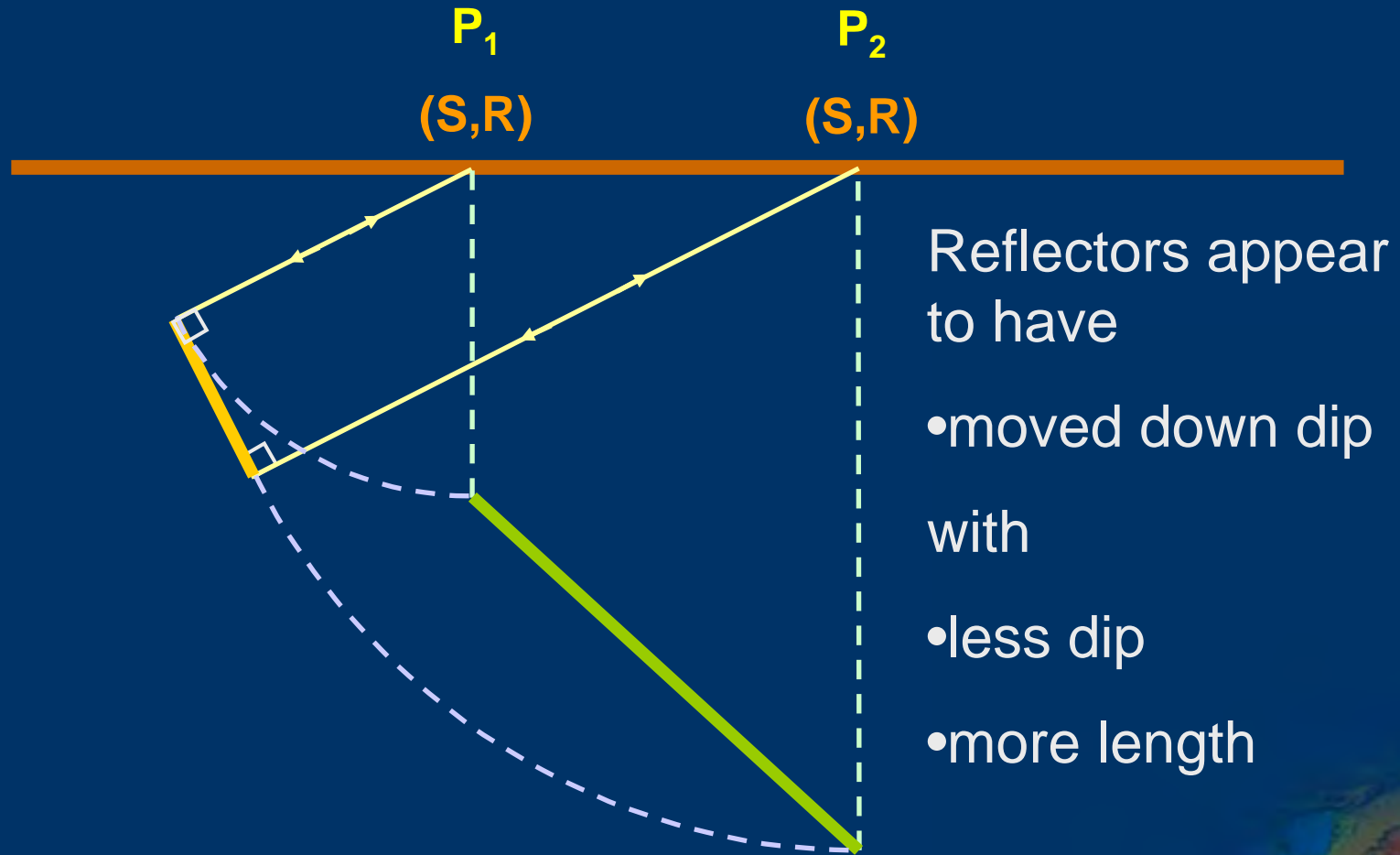


But

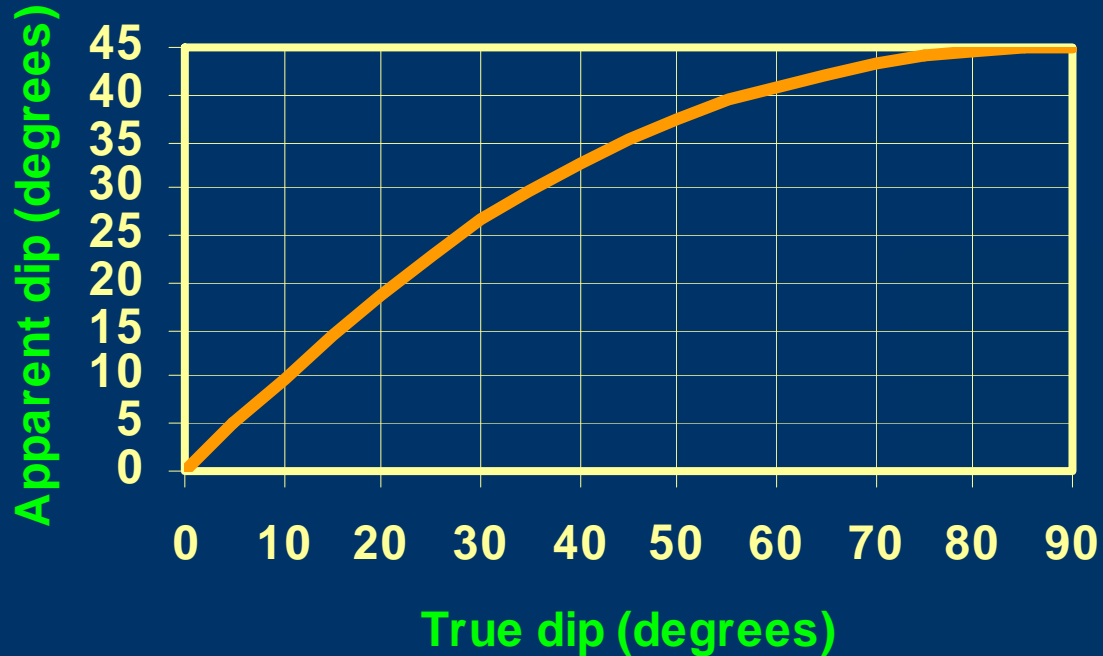
Seismic data are recorded in (two-way travel) time and the traces are displayed vertically with time increasing downwards



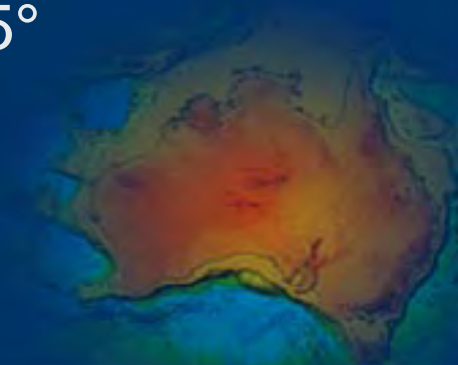
Imaging of Dipping Reflectors on Stack Section



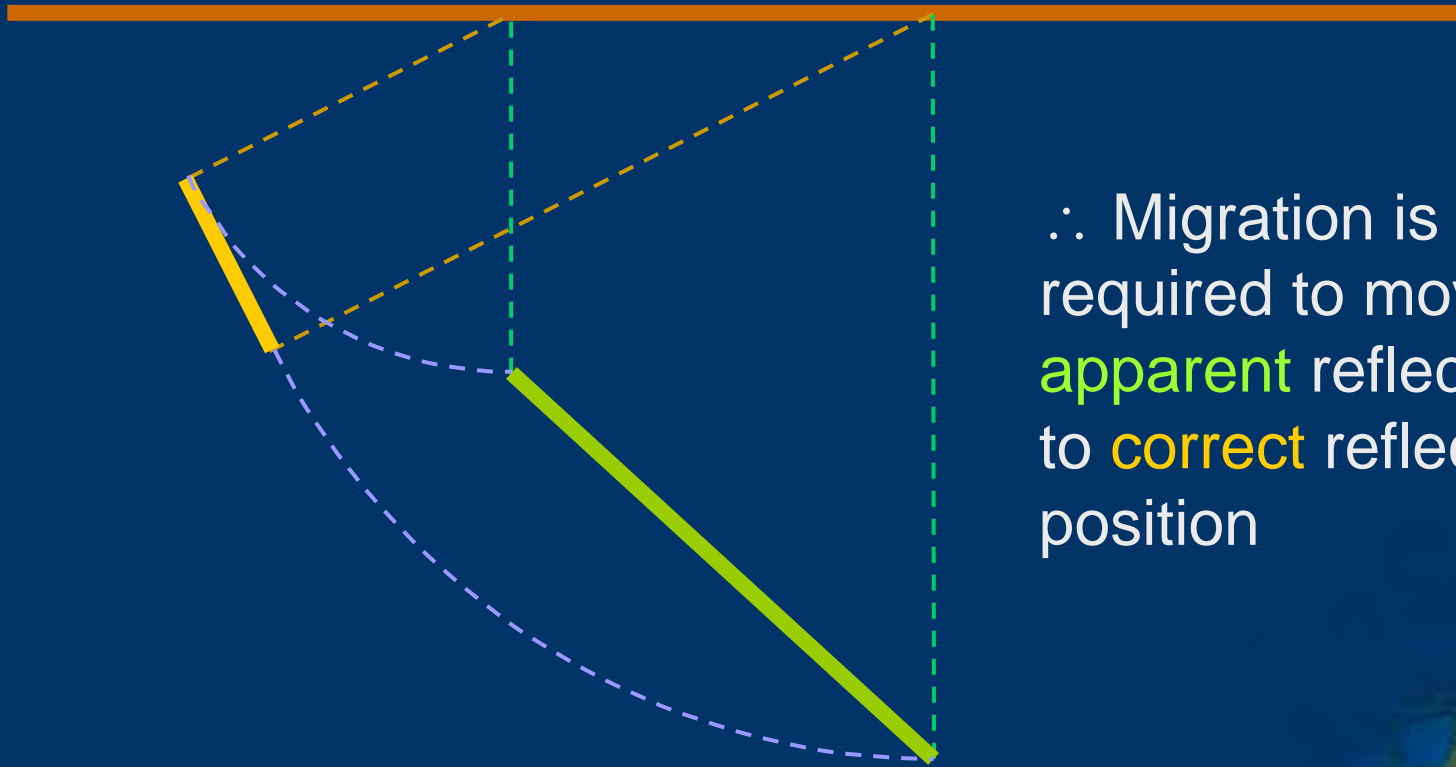
Apparent Dips on Un-migrated Stack Sections



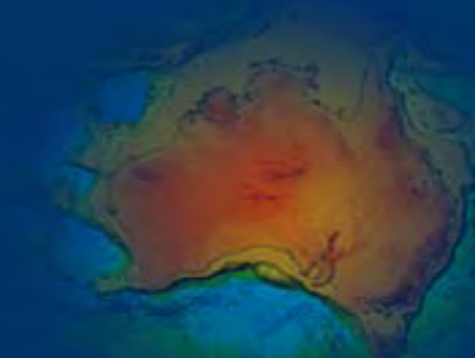
Note that the apparent dip will not exceed 45°



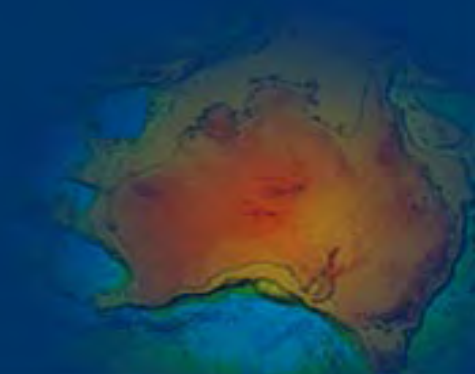
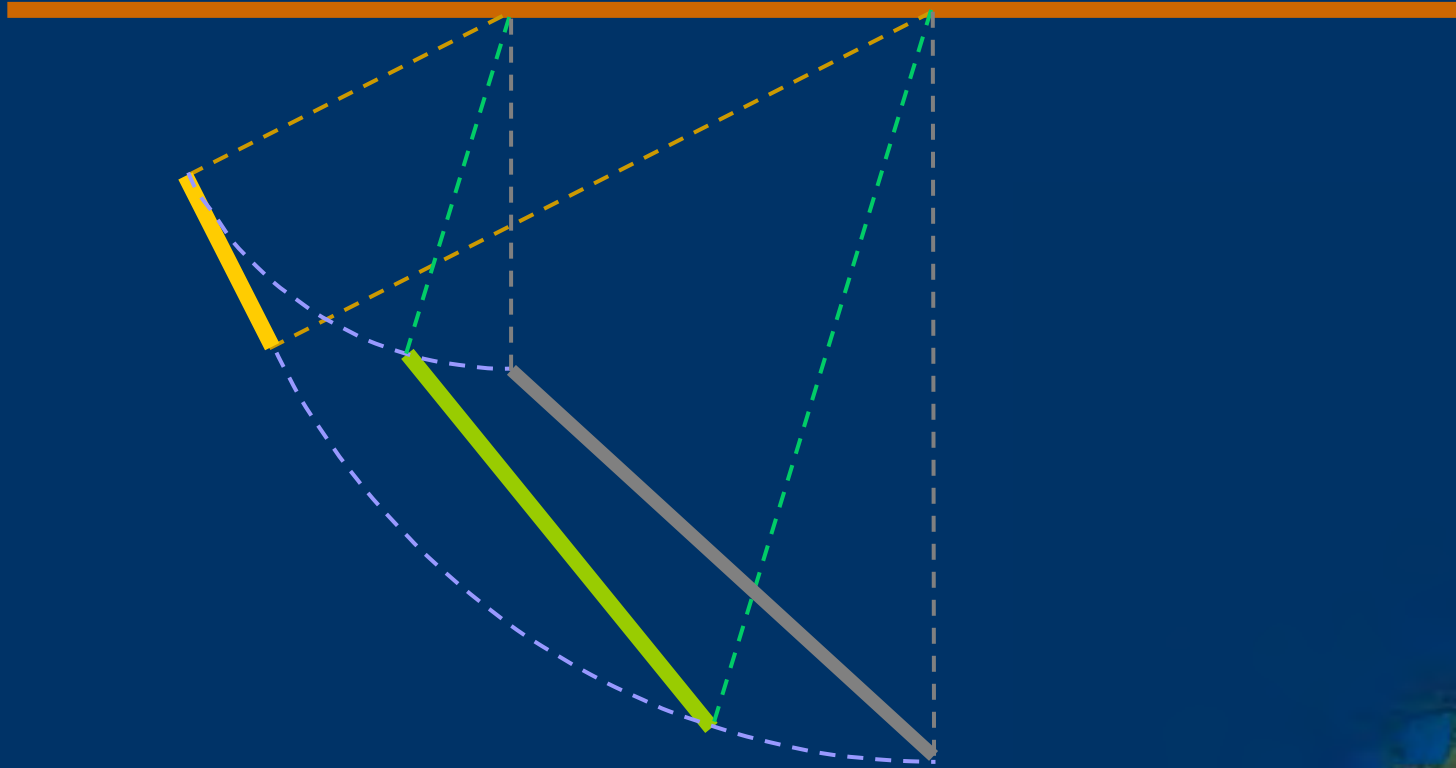
Migration of Dipping Reflector



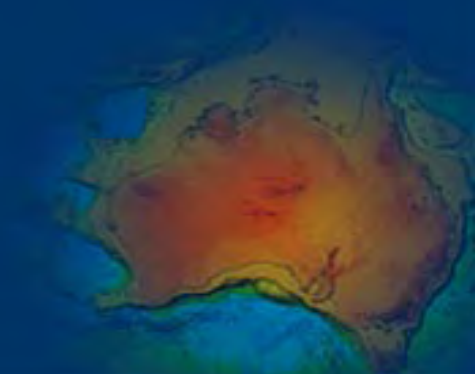
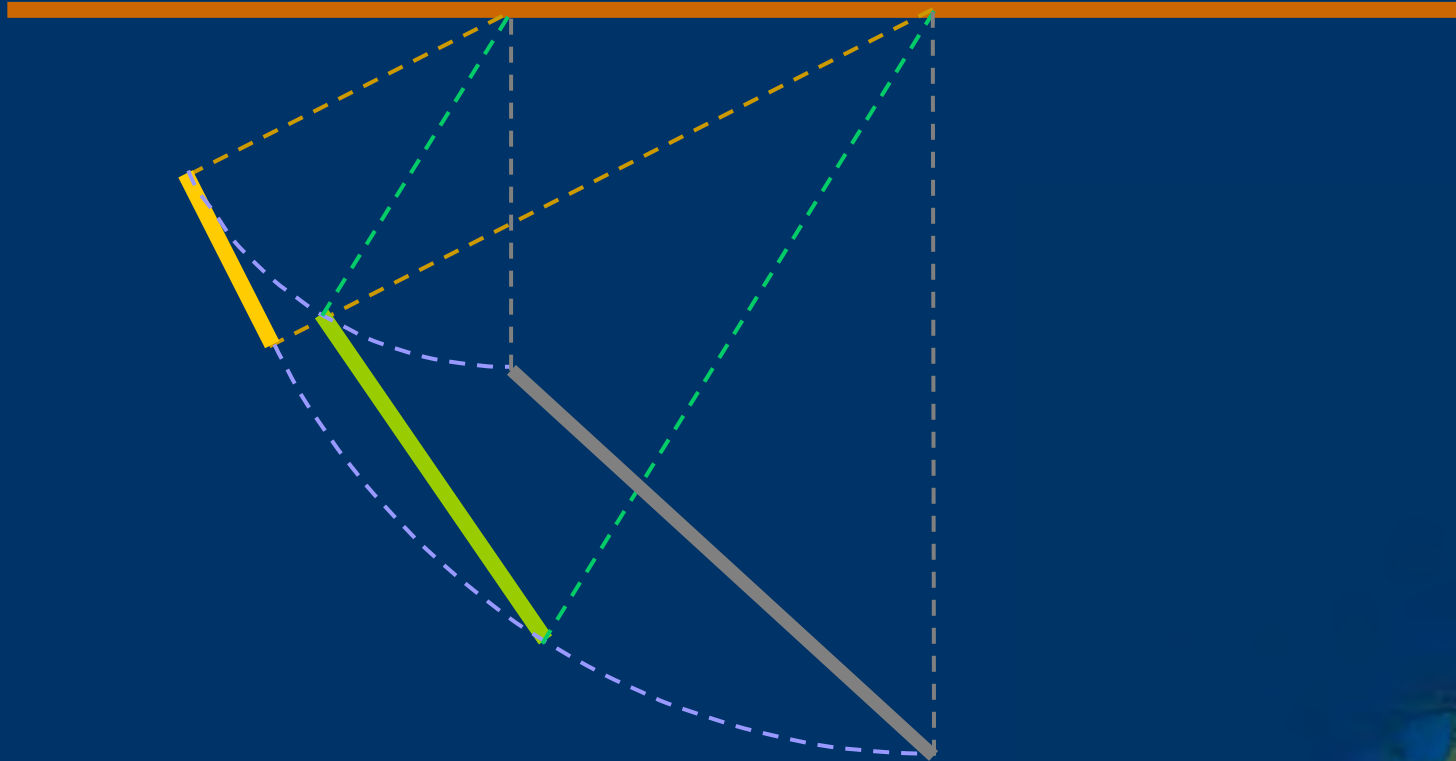
∴ Migration is required to move **apparent** reflector to **correct** reflector position



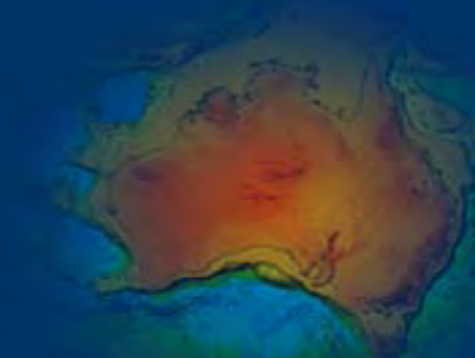
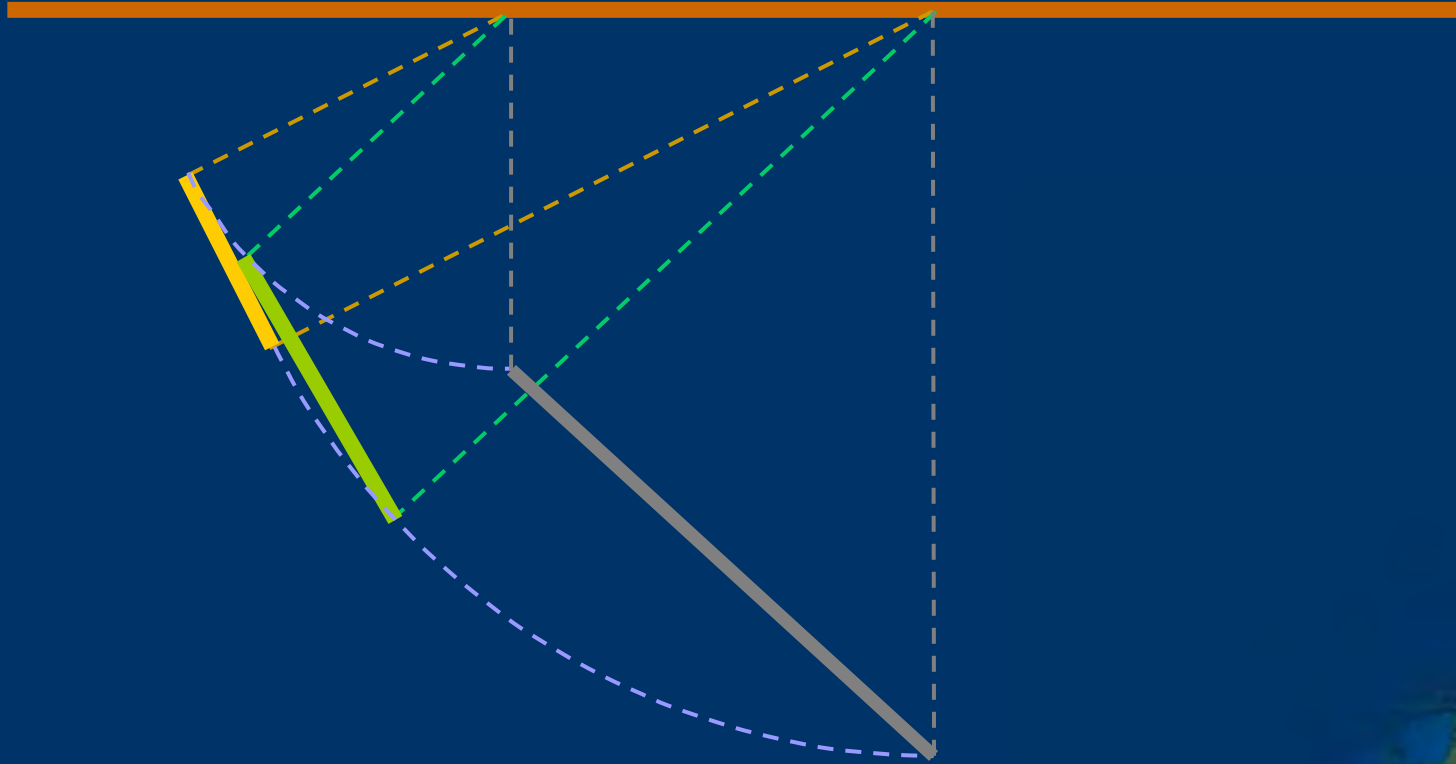
Migration of Dipping Reflector



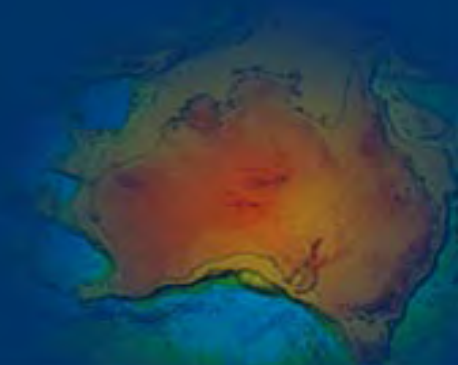
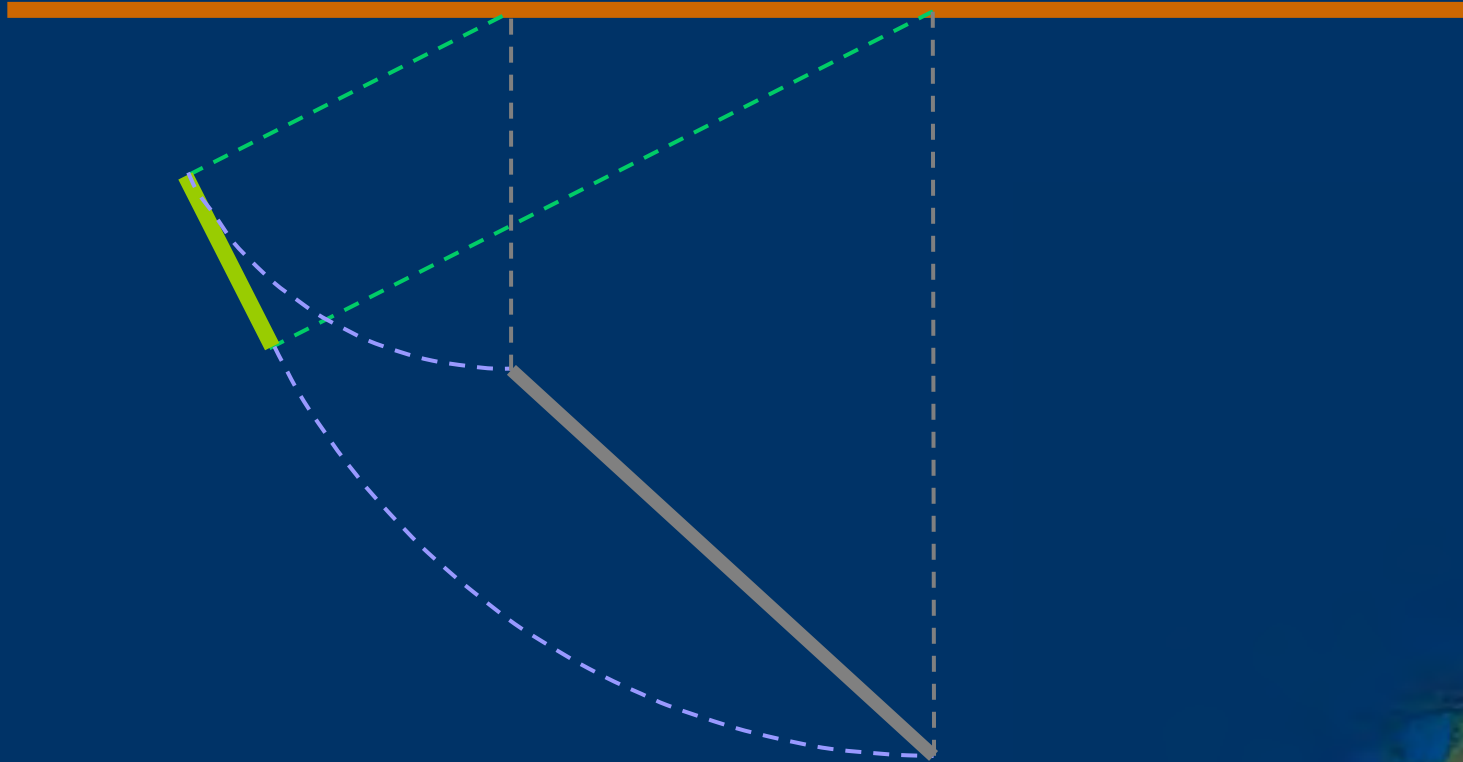
Migration of Dipping Reflector



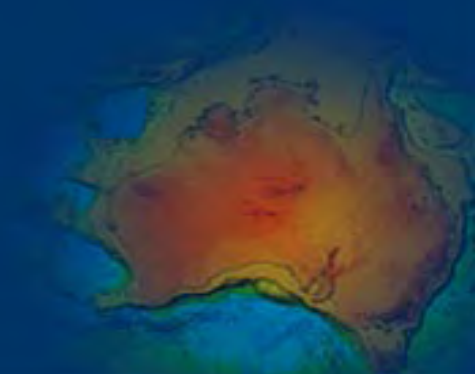
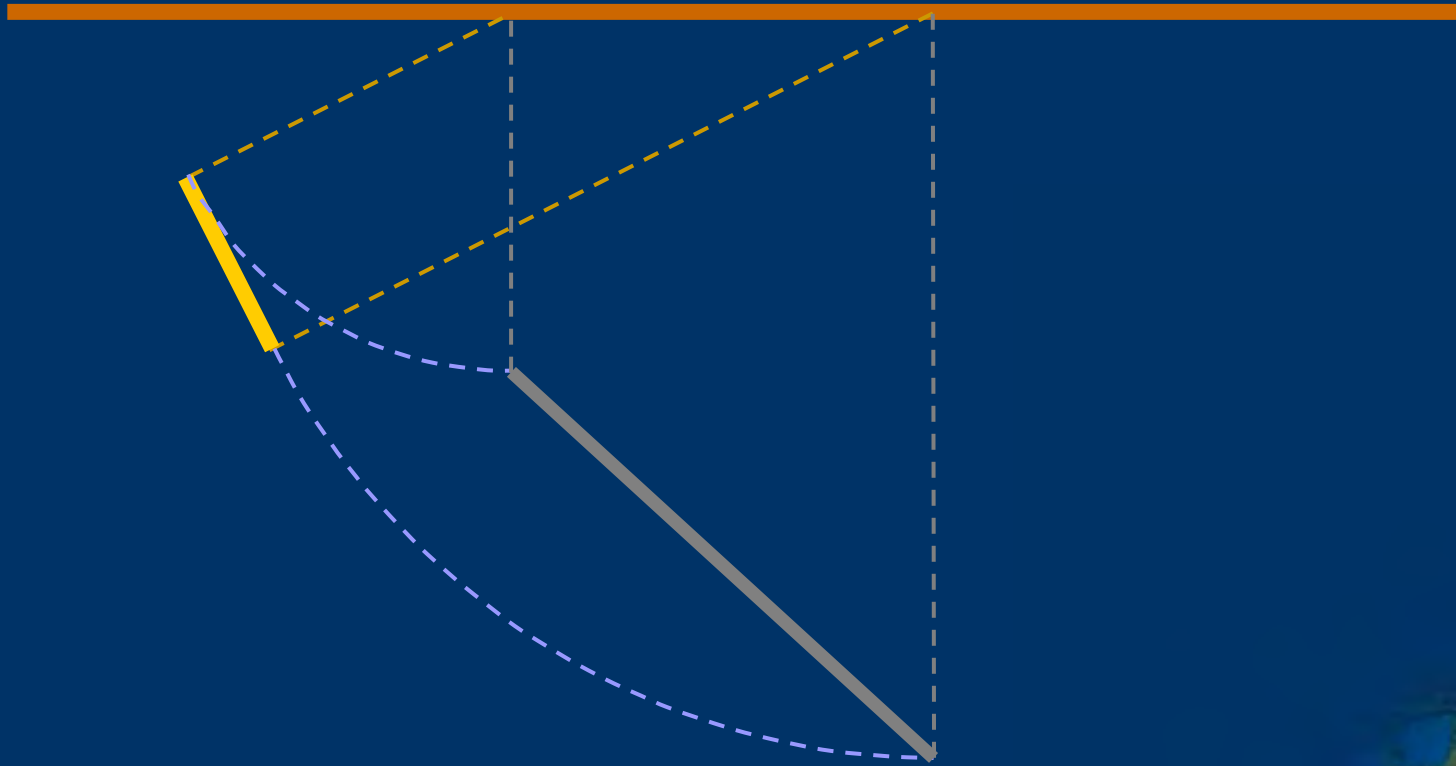
Migration of Dipping Reflector



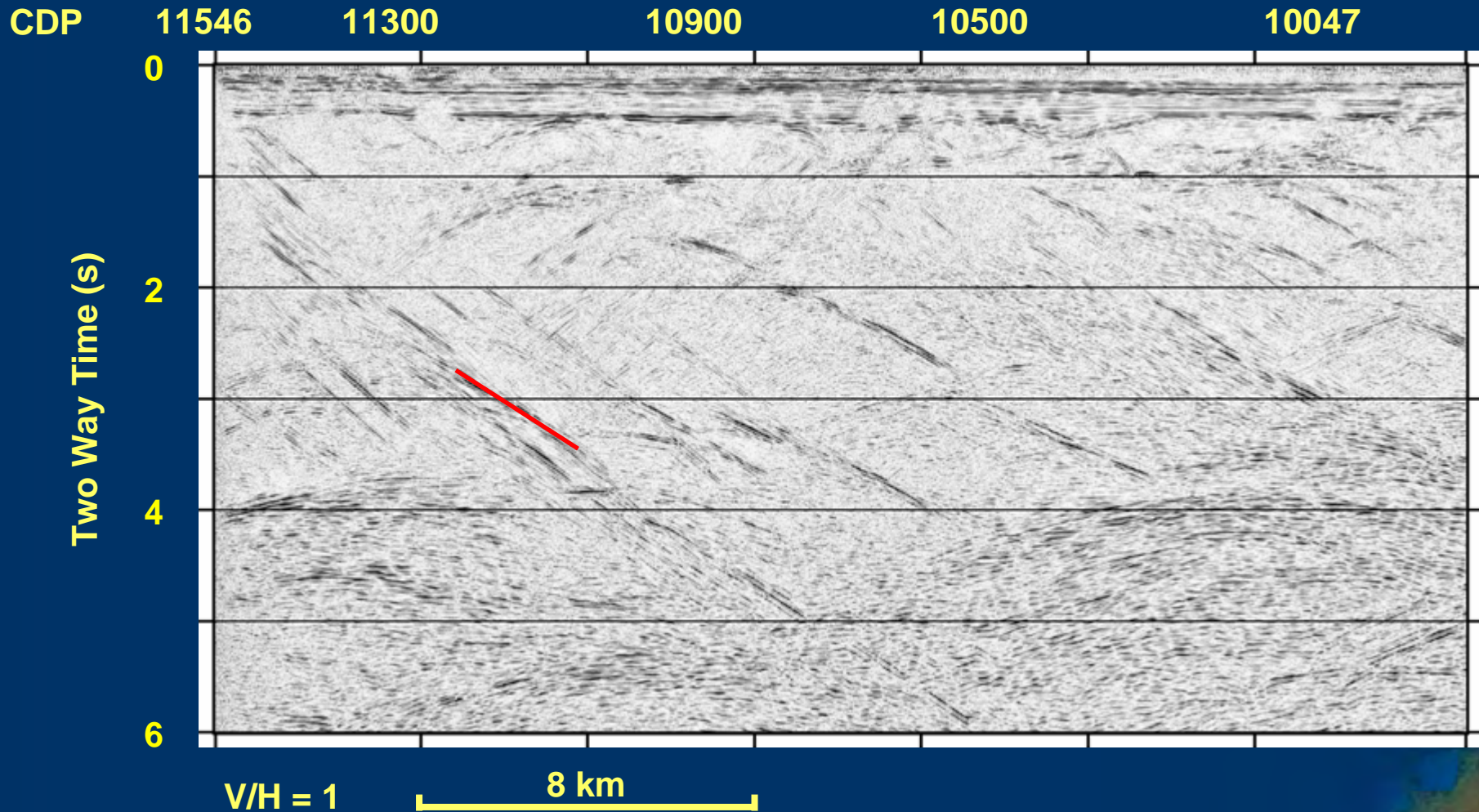
Migration of Dipping Reflector



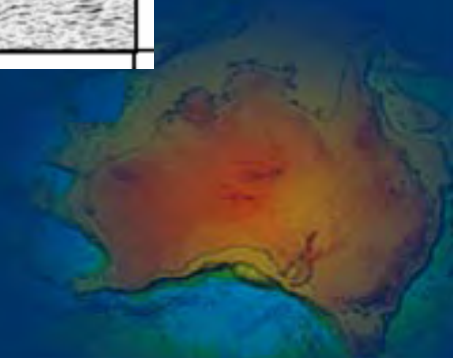
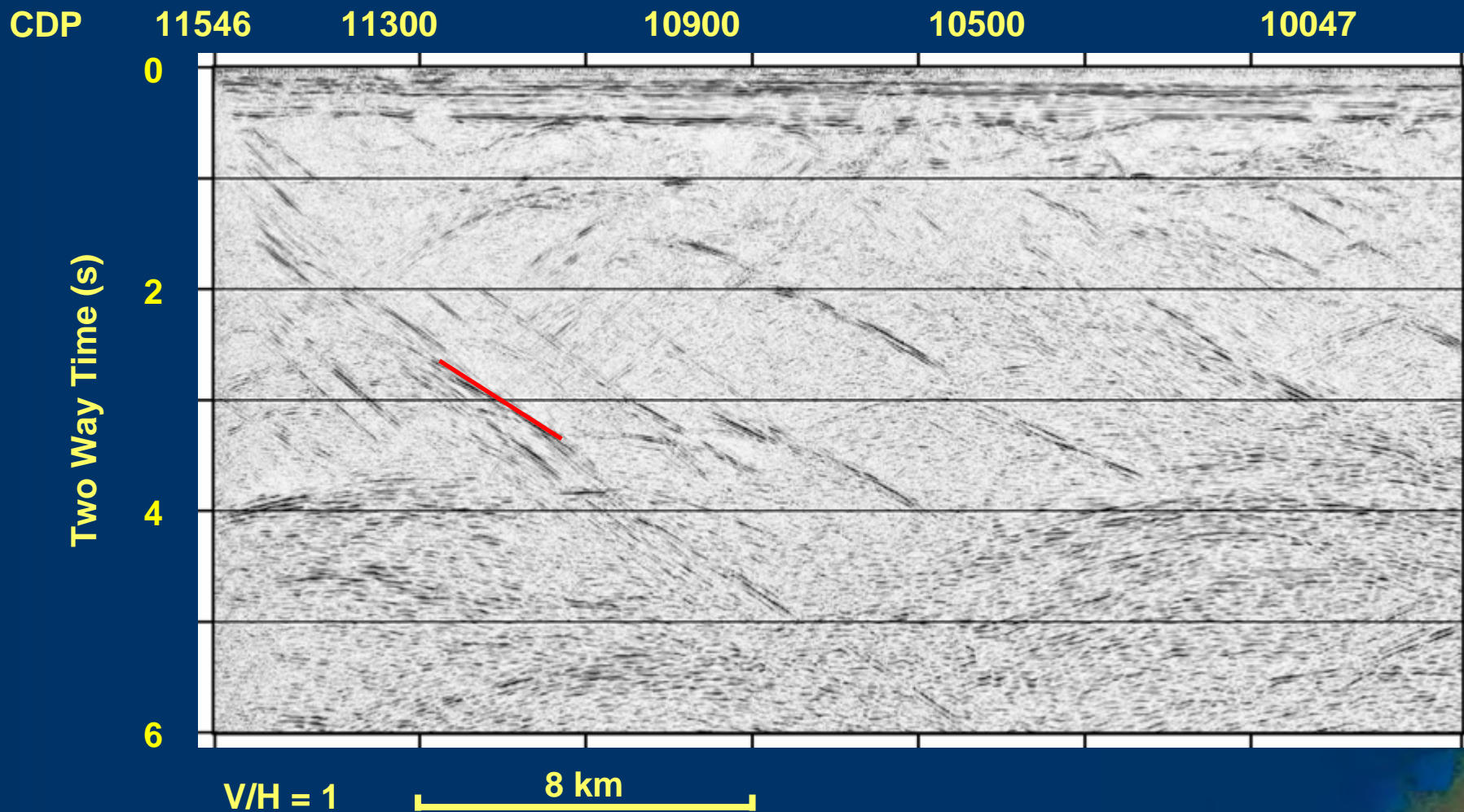
Migration of Dipping Reflector



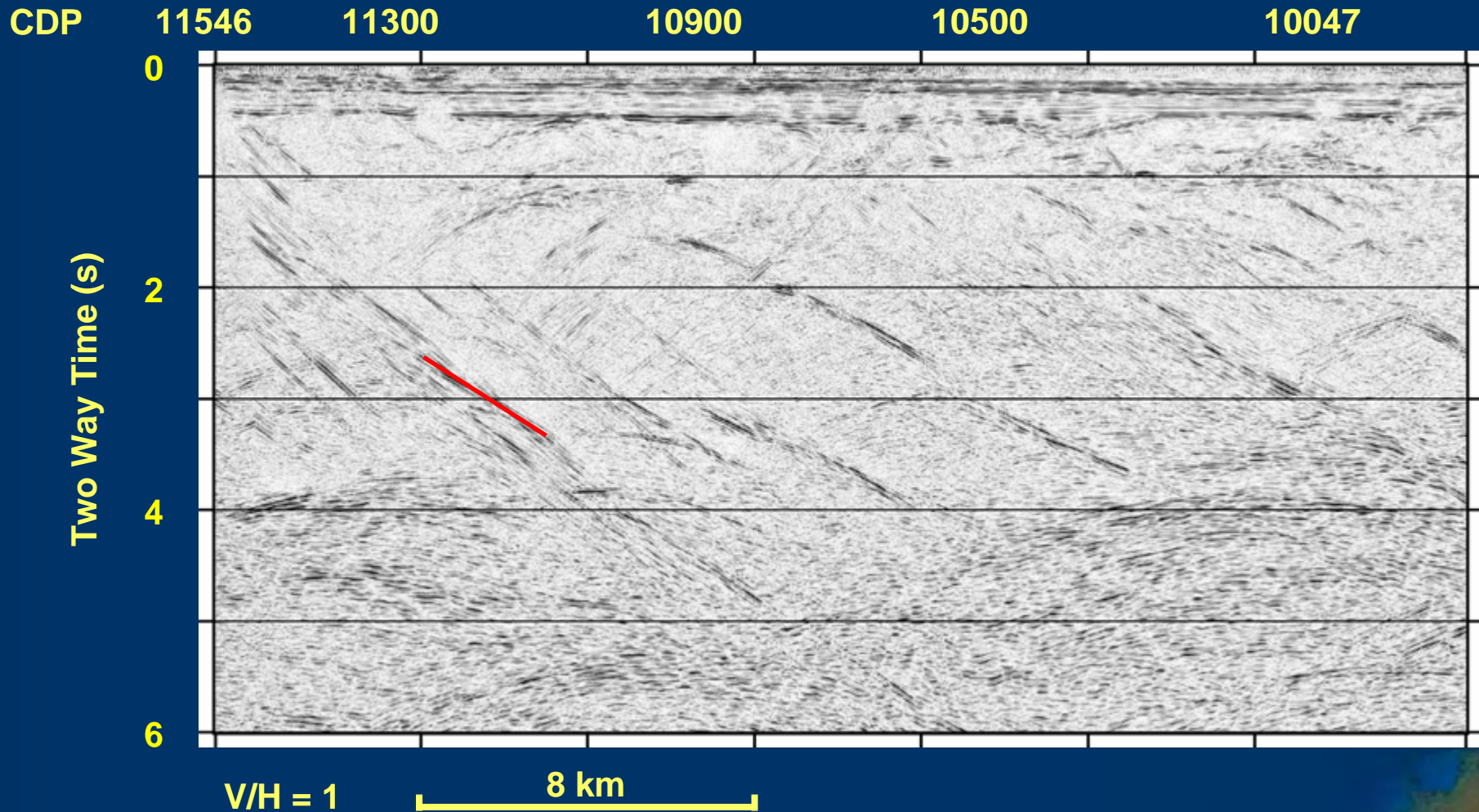
Examples: Migration 03GA-OD1



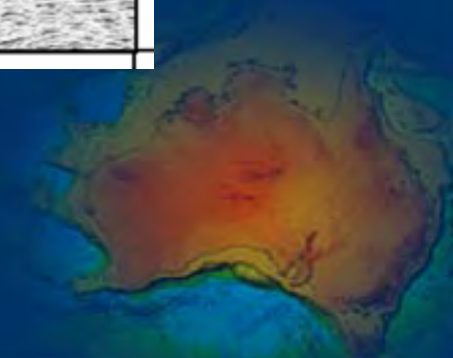
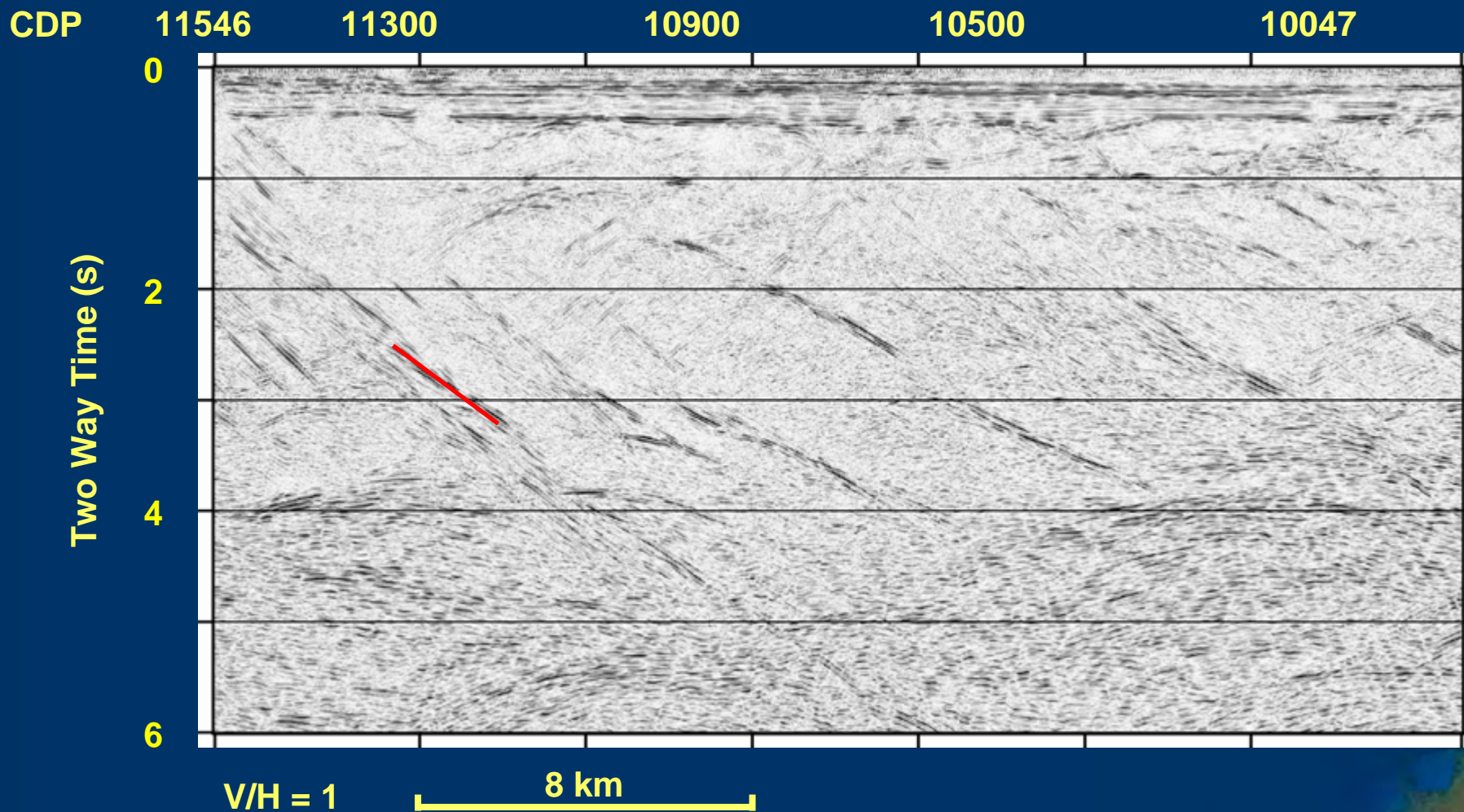
Examples: Migration 03GA-OD1



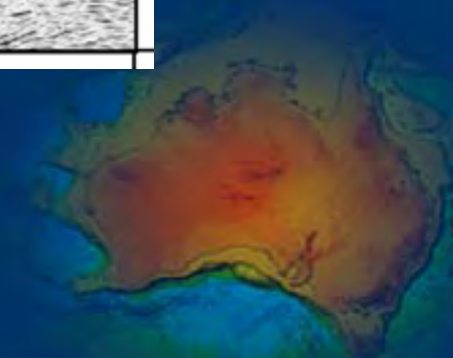
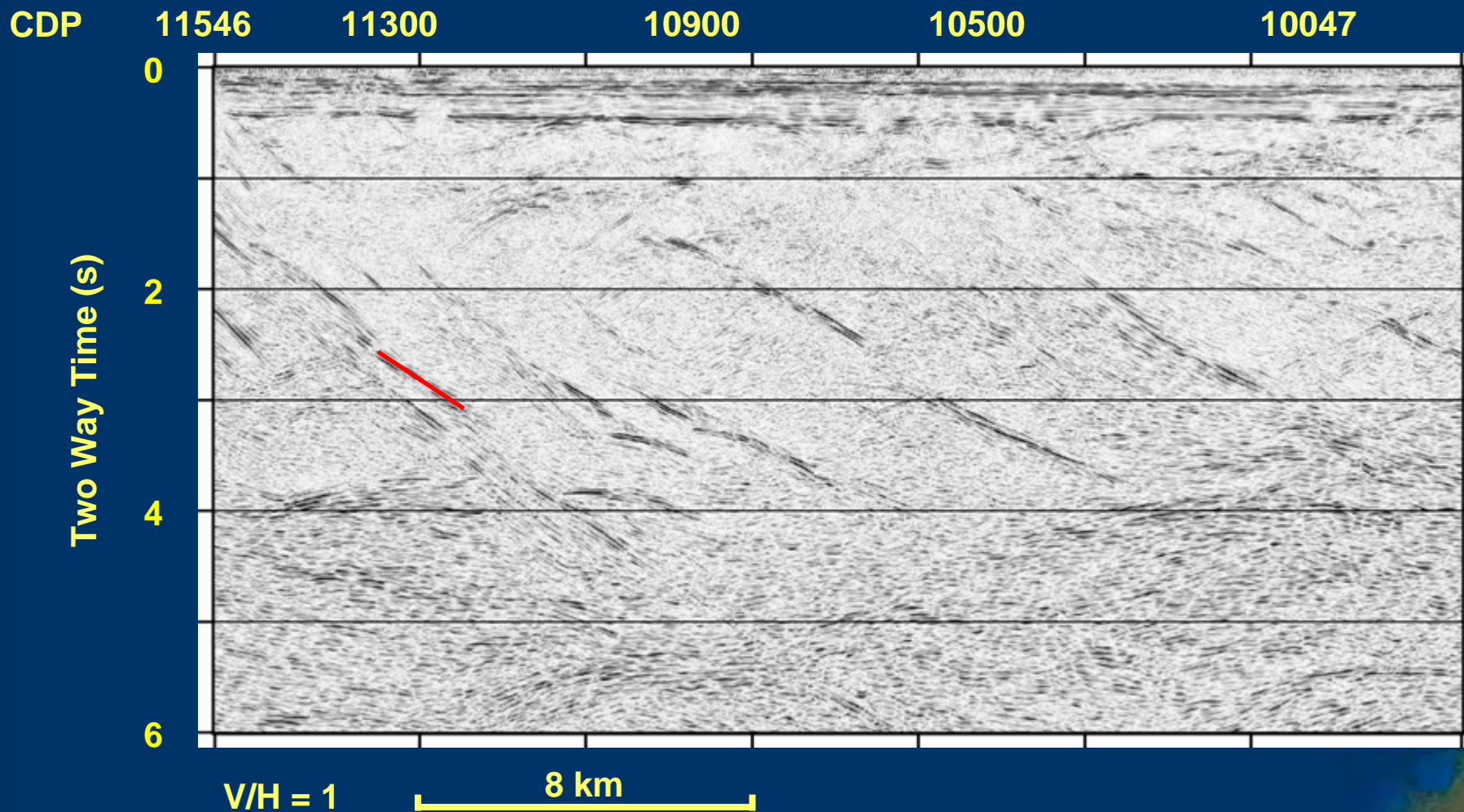
Examples: Migration 03GA-OD1



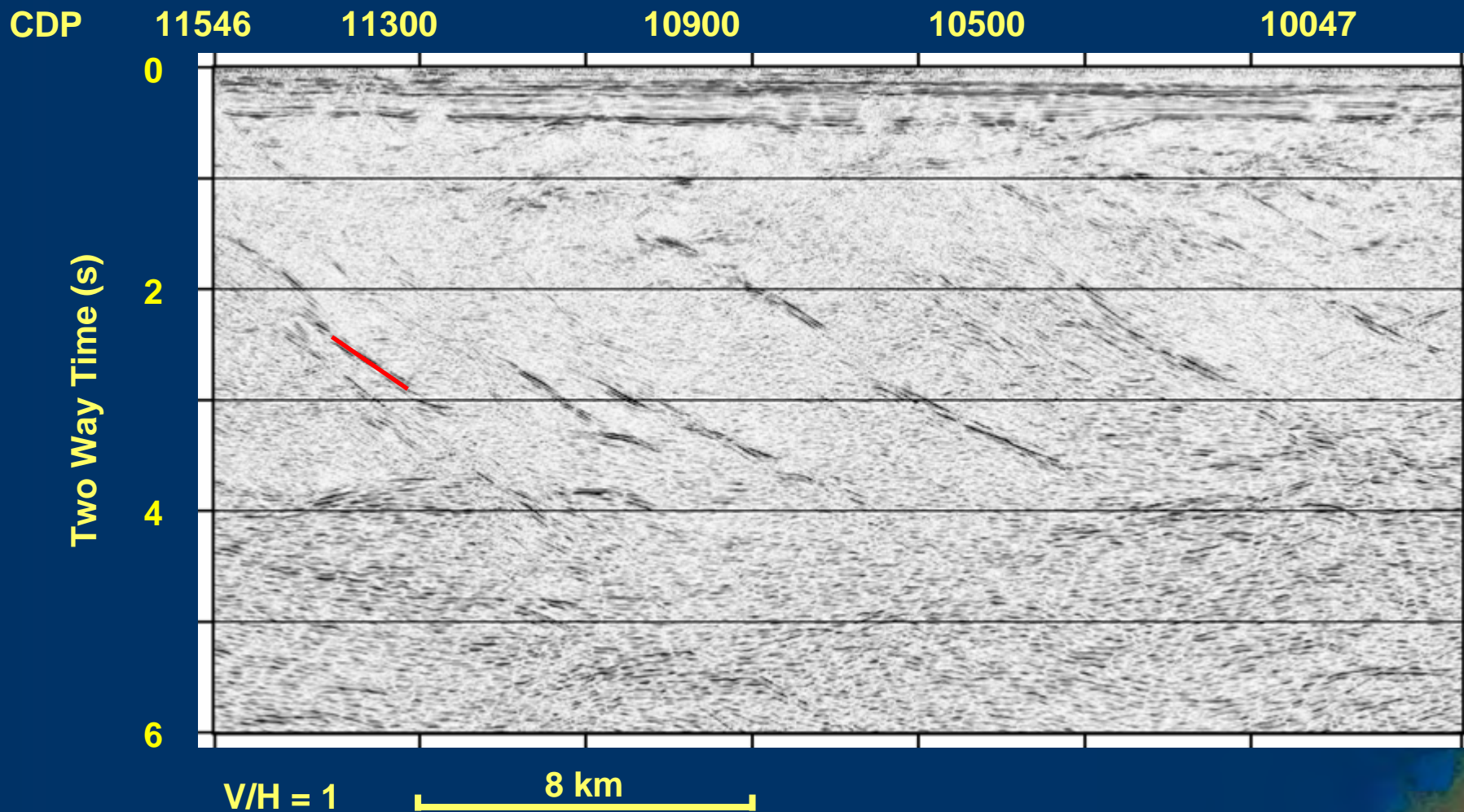
Examples: Migration 03GA-OD1



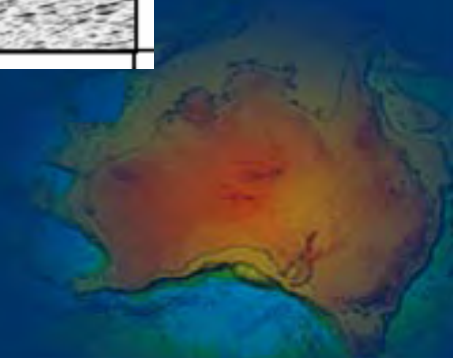
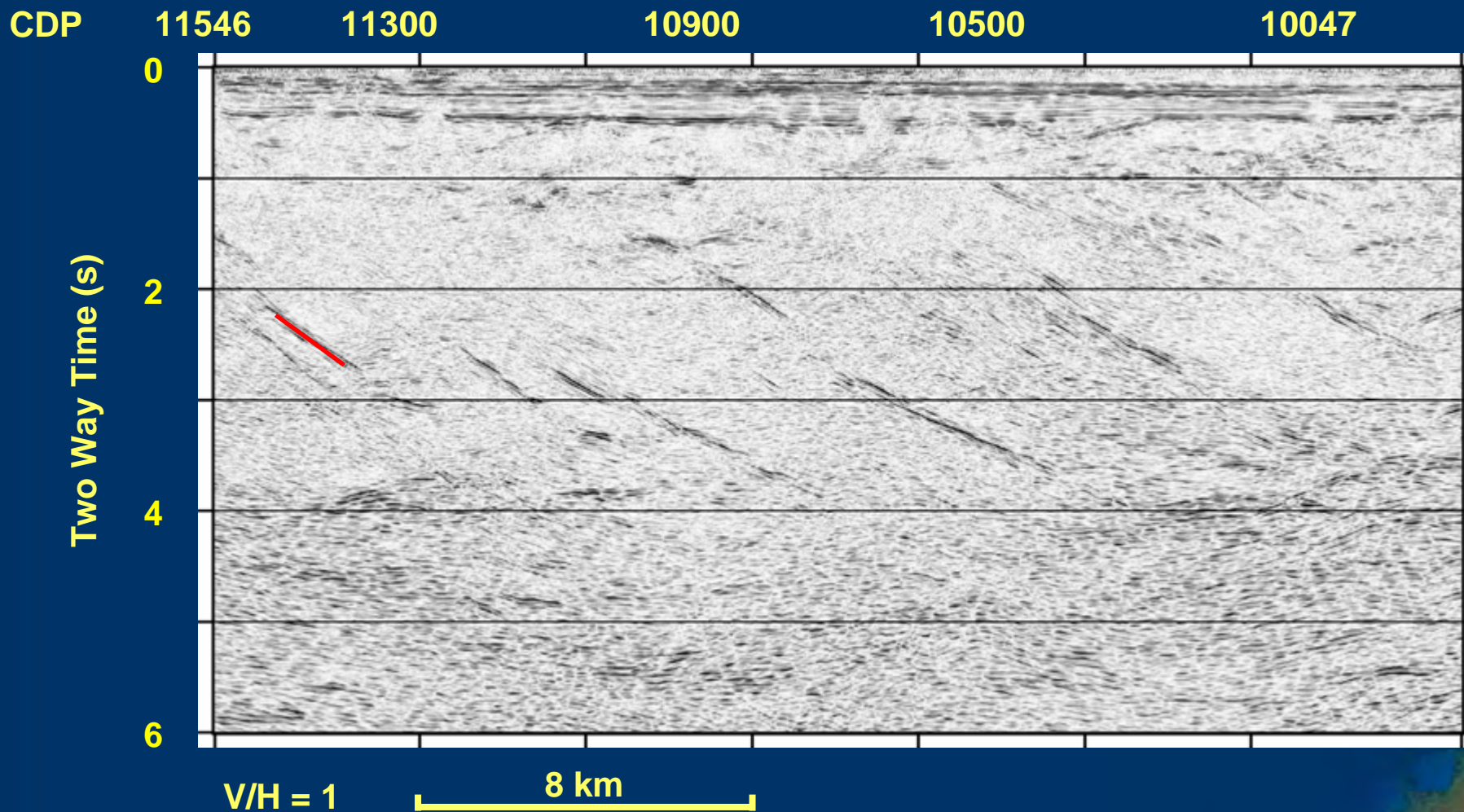
Examples: Migration 03GA-OD1



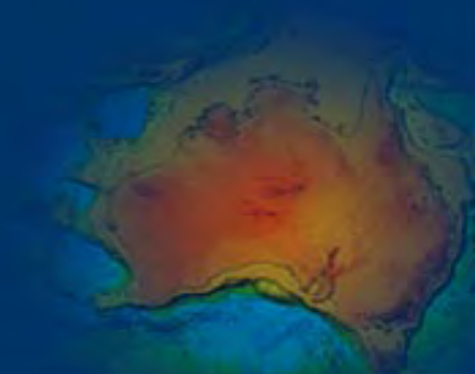
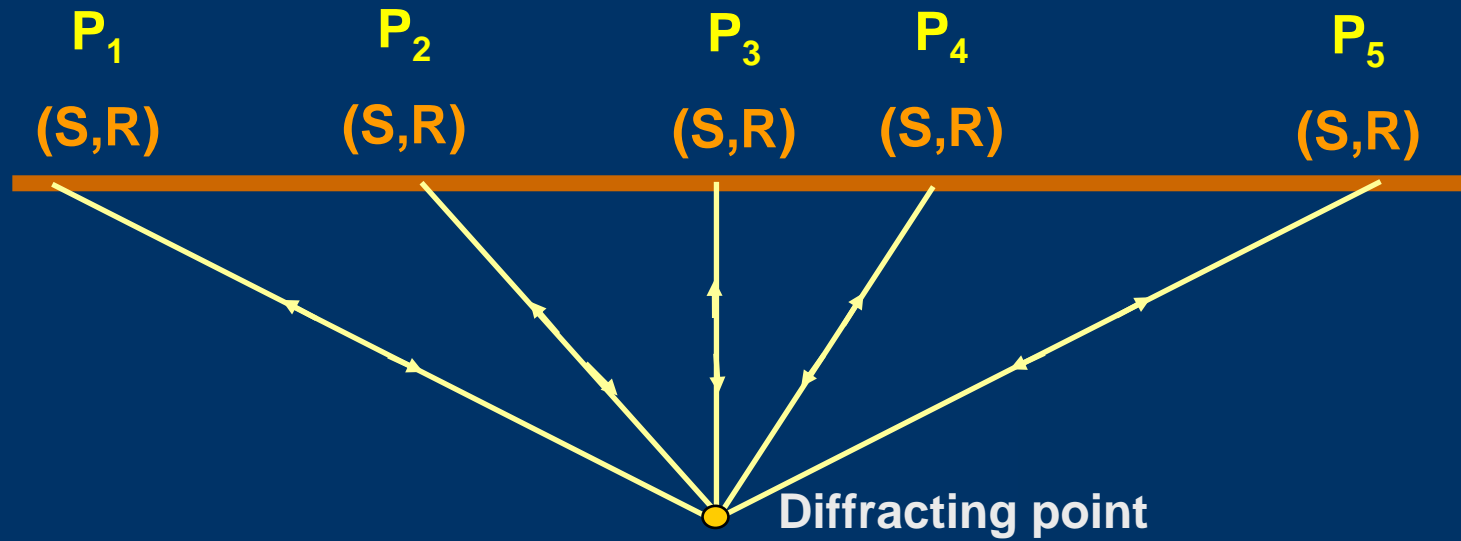
Examples: Migration 03GA-OD1



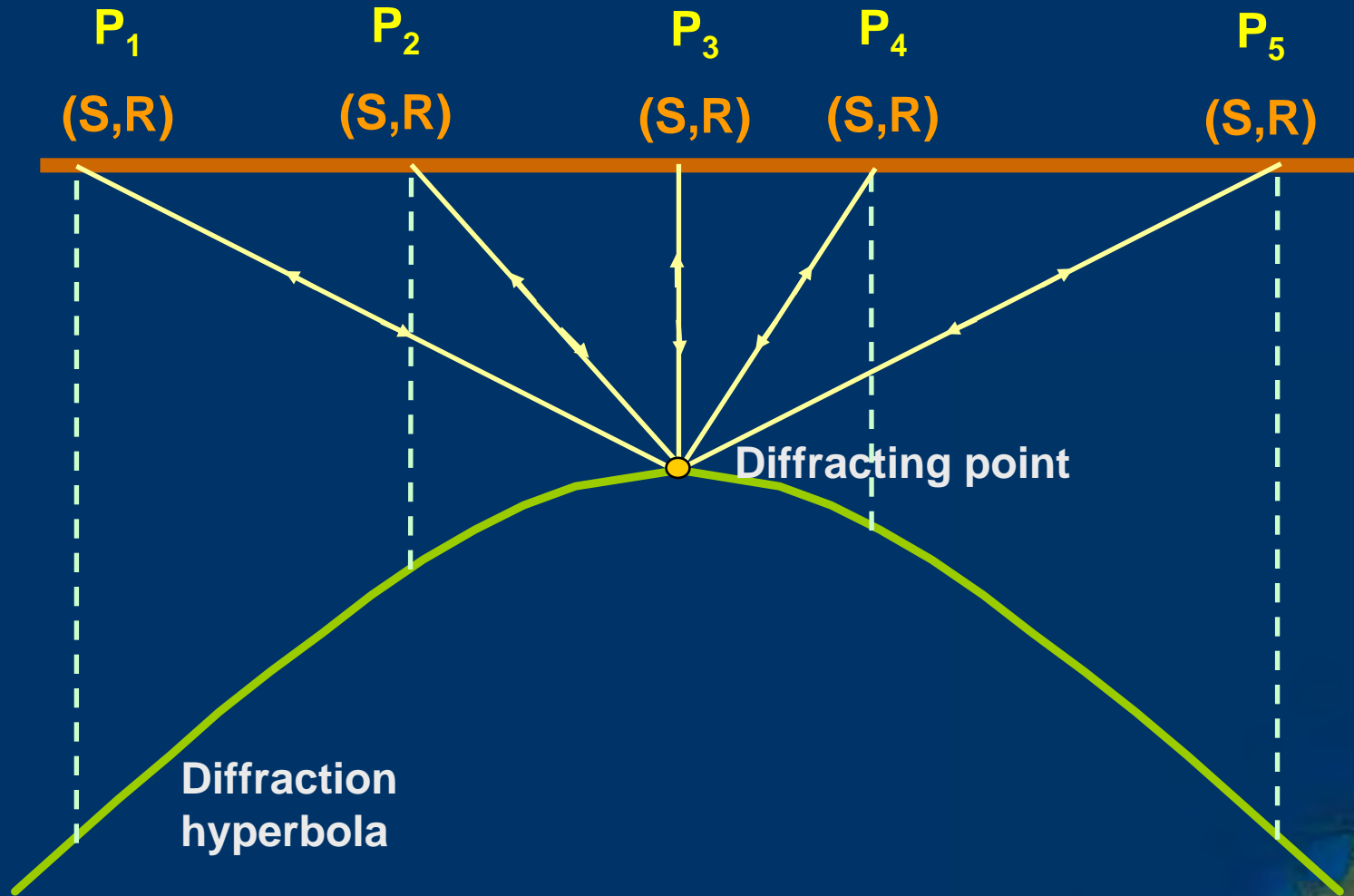
Examples: Migration 03GA-OD1



Generation of Diffractions



Generation of Diffractions

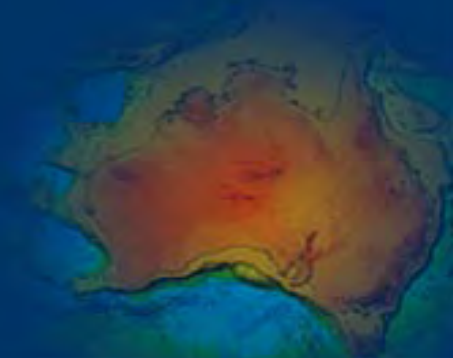


Migration improves a seismic image by

- moving reflectors to their correct positions
- steepening the dip of dipping reflectors
- collapsing diffractions

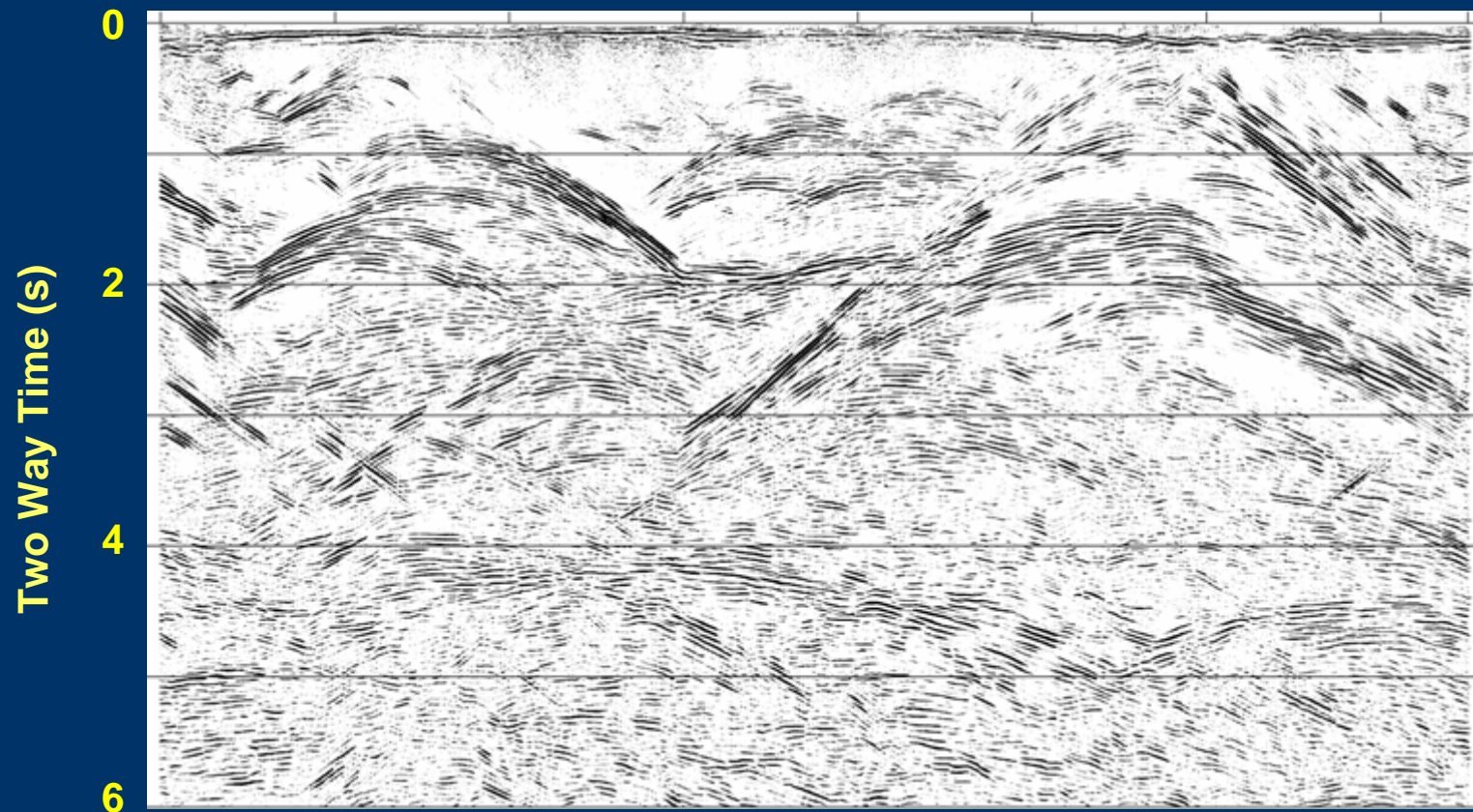
Migration can be evaluated by

- appearance of diffractions (curves vs 'smiles')
- juxtaposition of reflectors of different dip



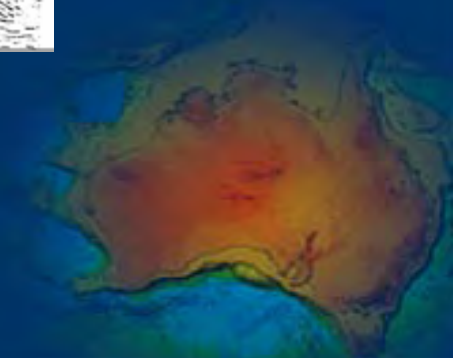
05GA-T3 - Pre Migration

CDP 5200 5000 4800 4600 4400 4200 4000 3800



V/H = 1

6km



05GA-T3 - Post Migration

CDP

5200

5000

4800

4600

4400

4200

4000

3800

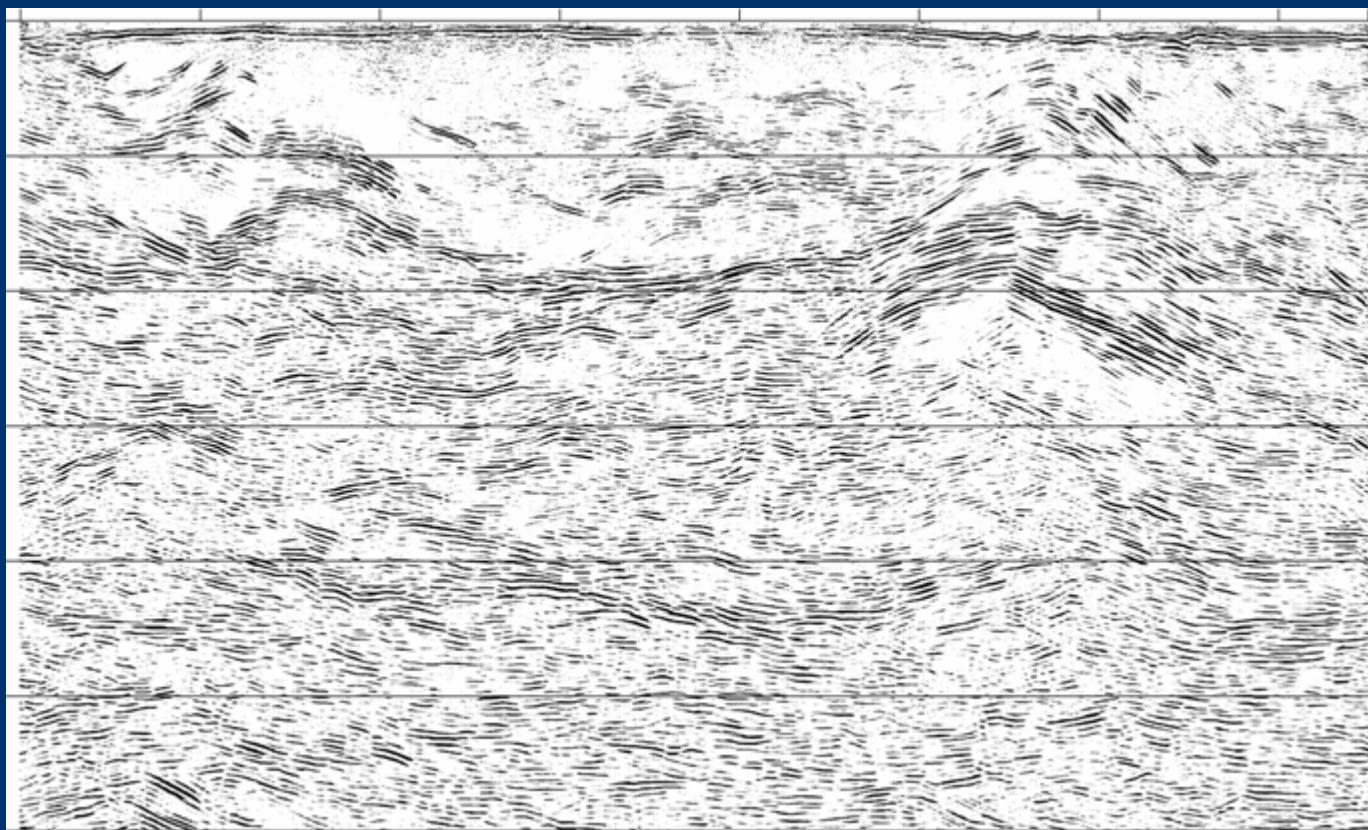
Two Way Time (s)

0

2

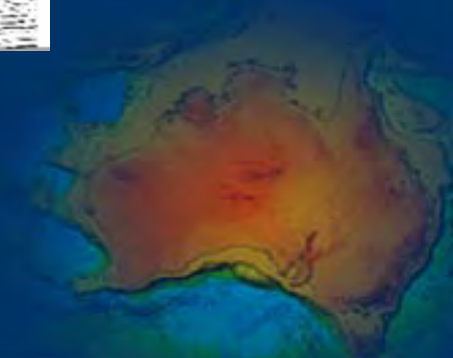
4

6

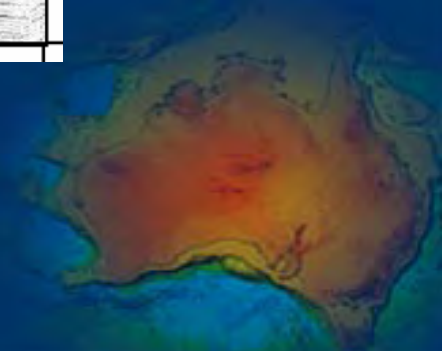
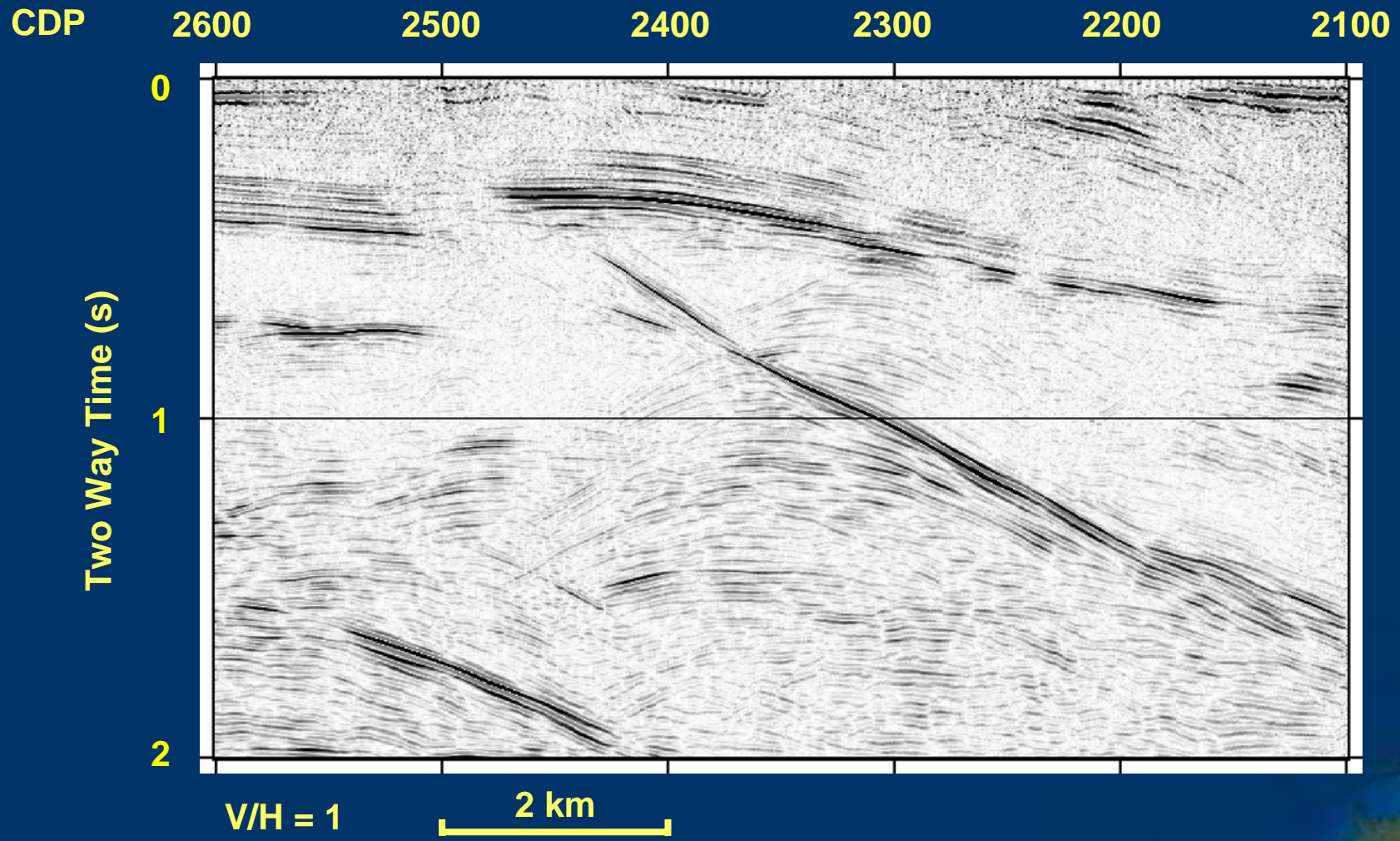


V/H = 1

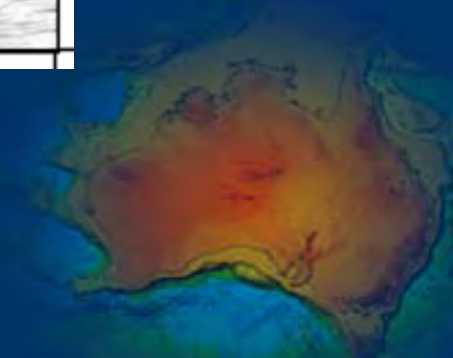
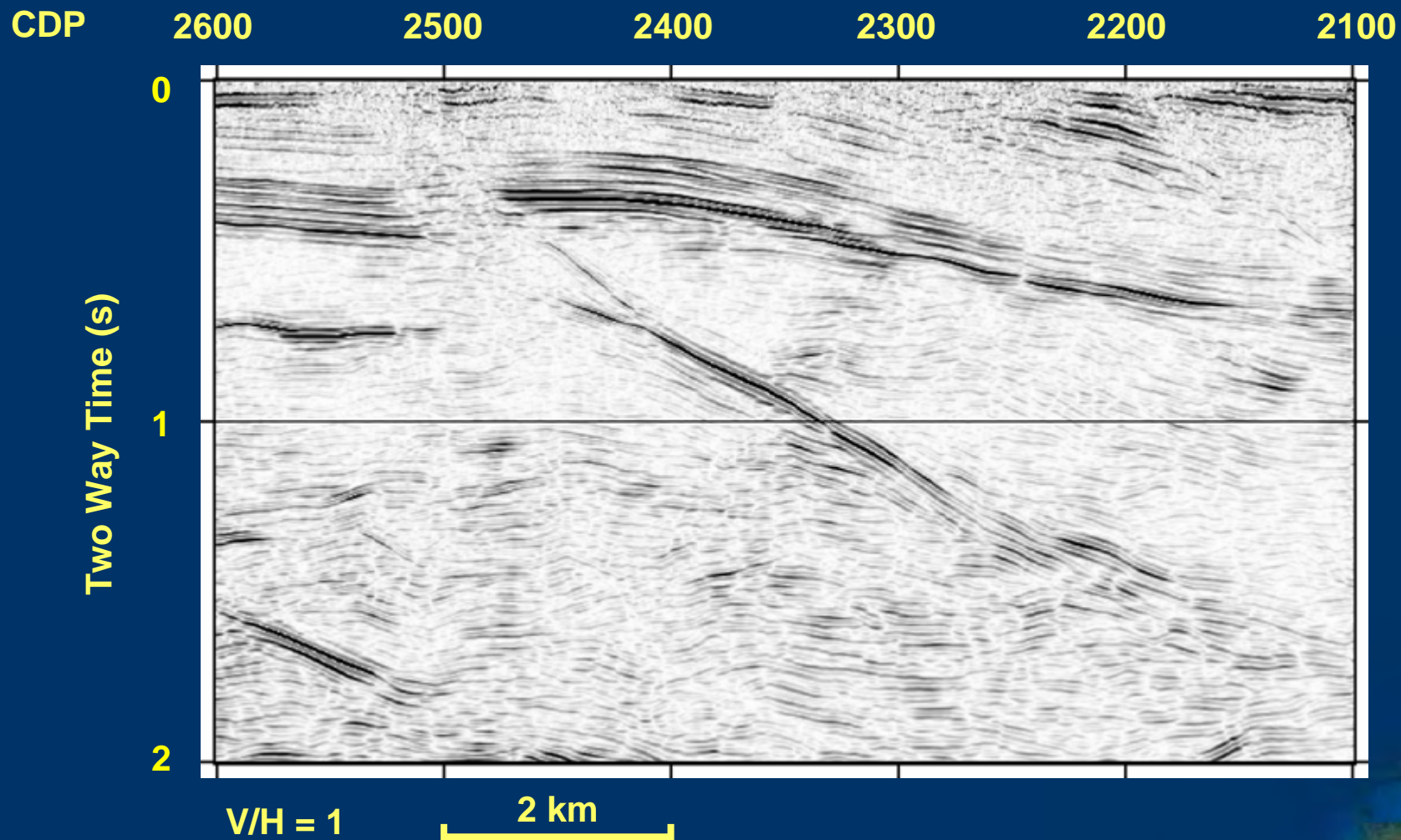
6km



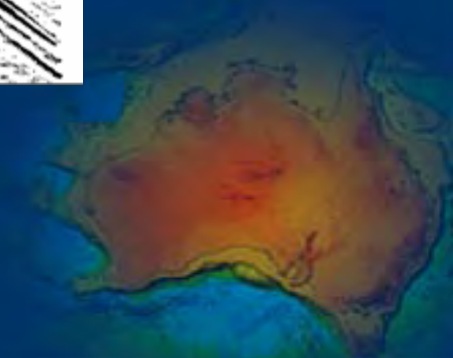
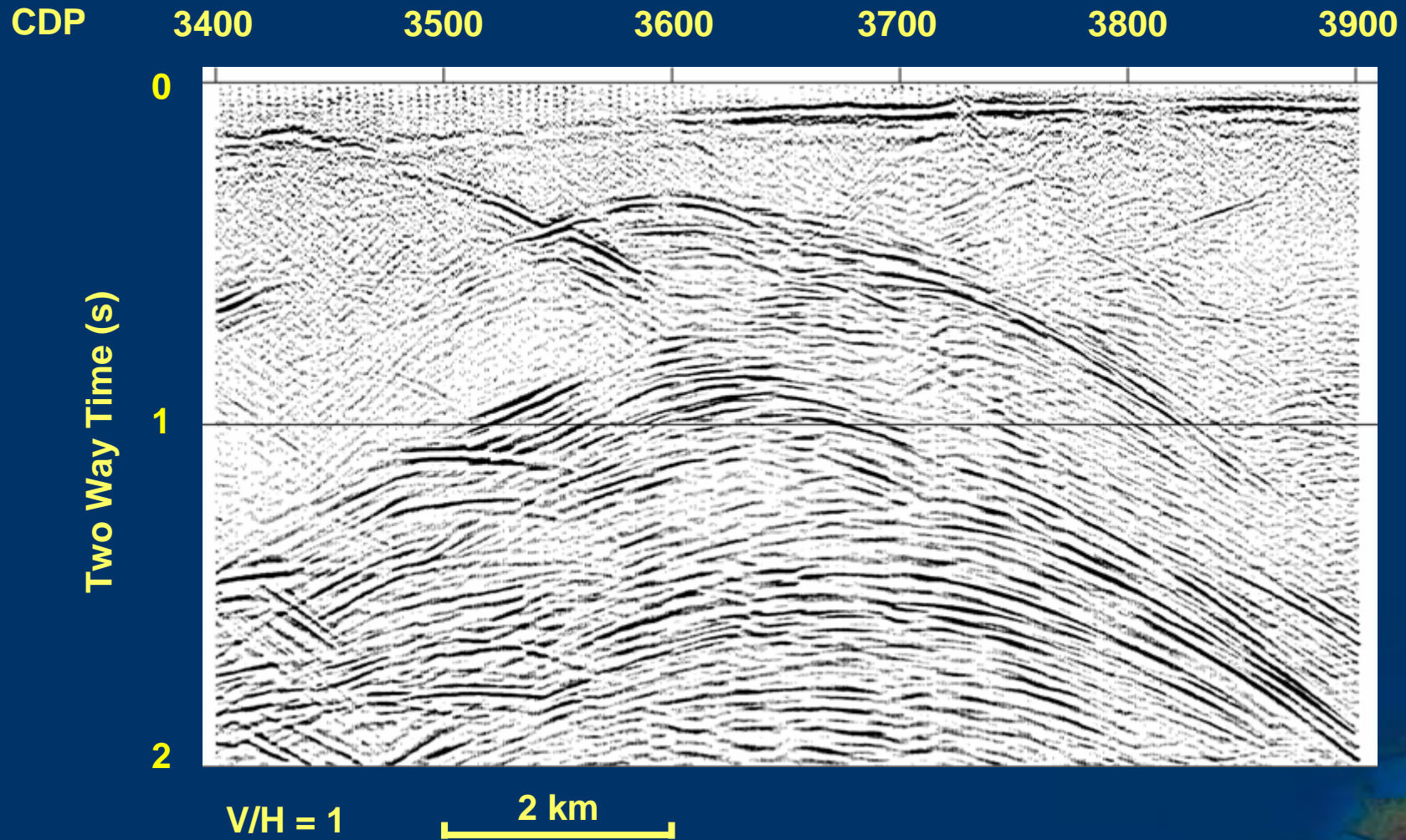
05GA-T3 - Pre Migration



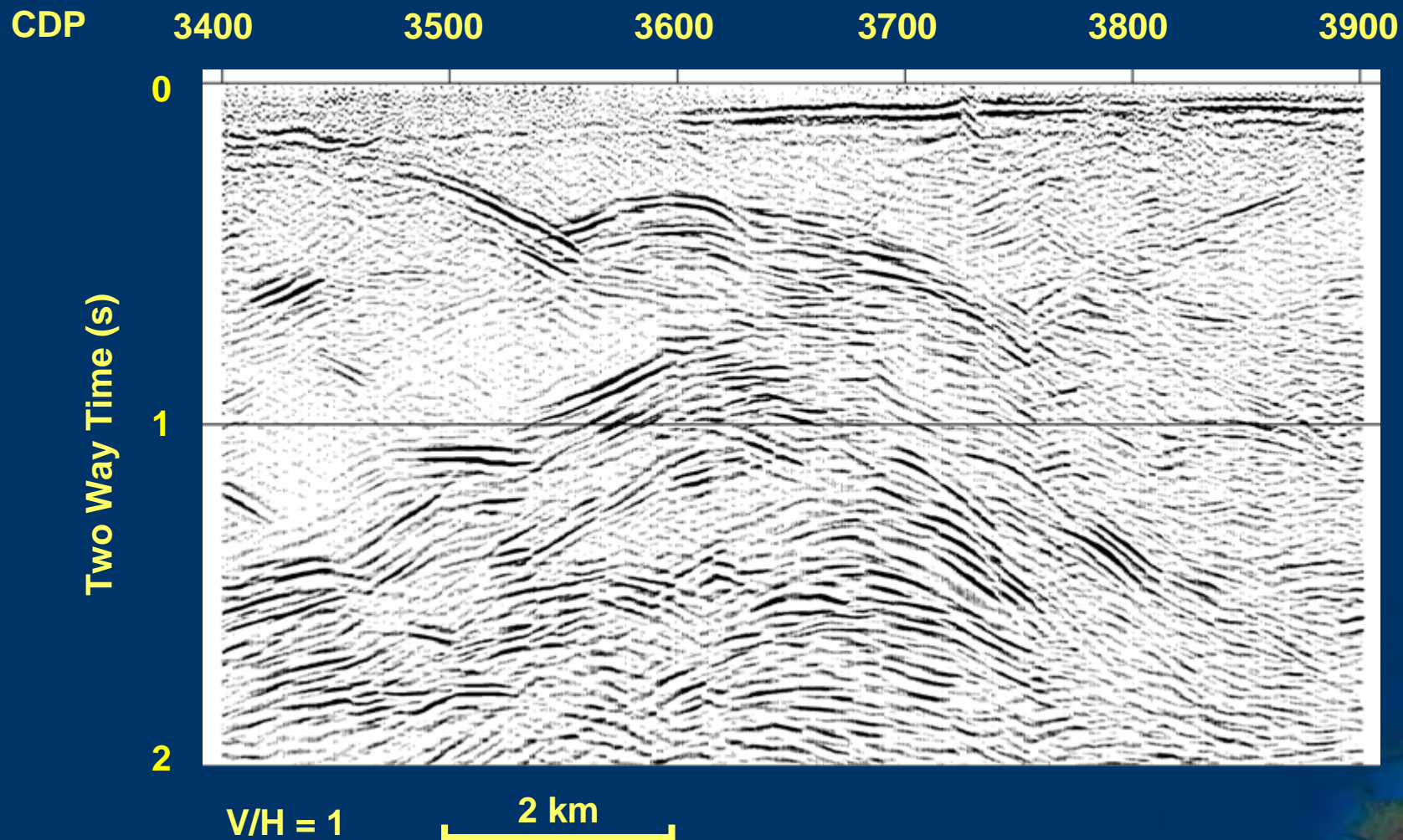
05GA-T3 - Post Migration



05GA-T2 - Pre Migration



05GA-T2 - Post Migration

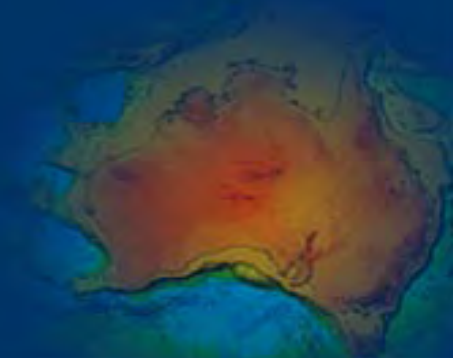


Migration improves a seismic image by

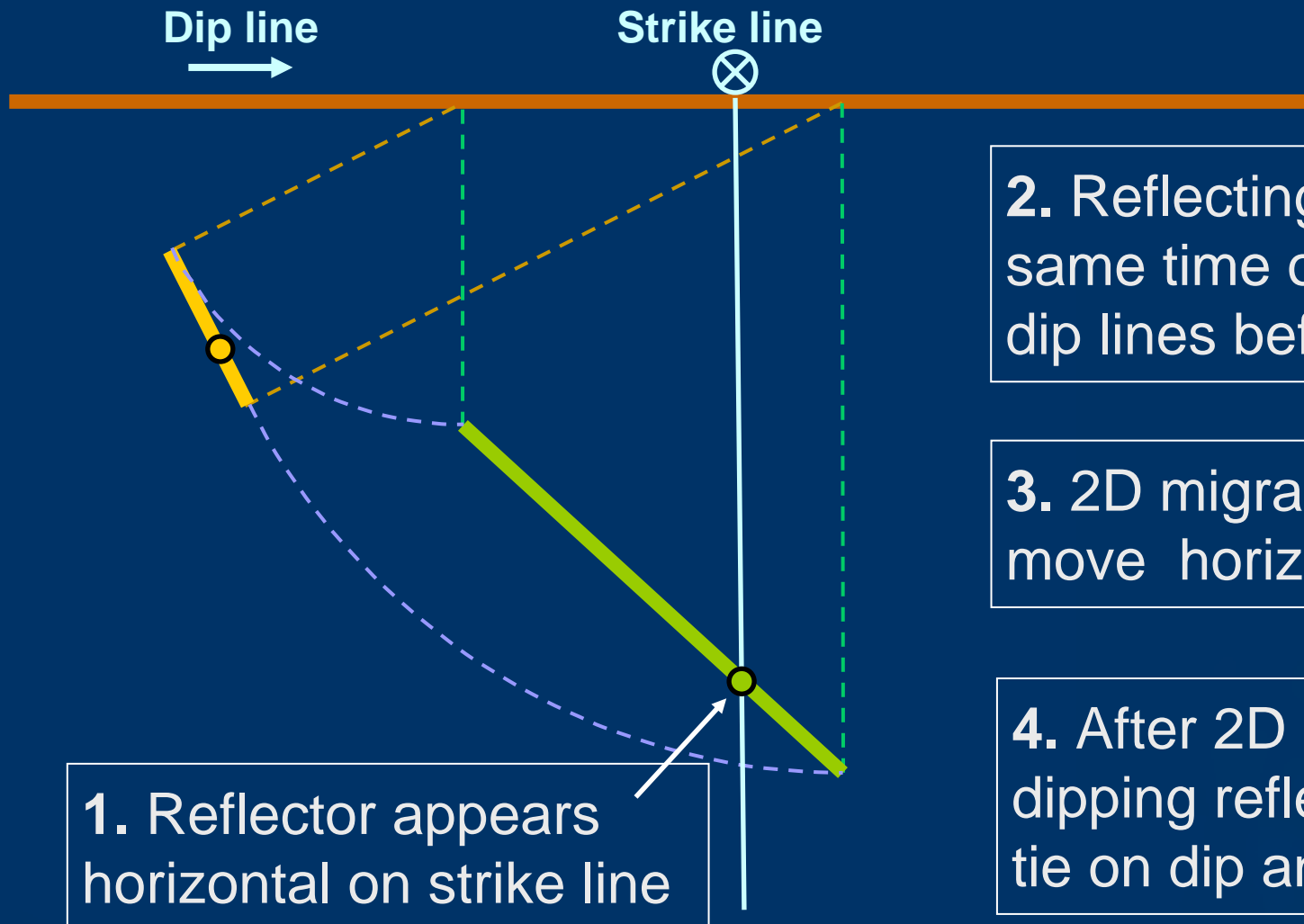
- moving reflectors to their correct positions
- steepening the dip of dipping reflectors
- collapsing diffractions

Migration can be evaluated by

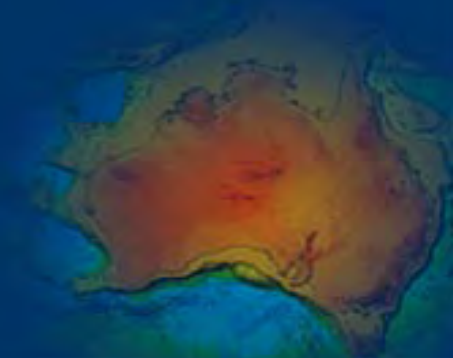
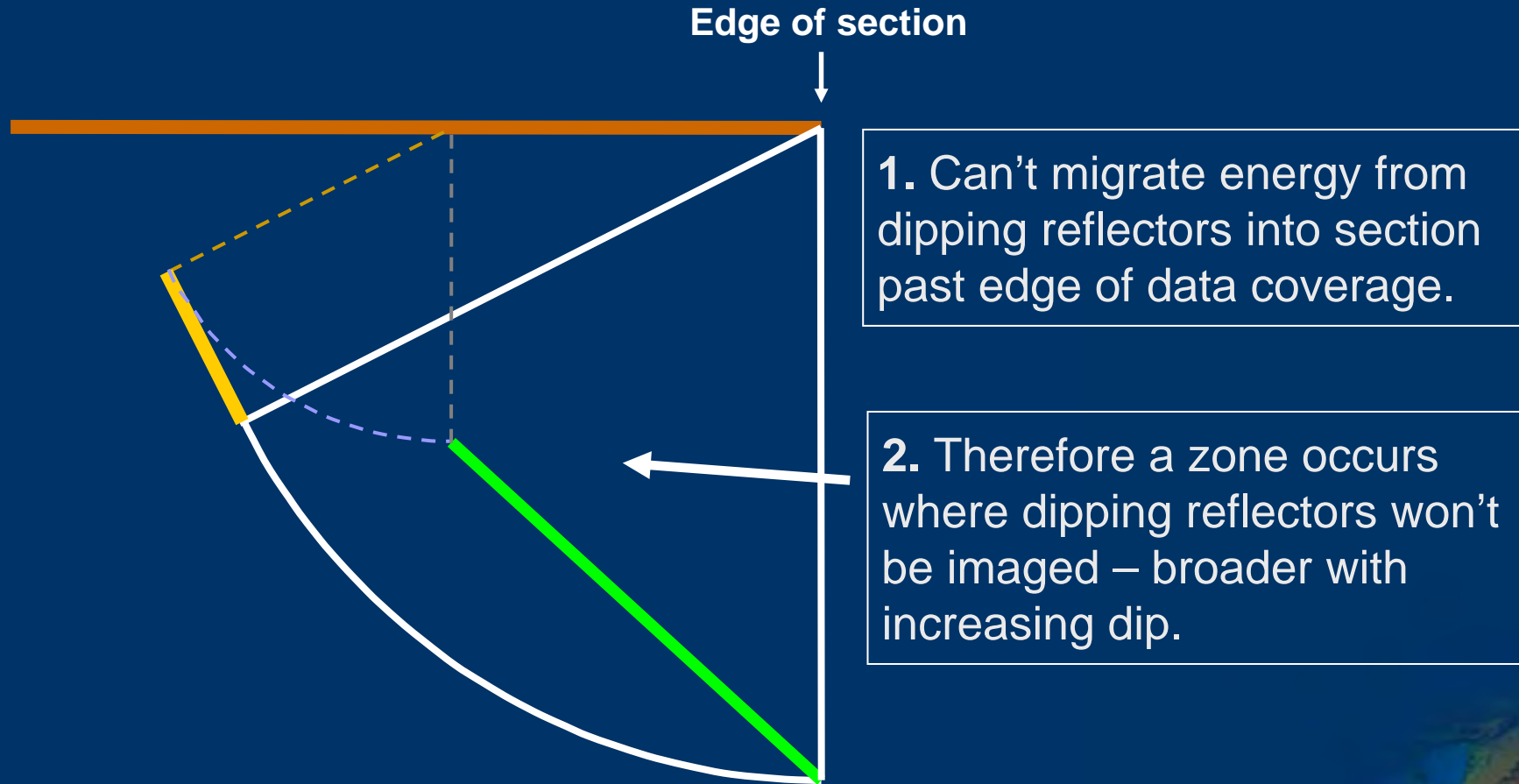
- appearance of diffractions (curves vs 'smiles')
- juxtaposition of reflectors of different dip



Limitation of 2D Migration



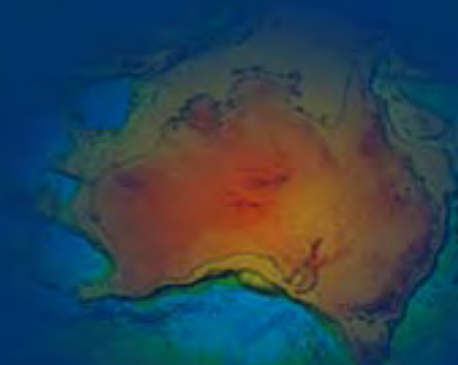
Edge effects - Migration Aperture



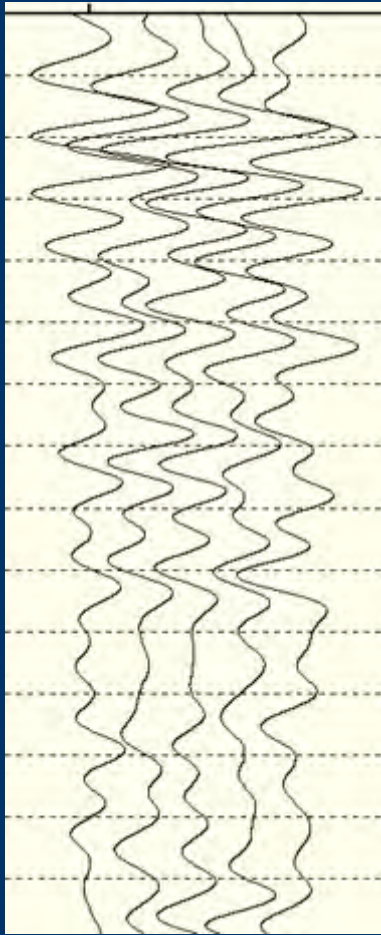
Display of seismic data

Important for interpretation and presentation

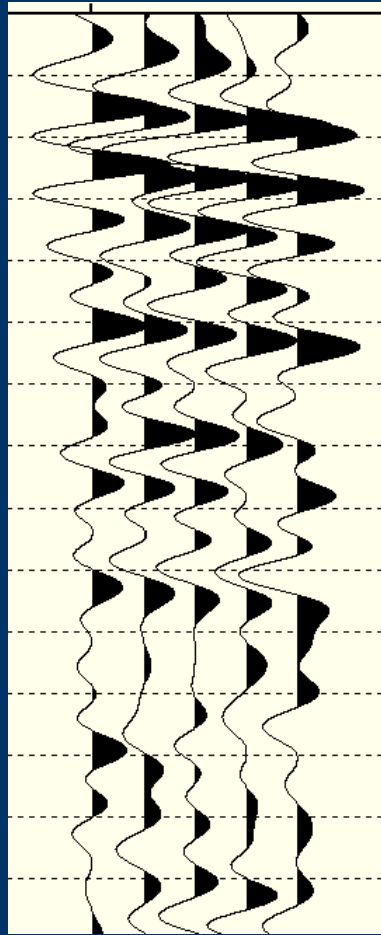
NB: Displayed in two way rime not depth



Types of B/W Seismic Displays



Wiggle Trace



**Variable Area
Wiggle Trace**



Variable Area



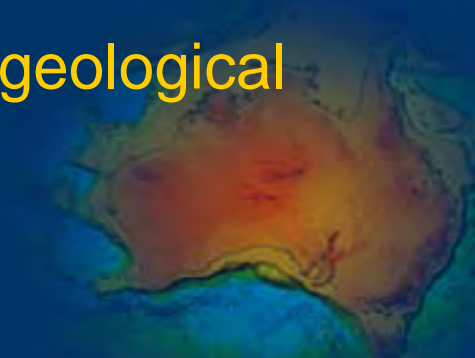


Australian Government

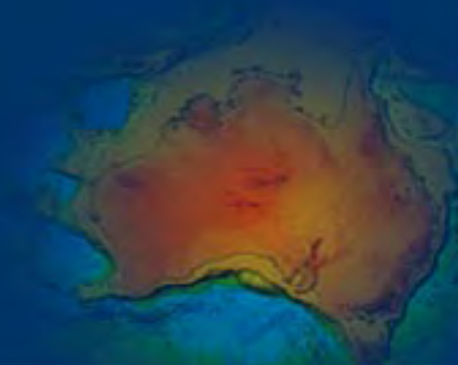
Geoscience Australia

ANSIR NATIONAL RESEARCH
FACILITY FOR
EARTH SOUNDING

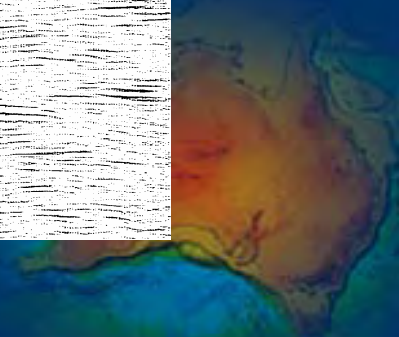
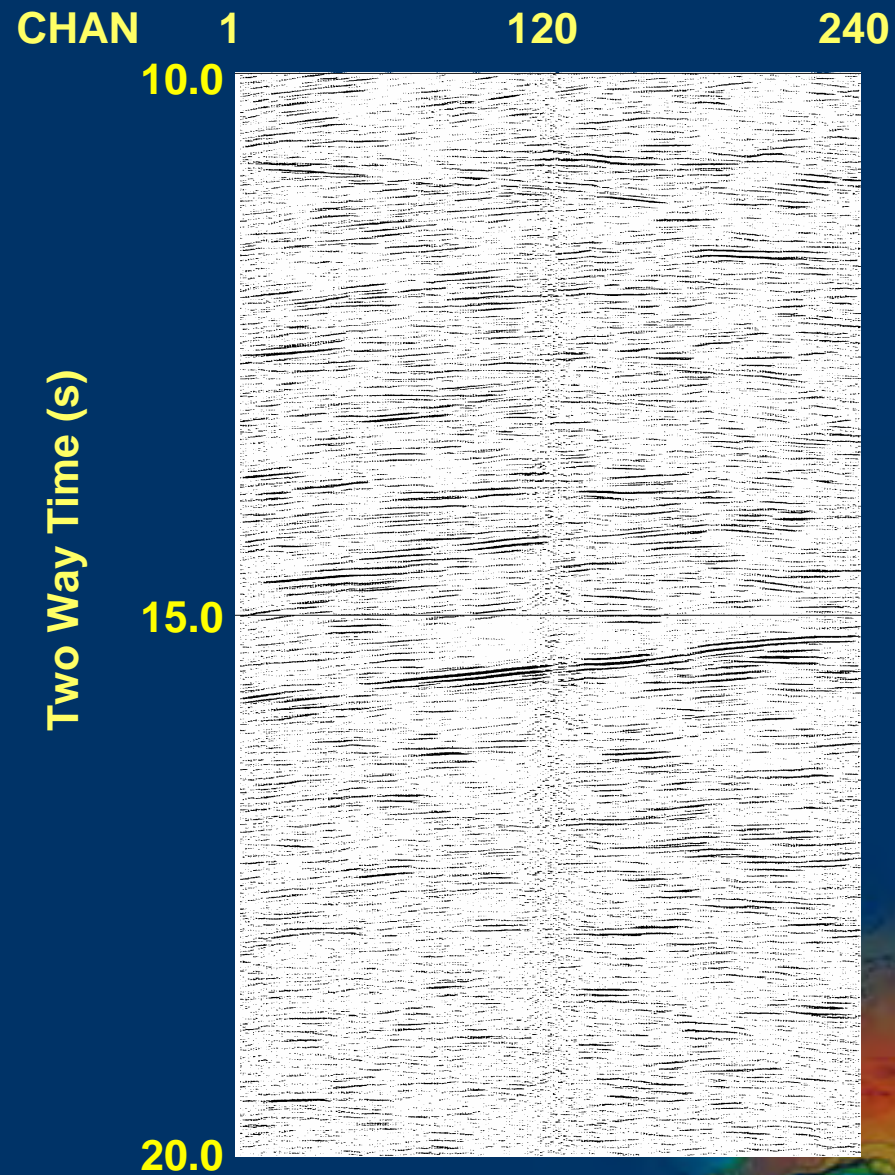
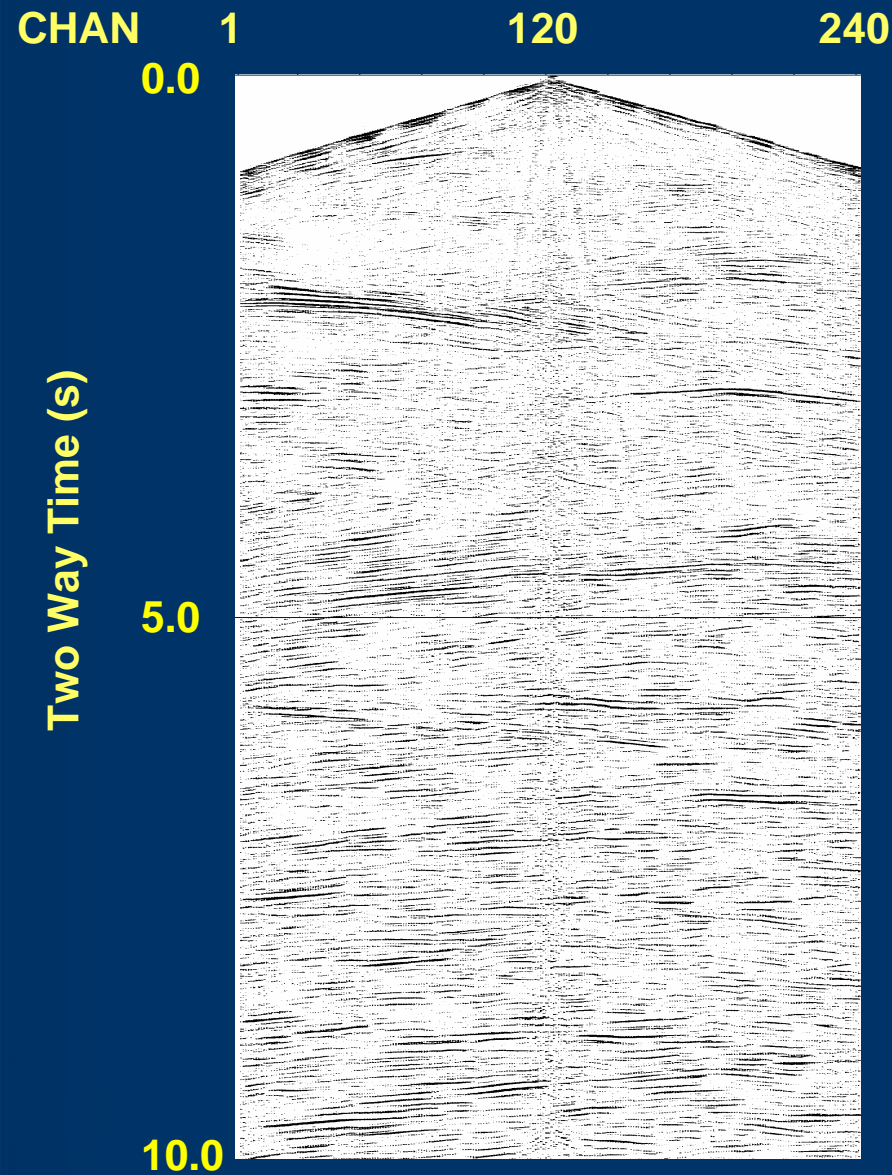
- 720 km of high-fold deep seismic reflection data acquired
- Acquisition and processing parameters designed to enhance reflections and allow for imaging steep dips
- Migration of seismic data essential in complex structures
- Caveats: Need impedance contrast and some continuity
Resolution less than for young sedimentary basins
Earlier deformation might be masked by later
- Seismic sections provide crustal scale framework for geological interpretation of the Tanami Province



- **Extra slides for answering questions**



Example of shot record (enhanced)

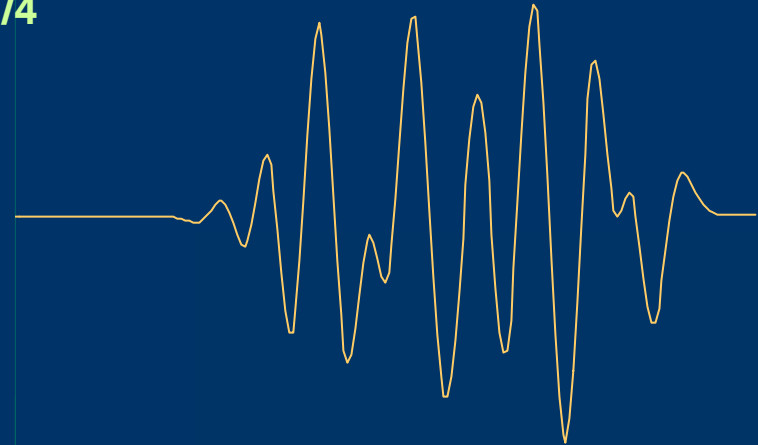
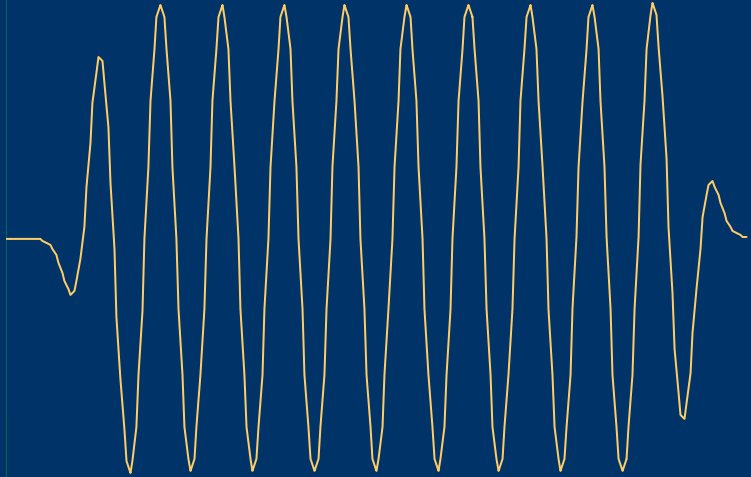


Reflectivity of Shear Zones - 20 layers

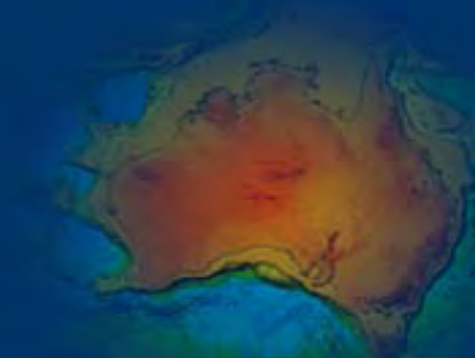
Uniform
thickness

Random
thickness

Wavelength/4

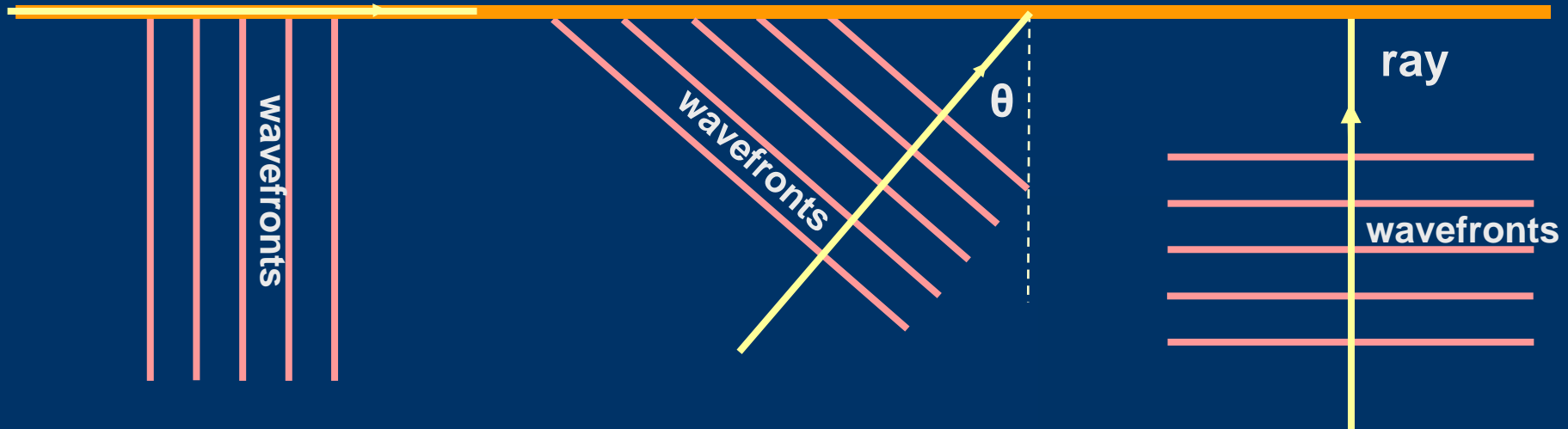


Wavelength/20



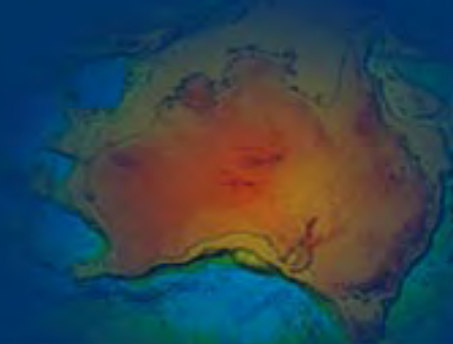
Apparent Wavelength

$$\lambda_a = \lambda / \sin\theta = V / f \sin\theta$$



Horizontal incidence
- true wavelength

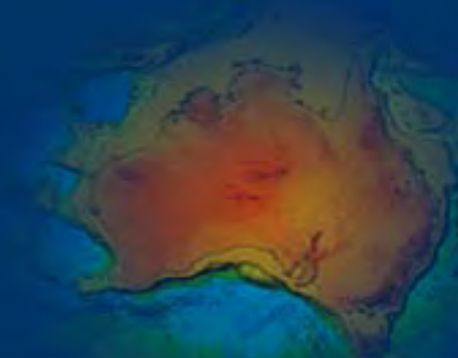
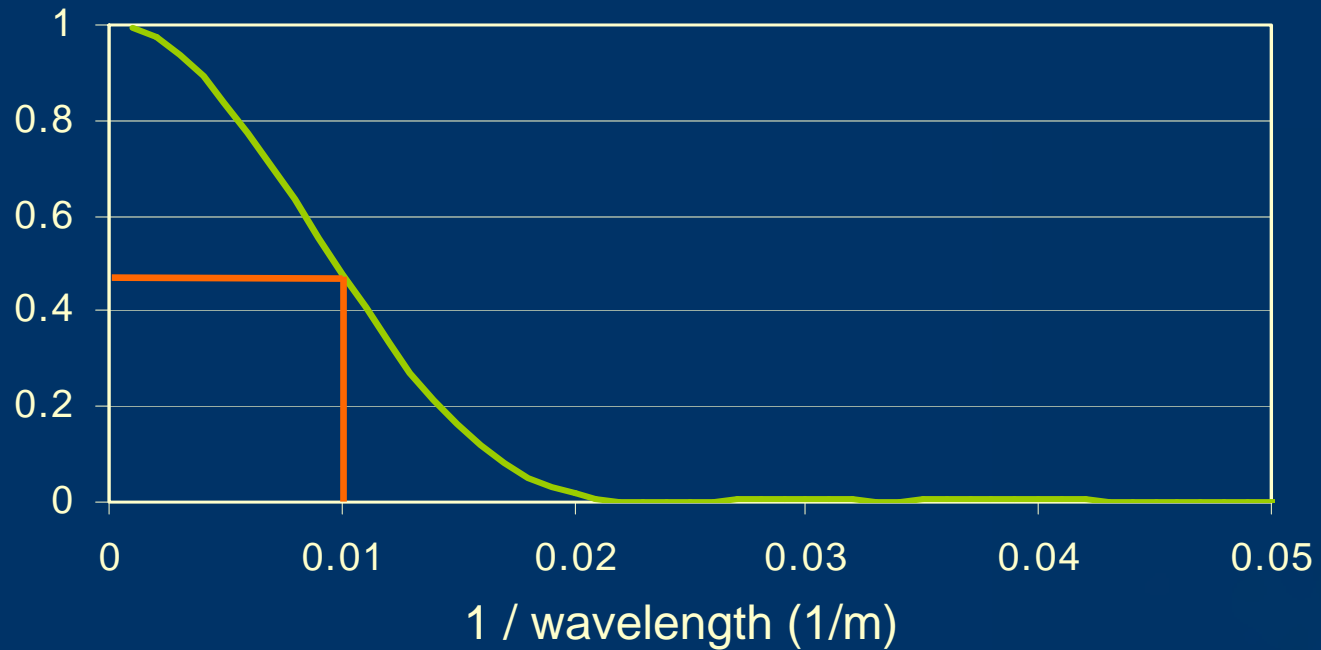
Vertical incidence
- infinite wavelength



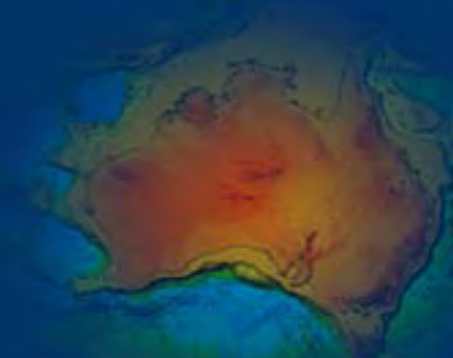
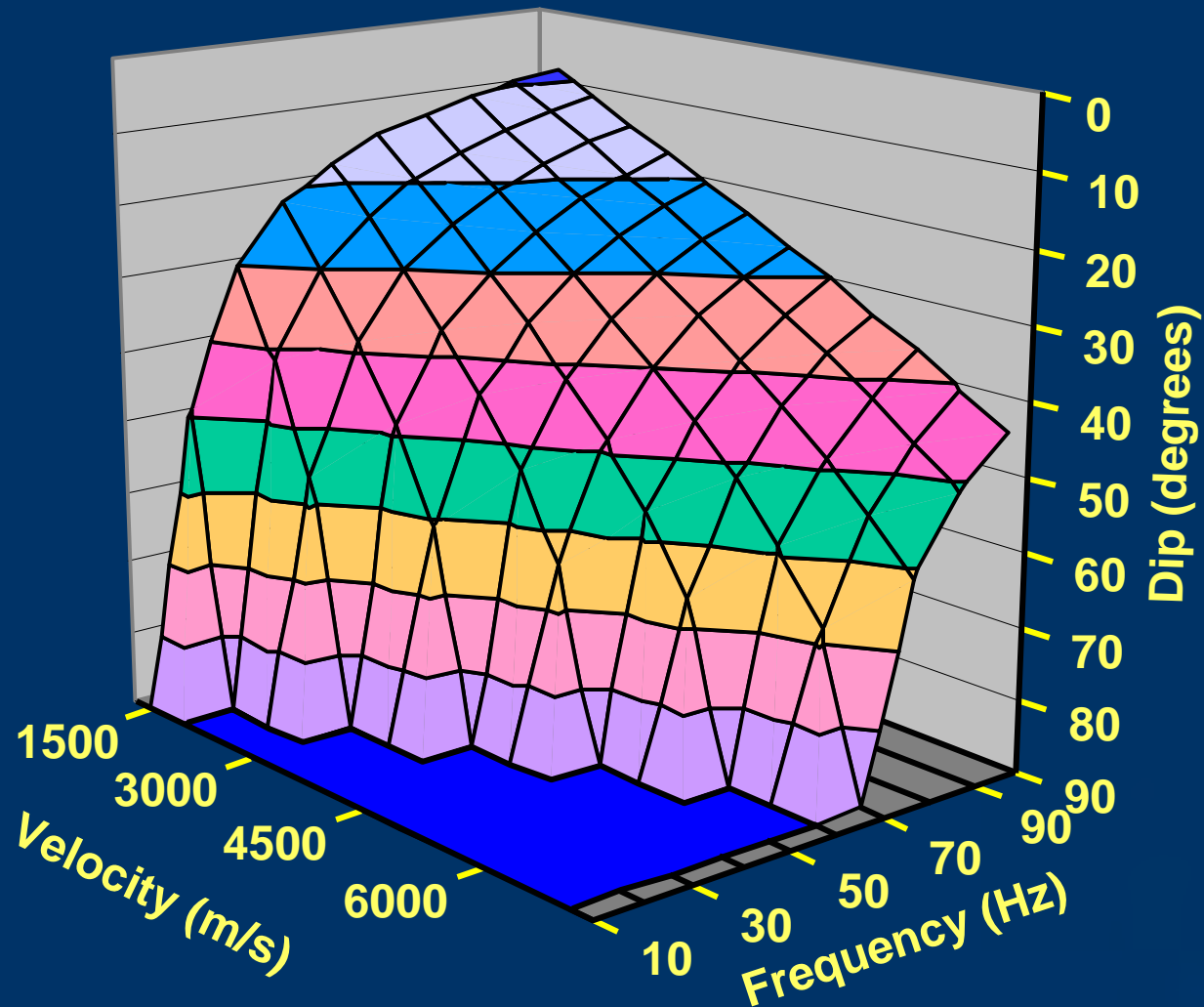
Combined Array Response

3 IVI Hemi-60 vibrators, 15 m pad-pad, 10 m moveup

12 geophones in-line over 40 m

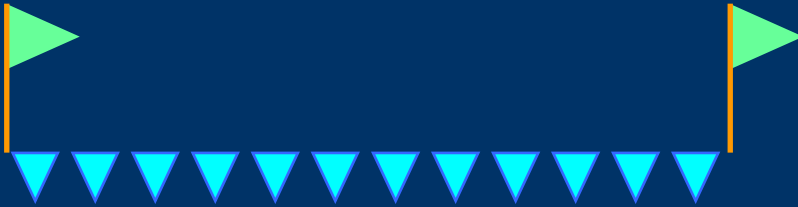


Dips recorded for a typical survey



Line and Source Geometry

Receiver groups centred between pegs



Source array centred on peg

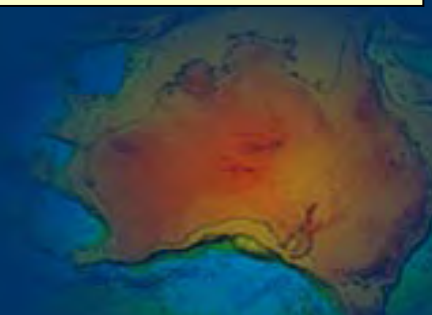
Take surveying coordinates for stations (pegs)

Subtract "bias" for E & N

Interpolate for processing station

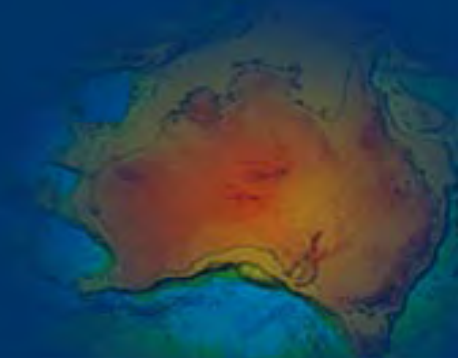
Locate "shots" on peg

Define spread pattern to associate each channel for each shot with a station

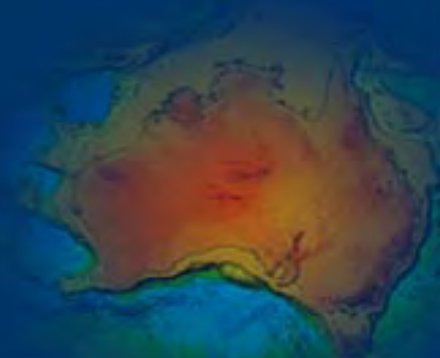
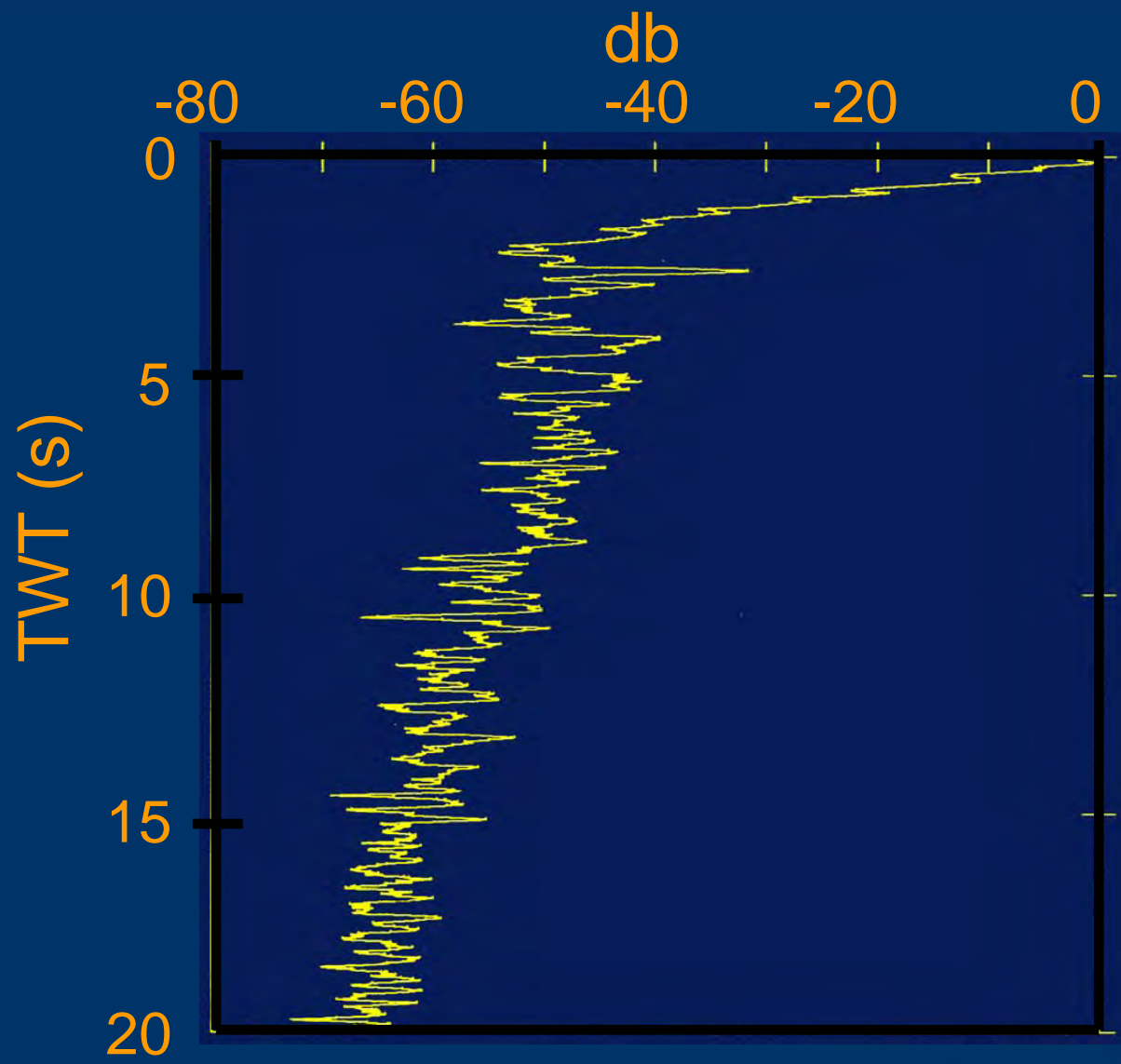


Gain Recovery

Compensates for energy loss at later two-way travel times due to spherical spreading and intrinsic attenuation of seismic waves.



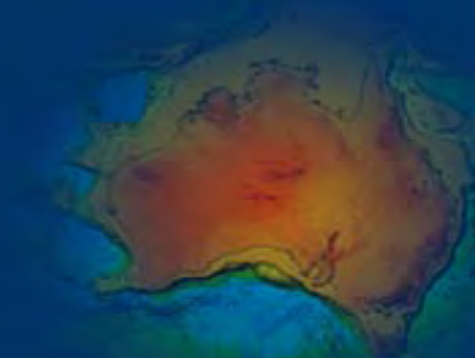
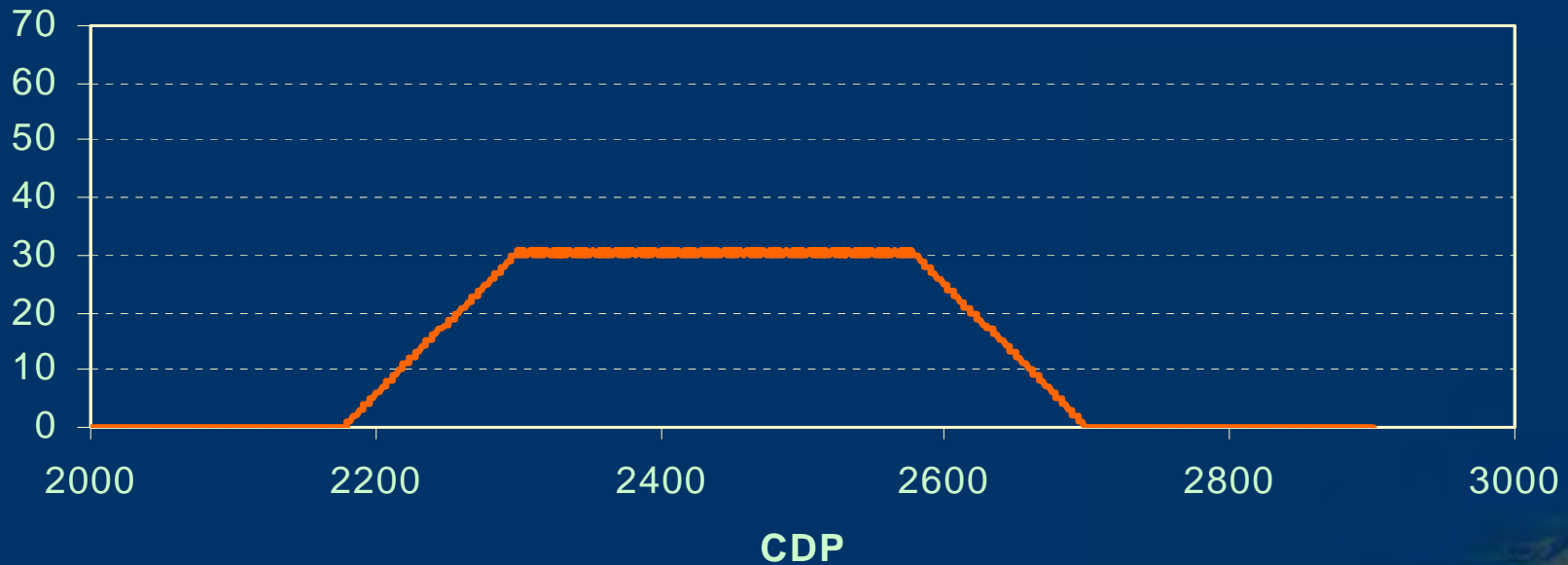
Reflector Strength



Why is stack quality generally lower in top 1/2 second?

Effective fold is lower due to muting of outside traces to remove first arrivals and excessive moveout stretch

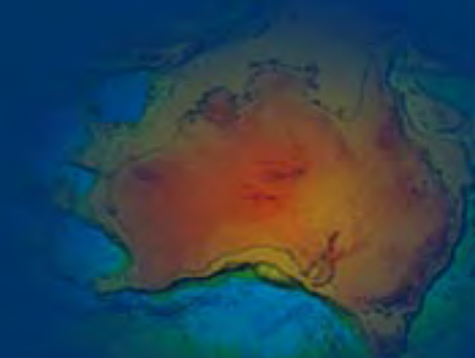
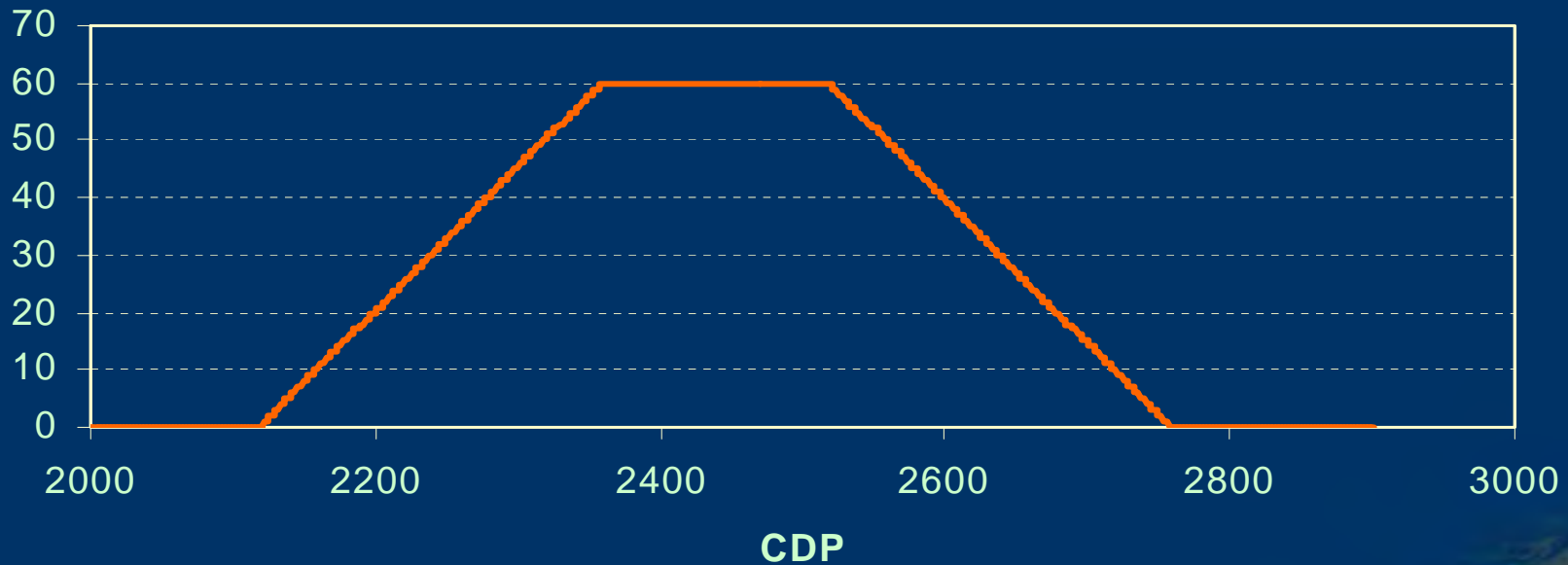
FOLD AT TARGET TWT OF 0.5 S



Why is stack quality generally lower in top 1/2 second?

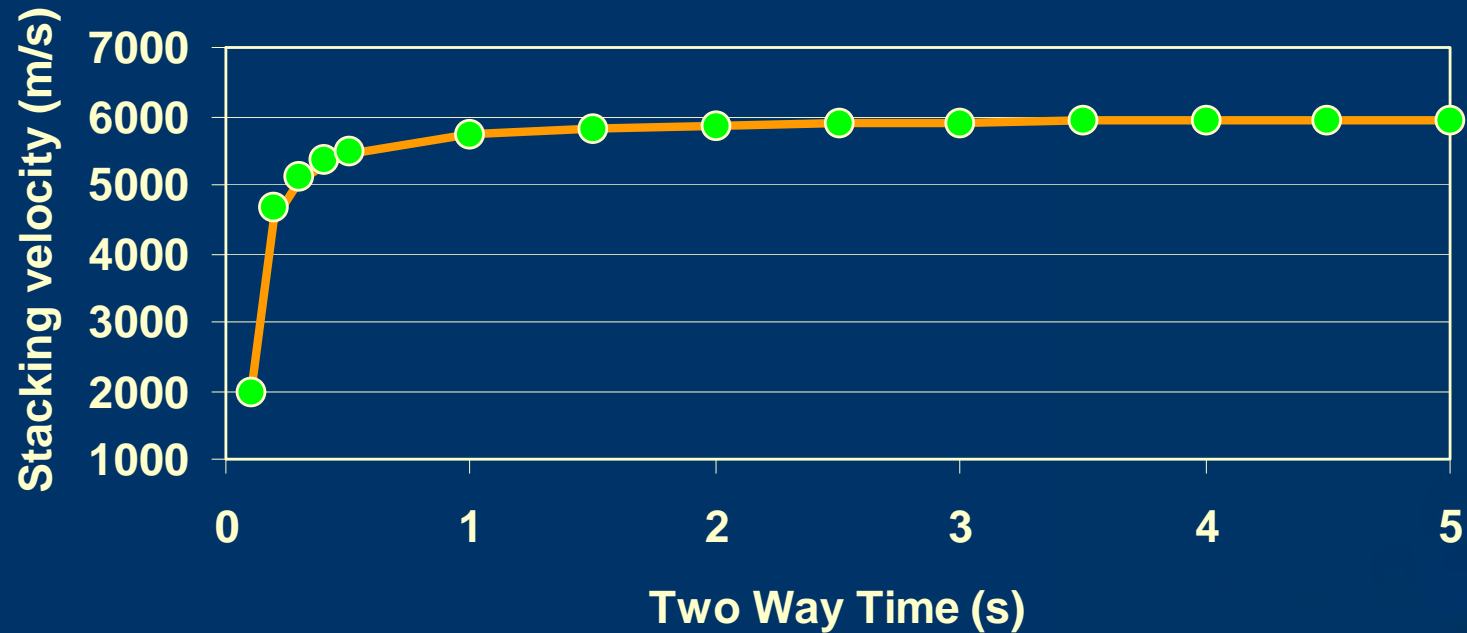
Effective fold is lower due to muting of outside traces to remove first arrivals and excessive moveout stretch

FOLD AT TARGET TWT OF 1 S

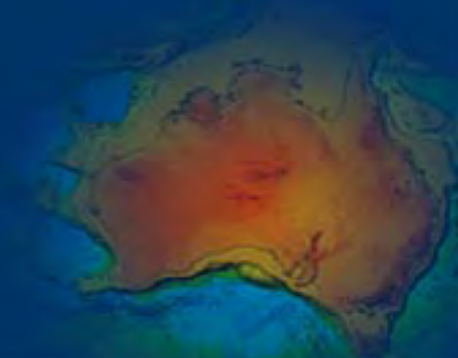


Effect of Regolith on Stacking Velocity

100 m regolith layer (2000 m/s) overlying bedrock (6000 m/s)

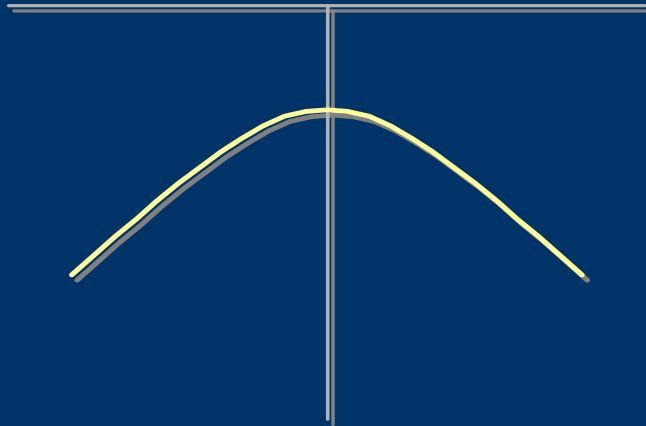


— Dix formula ● Ray tracing



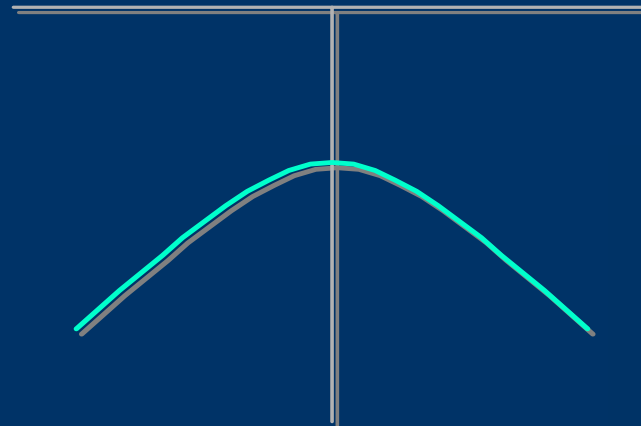
Effect of Static Shifts on Stacking Velocity

No shift



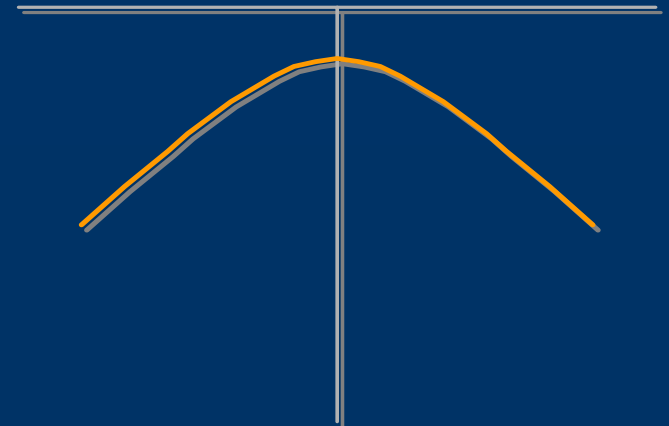
No change

+ve shift

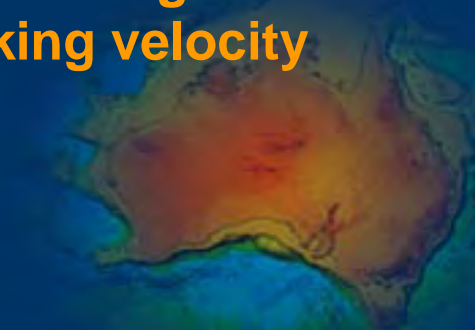


Too much curvature for new time → lower stacking velocity

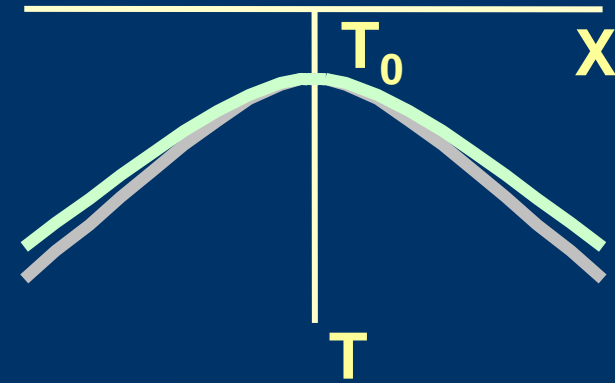
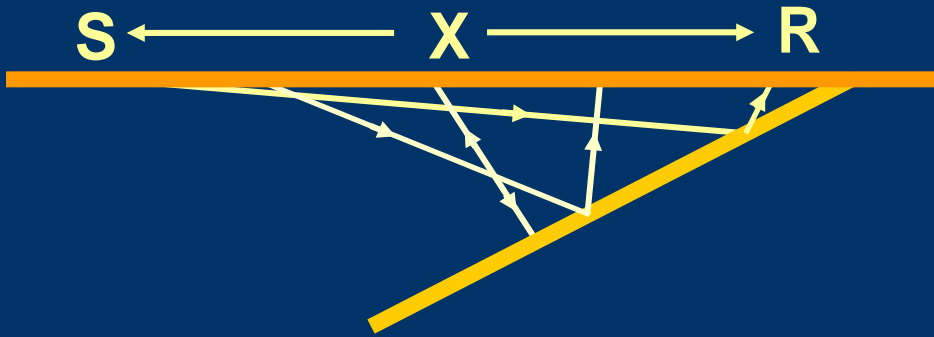
-ve shift



Too little curvature for new time → higher stacking velocity



Dip Moveout Correction (DMO)



DMO corrects

- reflecting point smear
- moveout velocity for dip

DMO

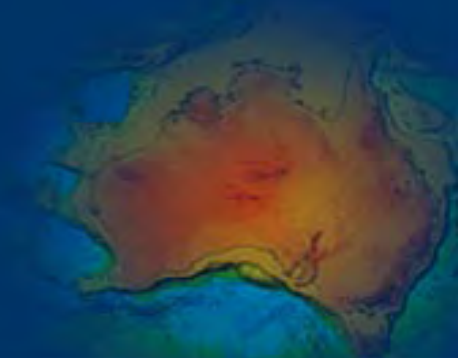
- is partial pre-stack migration
- needs common offset sections

$$T^2 = T_0^2 + X^2 \cos^2 \alpha / V^2$$

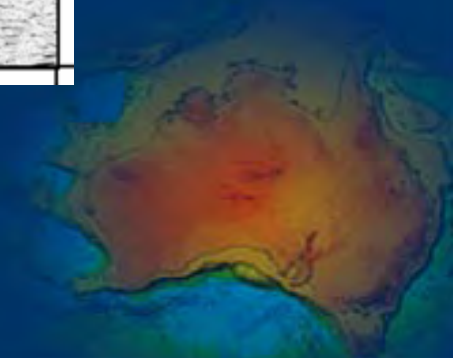
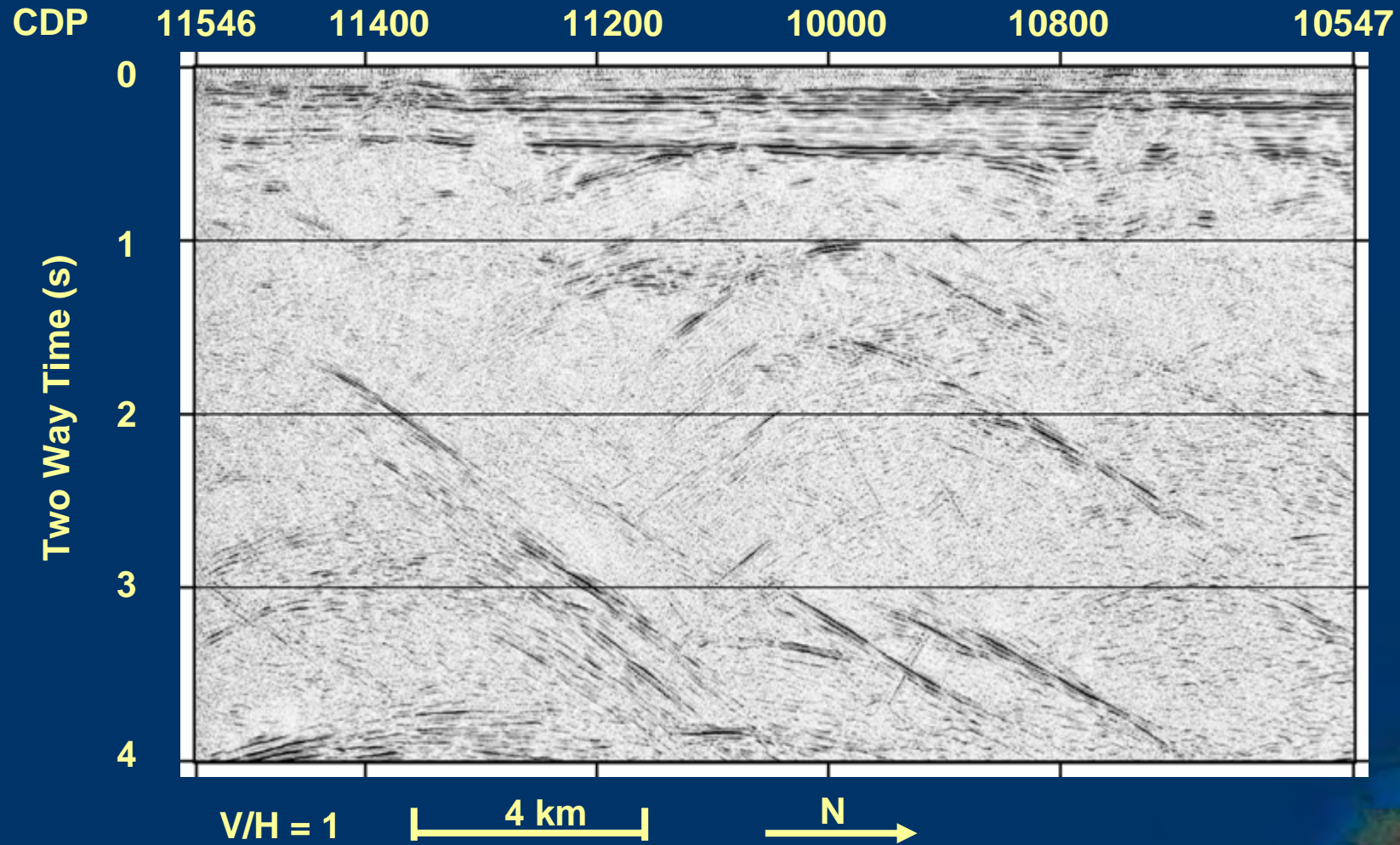
$$= T_0^2 + X^2 / V^2 - X^2 \sin^2 \alpha / V^2$$

normal
moveout

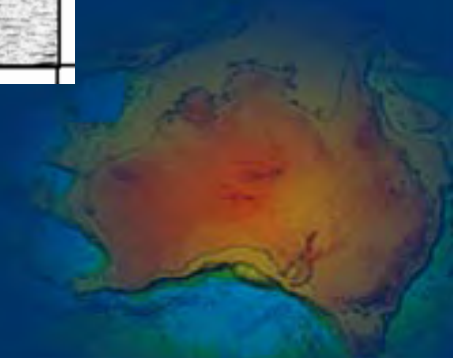
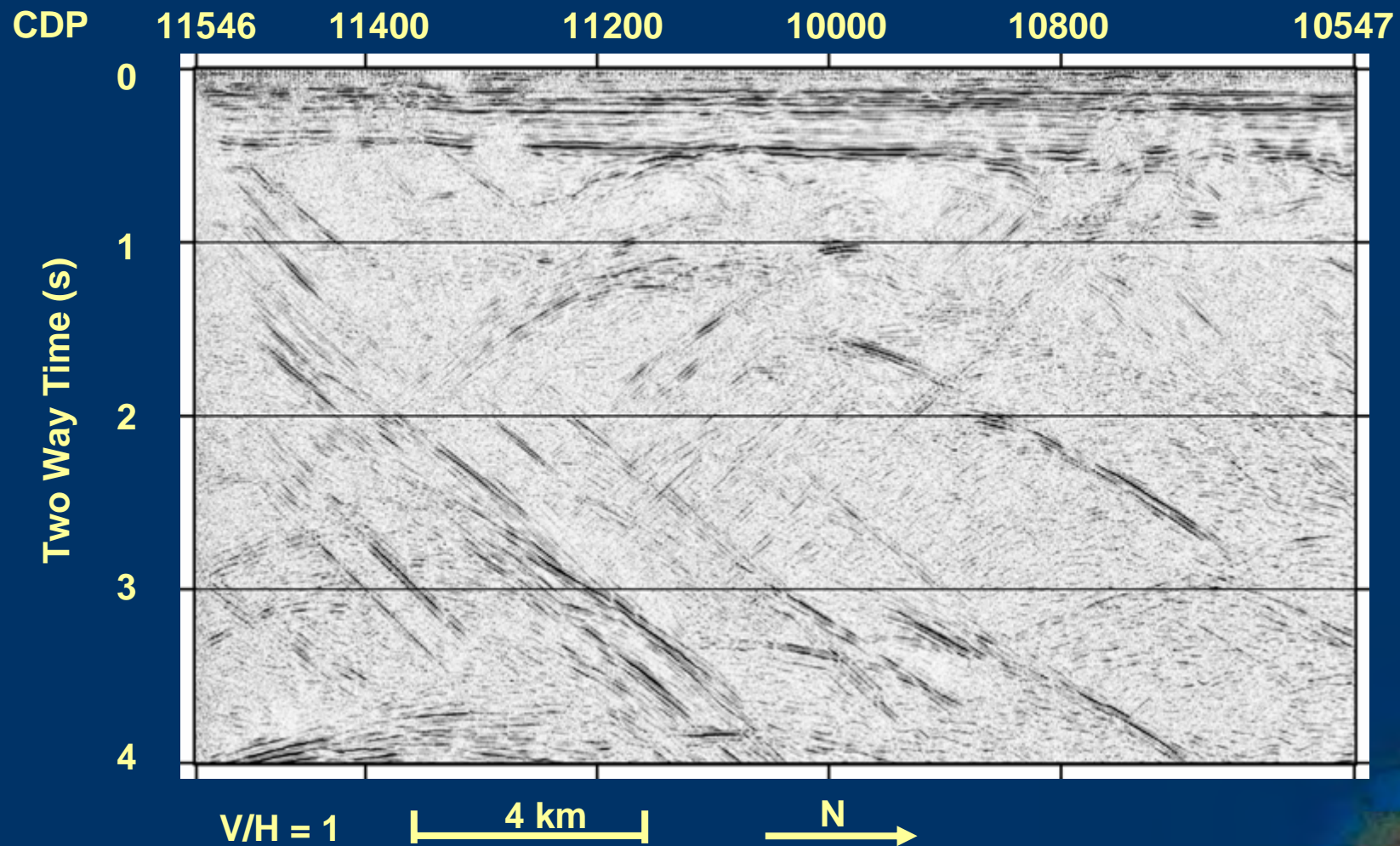
dip
moveout



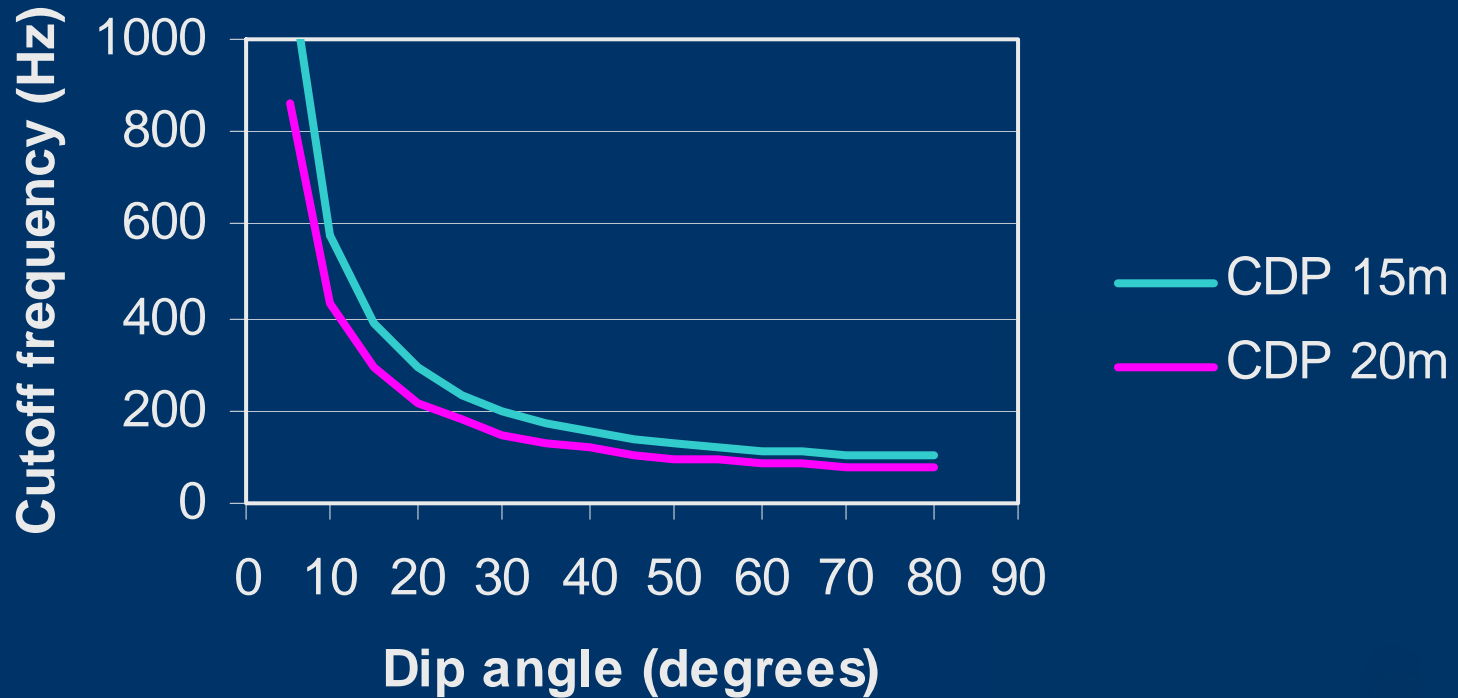
Gawler Line 03GA-OD1 - Before DMO



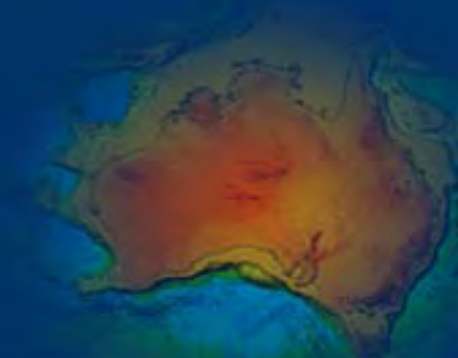
Gawler Line 03GA-OD1 - After DMO



Migration - Spatial Aliasing



Frequencies below curves will not be aliased

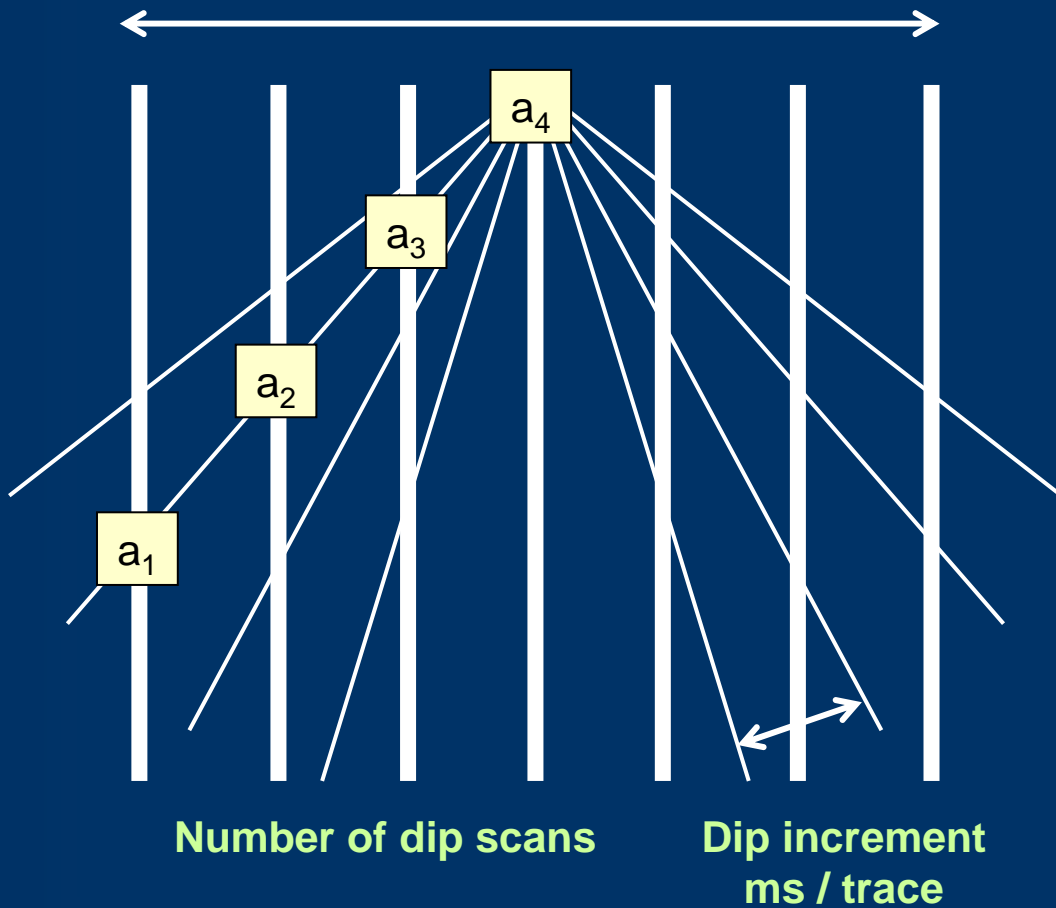


Semblance Coherence Filtering

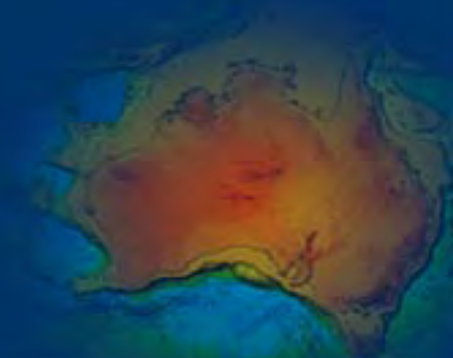
(total incoherence) $0 < \text{Semblance} < 1$ (complete coherence)

Trace window

4 step process



- Compute semblance across window along each dip
 $(\sum a_i)^2 / N \sum (a_i)^2$ (Here $N = 7$ traces)
- Compute coherence as power of semblance
- Smooth data in direction of maximum semblance
- Filter data using coherence weights



Semblance Filtering (*improving the image*)

